

← A4 →

← LETTER →

196
CLADDEY ROAD
FRAYET ROAD
ENGLISH DRAIN
HARVEY DRAIN
MAYONEY DRAIN

← CENTER →

1909

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

← A4 → ← LETTER →

Sec 20 walk 21. Wayne 1
to Quilwood north

Sec 17 + 16
" 8 + 9
to Rockville Road.

Sec 5 + 4
" 32 + 33

Book 6

← A4 → ← LETTER →

Sta -2 *Gladden Road Nursery going North* 3

Sta			100	fill	cut
0.	5.45		105.45		
1.	4.70	+75	106.20		
2.	4.00	+70	106.90		
3	3.90	+10	107.00		
4	7.20	-3.36	103.70		
4+45	7.10	+10	103.80		
5	7.48	-33	103.47		
6	7.85	+38	103.85	6"	
7	5.43	+1.62	105.47	8"	
8	3.02	+2.41	107.88	4"	
9	2.04	+98	108.86	8"	
10	2.60	-56	108.30		
11	2.81	-21	108.09		
12	2.30	+51	108.60		
12.50	7.45				
13	5.25	+2.20	110.80		
14	4.50	+75	111.55		
15	4.40	+10	111.65		

Bridge 16 ft road way
 11 12 " water way
 10 ft wing on south west side
 straight out.

Sta.	ft		1606 10"	
16	4.58	-18	111.47	fill cut
17	4.48	+10	111.57	
18	4.09	+39	111.96	
19	3.80	+29	112.25	6"
20	5.90	-2.10	110.15	8"
21	8.80	+40	110.55	4"
22	6.55	+1.75	112.30	
23	5.25	+1.30	113.60	
24	4.20	+1.05	114.65	10"
25	7.95	-3.75	110.90	
26	8.85	-.90	110.00	12"
27	8.90	-1.19	109.95	
28	9.42	+1.40	110.35	
29	6.92	+2.50	112.85	
30	7.80	+3.94	116.79	
31	6.80	+6.44	123.23	20"
32	4.95	+1.85	125.08	
33	4.60	+3.5	125.43	

← LETTER →

57

Sta.				full run
34	4.20	+40	125.83	
35	4.53	-.33	125.50	
36	5.25	-.72	124.78	8"
37	5.45	-.20	124.58	
38	5.40	+05	124.63	
39	5.35	+05	124.68	
40	6.70	+05	124.68	
40	5.55	+1.15	125.83	
41	5.02	+53	126.36	
42	4.65	+37	126.73	
43	4.38	+27	127.00	
44	4.42	-.04	126.96	
45	4.05	+37	127.33	
46	3.71	+34	127.67	
47	3.18	+53	128.20	
48	2.65	+53	128.73	
49	2.01	+64	129.37	
49	7.85			
50	6.85	+1.00	130.37	6"

			130.37	full cut
51	7.50	-.65	129.72	8"
52	9.55	-2.05	127.67	12"
53	7.77	+1.28	128.95	
54	5.07	+2.70	131.65	8"
55	3.15	+1.92	133.57	8"
56	2.18	+.97	134.54	
57	^{1.20} 3.20	+.98	135.52	
58	2.19	+1.01	136.53	2"
59	^{6.80} 0.75	-4.66	131.92	10"
60	^{10.00} 2.71	-9.05	122.87	
61	3.88	-1.17	121.70	6"
62	4.68	-.80	120.90	"
63	4.60	+1.08	120.98	"
64	4.70	-1.0	120.88	"
65	4.90	-2.0	120.68	"
66	4.65	+2.5	120.93	"
67	3.90	+2.5	121.68	"

Bridge

Y

Sta				
68	121.62		fill	cut
	^{3.20}			
68	121.90	+ .70	122.38	
69	6.95	+ 1.95	124.33	
	^{4.57}			
70	4.53	+ 2.38	126.71	
71	5.75	- 1.22	125.49	
72	8.22	+ 2.47	127.96	
73	7.61	+ .61	128.57	10"
74	6.62	+ .99	129.56	
75	4.90	+ 1.72	131.28	
	^{1.60}			
76	9.41	+ 3.30	134.58	
77	1.80	+ 9.61	142.19	10"
78	2.05	- .25	141.94	
79	1.75	+ .30	142.24	
	^{0.45}			
80	5.17	+ 1.36	143.54	
81	3.63	+ 1.34	144.88	
82	3.64	+ 1.9	145.07	
83	4.20	- .56	144.51	
84	4.57	- .37	144.14	

hill to cut out

Sta			14414
85	5.03	-1.46	143.68
86	5.22	-.19	143.49
87	5.81	-.59	142.90
88	6.70	-.69	<u>142.21</u>
89	6.75	-.05	142.16
90	5.90	+1.65	142.81
91	4.60	+1.30	144.11
92	1.55	-.12	143.99
93	2.05	-.56	143.49
94	3.10	-1.05	142.44
95	4.45	-1.35	141.09
95+65	4.65	-.20	<u>140.89</u>
96	4.64	+1.01	140.90
97	1.18	+3.46	144.36
98	3.52	+4.03	148.39
99	3.22	+1.30	148.69
100	2.98	+2.44	148.93
101	2.81	+1.97	148.90
102	4.40	-1.59	148.31

fill out

Bridge 14" Sewer

concrete Sewer 3' x 6'

