

LETTER

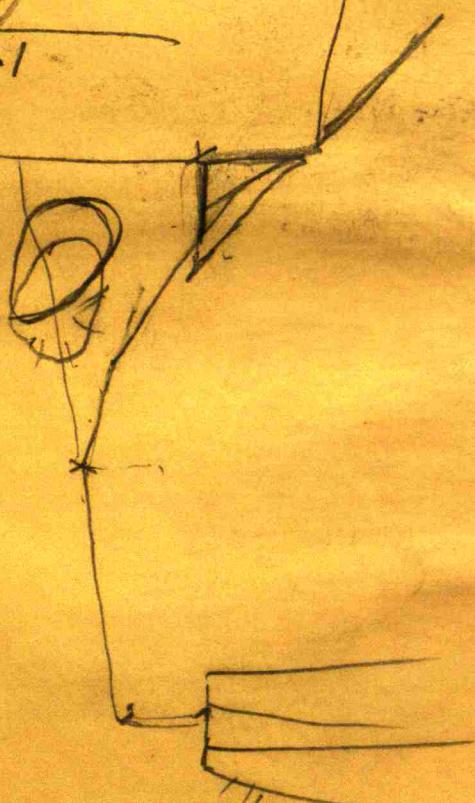
1910

ROY MOORE SURVEY  
MC CLELLAND ET AL ROAD  
SUGAR GROVE BRIDGE  
DAVIS BRIDGE

$\frac{40.4}{1.55}$   
 $\underline{38.90}$ 

 $\frac{21.9}{89.1}$   
 $\underline{60.9}$   
 $\underline{39.12}$   
 $\underline{2.1}$ 
  
 0- 1-  
18m from 18fr

$\frac{655}{160.9}$   
 $\underline{494.1}$



Com E. side bridge  
 then S. 87° W. 1219' to N side  
 bridge,  
 then S. 87° W. 391-8 sta.  
 " N 110° W. 494.4'  
 to Sta 6+55.  
 then N 11½° E 45"  
 " N 22° E. 100'  
 then N. 78'

2

STA B.S. H.I. F.S. Rod  
 BM 2.15 ~~6.00~~ ~~6.00~~  
 1+60<sup>9</sup>' 10.40 6.30  
 2 160.9 10.70  
 3 121.9 11.20  
 4 39 7.80  
 5 8.50  
 6 9.25  
 0 6.30 97.05 9.25  
 6+55 3.90  
 7 2.60 93.15  
 8 4.05 94.45  
 8+78 4.05 93.00  
 9 3.85 93.00  
 10 3.45 93.20  
 11 1.00 93.60  
 12 1.15 96.05  
 0 7.90 103.80 1.15 95.90  
 13 2.55

3

Elev.
97.85
93.70
89.30
88.80
92.70
91.50
90.75
93.15
94.45
93.00
93.00
93.20
93.60
96.05
95.90
101.25

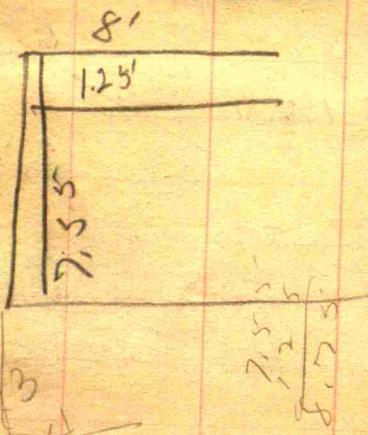
STA	B.S.	H.I. 103.80	F.B.	Rod	Elev
14				.90	102.90
15				1.50	102.30
①	.50	102.80	1.50		
16				7.30	95.50
17				7.45	95.35
18				6.50	96.30
19				5.50	97.30
20				8.15	99.65
②	2.95	102.60	3.15		
21				3.90	98.70
22				4.30	98.30
23				3.85	98.75
24				.70	101.90
③	5.45	107.35		70	
25				6.20	101.15
26				5.45	101.90
27				4.50	102.85
28				3.00	104.35

$$\begin{array}{r} 102.80 \\ -6.95 \\ \hline 95.85 \end{array}$$

$\frac{20}{33}$

5

BM. S.side Boiler Sides = 6.95 = 95.85  
 Top Hill Hadley's Sals 2ft Cut  
 15+54' iron Boiler, 5.7' dia 16.7' long,  
 South side far enough - Concrete Head  
 In 3.3' <sup>S</sup>Concrete Head,



Mc Clelland Rock?



