

← LETTER →

1909

OSLER GOOD ROAD  
LUCY KING DRAIN

20

Indianapolis, Indiana

2 Leslie Good Rd.  
17-2E

8+77' Cen old Wooden bridge  
13+19.8' Turn East. 442'  
20+91.75 " North Def. L. 87°12'  
39+88.5 Def. R. 57' = Peg 15' W. of cent.  
43+65' - Old Wooden Br.  
47+51 " + " roads S.E. cor. Wm  
52+60 = 15 24" Sewer = Should be  
60+76.5 Cor. Stone N.E. cor. Wright's  
65+70' is 24" Sewer = 6' Bridge  
69+69' is 12" Box sewer = 18"  
79+92.5: Leaves Co. line  
↳ 90° 19' Def. R.  
89+12.4 Def. L. 55° 49'  
95+00 Def. R. 6° 58'  
99+00 Def. L. 3° 48'  
102+55.4 Def. L. 28° 48'  
103+00 Def. L. 9° 36'  
104+00 Def. L. 7° 50'

6' Span

In front Wm Tamlinson's house  
5' Skew Left Wheel forward  
Hamiltons Def. R. 3° 28'  
(6' Bridge)  
Formerly Wm Hamilton & S.E. cor Leslie Good  
Def. R. 3° 19'

78+89 Cor road run West

R.  
Turn at Ad. Wilson's  
2nd Stat. below Ad. Wilson's house  
Near culvert. Not  
Corner of S.P. Wilson's yard & road.

90+45

23

Sta. <sup>4</sup> + -  $\pi$  Rod

104+81.2 Defl. L. 23° 28'

105

105+53.9 Defl. R. 50° 48'

121+56.4 Defl. L. 32° 35'

122+00 Defl. L. 40° 26'

122+90.93 Defl. L. 13° 35'

133+00 Defl. R. 16° 12'

134+92.6

Road running east

Turn at Lavett D. W.

In front of C. B. Bragg's house

End of course

10									11
Sta.	+	-	π	Rod	Flev.				
						502	Top	at end of course	
π	2.70		502.70						
0				7.50	95.20				95.20
1				6.85	95.85				96.40
2				3.45	97.22				97.40
3				4.20	98.50				98.55
4				3.25	99.45				99.20
5		96.60		3.70	99.00				99.20
6		97.39		4.70	98.00				98.20
70				6.10	96.65				96.80
π	.79		497.39					S. J. Starkey	
B.M.		9.31			88.08			Gate at stat. 4 going east	
B				6.50	90.89			Big rock just west of bridge	
B+77		7.28			90.11			Center of bridge north of Starkey's	
		10.8?			88.59			Down stream side.	
		8.8			88.21				
9		92.89		7.85	89.54				91.40
10		8.82			92.34				92.20
110		701.71		5.05	92.25				92.20
π	8.82		501.71	4.50	92.89				92.30
			501.61						

Sta. + -  $\Sigma$  Rod

12			501.71	6.2	95.51 95.86
B.M.		4.49			97.22
13				5.0	96.71 96.65
14				4.6	97.11 97.05
15		97.21 3.00 102.21		3.9	97.81 97.76
16.0			102.21	4.5	97.21 97.16
$\Sigma$	5.00		502.10		
17				4.4	97.70 97.61
18				4.7	97.46 97.45
19		93.85 5.11 98.96	93.74 5.11 98.85	5.1	97.00 96.95
20				6.8	95.30 95.35
B.M.C.		8.36			95.41
$\Sigma$	5.11		98.96 <del>98.85</del>		
21				4.8	94.15 94.16
22				4.6	94.20 94.36
23		95.76 3.71 99.47	95.60 3.71 99.31	2.8	96.00 96.16
24.0				3.2	95.60 95.76
$\Sigma$	3.71		99.47 <del>99.30</del>		
25				4.0	95.31 95.47

S.E.  
Rock at corner

At corner

Corner stake at N. defl.