8"

Sta			148.51
103	147.00	-2.60	145.71
104	9.51 2.15	-2.51	143.20
105	3.97	-1.79	141.41
105+64	4.23		
106	4.25	-1.26	140.15
107	5.03	-.78	139.37
108	9.65	+2.38	141.75
109	7.00 0.00 6.98	+4.99	151.74
110	6.52	+1.46	152.20
111	5.60	-.08	152.12
112	4.99	+1.03	152.75
113	4.46	+1.53	153.28
114	4.25	+1.21	153.49
115	4.10 8.15	+1.5	153.64
116	7.10	+1.05	154.69
117	6.26	+1.84	155.53
118	4.65	+1.58	157.11
119	4.03	+1.65	157.76
120	3.69	+1.34	158.10

fill cut

7x16

R.R. Right

← A4 →

← LETTER →

sla			158.10
12 1/8	4.85	+ 1.16	156.94
121 8/8	5.02	- 1.20	155.74
122	5.98	+ 1.09	155.81
122+37	6.70	+ 2.8	156.09

bridge 2 X 3'

17

10	Fragie Road full cut		
0	4.10		104.10
1	2.60	+1.50	105.60
2	3.90	-1.30	104.30
3	6.95	-3.05	101.25
4	9.00	-2.05	99.20
4+11			8"
5	8.15	+ .85	100.05
	4.00		
6 P	5.45	+4.15	104.20
			12"
7	5.05	+ .40	104.60
8	4.85	+ .20	104.80
			6"
9	4.60	+ .25	105.05
10	4.85	- .25	104.80
11	4.27	+ .58	105.38
	4.21	+ .06	
12 P	0.25		105.44
13	1.38	-1.13	104.31
			6"
14	4.50	-3.12	101.19
15	7.51	-3.01	98.18
			6"
16	6.91	+ .60	98.78

Rockville Road going east
North side Interstate

19

	691		98.78
10/20			
10/24	Boiler Sevens		
	5.95	+ .96	99.74
17	7.46	- 1.51	98.23
	^{5.23}		
18 P.O.	8.98	+ 2.23	100.46
19	7.95	+ .96	101.42
20	7.12	+ .83	102.25
21	5.67	+ 1.55	103.80
22	4.44	+ 1.23	105.03
23	3.55	+ .89	105.92
24	3.51	+ .04	105.96
25	3.30	+ .21	106.17
	^{2.95}		
26 P.P.	7.80	+ .35	106.52
27	6.43	+ 1.37	107.89
28	5.23	+ 1.20	108.09
29	4.64	+ .59	108.68
30	5.05	- .41	108.27
31	5.74	- .69	107.58
32	7.20	- 1.46	106.12

on top of Boiler Sevens

	Sta	2220		106.12	fill	cut
	33	7.0	9.40	0.25	-2.20	103.92
	34		2.50	-2.25		101.67
	35		4.61	-2.11		99.56
	36		6.52	-1.91		97.65
	37		7.80	-1.28		95.37
	37+38		6.00	+1.80		98.17
	38		7.52	-1.52		95.65
	39		6.95	+ .57		96.22
	40		4.22	+2.73		98.95
	41		6.40	+3.10		102.05
	42		3.00	+3.40		105.45
	43		4.20	-1.26		104.25
	44		5.05	- .85		103.40
	45		6.80	-1.75		101.65
	45+46		8.15			
	46		8.45	-1.65		100.00
	46+47		8.85			
	47		8.55	+ .30		100.30

on south edge of bridge

Bridge change to 46 + 5' recommended

Sta.	85x		100.30	Full cut
48	7.95	+1.60	100.90	12
49	5.95	+2.00	102.90	
50	4.45	+1.50	104.40	
51	2.60	+1.85	106.25	
52	1.75	+1.85	107.10	
53	0.73	+1.02	108.12	
54	8.35	+3.8	108.50	
54	7.0	4.20	108.30	
54	4.60	-2.0	106.30	154' 3"
55	6.40	-1.80	106.50	
56	6.40	0.00	106.50	
57	5.95	+1.50	106.95	12"
58	5.38	-3.86	103.09	
59	8.32	-2.94	100.15	12"
59+25	7.30	+1.82	101.17	
60	8.95	-1.65	99.52	12"
61	7.64	+1.31	100.83	
62	5.20	+2.44	103.27	

on S end of Bridge

Sta	26 ²⁰		103.27
69	1.65 9.56	+8.55	106.82
64	5.75	+3.81	110.63
65	4.37	+1.38	112.01
66	3.86	+1.52	112.53
67	4.15	-.29	112.24
68	4.85	-.70	111.54
69	5.60	-.75	110.79
70	6.35	+1.25	111.04
71	4.27 5.65	+1.08	112.12
72	5.04	+1.61	112.73
73	5.20	-.16	112.57
74	5.45	-.25	112.32
75	5.27	+1.8	112.50
76	4.17	+1.50	113.00
77	4.30	+1.47	113.47
78	3.37	+1.93	114.40
79	2.20	+1.17	115.57

fill cut

12°

Carey Road
Milk Run

27

← A4 →

← LETTER →

Est	220		115.57	Full	cut
80	3.05	-.85	114.72		
81	3.55	-.50	119.22		
82	2.60	+ .95	115.17		8"
83 n.p.	^{3.90} 2.60	-1.30	113.87		
84	3.37	-.77	113.10		
85	3.22	+ .15	113.25		2 1/2"
86 n.p.	^{9.85} 9.01	-6.13	107.12		
87 n.p.	^{7.76} 3.83	-7.75	99.37		
88	5.62	-1.79	97.58		
89	6.40	+ .88	96.70		
90	6.15	+ .25	96.95		
91	3.55	+2.60	99.55		
92	6.25	-2.70	96.85		
93	6.15	+ .10	96.95		
94	5.55	+ .60	97.55		
95	3.60	+1.95	99.50		
96 n.p.	^{.40} 9.57	+3.20	102.70		
97 n.p.	^{3.10} 8.67	+6.47	109.17		