8

	Sta B.S	H.d F.S.	Rod
41		164.85	7.65 157.20
42			7.50 157.35
①	6.90	164.25	7.50
43			4.50 159.75
44			4.25 160.00
45	-		3.20 161.05
46			4.15 160.10
47			3.60 160.65
①	6.30	166.95	3.60
48			5.15 161.80
49			4.65 162.30
50			5.25 161.70
51			5.25 161.70
52			2.80 164.15
①	4.00	168.15	2.80
53			4.50 163.65
54			4.25 163.90
55			3.90 164.25

9

40

Sta	B.S.	N.S.	F.S.	Rod
56		168.15		5.00 163.15
①	2.50	164.90	5.75	BM. Stow Cor. See Road S. = 162.40
57				2.60 162.30
58				2.10 162.80
59				.85 164.05
60				3.30 161.60
61				3.90 161.00
62				4.50 160.40
63				5.40 159.50
64				4.40 160.50
65				5.20 159.70
66				5.00 159.90
①	1.40	161.80	5.00	
67				2.55 158.75
68				7.30 154.00
①	.70	150.00	12.00	
69				7.00 143.00
70				11.05 138.95
BM	10.75	S. 8 cor Horden Bridge		139.25

41

168.15  
3.20  
162.40

168.15  
3.20  
162.40

130.75  
92.5

12

B.S. H.D. F.S. Rod  
 0 3.95 143.20 10.75

71 4.85 138.85  
 72 2.55 140.65  
 73 6.80 135.40  
 0 4.65 137.25 10.60

74 7.40 129.85  
 75 6.70 130.50

0 11.70 148.20 .75

76 8.50 139.70

0 10.20 157.75 0.65

77 8.70 149.05  
 78 1.85 155.90

0 5.20 .20

79 4.60  
 80 4.30  
 81 3.70  
 82 3.40  
 83 3.40  
 84 2.90

← LETTER →

13

70 + 34' = 7 Bridges Total Bridge above  
 Water line - 6.90

74 is 19% of S. end of East  
 abutment  
 75 Blue Abner Creek

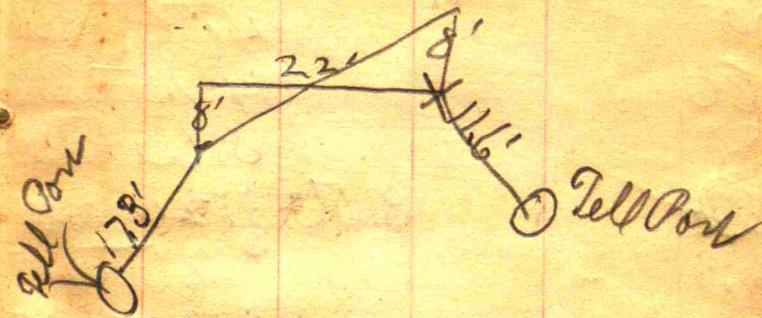
10.60  
 10.4.65  
 10.4.90  
 5.25  
 4.20  
 10.20  
 12.75  
 12.95  
 7.40  
 7.60  
 7.10  
 2.10

10.95  
 10.65  
 10.40

Sta B.S. H.D. F.S. Rev

0	5.30
85	2.90
86	<del>4.25</del>
87	<del>3.90</del>
88	<del>4.40</del>
89	<del>4.00</del>
90	<del>3.35</del>
91	5.70
92	3.50
	5.30
	5.15
	4.95

15



Sta 72 - Vert. of top of hill  
N. of creek

16

3.50

St. B.S. N.D. F.S. Roy

5.15 162.70 .20

79	4.50	158.20
80	4.15	158.55
81	3.60	159.10
<del>82</del>	3.50	3.20 159.50
83	3.25	159.45
84	2.75	159.95
(1)	5.50	165.45 2.75
85	4.70	160.75
86	8.70	161.75
87	3.35	162.10
88	3.85	161.60
89	3.50	161.95
90	2.85	162.60
(1)	5.65	168.00 3.10
91	5.25	162.75
92	5.10	162.90
93	4.85	163.15

