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1916  
BARNETT DRAIN 5702 Pages  
DUCAN DITCHES WM. BATZ DRAIN  
AVON SCH. HOUSE DRAIN

56

6

Avon School Hs -  
56, 76, 75

Thurston 220

4

## Avon School House Drain.

Stat.	P.S.	H.I.	F.S.	Elev	Grat	Cut	Cut/b		
BM 18				50.00	40.00		10.00		
18A	1.88	51.88						N.E. cor wide walk } On corner of walk }	
17	3.80		3.00	48.08	39.60		8.48		
16			4.84	47.04	39.20		7.84	2.93 x 2 x 100 27	45.53 43.56 1.97 1.9
150			5.34	46.54	38.80		7.74	20.0	43.50 38.20 5.30
π	3.84	50.39							
14			4.85	45.53	38.40		7.13		1.80
13			5.15	45.23	38.00		7.23		
12			6.82	43.56	37.60		5.96	36.80 29.80 7.00	2.40 37.60
11			7.51	42.87	37.20		5.67	9.17 97	
100			8.31	42.07	36.80		5.27	40.78 30.50	37 36.00
π	3.06	45.13							
9			4.35	40.78	36.40		4.38	40.53 36.80 3.73	43.56 37.80 5.76 5.80 6.0
8			4.60	40.53	36.00		4.53		
7			5.28	39.85	35.60		4.25		
6			6.38	38.75	34.40		4.35	35.60	42.07 36.80 5.27
5			6.82	38.31	33.60		4.71	35.20	3.55

6

Stat.	B.S.	I.I.	F.S.	Elev	Grade
40		45.13	8.15	36.98	<sup>32.95</sup> 32.80
π	3.94	40.92			<sup>32.19</sup>
3			5.28	35.64	32.05
			5.87	35.05	<sup>31.1</sup>
2			6.25	34.67	31.50 <sup>29.64</sup>
1			7.54	33.38	30.55 <sup>29.80</sup>
0			8.08	32.84	29.80
			11.37	29.55	

Cut. Cu. Yds

4.03

4.18

3.46

3.59

2 + 60 Stake at band

3.26

3.37

2.74

2.83

3.04

At R.R. fence

Sewer under R.R.

3.00

36.00

32.00

3.00

32.00

30

78

Check back

1	40.92	7.54	
40		3.92	37.00
π	9.50	46.58	
90		5.85	40.73
π	10.05	50.78	
16		3.83	46.95

8	Avon School				House Drain.	9	
Stat.	B.S.	H.I.	F.S.	Elev.	Grade	Cut	Cu. Yds
B.M.				50.00			Stat 18. of other ditch.
	2.87	52.87					On walk at 1st window N of E. door
6125			3.10	49.77	40.00		9.77
56			6.55	46.32	39.60		6.72
							9.77
5			3.90	48.97	39.20		In barn
40			4.55	48.32	38.80		9.52
π	2.68	51.00					8.69
3			3.91	47.09	38.40		5' S. of Sch. fence
2			6.16	44.84	38.00		6.84
10			7.64	43.36	37.60		5.76
π	5.51	48.87					4.94
10			6.73	42.14	37.20		OF first ditch.

Aug. 19, 1916

12

Stat	B.S.	I.I.	F.S.	Elev.
B.M. 0	5.78 8.40	55.78	50.00	46.00
	7.50		48.28	
1	4.13		51.65	45.92
	8.20		47.58	
2	3.85		51.93	45.84
	8.85		46.93	
3	4.40		51.38	45.76
	8.95		46.83	
4	4.15		51.63	45.68
	9.00		46.78	
50	4.61		51.17	45.60
	9.05		46.73	
π	6.00	57.17		
6			6.09	51.09 45.52
			10.75	46.92
7			4.02	53.15 45.44
			10.85	46.32