29

South end of Iron Bridge

← A4 →

← LETTER →

	8.67		109.17
98	2.47	+6.20	115.37
99	1.85	+6.2	115.99
100	1.63	+2.2	116.21
101	4.90	+3.27	112.94
102	9.20	-4.30	108.64
103	6.96	+2.84	111.48
104	^{2.97} 7.55	+3.41	114.89
105	4.67	+2.88	117.77
106	4.98	-.31	117.46
107	5.75	-.77	116.69
107+35	6.05	-.30	116.39

end.

Grade began
Sept 15 1905

31

1 day Chas Harvey 2.00
 2 Geo. Tucker 3.00
 1 John Tucker 1.50
 75 stakes .75
 Pt, 35.25

South 70 ft
 E 1140 ft
 find wpt,

Begin N 70 E 1142 ft
 cor sec 20
 and running thence
 S 22 E to stake 5 400
 thence S 15 E " 7+39 239
 " S 43 W " 15 761
 " S 48 W " 25 1000
 " S 42 W " 33 800
 " S 19 W " 37+60
 and ending 57.60

Area No 1

Begin 580 ft
 N 70 E of Sec cor 20
 and running thence S 53 W
 to stake 9+40
 thence S 20 W " 10+48
 " S 23 E " 20+406
 " South " 24+90
 and ending at
 stake 20 on main
 line

1942 feet of open
 drain

2490
 2048
 442
 1140
 2000
 24190

34 English Drain
Sta Mann Drain

	B.M.	1.65	S.E. cor walk	10.45		
0	1.95		4.50	5.00		
1	3.10	-1.15	-60	-55	4.45	29
2	3.40	-30	-60	+30	4.75	28
3	5.00	-1.60	-60	-1.00	3.75	26
4	6.00	-1.00	-60	-40	3.35	22
5	6.35	-35	-60	+25	3.60	22
6	6.55	-20	-50	+30	3.90	23
7	6.40	+05	-50	+55	4.45	25
7+39	7.00	-50	-20	-30	4.15	26
8	6.60	+40	-30	+70	4.85	27
					6.8	
T.P.	6.15					
9	6.25	-10	-30	+20	5.05	30
10	5.15	+1.10	-30	+1.40	6.45	35
11	4.65	+50	-30	+80	7.25	42
12	5.75	-1.10	-30	-80	6.45	42
13	6.10	-35	-30	-05	6.40	40
						415

Plainfield

S.E. cor walk

18"
15
14

← A4 →

sta 38 2.05

28	7.30	-25	-40	+15	6.85	73
29	5.25	+2.05	-40	+2.45	9.35	90
30	6.75	-1.50	-40	-1.10	8.20	97
31	^{5.08.85} 5.40	+1.35	-40	+1.75	9.95	100
32	7.05	-1.65	-40	-1.25	6.70	103
33	6.95	+1.0	-40	+50	9.20	99
34	^{2.20} 6.15	+80	-40	+1.20	10.40	109
T.P.	1.30				OK	
35	3.90	-2.60	-15	-2.45	7.95	103
36	4.15	-.25	-15	-10	7.85	87
37	8.60	-4.45	-15	-4.30	3.55	63
37+60	10.55	-1.95	-15	-1.80	1.75	17
	12.85	-2.30			OK	941

1.31
1.35

11.55
-95
1.65
1.31
4.65
20.15

6.70

← LETTER →

39

Bottom of Creek

Sta.	Armer. No. 1.	State	B.L.		Depth	Harvey, or Plainfield	
B.M.	5.35						walk at "0" 41
0	5.70				6.00	Augd, 5.15	
1	5.80	-10	-40	+30	5.30	31 5.25	
2	5.60	+20	-40	+60	5.90	34 5.15	
3	5.35	+25	-40	+65	6.55	38 4.75	
4	5.55	-20	-40	+20	6.75	41 5.05	
5	5.50	+05	-40	+45	7.20	43 4.90	
6	5.50	00	-40	+40	7.60	45 4.95	
7	5.50	00	-40	+40	8.00	48 4.95	
8	7.10	-1.60	-40	-1.20	6.80	45 6.60	
9	^{5.70} 7.65	-5.5	-40	-15	6.65	42 7.15	
TP	5.35	9+40			7.0	9+40 5.50	
10+20	4.55	+80	-40	+1.20	7.85	60 5.60	
11	5.65	-1.10	-40	-70	7.15	62 5.70	
12	5.30	4.35	-40	+75	7.90	63 5.40	
13	5.05	+25	-40	+65	8.55	68 5.35	
14	5.80	-75	-40	-35	8.20	70 6.20	
					6.90		