17

91 to W. end one Grade

18

Sta B.S. N & F.S. Rod			
94		3.45	164.55
95		1.55	166.45
B.M. 10	Geo. Stone	Board \$10.00	N
① 6.60	174.50	.10	
96		6.30	168.20
97		3.85	170.65
98		1.60	172.90
99		1.55	172.95
100		1.20	173.30
① 5.70	179.00	1.20	
101		5.30	173.70
102		4.35	174.65
103		3.20	175.80
104		2.75	176.35
105		1.50	177.50
① 7.95	185.45	1.50	
106		6.90	178.55
107		5.60	179.85

19

$\frac{18}{3} \times$

95 + 55' = 12" Sewer 20'

---

91 + 63' = Sewer

Old Bridg  
6' Mid 2' Deep

New - See where 18"

---

80 - Sewer

T 12' Til. Ditch down  
to N Earley

105' to head of ditch

<sup>20</sup>  
SL BM H & FS Qoy  
108 3.90 181.55  
109 2.80 182.65  
109 + 68' 2.40 183.05  
BM 1.15' Cen. Ston St, 2nd of Plot  
<sup>=</sup>  
Elev = 184.30

<sup>21</sup>  
Comifit Sla 27  
67-OK

68- S. half way 6.5'  
higher than cen. road  
now

68+60' is 12' high

69- S. line 30' is 6' high  
from level road now

69 now is about level with  
road running S.

145.0

26.20

157.20  
103.85  
43.35

- 37 - 8.5' grade at bottom  
38. S. 2'  
38 N 18"  
  
37. Road way 20'  
at bottom of present  
grade.  
37 S. 8.5' now  
37 N 7" "  
36 + 26' N cut leaves off  
+ fill commences  
  
36 No cut on N  
36 S  $\frac{1}{2}$  Road way 10 ft  
36 S. 14' bank  
35 S 12" 11"  
  
35 + 50 No cut on S bank

- 23
- 34 - 10 ft N. of Cen is lower  
edge of fill - full 2'  
35 Cen was Edg 8 ft  
36. " " 10 ft edge of fill  
  
36 on N. fill now 20'  
35 " " " " 10'