LETTER

Clear, hot

Wm Batz

Dicks Park Carter  
Rod Carricks

13

Low point in retaining wall at 0

14

Stat	RS	H.L.	F.S.	Elev.
8		57.17	4.07	53.10 46.36
		1	11.15	46.02
9			6.72	50.45 45.28
			11.00	46.17
100			6.85	50.32
π	3.60	53.92		45.20
10			✓	45.92
11			6.00	47.92 45.12
B.M.			5.81	48.11
11			8.25	45.67
12			4.00	49.92 45.04
			8.30	45.62
13			4.53	49.39 44.96
			8.46	45.52
140			5.32	48.60 44.88
			8.50	45.42
π	5.90	54.50		

15

Lowest point in header

16

State B.S. H.I. F.S. Fly

15 54.50 6.99 48.06 ~~47.80~~

9.30 45.20 ✓

160 5.25 49.25 44.72

9.50 45.00

π 4.21 53.46

17 4.00 49.96 44.63

8.80 44.66

180 3.32 50.14 44.55

8.75 44.61

π 3.40 53.54

19 4.00 49.54 44.47

9.20 44.34 ✓

20 3.88 49.66 44.39

8.80 44.74

210 3.47 50.07 44.32

✓ 4.458

π 3.15 53.22

46.00  
44.80  
1.2015 117  
0  
008

18

Stat	B.S.	H.I.	F.S.	Flor
		53.22		
22			3.70	49.52 49.24
			8.80	44.42
<del>230</del>			3.44	49.78
		53.29		
π	3.50	6.28		
0			4.47	48.81
π	2.86	51.67		
0			2.60	49.07
π	4.88	53.95		
0 33			6.23	47.72
π	4.49	52.21		
33			8.30	43.91
34			4.62	47.59 43.44
35			✓	43.85
35			4.83	47.38 43.36
			✓	43.78
36			4.18	48.03 43.28
			✓	43.59

23	44.21
24 ✓	44.13
25	44.06
26	43.98
27	43.90
28 ✓	43.82
29	43.75
30	43.67
31	43.59
32 ✓	43.51

19



20	Stat.	B.S.	H.L.	F.S.	Elev.
	37		52.21	4.70	47.51 43.20 43.40
	38			4.60	47.61 43.13 43.21
	<del>39</del>	3.97	51.58		
	39			4.48	47.10 43.05 43.02
	40			3.73	47.85 42.91 8.75 42.83
	41			3.89	47.69 42.81 8.50 43.08
	42			3.65	47.93 42.82 8.75 42.83
	43			3.98	47.60 42.74
	<del>43</del>	4.85	52.95		
				9.50	42.95
	44			5.49	46.96 42.66 9.75 42.70

~~42~~  
~~42.83~~  
~~1.59~~  
 43.91  
~~42.83~~  
~~1.18~~  
 11

21

22	Dtal	B.S.	H.I.	F.S.	Flev
45			52.45	4.80	47.65 42.5
				9.65	42.80
46				4.69	47.76 42.5
				9.85	42.60
47				4.64	47.81 42.45
				10.00	42.45
48				5.42	47.03 42.35
				9.55	42.90
490				4.65	47.80 42.20
π	4.39	52.19			
49				9.90	42.29
50				4.76	47.43 42.19
				9.75	42.49
51				4.58	47.61 42.10
				10.15	42.09
52				4.79	47.40 42.00
				9.54	42.65

23

24	Stat.	B.S.	H.I.	F.S.	Flav
	53		52.19	4.52	47.67 41.96
				9.90	42.29
	54			4.57	47.62 41.89
				9.45	42.74
	B.M. 0		2.80	49.39	
	$\pi$	2.83	52.22		
	54			4.00	48.22 41.81
				10.50	41.72
	55			3.88	48.34 41.73
				"	41.72
	56			4.68	47.54 41.65
				"	41.72
	57			4.04	48.18 41.51
				10.50	41.72
	58			4.55	47.67 41.50
				"	41.62
	59			4.30	47.92 41.43
				10.70	41.52

Bate Ditch

54+30 road E & W

Top N. parapet directly over stream

Two No 54

26

Stat B.S. H.L. F.S. Elev

7 4.22 52.14 9.792

60 4.00 48.14 41.34

10.75 41.39

61 4.57 47.57 41.27

10.90 41.24

62 4.56 47.88 41.19

11.00 41.14

63 4.17 47.97 41.11

11.05 41.09

64 4.26 47.88 41.03

10.85 41.29

66 0 4.40 47.74

7 3.94 51.68

65 4.14 47.54 40.96

10.60 41.08

66 3.38 48.30 40.88

27

28

Stat

B.S

H.I.