← A4 →

← LETTER →

sta.	42 stake 3.50	B. 10				820	8.20	cu yd.		43
15	6.20		-45	-40	00	8.20	62	6.70		
16	7.80	9.45	-1.60	-40	-120	7.00	63	8.20		
17	8.65	<u>7.50</u> 1.65	-8.5	-40	-45	6.55	56	9.05		
18	9.10	10.15	-45	-40	-05	6.50	^{TP} 54	5.25		
19	8.80	3.45	+30	-40	+70	7.20	50	4.55		
TP	4.55					OK				
20	4.70	-15	-40	+25		7.45	61	4.45		
20+46	4.30	+40	-20	+60		8.05	63	4.85		
21	4.75	-45	-20	-25		7.80	66	4.85		
B.M.	4.20									
22	4.15	+60	-40	+100		8.80	69	4.25		
23	4.15	00	-80	+30		9.40	74	4.55		
24	5.10	-95	-30	-65		8.45	73	6.30		
25 0.25	5.90	-80	-30	-50		7.95	68	11.05	on tile in m. beam	
26 on main l.						OK	765			
B.M.	7.00									

CULTURE WALK

Tile	6087.25
Construction	927.00
Atty Fee	150.00
Haelling tile	150.00
Court Cost	75.00
Painting	100.00
Spec & Reports	150.00
Subt. Const	100.00
Incidental	150.00

\$7889.25
 6592

 1297, 25

C. C. Walls
 2% off for No 2.

5864.
 150
 75
 103
 150
 250

 6592

1400 ft red tile 18" — 1-10" T.

16 " " " 10"

900 " vitrified tile 18"

2200 " " " 24"

1260 " " " 33"

16 " " " 10"

32 " " " 12"

1 10" T
 6 6" T S G
 2 10 T S
 6 6" T S G
 3 10" T S
 1 24" T S

25	5.70				7.05
26	4.70	+1.00	-30	+1.30	8.35
27	6.60	-1.90	-30	-1.60	6.75
28	6.55	+0.5	-30	+35	9.10
29	4.45	+2.10	-30	+2.40	9.50
30	6.30	-1.85	-40	-1.45	8.05
31	5.20	+1.10	-40	+1.50	9.85
32	6.85	-1.65	-40	-1.25	8.30
P.P.	5.63				
33	5.15	+48	-40	+88	9.18
34	3.97	+1.18	-40	+1.58	10.76
35	6.80	-2.83	-15	-2.68	8.05
36	7.40	-60	-15	-45	7.60
P.P.	2.74				
37	7.07	-4.33	-15	-4.18	3.42
37+60	8.90	-1.83	-15	-1.68	1.75

← A4 →

← LETTER →

Main drain grades

51

0	.90				4.00
1	2.00	-1.10	-1.00	-10	3.90
2	3.30	-1.30	-1.00	-30	3.60
3	4.10	-.80	-1.00	+20	3.80
4	4.60	-.50	-.40	-10	3.70
5	5.00	-.40	-.40	+00	3.70
6	5.30	-.30	-.30	00	3.70
7	5.60	-.30	-.30	00	3.70
8	5.55	+05	-.30	.35	4.05 6.65
T.P.	6.55				
9	6.55	00	-.20	+20	4.25
10	5.50	+1.05	-.20	+1.25	5.50
11	5.15	+35	-.20	+55	6.05
12	6.30	-1.15	-.20	-.95	5.10
13	6.55	-.25	-.20	-.05	5.05
14	6.85	-.30	-.30	00	5.05
15	3.40	+3.45	-.30	+3.75	8.80

	3.40				8.80
16	7.30	-3.90	-30	-360	5.120
G.P.	3.80				6K
17	4.10	-30	-40	+10	4.30
18	4.40	-30	-40	+10	5.40
19	4.60	-20	-40	+20	5.60
20	5.00	-40	-40	-00	5.60
21	5.00	00	-40	+40	6.00
22	6.30	-1.30	-40	-90	5.10
23	5.70	+60	-40	+1.00	6.10
24	6.50	-80	-40	-40	5.70
25	6.65	-15	-10	+25	6K

Profile sent June 13

in title al month ⁵⁸

54

					depth
0	5.15				5.00
1	5.25	-10	-40	+30	5.30
2	5.15	+10	-40	+50	5.80
3	4.75	+40	-40	+80	6.60
4	5.05	-30	-40	+10	6.70
5	4.90	+15	-40	+55	7.25
6	4.95	-05	-40	+35	7.60
7	4.95	00	-40	+40	8.00
8	6.60	-1.65	-40	-1.25	6.75
9	7.15	-55	-40	-15	6.60
10	5.50				6.75
9+40	5.60	-10	-20	+10	6.70
10+20	5.00	+60	-30	+90	7.60
11	5.70	-70	-40	-30	7.30
12	5.40	+30	-40	+70	8.00
13	5.35	+05	-45	+50	8.50
14	6.20	-85	-45	-40	8.10

55

56

	6.20				8.10
15	6.70	-50	-45	85	8.05
16	8.20	-1.50	-45	-1.05	7.80
17	9.05	-85	-40	-45	6.55
N.P.	5.25				6.15
18	5.25	00	-40	+20	6.95
19	4.55	+70	-40	+1.10	8.05
20	4.45	+10	-20	+30	8.55
21	4.85	-40	-40	-30	8.55
22	4.25	+60	-85	+35	9.20
23	4.55	-30	-85	-25	8.95
24	6.30	-1.75	-85	-1.50	7.25
25	11.05	-4.75	-50	-4.75	2.50
					6.15

