
1911
ANDOLPH ROAD
HAYS DRAIN
C.W. McClain

LEVEL CIRCUIT STA. ALLEY

Sta.	B.S.	H.I.	F.S.	Elev.	Notes
SL.B.M.				613.91	
T.P.	2.284	616.194			
⊙			5.299	610.895	
T (2)	4.031	614.926			
⊙ (2)			3.247	611.679	
T	2.470 2.570	614.249			
B.S. of W.P.	6.082	617.761			
			3.374	614.387	
T	2.410	616.719			
⊙			2.193	614.526	
T	3.659	618.187			
⊙			7.078	611.109	
⊙			8.660	609.527	
T	8.170	617.697			
⊙			3.470	614.227	
T	1.940	619.167			
B.M.			2.699	616.468	

ALONG N. GRANT, N.W. Ave. AND N. St.

Elev of water plug N.W. Ave and Grant

Elev. of Water Plug N.W. Ave and Grant

Reading 2.5 on rod. Top of N.W. proj.

Elev. of Water Plug at W.A. Ave and N. St.

LEVEL CIRCUIT STADIA LEVEL

Sta.	+B.S.	H.I.	-F.S.	ELEV.
S.L.B.M.				613.91
T (1)	2.156	616.068		
⊙ (1)			-5.077	610.989
T (2)	4.376	615.365		
⊙ (2)			-5.186	610.179
T (3)	6.114	616.293		
			-1.586	614.707
⊙ (3)			-6.704	609.589
T (4)	5.[illegible]	[illegible]	615.318	
⊙ (4)			-2.578	612.740
T (5)	1.410	614.150		
			-5.696	608.454
⊙ (5)			-3.513	610.637
T (6)	6.251	616.588		
S.L.B.M. 26036			-2.994	613.894
			-26.048	
			+26.036	
			-.012	(Check)

Leveled O.H. Gosswein Oct. 4, 19[illegible]
Rodman C.W. McClain Clear and Warm
ALONG N. GRANT N.W. AVE. AND N. 5[illegible] ST.

615.0	615.0	615.50
5012	5012	5055
3015	3015	3015

Water Plug Grant St. and N.W. Ave. Top nut next to Grant St.

N. nut on [illegible] [illegible] N.S.K.

OCT 7 - 1911

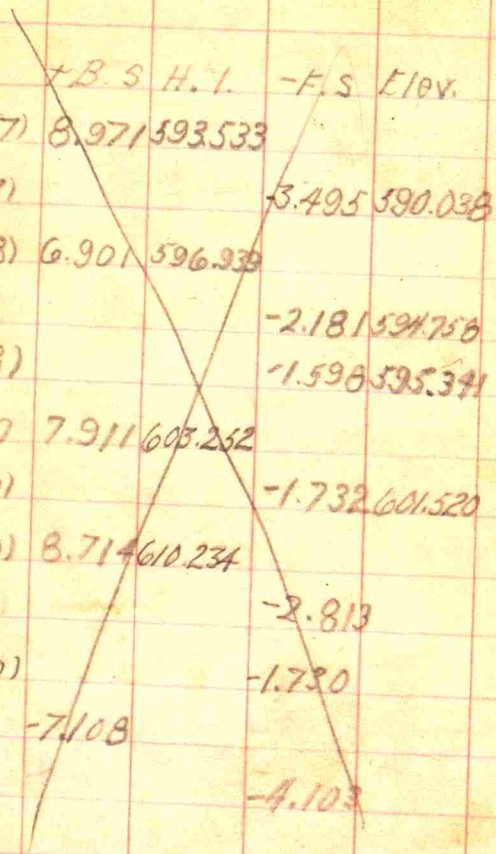
LEVEL CIRCUIT, SEA LEVEL

Sta	+B.S	H.I.	-F.S	Elev. S.L.B.M.
				617.91
⊼ (1)	3.117	617.027		
⊙ (1)			-1.432	615.595
⊼ (2)	3.104	618.499		
⊙ (2)			-7.715	610.784
			-5.535	612.964
⊼ (3)	1.482	612.966		
⊙ (3)			-8.904	603.362
⊼ (4)	1.141	604.503		
			-2.966	601.537
⊙ (4)			-8.953	595.550
⊼ (5)	2.024	597.574		
⊙ (5)			-8.547	589.027
⊼ (6)	0.874	589.901		
			-5.383	584.518
⊙ (6)			-5.339	584.562