F.S

67

51.68

2.68

49.00

40.80

41.08

68

4.11

47.57

40.72

41.08

69

40.65

weeds

70

40.57

"

~~70~~

3.96

47.72

71

4.18

51.90

71

4.58

47.32

40.81

72

10.10

41.80

40.91

"

~~73~~

5.20

46.70

73

5.09

51.79

73

4.94

46.83

40.34

74

11.30

40.99

4.10

47.69

40.26

11.20

40.59

29

30

Stal	BS	H.I.	F.S.	Elev
75		51.79	4.82	46.97 40.18
			11.35	40.44
76			4.57	47.22 40.10
			11.60	40.19
77			5.28	56.51 40.13
			11.50	40.29
78	0		5.11	46.68 39.85
			11.30	40.99
$\pi$	4.44	51.12		
79			4.37	46.75 39.87
			10.50	40.62
80			4.12	47.00 39.71
			10.75	40.37
80			4.14	46.98 39.72
			10.80	40.32
81			3.97	47.25 39.64
			10.90	40.22

31

Tavo No 80

32

Stat. B.S. H.L. F.S. Elev

82 51.12 4.11 47.01 39.80

40.11

B.M. O 3.78 47.34

K 2.76 50.10

83 3.15 46.95 39.99

10.10 40.00

84 3.30 46.80 39.91

10.15 39.95

85 4.50 45.60 39.33

10.05 40.05

86 4.21 45.89 39.25

10.90 39.20

87 3.90 46.20 39.13

9.75 40.35

88 4.74 45.36 39.10

10.00 40.10

89 O 5.14 44.96 39.11

10.20 39.90

33

Top wooden piece on top of Floor I to

36

## Batz Ditch

Stat	BS.	H.L.	F.S.	Elev
97		49.60	3.95	45.75 38.31
			10.20	49.40
98			5.51	44.09 38.31
			10.30	39.30
99			4.94	44.66 38.22
			10.40	39.20
100			4.76	44.84 38.14
			10.55	39.05
101			4.78	44.92 38.08
			10.60	39.00
1020			4.80	44.80 38.00
			10.55	39.05
π	4.81	49.61		
103			4.85	44.76 37.92
			✓	38.90
104			5.68	43.93 37.83
			10.90	38.71

37



38

Stat.	B.S.	H.I.	F.S.	Elev.
105		49.61	5.84	43.73 37.77
			11.00	38.61
106			6.12	43.49 37.61
			11.15	38.46
107			6.21	43.40 37.61
			✓	38.50
1080			6.98	43.13 37.50
7	6.05	49.18		
			10.55	38.63
109			6.22	42.96 37.40
			10.90	38.28
110			6.00	43.18 37.30
			10.85	38.33
111			6.10	43.08 37.30
			10.90	38.28
112			6.40	42.78
			10.95	38.23 37.20

39

40	Stat.	BS.	H.L.	FS.	Flv
	113		49.18		37.15
				10.50	38.68
	114			6.58	42.60 37.07
				11.10	38.08
	115			6.65	42.53 36.91
				11.25	37.93
	π	7.40	49.93		
	116			6.72	43.21 36.12
				11.90	38.03
	117			6.58	43.35 36.84
				12.05	37.88
	118			7.18	42.75 36.76
				12.15	37.78
	119			7.24	41.99 36.68
				12.00	37.93
	120			7.19	42.74
				12.30	47.63 36.61