57

on tile main drain

rain gauge this only,

Maloney Kresin

Sta B. 200

0.	6.10					6.00.		Average depth	
1	6.10	9.10	3.00	15	+15	6.15	19	in bottom of	2.15
2	5.75		+3.5	15	+50	6.65	20	old ditch	
3	5.70	9.70	+0.5	15	+20	6.85	21	from 0 to 81	1.85
4	6.10		-40	15	-25	6.60	21	1.30'	
5	5.60	10.00	+50	15	+65	6.25	22		1.85
7.P.	5.15					OK			
6.	6.10		-95	-15	-80	5.45	22		
7.	4.70	10.40	+1.40	-15	+55	7.00	26		1.30
7.P.	4.20					OK			
8.	5.60	10.10	-1.40	-15	-1.25	5.75	29		1.25
9.	3.85	4.50	+1.75	-15	+1.90	7.65	31		
10	7.45	10.15	-1.60	-75	-45	7.20	34		1.50
11	5.15	5.70	-70	-15	-55	6.65	36		L
12	5.00	10.50	+15	-15	+30	6.95	31		1.45
13	7.40	5.50	-2.40	-15	-5.25	4.70	26		
						OK			
									338

Pond 11.50 low 15.70
 State G. 10.20 back 11.20
 engd. 6.50

6

62

Stake B.D.

J.P.	4.80	8.20				4.40		
14	4.60		+20	20	+40	5.10	23	
15	5.50	8.45	-90	20	-70	4.40	22	1.35
		3.05						
16	5.10		+40	20	+60	5.00	22	
17	5.90	9.20	-80	20	-60	4.40	22	1.10
		3.30						
18	6.50		-60	20	-40	4.00	16	
19	7.80	9.70	-1.30	20	-1.10	2.90	15	1.50
		1.90						
20	6.70		+1.10	20	+1.30	4.20	20	10.50
21	7.70	10.50	-1.00	20	-80	3.40	21	5.70
		2.80						1.60
J.P.	5.80					6K.		
22	5.20		+60	20	+80	4.20	21	
23	5.50	8.75	-30	20	-10	4.10	23	.85
		3.25						
24	5.20		+30	20	+50	4.60	24	clean old ditch at 23 + 60
25	4.95		+85	20	+1.05	5.60	28	tender at 27 + 50
26	5.60		-1.25	20	-1.05	4.60	28	
27	6.55		-.95	20	-.75	3.85	23	
J.P.	5.90					6K.	308	

63

Sta	Slats	B.D.			
28	5.70	9.10	+20	-2.0	+40
29	5.20	3.40	+50	20	+40
30	5.30	9.25	-10	20	+10
31	6.15	3.95	-85	20	-65
32	5.90		+25	20	+45
33	6.80		-90	20	-70
34	6.90		-10	20	+10
35	6.80		+10	20	+30
36	7.0		-30	20	-10
T.P.	5.85	8.90			
37	5.90	3.05	-85	-15	+10
38	5.25	8.90	+65	-15	+80
39	6.25	3.65	-1.00	-15	-85
40	6.60		-35	-15	-20
41	6.60		00	-15	+15
T.P.	6.40				
42	6.50		-10	-15	+05

486	S 5° W	from 27 to 31	
4.25	22		1.85
4.95	25		
5.05	28		1.10
4.40	S 8° W	from 31 to 35+50	4.50
4.85	S 30° E	35+30 to 37+30	1.2
4.15	21		
4.25	24		
4.55	24		
4.45	25		1.40
OK			5.2
4.55	25	old ditch leaves old ditch	
5.35	27	at 37+50	1.70
4.50	27	Schaumburg's corn	
4.30	S 24° E	from 37+30 to A1	
4.45	24	leaves old ditch at 37+50 and	
OK			
		enters at 48	
4.50	25		
	376		

						← LETTER →			
68	Stake	BU							69
59	^{4.40} 5.30		-90	-15	75	6.15	11	from 68 to 75	37.
T.P.	5.50					OK.	52	from 75 to 77	
60	6.80	4.20	-1.30	-15	-1.15	5.00			31.
61	6.00	10.20	+80	-15	+95	5.95	1.75		30.
62	5.70	^{4.20}	+30	-15	+45	6.40	J		34.1
63	6.00	10.10	-30	-15	-15	6.25	2.15		35.
64	6.30	^{4.10}	-30	-15	-15	6.10			34.
65	7.00		-70	-15	-55	5.5			32
66	7.70		-50	-15	-55	5.00			29.
T.P.	5.70								
67	4.85		+85	-10	+95	5.95			30.
68	5.05	9.20	-20	-10	-10	5.85	1.70		32.
69	5.15	^{4.15}	-10	-10	00	5.84			32.
70	6.00	9.55	-85	-10	-75	5.10	1.55		30.
71	6.80	^{3.58}	-80	-10	-70	4.40			27.
72	6.85	9.95	-05	-10	+05	4.55	1.35		24.
73	6.38	^{3.10}	+55	-10	+65	5.70			27
						OK.			464

Sta.	Slope	BLD			
89	5.80		-20	-15	-10.5
90	6.25		-45	-15	-30
91	6.00		+25	-15	+40
T.P.	4.50				
92	5.35		-85	-15	-70
93	5.20	9.20	+15	-15	+30
94	5.55	4.00	-35	-15	-20
95	6.05	9.20	-50	-15	-35
96	6.50	3.15	-45	-15	-30
97	7.20	9.65	-70	-15	-55
T.P.	6.35	21.45			
98	5.05		+1.30	-15	+1.45
99	5.15		-10	-15	+05
100	4.20	9.20	+95	-15	+1.10
101	5.00	5.00	-80	-15	-65
102	5.45	10.00	-45	-15	-30
103	5.85	4.55	-40	-15	-25

6.05

5.00.