ALONG

N. nut of Water plug cor. State St. & Bra. St.

N nut of water plug cor



	+B.S	H.I.	-F.S	Elev.
⊼ (7)	8.971	593.533		
⊙ (7)			3.495	590.038
⊼ (8)	6.901	596.939		
			2.181	594.758
⊙ (8)			1.598	595.341
⊼ (9)	7.911	603.252		
⊙ (9)			1.732	601.520
⊼ (10)	8.714	610.234		
			2.813	
⊙ (10)			1.730	
	7.108			
			4.103	

	+B.S.	H.I.	-F.S.	FLEV
				613.91
T (1)	2.930	616.860		
		616.841		
D (1)			-2.480	614.380
T (2)	2.817	617.697		
D (2)			-4.729	612.968
	1.010	611.958		
T (3)	.996	613.954		
D (3)			-6.477	604.481
			-6.64	607.314
	2.790	607.271		
T (4)	2.35	609.464		
D (4)			-9.354	597.917
			-5.457	600.807
	.766	598.657		
T (5)	.756	601.563		
D (5)			-7.526	594.157
			-7.301	594.262
	3.644	594.801		
T (6)	1.210	595.472		
D (6)			-11.637	583.163
			-8.446	587.026
	1.740	584.909		
T (7)	1.296	583.948		
D (7)			-4.843	
			-5.845	583.153
T (8)	7.101			

M. not on midpoint of South and State Sts.

M. not on midpoint of South and State Sts.

LEVEL CIRCUIT, SEA LEVEL ALONG N. GRANT STATE TO S.E. [illegible] TO [illegible]

Leveler C.W. McClain Oct 6 '911
Rodman O.F. [illegible] [illegible]

	+B.M.	H.I.	−F.S.	Elev.	Remarks
S.L. B.M.				613.91	
π (1)	2.950	616.860			
O (1)			−2.480	614.380	
π (2)	3.317	617.697			
O (2)			−4.729	612.968	N. nut on hydrant at Grant and State Sts
π (3)	1.010	613.978			
O (3)			−6.477	607.501	
π (4)	2.790	610.291			
O (4)			−9.354	600.937	Top of hydrant at State and [illegible] Sts
π (5)	.766	601.703			
O (5)			−7.526	594.177	
π (6)	3.644	597.821			
O (6)			[illegible]	586.189	
π (7)	1.740	587.929			
O (7)			−4.843	583.086	Top of N. nut on hydrant at S[illegible] [illegible] Salisbury
π (8)	7.943	591.029			
O (8)			−1.372	589.657	

T(9)	7.025	596.652			
			-2.402	594.250	West bk water plug at N. end Docks.
D(9)			-1.094	595.086	
T(10)	9.515	605.16			
D(10)			-1.526	603.377	
T(11)	6.574	610.951			
D(11)			-1.722	609.429	Water plug at N. St. and N.W. Ave.
T(12)	6.570	614.999			
D(12)			-2.350	612.649	
T(13)	9.231	616.340			
S.L.B.M.			-2.474	613.866	
			S.L.B.M.	613.910	
				.044	Error

S.L. B.M.	+B.M.	H.I.	−F.S.	ELEV.
S.L.B.M.				6.8.40
π(1)	5.413	623.883		
⊙(1)			−1.413	622.430 621.520
π(2)	6.122 ~~6.2~~	628.602		
⊙(2)			−1.710	626.892
π(3)	4.980	631.862		
⊙(3)			−2.986	628.876
π(4)	5.039	633.915		
⊙(4)			−2.109	631.806
π(5)	6.961	638.76[illegible]		
⊙(5)			−1.045	637.722
π(6)	7.274	644.99[illegible]		
			−3.706	[illegible]41.290
(Check back)				
π(1)	8.618	649.908	−.964	
			−.964	648.944
π(2)	6103	65[illegible].012		

Hydrant at [illegible] in front of [illegible] House

S. end W. retaining wall of concrete culvert on
N. Salisbury Road

	+B.S.	H.I.	-F.S.	ELEV.
⊙ (2)			-1.159	659.80
TP (3)	6.359	659.210		
⊙ (3)			-3.987	653.829
TP (4)	+6.204	661.333		
			-6.58	
	6.362			