← LETTER →

OL  
41

Stake gone

Stat.	B.S.	H.I.	F.S.	Flev
121		49.93	7.88	42.05 36.53
			"	37.90
122 0			8.11	41.82 36.45
			"	37.80
π	6.81	48.63		
123			7.46	41.17 36.37
			11.10	37.53
124			6.51	42.12 36.30
			11.10	37.53
125			6.20	42.43 36.22
			11.60	37.03
126			7.18	41.45 36.14
			11.90	36.73
127			6.98	41.75 36.06
			11.85	36.78
128 0			7.38	41.25 35.98
			12.00	36.63
π	6.22	47.47		

44

## Batz Ditch

Stat.	R.S.	H.L.	F.S.	Elev.
129	4.7.47		6.15	41.32 35.90
			10.80	36.67
130	⊙		6.45	41.02 35.82
			10.90	36.57
π	5.40	46.42		
131			3.91	42.51 35.74
			9.95	36.47
132			4.68	41.74 35.66
			9.85	36.67
133			4.86	41.56 35.59
			9.95	36.47
134	⊙		5.30	41.12 35.51
			10.25	36.17
π	5.81	46.93		
135			6.58	40.35 35.43
			10.90	46.03
136			5.61	41.32 35.36
			10.90	36.03

45

Rain

Began Aug 21. Baldwin &amp; P. de Carter

46

Stat	P.S.	H.I.	F.S.	Elev
137		46.93	6.08	40.85 35.28
			10.90	36.03
138			6.03	40.90
			11.20	35.73 35.20
139			6.60	40.33 35.05
			11.30	35.63
140			8.90	38.03 34.86
				35.68
1410			7.87	39.06 34.80
			11.20	35.73
π	8.10	47.16		
142			8.95	38.21 34.70
			11.60	35.56
143			7.10	40.06 34.60
			11.85	35.31
144			6.66	40.50 34.50
			11.85	35.31

$$\begin{array}{r} 138 \\ 15 \\ \hline 123 \\ 62 \\ 15 \\ \hline 71 \end{array}$$

$$\begin{array}{r} 44.80 \\ 35.20 \\ \hline 8.60 \\ 4.80 \\ \hline 40.00 \end{array}$$

$$\begin{array}{r} 1259.60 \\ 875 \\ \hline 450 \end{array}$$

$$\begin{array}{r} 6138 \\ 31 \\ \hline 107 \end{array}$$

$$\begin{array}{r} 9.60 \\ 2.40 \\ \hline 35.20 \\ 37.60 \end{array}$$

42.40

No grade stake

No grade stake

47

1077

3

48

Stat.	B.S.	H.L.	F.S.	Flor
145		47.16	7.64	39.52 34.40
			12.15	35.01
146			7.19	39.97 34.30
			12.10	35.06
147			7.55	39.61 34.20
			12.35	34.81
1480			7.64	39.52 34.10
147	6.30	45.82		
149			5.79	40.03 34.00
			10.90	34.82
150			6.16	39.66 33.10
			11.25	34.57
151			5.57	40.25 33.80
			11.00	34.82
152			6.53	39.29 33.70
			11.15	34.67

49

50

Stat.	B.S.	H.I.	F.S.	Elev
1530		4582	5.69	40.13 33.60
			11.10	34.72
π	4.92	4505	5	
154			5.71	39.34 33.50
			10.55	34.50
155			5.55	39.50 33.40
			10.80	34.25
156			5.06	39.99 33.30
			11.00	34.05
157			5.87	39.18 33.20
			11.20	33.85
158			5.68	39.37 33.10
			11.25	33.80
159			5.58	49.47 33.00
			11.45	33.60
1600			5.59	39.46 32.90
			11.40	33.65

51

52	Stat	B.S.	H.I.	F.S.	Elev
	$\pi$	4.85	44.31		39.46
	161			3.70	40.61 32.80
				10.85	33.46
	162			3.97	40.34 32.70
				10.75	33.56
	163			5.23	39.08 32.60
				10.80	33.51
	$\circ$			6.96	37.35
	$\pi$	5.77	43.12		
	164			6.00	38.12 32.50
				9.75	32.47
	165			5.20	36.92 32.40
				10.00	32.12
	$\pi$	4.50	41.50		
	166			4.46	37.04 32.30
				10.35	31.15
	$\circ$			9.40	32.10
	$\pi$	9.98	41.58		