4.70.

5.10.

B.K.

4.40.

4.70. leave old ditch at 89

4.50. creels at 92 + 50

4.15. leave at 97 + 50

3.85. creels at 100.

3.30. .85

6K

S 426 from 89 to 93

4.75. S 188 " 93 " 95 - 22

4.80. S 147 " 95 " 97 + 50 - 26

5.90. S 577 " 90 " 91 + 10 " 105 - 30

5.25. S 408 " 101 to 111 + 34 term 31

4.95. AD

4.70

28.

27.

27.

26

24

24 ✓

23.

22.

22.

22

26

30

31

28

27

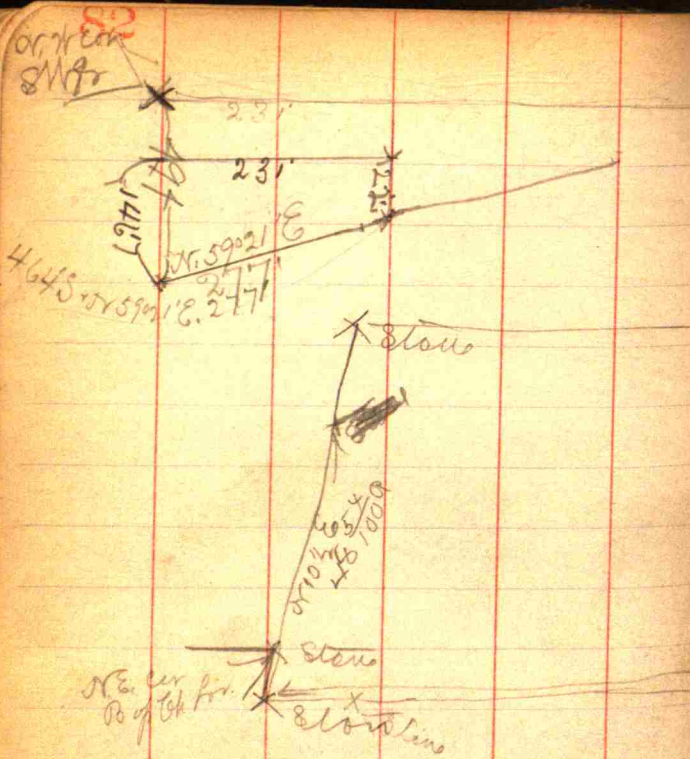
385

74						75					
	Slake	13.10				470	20	Size of tile			
104	5.10		+75	-15	+90	5.60		8" to slake	6	28	
105	6.40	10.90	+1.30	-15	-1.15	4.45		10" " "	6	25-28	
T.P.	3.70	4.50				6.10		10" " "		25	
106	6.30		-60	-20	-40	4.05		" "			23
107	6.10	10.80	+20	-20	+40	4.45					23
108	6.50	$\frac{6.10}{9.70}$	-40	-20	-20	4.25					27
109	6.70	10.80	-20	-20	-00	4.25					26
110	7.25	$\frac{6.70}{9.10}$	-55	-20	-35	3.90					22
111	8.15		-90	-20	-70	3.20					20
111+34	10.80	12.00	-2.65	-20	-2.45	1.75					5
		$\frac{1.20}{40}{80}$									202