LEVEL CIRCUIT SET LEVEL FROM [illegible]

S.L.B.M.	+S.M.	H.I.	-F.S.	ELEV.
				618.40
B.M.	6.777	625.177		
(1)			-2.856	622.321
(2)	7.325	629.646		
			-1.426	623.220
(2)			-1.862	627.784
T(3)	6.914	634.698		
(3)			-2.280	632.418
T (4)	8.952	641.370		
(4)			-1.948	639.422
T (5)	8.857	648.276		
			-6.287	641.989
⊙ (5)			-3.254	645.022
T (6)	9.709	654.731		
(6)			-4.572	650.159
	Check back.			645.022
T. (1)	9.709	654.731		

LEVELER D. H. GOSSWEILER
RODMAN C. [illegible]
[illegible]

N. nut on water plug on Thorn. St. S. Prim. se

N. nut on first hydrant N. of Tunnel on Sals.

✓

S. retaining wall of first culvert on Sals.

Cross on rock at entrance of first lane N. of Culvert

First water plug N. of rock mentioned above

E. I. B. M. of rock mentioned above

	+B.M.	H.I.	-F.S.	ELEV.		
π(1)	1.646	646.568				
			-4.58	641.988		S. retaining wall of first ... on Salisbury
⊙(1)			11.443	635.125		
π(2)	0.787	635.912				
⊙(2)			-8.220	627.692		
π(3)	2.800	630.492				
			-2.258	628.234		N. nut on first hydrant N. of Thorne ... on Salisbury
⊙(3)			-7.237	623.255		
π(4)	2.367	625.622				
			-7.199	618.418		Check on S.L.B.M. of 618.40
				618.40		
				0.013	Error	
S.L.B.M.				650.159		Top of first water tap N. of 1st culvert on Salis.
π(1)	8.784	658.943				
⊙(1)			1.640	657.303		
π(2)	0.310	657.613				
⊙(2)			.830	656.783		

✓

	+B.M.	H.I.	-F.S.	Elev.	
A (3)	8.743	673.596			
⊙ (3)			0.872	672.724	
A (4)	9.234	683.889			
⊙ (4)			2.394	681.495	Boulder at Rotacrks line.
A (5)	6.139	687.634			
⊙ (5)			1.872	685.762	
A (6)	6.282	692.043			
⊙ (6)			0.963	691.080	
A (7)	8.597	702.677			
			2.122	700.555	First boulder N of Rotacrks line
⊙ (7)			1.450	701.227	
A (8)	8.758	709.985			
⊙ (8)			1.734	708.251	
A (9)	7.790	715.992			
⊙ (9)			0.789	715.203	
A (10)	7.539	722.736			
⊙ (10)			1.679	721.057	Elevation of rock
	(Check back to water tap)				

	B.S	H.I.	F.S	Elev.	
T (1)	1.479	702.796			
⊙ (1)			1.285	711.491	
T (2)	1.286	712.577			
⊙ (2)			1.448	702.229	
T (3)	1.423	703.652			
⊙ (3)			5.354	698.298	First boulder S. of Town
T (4)	0.730	699.028			
⊙ (4)			0.340	688.688	
T (5)	1.115	689.803			
⊙ (6)			8.106	681.697	Boulder at Kennebec Lake
T (6)	2.215	683.912			
⊙ (6)			10.247	673.665	
T (7)	1.690	675.355			
⊙ (7)			1.303	674.052	
T (8)	0.928	674.980			
⊙ (8)			12.987	662.042	First winter top S of tank
		Check	1.521	661.459	
		Error	.017		

Leveler C. W. McClain
Rodman O. H. Ba[illegible]n

PROFILE LEVEL COURSE FROM HARRISON TO LUTZ BY CHAU[NCEY]