53



54

## Batz Ditch.

167	41.58	4.70	36.88	32.20
		9.40	32.18	
168	5.00	36.58	32.10	
		9.50	32.08	
169	5.32	36.26	32.00	
		9.45	32.13	
<del>170</del>		6.00	35.58	
$\pi$	5.64	41.22		
170		5.60	35.62	31.90
		9.00	32.22	
B.M.		2.38	38.84	
1710		5.84	35.38	31.80
$\pi$	6.40	41.78		
		9.40	32.38	
172		9.94	36.84	31.70
		10.00	31.78	
173		5.46	36.32	31.60
		10.20	31.58	

55

Top stone slab E. side N. end bridge

56

Stat	B.S.	H.L.	FS	Flev
174		41.78	6.28	35.50 31.50
			10.40	31.38
175			6.97	34.81 31.40
			10.55	31.23
176			6.70	35.08 31.30
			10.30	31.48
177			7.11	34.67 31.20
			10.50	31.28
1780			7.23	34.55 31.10
			10.75	31.03
π	5.72	40.27		
179			6.65	33.62 31.00
			9.30	30.97
180			5.26	35.01 30.80
			9.50	30.77
181			5.78	34.49 30.80
			9.70	30.37

57

58

Stat.	B.S.	H.I.	P.S.	Flev	
182		40.27	5.88 <del>6.99</del>	34.39	30.70
			9.75	30.52	
183			6.33	33.94	<u>30.60</u>
			10.00	30.27	
184			6.94	33.33	30.40
			9.85	30.42	
1850			6.84	33.43	30.20
			10.00	30.27	
186T	6.80	40.23			
186			5.81	34.42	30.05
			10.10	30.13	
187			5.92	34.31	29.85
			10.70	29.53	
188			6.59	33.64	29.70
			10.70	29.53	
189			6.33	33.90	29.65
			10.75	29.48	

183  
138  
45

35.20  
30.60  
44.60  
45  
100

85  
59

60

Stat.	B.S.	H.L.	F.S.	Ele
190		4023	6.62	33.61 29.50
			10.75	39.48
191			5.12	35.11 29.35
			10.90	39.33
1920			6.33	33.90 29.20
			11.00	29.23
$\pi$	5.19	39.09		
193 BM			3.65	35.49
193			6.05	33.04 29.05
			✓	29.00
194			6.90	32.19 28.90
			10.55	28.39
195			6.58	32.51 28.75
			10.60	28.99
1960			5.90	33.19 28.60
			10.70	28.39
$\pi$	4.48	37.67		

61

Top of stump (highest point) near  
fence between 192 & 193

62

Stat	B.S.	H.L.	F.S.	Elad
197		37.67	5.11 <del>1.68</del>	32.56 28.45
			9.65	28.02
198			5.85	31.82 28.80
			✓	28.00
<del>1990</del>			4.10	33.57
π	5.00	38.57		
199			4.82	33.75 28.15
			✓	29.90
200			4.64	33.93 28.00
			11.10	27.97
2010			5.48	33.09
π	4.66	37.75		
201			4.42	33.33 27.85
			✓	27.60
2020			5.22	32.53 27.70
π	4.54	37.07		
			✓	27.40

68

64

Stat.	B.S.	H.I.	I.S.	Elev
2030		37.07	4.15	32.92 27.85
			9.80	27.27
<del>204</del>	4.66	37.58		
0			6.07	31.51
$\pi$	4.92	36.43		
204			5.00	31.43 27.40
			$\checkmark$	27.20
2050			4.57	31.96
$\pi$	4.85	36.81		
205			4.97	31.84 27.25
			10.15	26.66
0			5.20	31.21
$\pi$	5.17	36.38		
206			4.71	31.67 27.10
			10.15	26.23
0	6		6.25	30.13
$\pi$				