Total No Cubic Yds

{ 3004

$\frac{1.59}{72}{74}$



12.3x

6.67 $\frac{1}{2}$
 2.67 $\frac{1}{2}$

 9.35 30

10 $\frac{1}{3}$ 165
 165

 1650

66 $\frac{1}{2}$ 760 | 2.6 75
 132
 440
 660

 500
 460

 280

83
 Cen Sur 35

x 34970
 x stone

128549
 100

34970
 x 100

 3497000

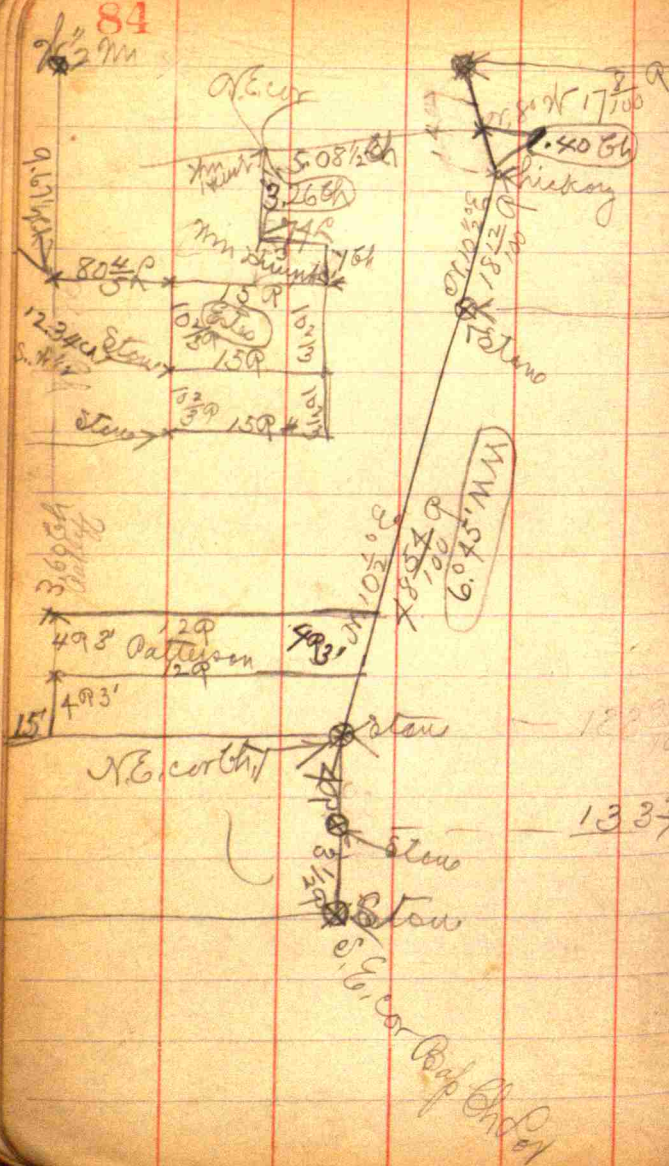
52000

133 $\frac{22}{100}$ P.

x stone

Probably in Amos

84

128 $\frac{25}{100}$ Q128 $\frac{54}{100}$ Q128 $\frac{92}{100}$ Q133 $\frac{22}{100}$ Q

Cen 85

37 $\frac{97}{100}$ Q

Stew

52 $\frac{47}{100}$ Q

Cen E. of Cen

Stew

← A4 →

86
From N. E. cor Ch. Pav
N. $10\frac{1}{2}^{\circ}$ E, 2.10 R to S. E. of Isan Putteff

← LETTER →

87

144 10 2

← LETTER →

3864,

115

2100

3864

0797

2127

37-60

23

400

11260

~~750~~

600.

20001

11441

243.

350

2222

32

3737

1100

104

4400

1100

24

900

24300

265

1400

106000

265

100

3711

1

4

890

141

4250

6230

667.100

Beg. 4.8 1/2 ch east of
 on N N W 1/4 Sec 11
 Twp. 15, 1 E.
 thence S 22 1/2 rd, N
 thence E 14 1/2 rd
 thence N 22 1/2 rd
 thence W 14 1/2 rd. to
 place of begin.

$$\begin{array}{r}
 3760 \\
 2490 \\
 \hline
 16h) 6250 \quad (382 \\
 \underline{496} \\
 1290 \\
 \underline{1320} \\
 300
 \end{array}$$

$$\begin{array}{r}
 382 \overline{) 14864.00} \quad (153 \\
 \underline{382} \\
 2044 \\
 \underline{1910} \\
 1340
 \end{array}$$

3292 21

$$\begin{array}{r}
 12 \\
 1.8 \\
 \hline
 96 \\
 12 \\
 \hline
 2.16 \\
 4 \\
 8.64 \\
 12 \\
 \hline
 128 \\
 64 \\
 \hline
 7.68
 \end{array}$$

$$\begin{array}{r}
 7 \\
 5.2 \\
 \hline
 12.2
 \end{array}$$

.798⁶ 147
 1
 8' 7 1/2"

$$\begin{array}{r}
 4.79 \frac{1}{2} \\
 1.75 \\
 \hline
 3 - 4 \frac{1}{2}
 \end{array}$$

$$\begin{array}{r}
 6 \frac{1}{2} \\
 4 \\
 6.25 \\
 4.5 \\
 \hline
 1.75
 \end{array}$$

$$\begin{array}{r}
 6 \frac{1}{2} \\
 4 \overline{) 26.5} \\
 \underline{21.8} \\
 4.7
 \end{array}$$

$$\begin{array}{r}
 14 \\
 9 \\
 23.50 \\
 16.5 \\
 \hline
 7
 \end{array}$$

$$\begin{array}{r}
 .795 \\
 1.75 \\
 \hline
 81.25
 \end{array}$$

$$\begin{array}{r}
 39 \frac{1}{2} \\
 25 \\
 \hline
 14 \frac{1}{2}
 \end{array}$$

$$3 - 3.066$$

$$4.92$$

$$1.41$$

$$\begin{array}{r}
 3168 \\
 792 \\
 \hline
 396
 \end{array}$$

$$\begin{array}{r}
 12 \overline{) 148.4} \quad (9.57 \\
 \underline{108} \\
 40.4
 \end{array}$$

198

N Salem.