Sta.	B.S.	H.I.	F.S.	R.	Elev.	
B.M.					(100)	Harrison St. 53[illegible] Water [illegible] of [illegible] Ave. and Chauncey Ave.
	3.02	103.02				Property level [illegible] street
1				4.9	98.12	Intersection of Chauncey [illegible] Ave.
2				4.9	98.12	Chauncey [illegible]
3				4.2	98.82	
4				4.1	98.92	
5				4.7	98.32	
B.M.	(500 ft)		4.19		(98.62)	NE corner of steps [illegible] in front of house No. 2[illegible]
6				5.0	98.12	
6 7				5.6	97.42	
8 0				5.8	97.12	Intersection of [illegible]
T.P.	2.42	99.54				Chauncey
9				3.1	96.44	Wood St 40 ft wide [illegible]
10				4.1	95.4[illegible]	South of Chauncey property level same
11				4.7	94.84	as that of St
B.M.	(1000 ft)		4.06		(95.48)	W corner of extreme end of [illegible] facing
12				5.5	94.0[illegible]	to [illegible] 117

S	B.S.	⊼	÷	R	Elev	
						State St. 40 ft wide
+85				5.8	93.74	Intersection of Chauncey and State St.
⊙ 13				5.2	94.34	Property level [illegible] 3' above St.
				(5.17)	(94.37)	Hydrant at Chauncey and State St. [illegible]
⊼	8.81	103.18				State St. is asphalt with car track in
⊙ 14				4.3	98.88	middle. It has considerable slope to the
⊼	8.29	107.17				east of intersection with Chauncey
15				3.7	103.47	Intersection Main and South Sts
16				2.9	104.27	S. St. 40 ft. wide. Property level same as St.
B.M. ⊙	(1500 ft)		2.62		(104.55)	S.W. corner lower step W. entrance M.E. church.
⊼	8.91	113.46		~~7.8~~		Keon flats comes out to edge of side-
17				7.8	105.66	walk of Main St
18				6.2	107.26	Main St. 40 ft. wide
+38				5.3	108.16	Intersection of Main and Columbia
				2.76	(110.70)	N. nut on hydrant at "
19				4.8	108.66	Columbia St 40 ft wide
20				3.7	109.76	
21 ⊙				2.41	111.05	
⊼	6.37	117.42				

Sta.	B.S.	H.I.	F.S.	Elev.	
B.M.	(2000)		5.33	110.29	Water tap at W.W. corner of N and Main
+67					
			5.7	111.7	Intersection N and Main Sts.
22			3.8	110.6	Top of curb in Main at North
23			5.4	111.8	North St. 40 ft. wide
24			4.7	112.7	Property line on level with St.
+91			4.4	113.3	Intersection of Main and Wiggins
25			4.2	113.2	Wiggins St. 40 ft. wide
B.M.	(2500 ft)		2.00	114.3	Nat. Hydrant at Wiggins and Main
26			4.33	113.1	
27			4.7	112.7	
28			4.8	112.6	
+250			4.54	112.98	Intersection of Fowler and Main
T	3.16	116.04			Prop. line 2 ft. above St. level Fowler
29			4.3	111.7	Fowler 40 ft. wide
30			6.4	109.6	Property surface between Fowler and L.
B.M.	(3000 ft)		8.12	107.92	8 about 1' above street on W. and level on E.
31			8.2	107.8	Water tap in front of house #22 Main
32			6.7	109.3	

	B.S.	H.I.	F.S.	R.	Elev.
+79				1.5	114.5
		Check back			
					114.54
T (1)	1.5	116.04			
O (1)			-3.00		113.04
T (2)	3.8	116.84			
			-2.42		114.42 Hydrant at Wagner and Main
O (2)			6.80		108.04
T (3)	.5	108.54			
			-3.95		104.59 Bolt on church steps S.W. corn. SS room ent.
O (3)			-1.3		96.64
T (4)	6.5	103.14			
O (4)			4.6		98.54
T (5)	5.1	103.64			
O (5)			3.56	100.08	

Check 100.08 Error.

V

JAN 9 - 1912

DEDUCT RESULTS ..... DRAFTING .....
GRADE 80.

38

Randolph Road

Stat	+	−	Elev.
B.M.			100
	61		100.61
0		5.40	95.21 95.21
1		5.10	95.51 95.86
2		4.10	96.51 96.51
3 ⊙		4.05	96.56 96.51
	5.19		101.75
4		5.15	96.60 96.51
5		5.00	96.75 96.51
6 ⊙		7.21	94.54 94.60
	4.00		98.54
7		4.00	94.54 94.60
8		4.75	93.79 94.60
9 ⊙		4.28	94.26 94.60
	7.04		101.30
10		5.88	95.42 95.86
11		2.90	98.40 97.00
12		4.80	96.50 97.00

39

Iron post top at 0+50

10" crown in sub-grade

7+80 18" sewer in good cond.
Concrete around pipe for form

18" sewer in good cond.