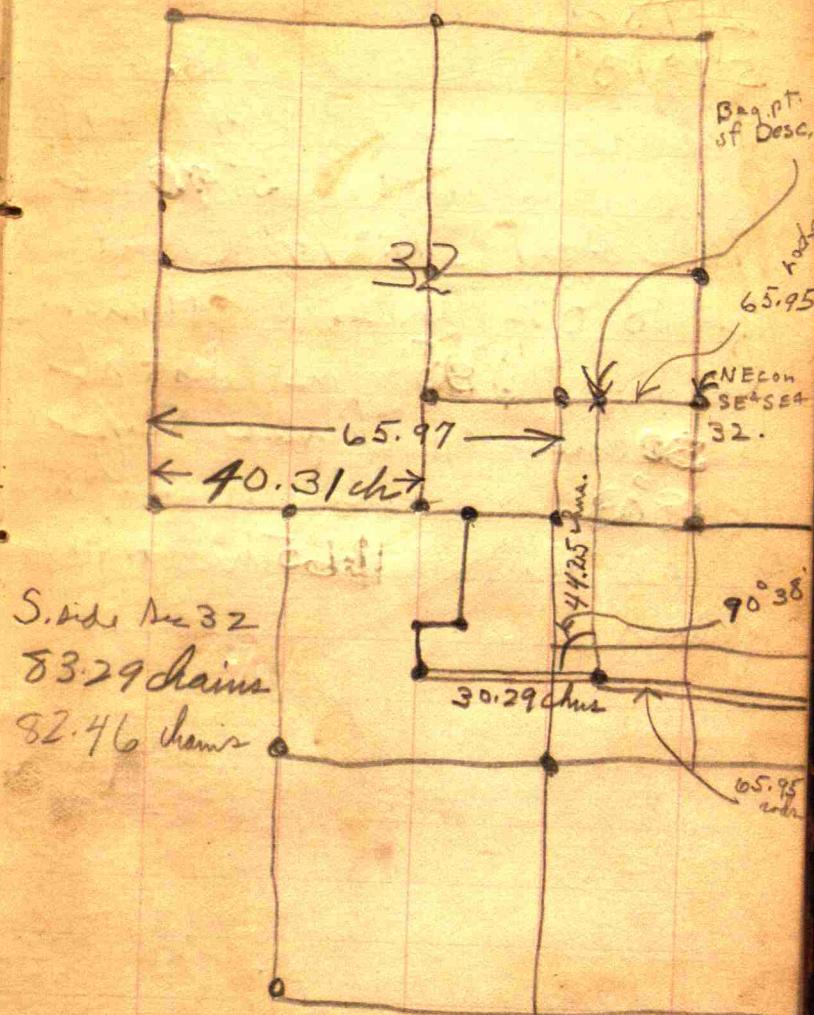
32

Survey for Roy Moore

Sec 5 & 32 T p 16 N R 2 W

Located Beg pt of Desc. 16.49<sup>t</sup>  
tho W of N.E cor SE<sup>4</sup>SE<sup>4</sup> Sec. 32.  
Chained S along Moore E line to  
Cerr. at dist off 44 27.5 chains.  
Thence Def. right 89° 32' and running  
5 89° 22' W, a dist of 30.29 chains to  
Moore S.W. cor. Thence Def. r 90°  
38' and running thence N 4.495  
chains. Thence E. 4,275 chains  
thence N 80 chains tho a point  
on the ~~H. L.~~ line dividing  
Sec 5 and 32. Thence Def. R. 90°  
and running E or side dividing  
line to a point in the bar of the  
stream known as the W. Fork  
of Eel River a dist of 19.64 chains  
Thence Def L 71° 30' a dist of 3.76 chs  
Thence Def L 49° 16' a dist of

33



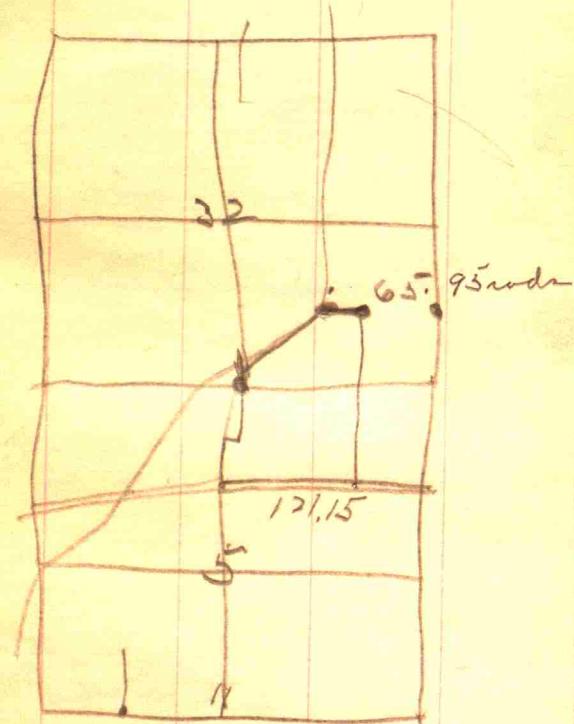
34

2.78 ch. Then 10° R  
 $57^{\circ} 13'$  a dist of 3.59 ch  
 Then Def R  $49^{\circ} 47'$   
 a dist of 5.96 ch  
 Then Def L  $18^{\circ} 19'$  a dist  
 of 8.02 chains. Then  
 Def. L  $73^{\circ} 08'$  a dist of  
 5.20 chain, Then Def  
 R  $15^{\circ} 08'$  and Runing the  
 E a dist of 11.65 ch to place  
 of beg.

35

38

39



40

41

90°38' | 89°22' | 90°38'

136 McClelland Et al Rong

Sta	B.S.	H.F.S.	Rod
	B.M.	2.75	Cor Stone
0	2.75	102.75	2.75 100.00
1			3.10 99.65
2			3.95 98.80
3			5.20 97.25
4			6.70 96.05
5	X		8.85 92.55
0	3.80	96.35	8.35
6			4.80 91.55
7			4.85 91.50
8			8.25 93.10
9			3.10 93.25
10			2.95 93.40
11			1.60 94.75
12			.50 95.85
0	2.45	98.30	.50
13			1.30 97.00

B.M.	145	2.75
4 =	5.65	<u>145</u>
5 =	7.05	<u>130</u>

130	6.70	2.75
130	5.00	1.30

6+50 Saver 4'x2'x20'

no cut or finish  
7 to 14 Grade

	B.S.	N.I.	F.S.	Rod
8				
14		98.30		2.70 95.60
15		5		3.35 94.95
16	9 <sup>1</sup> / <sub>2</sub>	3 <sup>1</sup> / <sub>2</sub>		4.20 94.10
17	8 <sup>1</sup> / <sub>2</sub>	6 <sup>1</sup> / <sub>2</sub>		5.10 93.20
18	8			5.70 92.60
19				5.90 92.40
①	2.40	94.80	5.90	
20				3.05 91.75
21	5 <sup>1</sup> / <sub>2</sub>			3.35 91.45
22	9 <sup>1</sup> / <sub>2</sub>	6 <sup>1</sup> / <sub>2</sub>		4.00 90.80
23	9 <sup>1</sup> / <sub>2</sub>	5 <sup>1</sup> / <sub>2</sub>		4.05 90.75
24	9			4.60 90.20
25				4.60 90.20
26				4.70 90.10
① BM	1.00	90.50	5.70	
27				1.00 89.10
28				1.25 88.85
29				3.30 86.80