94.16

94.36

96.16

95.76

95.47

94.85

96.80

97.25

97.80

97.75

97.60

97.60

97.20

95.60

94.20

94.20

96.00

95.60

95.40

14  
Sta

+

-

π

Rod

26

99.36

99.47

4.9 94.46

94.57

7.8

91.67

26+6.0

4.9

97.4

27

92.87

95.74

4.0 95.31

95.47

280

103.01

102.90

3.8 93.76

95.87

π

103.14

103.01

~~102.90~~

29

5.3 97.10

97.21

30

4.3 98.65

98.71

31

101.11

101.40

2.5 100.55

100.57

320

105.16

105.05

1.90 101.00

101.11

π

4.05

105.16

~~105.05~~

33

4.5 100.5

100.66

34

4.7 100.25

100.46

35

99.36

99.25

5.1 99.3

100.06

360

104.30

104.19

5.80 99.25

99.36

π

4.21

104.30

~~104.19~~

37

4.6 99.2

99.40

38

4.9 99.22

99.40

39

4.4 99.29

99.90

15

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

97.60

Station	+	-	16	17
S-100			104.30	100.66
400		100.00 2.38 <u>102.93</u>	103.04	100.66
T	2.38			100.66
B.M.		1068	101.25	104.66
41		89.93 1.13 <u>91.06</u>	93.23	93.23
o		13.00	90.04	90.04
T	1.13		91.17	89.93
42		80.03 1.75 <u>81.78</u>	81.88	85.08
o			80.03	85.17
T	1.75		77.77	80.03
43			76.8	76.8
73+65		5.65	72.8	72.8
B.M.		4.74	76.1	76.1
44			71.9	71.9
450		9.86	77.53	77.53
T			72.02	72.02
460		84.44 12.66 <u>97.04</u>	76.4	76.4
T			79.9	79.9
47			73.02	73.02
			75.91	75.91
			80.04	80.04
			88.55	88.55
			91.9	91.9
			96.05	96.05

88.55  
12.66  
101.15

100.66  
2.38  
103.04

90.04  
1.13  
91.17

100.66  
Gate on road at intersection

Pay on front of the gate  
Grass surface must be 90.60  
- 93.34

85.17  
84.30

76.8  
78.00

72.02  
Down stream side of

76.4  
76.58

80.04  
78.00

88.55  
88.55

91.9  
92.20

Stat	+	-	Rad Elev
47.57		3.1	99.97
48			99.55
49.0			99.39
T	4.20	104.40	100.20
50		200.29	96.18
51.0			101.70
T	1.18	94.48	97.24
52		90.37	93.30
52.60			39.19
53.0			86.08
T	5.17	89.74	81.36
54			80.5
54.60		9.76	84.57
54			84.57
55			30.50
56.0		9.8	75.9
T	11.94	98.76	74.10
57			82.30
58			86.34
59			84.65
55			89.80
56.0			99.30
T	9.36	108.66	104.86
57			100.70

97.04  
101.15

47.57			94.40
48			94.20
49.0			94.20
T			94.00
50			88.00
51.0			82.00
T			82.00
52			82.00
52.60			82.00
53.0			82.00
T			82.00
54			82.00
54.60			82.00
54			82.00
55			82.00
56.0			82.00
T			82.00
57			82.00
58			82.00
59			82.00







24

520

$$\begin{array}{r} 103.71 \\ 107 \\ \hline 110.78 \end{array}$$
506.52  
110.63110.78  
506.65

84

85

86

87

880

89

90

91

920

93

94

95

$$\begin{array}{r} 105.56 \\ 3.30 \\ \hline 108.86 \end{array}$$
108.86  
504.76
$$\begin{array}{r} 101.56 \\ 2.63 \\ \hline 104.19 \end{array}$$
104.19  
500.99
$$\begin{array}{r} 91.97 \\ 9.26 \\ \hline 92.23 \end{array}$$
92.23  
38.19

.26

95

Rod 544

6.2 95.61

6.3 101.5

4.3 102.28

3.2 102.08

4.5 102.13

5.22 101.46

4.17 100.62

4.3 97.41

7.2 97.31

7.30 97.26

97.11

3.0 97.11

7.9 92.24

91.97

6.5 81.40

103.71

104.78

106.68

107.08

106.28

105.56

104.79

101.56

101.46

101.56

101.19

96.49

85.73

25

92.60

100.70

101.90

105.00

102.25

101.85

100.90

98.45

96.20

97.00

gate

94.80

87.20

81.40

Stat

79.58  
79.43  
20.03

12.65

80.08  
75.93

79.58  
75.48

96

68.19  
1.00  
69.19

73.00

77.13

73.75

970

69.19

64.09

68.19

67.00

T

1.00

615.09

93

55.8

984.20  
60.09

60.20

57.45  
2.35  
59.80

10.75

58.41

54.9

57.45

52.50

990

2.35

59.50

53.3

57.45

52.50

100

4.1  
48.25  
1.13  
48.40

48.40

43.2

52.90

58.75

1010

44.15

48.25

54.35

T

15

44.30

44.10

54.35

102

40.50

102+40

18" sewer

32.80

103

38.58  
2.40  
40.98

37.15

41.20

37.60

104

35.20

39.30

35.60

1050

34.7

38.58

34.60

T

2.40

40.98

36.88

106

31.6

35.98

31.30

28

5.50		40.98	Red
10.00		36.88	2.9 29.10
10.00			2.20 27.90
10.00			1.35 26.55
10.00		31.65	
10.00		27.55	
10.00			2.7 23.85
10.00			6.7 20.80
10.00			1.5 22.10
10.00		27.31	
10.00		28.81	23.29
10.00		24.71	
10.00			2.1 21.4
10.00			4.7 19.90
10.00			5.2 19.57
10.00			4.4 20.31
10.00			4.3 20.30
10.00			2.2 22.75
10.00		35.55	
10.00		32.85	
10.00			8.00 24.45
10.00			6.00 26.45
10.00			2.00 29.20