South West St.
 West side $8\frac{1}{2}$ ft from
 Property line or $3\frac{1}{2}$ ft from walk
 East side stakes 1 ft from
 out edge of walk

N End Stakes 6" from
 out edge of walk

East Street

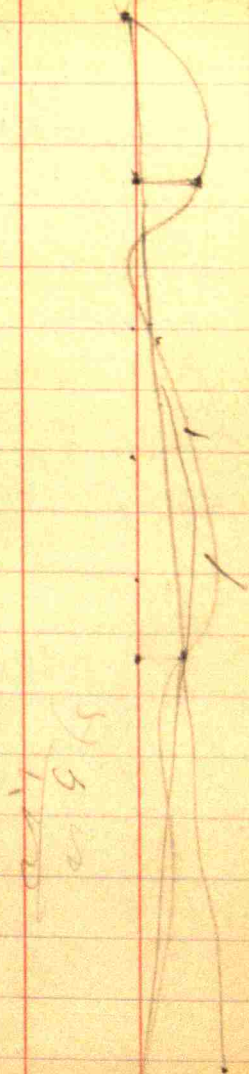
6" from walk line

7.95

7.40

.55

199

$$\begin{array}{r} 7 \\ 2 \\ \hline 19 \\ 3 \\ \hline 22 \end{array}$$


mm
150
26
Wagee Road # 265

2 2/3 M Little
907 Broadway.

Length main Building
50' 2"

Width 32' 2"

Length T 35' 7"

Width 32' 2"

off set from N 8' 7 1/2"

3760

2490

165) 6250 (3781

495

1300

1155

145

for grading. 7) 160 (22

1275) 10.00
875

242
10 1/2

24 (5)

14
16 1/2

34 1/2

2) 3 1/2
1

2) 3.15
1.05

1 1/2
12 1/2

17 1/2

29 1/2

21

6 1/2

5

18 1/2

25 1/2

43 1/2

2490

1942

165) 548 (33
495
530

John 1162

Gladden Road #300

1.5 X 12 r 3'6" wings 1.10' wing.	X
4.2 X 3 " " E	0
1.4 X 10 r	X
2.3 X 6 r	0
1.3 X 4 r	0
1.7 X 18 r	X
1.4 X 16 r	X
1.4 X 20 r	X
1.2 X 4 r	0

for grading

153

1.6 X 20 r	X
1 X 50 r	

1140
 1140

 45600
 1140

 1299600
 70
 70

 4900
 1299600

 1304500 | 1142
 1

 30
 21 | 21

 945
 224 | 896

 4900
 228

154

made

~~471~~ 2 x 3' concrete culvert

16+24

Boiler sewer to be provided with concrete wings 10 ft long 2 ft above boiler.

37+33

20' water way

made

4' above water

16' road way

5' wings straight back

44

made 2' x 4' concrete culvert

~~54+25~~

20 ft water way

made

6 ft above water line

10' road way

6 ft wings straight back

Bridges.

155

91' Truss Bridge 50 ft water way

7 ft above water line

16 ft road way 4 ft below

~~107+10~~ 2 x 3' concrete culvert
Wings 2 x 3 10 ft long

70

70

00

457 2x3 0

~~167~~

37+38 4x20 X

45+60 2x4 X

59+25 6x20 X

91 50x50 X

102+10 2x3 0

Walker B McClain

293-6

Plainfield

S Oak N 31 1/2 W 86 l

Beech N 6 1/2 E 83 l

54+490 1

590+150 2

526+450 3

532 0 4

561+730 5

572 6

596+650 7

5105+640 8

522+570 9

5x12

2x30

4x10

3x6 X

3x4 X

1x15

3x6 X

4x16

2x3 0

5280) 11134 (2.10

10560

5740

5280

4600

sta. 158

Gladden Rd.

4+48 Bridge 16 ft. road way

12 ft. water way

~~5 ft. wings~~

10 ft. straight cuts

8 ft. high 5 ft. above water line

~~20+15 2' x 3' concrete sewer~~

16' in clear

26+45 11' x 10' bridge

16 ft. road way

5 ft. wings

52 r 2 ft deep 6 ft wide

61 N 3' x 4 ft. concrete

let down culvert down

bed of stream

72 18 ft water way

to No 2 7 ft. above water line

5 ft clear

Bridges

16 ft road way

wings 5 ft straight back

88. 14" Sewer use the old
old lay in concrete

96 r 3' x 6' concrete culvert

straight wings

16 ft road way

105 r 16 ft. water way

4 ft above water line

16 ft road way wings straight

121+88 Bridge 2' x 3' X

122+97

5 }

3 5 }

160

20.00

5X 12

2X 3

4X 10

3X 6

3X 4

7X 18

14" Sew

3X 6

4X 16

2X 3

Tonn

Lukeluffey

Joe Prewitt

5.30

21.50

31.50

22

34.40

36.00

51.00

130.00

39.00

143.40

20.40

123.00

4.50

1.89

1.65

8.04

163.20

103.75

267.00

578.04

123.00

39.00

1.25

6.00

31.50

21.50

~~1.25~~ Prewitt

1.89 Haven

38 Snipes

1.25 Pulley

5.15

103.80

123.00

540.00

5.00

2.00

4.00

3.00

10.00

27.00

5.00

8.00

346.80

266.90
10.666

1980
 10565
 12257
 1697

3760
 2496
 6250
 3280

A of circle = πR^2 970
 V of cone = $\frac{Ah}{3}$ a = area base
 h = altitude

Corner for Baickett

80 120 | 600 | 30
 50 4
 120

35' 7"

4 08.12
 181
 21
 30
 12

26
 96
 48
 57
 175

36
 96
 216
 608
 1296

LETTER

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.