Randolph Road

Sta	+	− 101.30	Elev	
13		3.68	97.62	97.00
	4.98	102.60		
14		4.65	97.95	98.00
15		4.35	97.25	98.00
16		1.90	100.70	99.00
	2.65	103.35		
17		3.85	99.50	99.00
18		5.45	97.90	99.00
19+8		4.60	98.75	99.00
BM 0		3.36	(99.99)	
	5.95	105.44		
20		7.00	98.44	99.00
21		3.10	102.34	101.50
22		.10	105.34	104.00
23		1.75	103.69	
?	4.78	108.47		
24		4.90	103.57	104.00

14+50 18" sewer

19+56 gate to backlot
N parapet of bridge

Randolph Road

		+	108.47		
26	5		4.95	103.52	104.00
26	⊙		5.44	103.03	104.00
		5.40	108.43		
27			5.10	103.33	104.00
28			4.80	103.63	104.00
29			4.20	104.23	105.13
30	⊙		3.35	105.08	106.26
		6.70	111.78		
31			5.55	106.23	107.39
32			3.55	108.23	108.40
33			1.40	110.38	109.00
34	⊙		3.19	108.61	109.00
		3.53	112.14		
35			3.60	108.54	109.00
36			6.00	106.14	~~107.60~~ 107.84
37			6.55	105.59	~~106.20~~ 106.68
38	⊙		6.61	105.53	~~104.80~~ 105.48
		3.98	109.51		

15" 24"
Steel sewer in place 26' long

J. Fordills gate

24" 18"
36+80 12" steel sewer in place

Randolph Road

+	−			
	109.51			
4039	3.00	106.51	~~103.46~~	104.32
4140	5.70	103.81	103.16	
4241	8.20	101.31	102.00	
4240	7.65	101.86	102.00	
10.60	112.46			
43	8.65	103.81	104.66	
44	5.60	106.86	107.33	
45	2.60	109.86	110.00	
460	.85	111.61	110.00	
3.60	115.21			
47	3.50	111.71	110.00	
48	4.70	110.51	110.00	
49	5.55	109.66	110.00	
500	6.58	108.63	110.00	
535	113.98			
51	5.85	108.13	110.00	
	8.00	(105.98)		

12" steel
L shaped headw. on N end
15" x 30"

50+90 ~~8~~ 10' flat top T skew r.w.f.

Water level at 50+90

Randolph Road

	+	−		
		113.98		
		7.85	106.13	Top of tile at bridge
		4.00	109.98	Rhoades gate
52		4.50	109.48	110.00
53		.85	113.13	111.67
O		.66	(113.32)	
	6.00	119.32		
54		5.00	114.32	113.34
55		4.85	114.47	115.01
		8.15	111.17	
56		3.25	116.07	116.68
57 O		.75	118.57	118.35
	5.77	124.34		
58		4.90	119.44	120.00
59		4.35	119.99	
59		4.20	120.14	120.00
		6.10	118.24	
60 ⊙		3.80	120.54	120.00

Top of tile at bridge

Rhoades gate

36 Cement

Water level 54 +85 10's skew bad.

Randolphs yd. gate

18" pipe in place, bad conn.

Water level 18" to go in

	+	120.54 —		
	8.35	128.89		
61		6.55	122.34	122.75
61+10		5.40	(123.49)	
62		4.75	124.44	125.50
63		1.70	127.19	128.25
0		.65	(128.24)	
	8.20	136.94		
64		6.20	130.74	131.00
65		5.10	131.84	132.00
66		4.00	132.94	133.00
67.0		2.37	134.57	134.00
	4.65	139.22		
		3.10	(136.12)	
68		3.80	135.42	134.00
69		6.20	133.02	134.00
70.0		6.36	132.86	134.00
	7.77	140.63		
71		6.00	134.63	135.00