$$\begin{array}{r} 30.60 \\ 1.03 \\ \hline 31.63 \end{array}$$

$$\begin{array}{r} 27.31 \\ 1.50 \\ \hline 28.81 \end{array}$$

$$\begin{array}{r} 25.85 \\ 50.70 \\ \hline 35.55 \end{array}$$

29

33.28	29.40
32.04	28.00
30.60	26.60
27.95	23.80
24.95	21.00
24.15	
112.65	20.40
Center West	
24.11	19.80
23.61	19.90
24.41	20.00
24.57	21.45
25.85	23.00
27.55	24.60
29.55	26.20
32.65	29.00

30

Start  
 0.8.4  $\frac{35.49}{8.50}$   
 43.99

121

122

123

O

T

124

125

126

127

128

129

T

130

131

B.M.

132

32

35.55

43.99

40.09

$\frac{43.22}{5.90}$   
 49.12

77

5.90

49.12

46.19

46.27

43.17

151

Red

35.49

32.30

34.10

35.30

37.20

43.22

40.12

41.10

40.80

41.20

42.50

43.90

45.24

38.0

37.00

41.36

39.5

38.32

37.59

38.99

40.99

44.22

43.92

44.32

45.22

47.12

43.34

41.17

42.17

31.72

41.57

31

Rock east Lovers mill-dike

31.80

36.80

38.00

41.40

41.40

41.40

42.20

41.50

40.85

40.20

39.60

parapet

39.40

32

43.17

46.27

Rod

2.3 40.85

43.97

$$\begin{array}{r} 44.01 \\ 6.33 \\ \hline 50.74 \end{array}$$

44.01

50.74

47.64

5.1 42.45

45.64

42.45

3.5 44.15

47.24

44.00

33

40.90

11.27 course

36

Lucy King

0	21.09	7.40	13.69
		5.20	15.89
1		6.62	14.47
		4.57	16.52
2		7.13	13.96
		5.02	16.07
0		6.54	14.85
	602	<del>20.87</del>	
3		7.10	13.77
		5.03	15.84
4		7.77	13.10
		5.14	15.73

Drain

37

bottom tile

5	20.87	8.19	12.68
		5.22	15.65
6		8.48	12.39
		3.80	17.07
	5.98	<del>23.05</del>	
7		11.27	11.78
		5.58	17.47
8		11.46	11.59
		5.55	17.50
9		11.75	11.30
		5.20	17.85
	5.22	<del>23.07</del>	



10 23.07 12.23 10.84  
4.78 18.29

11 12.40 10.67  
6.25 16.82

3.14 19.96  
12 9.28 10.68  
3.78 16.18

13 9.25 10.71  
4.65 15.31

14 9.32 10.64  
6.70 13.21

4.48 17.69  
15 7.19 10.50  
4.78 12.91

16 7.70 9.99  
5.12 12.57

17	17.69	8.11	9.58
		4.40	13.29

4.00

---

17.29

18		8.20	9.09
----	--	------	------

		4.80	12.49
--	--	------	-------

19		8.55	8.74
----	--	------	------

		4.20	13.09
--	--	------	-------

20		9.05	8.24
----	--	------	------

		3.95	13.34
--	--	------	-------

21		9.40	7.89
----	--	------	------

		4.05	13.24
--	--	------	-------

		8.56	8.74
--	--	------	------

		9.50	7.79
--	--	------	------

		1.50	15.79
--	--	------	-------

---

1.74 17.53

22		9.84	7.69
----	--	------	------

		5.34	12.19
--	--	------	-------

bottom fuel sta 20  
 bottom boiler off  
 by Mr. Heade

23 17.53 10.18 7.35  
6.94 10.59

24 10.50 7.03  
5.96 11.57

25 10.88 6.65  
8.44 9.09

26 11.84 6.19  
8.75 8.78

27 11.65 5.88  
6.55 15.33 6.80 8.53

28 9.75 5.58  
7.36 7.97

0 7.32 8.01  
4.57 12.58

29

12.58

7.67 4.91  
4.42 8.16

30

8.14 4.44  
4.46 8.12

31

8.70 3.88  
3.20 7.38

7.63 15.01

32

12.50 2.61  
8.28 6.73

33

6.96 12.17

9.80 5.21

10.20 1.97

11.10 1.07

34

8.01 8.48

11.70 4.80

bottom runs of life  
detrit

46

34	Water	8.48	5.25	3.23
			8.48	00

47

Watermark W. H. C. C.