65

66

## Batz Ditch

π	5.20	35.33	5.20	30.13	
207			4.61	30.72	26.95
			9.50	26.83	
0			9.96	30.43	
π	4.50	34.93			
208			3.73	31.20	26.60
			✓	26.80	
0			4.84	30.09	
π	5.01	35.10			
B.M.			9.74	30.36	
			9.49	25.61	

$$\begin{array}{r} 204 \\ 183 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 26.80 \\ 30.60 \\ \hline 25 \overline{) 6.20} \\ 120 \end{array}$$

1.25

$$\begin{array}{r} 130 \\ 253.80 \\ \hline 15 \end{array}$$

67

Top retaining wall at end at  
208 + 85

68

## DUGAN Ditch

Stal	B.S.	H.I.	F.S.	Elev.
0	6.80	56.80		50.00
			9.90	46.90 46.60
1			5.33	51.47 46.50
			9.90	46.90
2			14.00	52.80 46.42
			10.05	46.75
3			4.90	51.90 46.30
			9.95	46.95
4			5.24	51.56 46.15
			10.05	46.75
5			3.72	53.08 46.00
			10.30	46.50
6			4.70	52.10 45.95
			10.65	46.15
7			5.92	50.88 45.70
			10.25	46.55
8	5.66	56.54		

869

Top retaining wall E side bridge



70

Stat	BS	H.I.	F.S.	Elev
8		56.04	3.91	52.63 45.55
			10.40	46.14
9			5.07	51.47 45.40
			10.20	46.34
B.M			6.49	50.05
10 O			5.26	51.28 45.25
			10.80	45.79
π	4.59	55.87		
11			4.64	51.23 45.08
			10.30	45.57
12 O			5.45	50.42 44.83
			10.30	45.57
π	5.60	56.02		
13			4.93	51.09 44.75
			10.60	45.42
14 O			4.61	51.41 44.63
				45.40
π	4.50	55.91		

71

Top header to tile ditch

72

Stat.	B.S.	H.I.	I.S.	Elev
15		55.91	5.35	50.56 44.46
			10.85	45.06
16		5.57	50.34	44.31
		10.90	43.01	
17		6.48	49.93	44.16
		10.95	44.96	
180		5.98	49.93	44.01
π	7.33	57.26		
		12.50	44.76	
B.M		6.28	50.98	
19		6.80	50.96	43.86
		12.50	44.76	
20		5.77	51.99	43.71
		12.60	44.66	
21		6.47	50.79	43.54
		12.70	44.56	
22		7.20	50.06	43.34

N wall top brick arch

74	Stat	B.S.	H.I.	F.S.	Elev
	0		57.26	7.62	49.64
	π	4.74	54.58		
	23			4.17	50.31 43.24
				<del>10.35</del>	44.40
	24			4.89	49.89 43.09
				10.35	44.23
	25			6.11	48.97 42.94
				10.60	43.98
	26			5.74	48.84 42.77
				10.90	43.68
	27			6.35	48.23 42.62
					43.60
	280			5.94	48.64 42.47
					43.90
	<del>28</del> π	4.30	52.94		
	29			5.41	47.53 42.32
				10.25	42.69

75

76

Stat.	B.S.	I.I.	F.S.	Elev
30		52.94	4.70	48.24 42.17
			10.10	42.89
31			5.80	47.14 42.00
			10.15	42.79
32			4.79	48.15 41.85
			10.50	42.94
33			5.15	47.79 41.70
34			10.50	42.94
34			6.93	46.01 41.35
			✓ " 42.40	
35 0			5.60	47.34 <del>41.20</del>
7	5.14	52.48	✓	42.20
36			6.28	46.20 40.95
			✓ 42.10	
37			6.19	46.29 40.69
			✓ 42.00	

77

46.60	
41.20	15.4
<u>35</u>	
5.40	
3.80	
<u>1.60</u>	
42.10	
0.516	

78

Stati	D.S.	H.I.	F.S	Elev
38		52.48	5.88	46.60 40.49
			✓	42.00
390			6.11	46.37 40.28
π	5.20	51.57		
39			10.35	41.22
40			4.58	46.99 40.07
			11.00	40.57
41			5.04	46.53 39.87
			11.20	40.37
42			4.96	46.61 39.66
			✓	40.21
43			9.66	46.91 39.46
			11.65	39.92
44			7.40	44.17 39.25
			11.60	39.97
45			5.82	45.75 39.05
			12.35	39.22

79

80

Stat. BS H.I.