Road to gate

Frank Martin's gate

69+45 24" 15" cor. in. good shape

Randolph Rd

	+	−			
		140.63			
72		4.60	136.03	136.00	
730		2.94	137.69	137.00	
	4.42	142.16			
74		2.70	139.41	138.00	
75		6.00	136.11	137.00	75+50 15" sewer
760		6.00	136.11	137.00	
	5.22	141.33			
77		3.35	137.98	137.00	
78		6.10	135.23	136.00	
79		7.00	134.33	135.00	79+20 15" sewer
800		7.00	134.33	135.00	8" pipe norvin.
	8.21	142.54			
B.M		8.25	(134.29)		Corner rock.
81		6.50	136.04	135.00	
82		7.65	134.89	135.00	
830		7.80	134.74	135.00	water level 82+80
	10.00	144.74			15" steel sewer good con

	+	144.74		
84 ⊙		7.57	137.17	136.50
	900	146.17		
85		7.40	138.77	138.00
86		5.20	140.97	139.50
87		4.65	141.52	141.00
		5.30	140.87	
88 ⊙		5.45	140.72	141.00
	5.93	146.15		
		4.55	141.60	
89		4.00	142.15	141.00
90		7.20	138.95	139.00
		8.85	137.30	
91 ⊙		7.48	136.67	137.00
	4.35	141.02		
92		5.00	136.02	137.00
92+50		7.55	133.47	

Road running W

Conn's gate b. lot.

Stone at Conns level with gates

36"

Water level Sewer to be used as a form and lengthened 18' at present

Randolph Rd

		141.02		
93		4.80	136.22	137.00
94		2.85	138.17	138.66
⊙		.66	(140.36)	
	7.28	147.64		
95		6.45	141.19	140.33
96		3.75	143.89	142.00
97		4.50	143.14	141.60
98		6.20	141.44	141.20
99 ⊙		7.57	140.07	141.10
	4.03	144.10		
100		4.80	139.30	141.28
101		4.80	139.30	141.46
102		4.35	139.75	141.64
103 ⊙		2.96	141.14	141.82
	7.57	148.71		
104		5.30	143.41	142.00
105		4.95	143.96	144.25

100 + 5 v 24" sewer

+		148.11		
106 ⊙		3.47	145.24	146.56
	9.43	156.67		
107		6.30	150.37	148.75
108		5.35	151.32	151.00
109		5.90	150.77	150.90
110 ⊙		5.00	151.67	150.80
	4.00	155.67		
111		4.25	151.42	150.70
112		4.95	150.72	150.60
113		4.95	150.72	150.50
114 ⊙		5.41	150.26	150.40
	4.68	154.94		
115		4.60	150.34	150.30
116		4.95	149.99	150.20
117		5.00	149.99	150.10
118		4.95	149.99	150.00
⊙		4.98	149.96	
	5.37	155.33		

12" sewer at 108 + 70 to be in ~~N+S~~ diagonally across corner of road

≈ 41

117 + 70 18" Sewer

118 + 35 36" "

3 rail ℄ ℄ & St ℄

Randolph Rd

		155.33		
119		4.50	150.83	150.25
120		4.95	150.38	150.50
		7.10	148.23	
121		4.85	150.48	150.75
1210		4.64	150.69	151.00
	6.35	157.04		
123		5.90	151.14	152.00
124		4.55	152.49	153.00
125		2.90	154.14	154.00
1260		1.65	155.39	150.00
	3.23	158.62		
127		4.30	154.32	154.00
128		4.50	154.12	154.00
129		4.75	153.87	154.00
130		4.80	153.82	154.00
1310		4.76	153.86	154.00
	3.55	157.41		

Water level at 119+35

Randolph Road

		157.41		
132		4.30	153.11	153.75
133		4.55	152.86	153.50
134		4.75	152.66	153.25
135		4.30	153.11	153.00
B.M.		4.55	(152.86)	Stone
136 ⊙		7.22	150.19	152.00 — 136+50 24" Sewer 10' Skew Lwt
	5.90	156.09		
137		5.46	150.69	152.00
138		5.30	150.79	152.00
139		5.10	150.99	152.45
139+48		3.20	(152.89)	152.99 — End of Curb
B.M.		4.90	(151.19)	S. rail of T.H. 1-45

62

Frank Hays Drain

Line	Length	Bearing
AB	1027	S65°30'W -
B.C	1900	N63°W -
C D	1700	S84°W -
D E	19170	S80°50'W -
E F	2471	S29°30'W -
F G.	3100	S59°00W -
G.H	3470	S40°25'W -
H J	4700	S24°20'W -
J K	5900	S51°W

Aug. 28 1916 Paul Carter } Asst.
Will Stewart }

63

O at 10'S & 5'E Mary Hadleys S.E corner. Pt. B. about 80' W. of Rail fence.