14 to 26 Change on Lillies

new } possible

89.10  
1.85  
90.9

90.10  
1.85  
91.95

21+67' 12" Sewer 18' fr

24+72" Sewer 12" 18' long

90+BM =  $\frac{1}{2}$  mission

but add } possible

140

STA B.S. HI F.S.

30	Rod	
31	5.10	85.00
32	6.65	83.45
33	7.85	82.25
0	9.40	80.70
34	2.90	83.60
35	9.40	79.55

35	78.90	
BM	1.65	
36	81.95	
37	4.30	79.30
38	3.35	80.25
0	1.15	82.45
39	7.55	90.00
40	1.15	

41	4.60	85.40
42	4.40	85.60
43	3.85	86.15
44	2.50	87.50
	4.30	85.70
	6.40	83.60

141

Rod

5.10	85.00
6.65	83.45
7.85	82.25
9.40	80.70

4.70	78.90
4.30	79.30

81.95	On top of large rock on or side ditch.
3.35	Bridge - Rod Bed Ditch - Water Line 10.00
1.15	" " Top old Bridge = 4.15

82.45	
7.55	90.00
1.15	

4.60	85.40
4.40	85.60

3.85	86.15
2.50	87.50

4.30	85.70
6.40	83.60

CUT 1 $\frac{1}{2}$ 

40  
 41  
 42  
 43  
 44

40  
 41  
 42  
 43  
 44

142

Sta B.S. H.I. F.S. Rod

0 3.90 87.50 6.40

45

4.60 82.90

46

4.65 82.85

47

3.85 83.65

48

3.20 84.30

49

3.45 84.05

50

3.80 83.70

0 7.45 91.15 3.80

51

7.85 83.30

52

5.70 85.45

53

6.70 84.45

53+26'

7.40 83.75

BM 7.15-

Stoneburg Road 84.00

143

6" fill

 $45 + 27 = 18$ " sewer 18' long

26

2" cut

 $50 + 64 = 12$ " sewer 18' long

1" fill

1

146

(51 $\frac{1}{2}$  ft low)

Sugar Grove Bridge.

S.E. cor. Stat. Grounds.

Beg. point N. 70° 26' E. fence Post 15 ft.

Run on S. side Creek  
15' N. of fence Post on S. side road  
29' S. W. to 11' 1" N. " "  
19.3 ft N. N. W. Brace for telephone post.

S. 31 $\frac{1}{2}$ ° N - Roads

O = 2 N 31 $\frac{1}{2}$ ° E 21 ft from pig pen

147

148

BM. 1.65  
~~0.15~~

0	8.35
1	2.65
2	<del>3 1/2 ft</del>
3	3.85
4	5.25
5	6.20
6	7.05
7	8.00
8	7.65
9	9.50
10	4.85
11	7.50
12	7.65
13	7.40
14	7.30
15	6.85
16	7.34
17	3.45
18	2.65
19	3.75
20	2.55

BM 1.70 Sent over Bank for

9.50  
3.35  
~~2.15~~11.40  
2.65  
8.7  
~~6.95~~  
19.1010.80 In Water 15.8 ft Sta 9  
11.40 " " 8 ft Sta 10

10.10 " S. abutment

10.40 Edge of Water

brace on N. side Done

150

## Davis Bridge

Sta B.S. H.D., F.S. Rod

BM. 2.87

0	.85
1	3.50
2	5.45
3	7.25
4	7.15
5	4.45
6	- .40

July 9. 12.65 ft

History May 24.2 ft

151

May 26

BM Tideline Post outside creek  
+ E. side of road.

North side of bridge in  
line with lensing feature  
Bottom W side of road  
+ with a large tree closest  
150 cfs inflow

End of bridge Post tree  
Mark S. N. about  $60^{\circ}$  W