17+03 Line fence between Hays & Fred Hines.

18 35

35+26 ℄ Road.

16°5°

48+82 Line. Bill Hig. E O. Hig W.

64

51
19 20 -
31 40
1 35

Line	Length	Bearing
KL	580.0	S 31 40 W -
LM	614.2	S 24-05 W -
MN	640.0	S 5°-25 E -
NP	71.00	S 11°-20' E -
PQ	715.8	S 46°-20' E -
QR	781.22	E
RS	856.9	S 0°-20' E -
ST	856.9	S 46 30 E
TV	870.0	

65

MN Down Corn row.
Line between Harris & O. Hig 6945

87 14' E & 52'S of corner

Frank Hays Drain

0	6.40	16.40		10.00	7.00	3.00	
			8.15	8.25			
1			6.22	10.18	7.34	2.84	
2			5.25	11.15	7.68	3.47	
3			5.75	10.62	8.02	2.60	
4 ⊙			4.70	11.70	8.36	3.34	
⅄	7.73	19.43					
5			7.88	11.55	8.72	2.83	
6			6.78	12.65	9.06	3.59	6+05 Hump 3' High
7			5.81	13.62	9.40	4.22	6+80 " Ends.
8 ⊙			6.32	13.11	9.74	3.37	
π	5.73	18.89					
9			5.66	13.18	10.08	3.10	
10			5.48	13.36	10.44	2.92	
11			4.14	14.70	10.78	3.92	
12			5.02	13.82	11.12	2.70	
13 ⊙			4.12	14.72	11.48	3.24	
π	5.52	20.24					

12

Aug 29 Paul Carter Rodman.

5.25

14		20.24	5.11	15.13	11.82	3.31
15			5.22	15.02	12.18	2.84
16			4.44	15.80	12.52	3.28
17 ⊙			3.20	17.04	12.86	4.18
π	8.23	25.27				
18			7.69	17.58	13.20	4.38
19			7.91	17.36	13.54	3.82
20			7.50	17.77	13.90	3.87
21			7.53	17.69	14.24	3.40
22 ⊙			5.95	19.32	14.58	4.74
π	6.44	25.76				
23			7.19	18.57	14.92	3.65
24			6.54	19.22	15.26	3.96
25			7.23	18.53	15.62	2.91
26			5.39	20.37	15.96	4.41
BM			5.58	20.18		N. end con. wall along Hays' fence
27 ⊙			5.90	19.86	16.30	3.56
π	6.91	26.77				

28		26.77	6.66	20.11	16.64	3.47
29			6.24	20.53	17.08	3.45
30			5.76	21.01	17.40	3.61
31			5.49	21.28	17.74	3.54
32			4.98	21.79	18.00	3.79
330			4.76	22.01	18.15	3.86
π	7.25	29.26				
34			6.71	22.55	18.29	4.26
35			7.79	21.47	18.43	3.04
B.M			3.65	25.61		W. end N. parapet.
36			6.26	23.00	18.58	4.42
37			5.87	23.39	18.72	4.67
380			4.36	24.90	18.86	6.04
⊥	6.88	31.78				
40			8.36	23.42	19.00	4.42 None No 39
41			7.80	23.98	19.14	4.84
⊙			7.16	24.62		
Λ	4.18	28.80				

181

32 11.00 34
96
140
128
12
4

42		28.80	5.95	22.35	19.29	3.66
43			3.98	24.82	19.43	5.39
44			6.67	22.13	19.57	2.56
45			5.18	23.62	19.72	3.90
46			5.60	23.20	19.86	3.34
47 ⊙			5.42	23.38	20.00	3.38
π	5.69	29.07				
48			5.09	23.98	20.14	3.84
49			5.11	23.86	20.28	3.58
50			4.62	24.45	20.43	4.02
51			4.97	24.10	20.58	3.52
52 ⊙			4.26	24.81	20.72	4.09
π	4.29	29.10				
53			4.57	24.53	20.86	3.67
54			4.97	24.13	21.00	3.13
55			4.87	24.23	21.14	3.09
56 ⊙			4.67	24.43	21.28	3.15
π	5.53	29.96				

57		29.96	5.37	24.59	21.43	3.16
58			4.86	25.10	21.58	3.52
59 ⊙			4.94	25.02	21.72	3.30
π	5.18	30.20				
60			5.23	24.97	21.86	3.11
61			5.18	25.02	22.00 (.14%)	3.02
62			4.80	25.40	22.35 (.35)	3.05
63			4.42	25.78	22.70	3.08
64 ⊙			4.12	26.08	23.05	3.03
π	6.27	32.35				
65			5.66	26.69	23.40	3.29
66			5.25	27.10	23.76	3.34
67			4.56	27.79	24.11	3.68
68			4.29	28.06	24.46	3.60
69			4.03	28.32	24.81	3.51
70 ⊙			4.09	28.26	25.17	3.09
π	5.13	33.39				

61 / 32 / 29 — .143 — 28) 40 — 28 — 120 — 112 — 8

71		33.39	4.94	28.45	25.52	2.93
⊙			3.93	29.46		
π	4.89	34.35			25.88	
72			5.68	28.67		2.79
73			5.14	29.21	26.23	2.98
74			4.41	29.94	26.59	3.35
75 ⊙			3.50	30.85	26.94	3.91
π	5.06	35.91				
76			4.35	31.56	27.29	4.27
77			4.87	31.04	27.64	3.40
78 ☿			4.55	31.36	28.00	3.36
π	5.04	36.40				
79			4.71	31.69	28.36	3.34
80			4.25	32.15	28.70	3.45
81 ⊙			3.90	32.50	29.06	3.44
π	5.63	38.13				
82			5.14	32.99	29.41	3.58
83			4.73	33.40	29.76	3.64

84		38.13	4.78	33.35	30.12	3.23
85 ⊙			3.90	34.23	30.47	3.76
π	4.88	39.11				
86			4.91	34.20	30.83	3.47
87			4.36	34.76	31.20	3.55

Check back.

π	4.23	38.98		
⊙			6.64	32.34
π	8.04	40.38		
⊙			8.38	32.00
π	3.65	35.65		
⊙			7.66	27.99
π	3.86	31.85		
99			5.75	26.10
99				
π	6.87	30.73		23.86
⊙			3.10	27.63

31.20 / 22 / 9.20 / 26) 9 8 / 1 40 / 1 30 / 10

Total cu. yds = 1,644.10

Av per 100' = 18.1

Av cut = 3.57

π	4.26	31.89	27.63	
38			7.09	24.80
			6.47	25.42

Stat	B.S	H.I.	F.S	Elev
S.L.B.M.				611.391
⊼ (1)	3.281	617.191		
⊙ (1)			3.599	613.512
⊼ (2)	3.096	616.608		
⊙ (2)			2.196	614.412
⊼ (3)	8.298	622.710		
⊙ (3)			3.055	619.655
⊼ (4)	4.610	624.265		
⊙ (4)			9.272	614.993
⊼ (5)	3.146	618.139		
⊙ (5)			4.300	613.839
⊼ (6)	5.541	619.380		
B.M			3.384	615.996
⊼ (7)	5.844	621.840		
⊙ (7)			4.460	616.380
⊼ (8)	0.175	616.555		
			2.746	613.809
⊼ (9)	5.340	621.336		

N.W. corner concrete approach to Triangle House.

Ledge on furnace room window

Knob of furnace door

110

Stat	B.S.	H.I.	F.S.	Elev.
⊙ (9)			0.075	621.261
⊼ (10)	7.948	626.209		
			0.103	626106
⊙ (10)			1.383	624826
⊼ (11)	12.087	636.913		
⊙ (11)			4.750	632163
⊼ (12)	4.952	637.115		
⊙ (12)			4.748	632.367
⊼ (13)	4.325	636682		
⊙ (13)			1.590	635.092
			1.800	634.882
⊼ (14)	2.233	637.115		
⊙ (14)			.850	636.265

.850

6 th step

111

Floor at foot of stairs.

Top of mantel

Top of floor at head of stairs

Top of water box in closet

Top of west end of bath tub

6th step on second stairs.