46 51.57 7.61 43.96 38.84

12.70 38.87

47

7.16 44.41 38.64

12.70 38.87

48

8.17 43.40 38.43

✓  
38.80

49

8.21 43.36 38.23

✓  
38.60

50 @

8.57 43.00 38.12

π

4.26 47.26

8.40 38.86

51

5.35 41.91 37.92

8.40 38.86

52

6.75 40.51 37.71

5

8.40 38.86

53

4.84 42.42 37.51

8.85 38.41

81

Stat.	B.S.	H.I.	F.S.	Elev
82				
54		47.26	5.50	41.76 37.31
			9.30	37.96
55			5.46	41.80 37.10
			9.30	37.96
56			5.04	42.22 36.90
			9.80	37.46
57			6.23	41.03 36.69
			✓	37.40
580			7.08	40.18 36.49
			✓	37.40
A	5.35	45.53		
59			5.02	40.51 36.28
			8.20	37.33
60			6.45	39.08 36.07
			8.70	36.83
610			5.13	40.90 35.87
			9.30	36.13
A	6.26	<sup>46.66</sup> <del>42.79</del>		

83

84

Stat

B.S.

H.I.

F.S.

Elev

62

46.66

~~42.39~~

5.75

40.91

~~36.64~~

35.66

10.60

36.06

63

6.30

40.36

35.46

12.25

35.41

64

5.84

40.82

35.24

11.30

35.36

65

7.84

39.82

35.04

11.40

35.26

66

7.25

34.41

34.83

11.35

35.31

67

9.22

37.44

34.62

11.90

34.76

680

7.84

38.82

34.42

34.80

7

4.15

42.97

69

5.95

37.02

34.21

8.15

34.82

85



86

Stat.	B.S.	H.I.	F.S.	Elev
70		42.97	5.45	37.32 39.01
			8.50	34.47
71			6.40	36.37 33.80
			8.20	34.77
72			4.10	38.87 <u>33.60</u>
			8.85	34.12
73			6.30	36.67 33.54
			8.90	34.07
74			6.30	36.67 33.48
			8.85	34.12
75			7.41	35.56
π	790	43.96		
75			8.09	35.37 33.42
				35.50
76			7.14	36.32 33.36
			8.90	34.56
77 B.M			4.20	39.26

41.20  
 33.60  
 37.70  
 20.5  
 14.5

87

Top stone slab W end N. side

← A4 →      ← LETTER →

## Dugan Drain Arm

90	Stat	B.S.	H.I.	F.S.	Elev
	0		55.35	8.35	47.00 43.00
				9.95	44.40
	1			9.46	50.89 42.90
				10.45	44.90
	2.0			5.45	49.90 42.80
				10.80	44.55
	π	220	52.10		
	3			3.70	48.40 42.70
				7.65	44.55
	4			0	42.60
				8.46	43.70
				5.24	46.80
	5			7.19	44.91 42.60
				8.45	43.65
	6.0			8.05	44.05 42.40
				9.00	43.10
	π	8.04	52.09		

Bottom of file.

91

92

Stat B.S. H.L.

7

52.09

8.42 43.67 42.30

9.00 43.09

8

7.30 44.79 42.20

✓  
43.00

9

8.69 46.40 42.10

8.85 43.14

10

5.16 46.93 42.00

8.85 43.24

11

4.62 47.47 41.90

9.10 42.99

12

4.49 47.60 41.80

9.50 42.59

13

4.35 47.74 41.70

9.45 42.64

140

4.09 48.00 41.60

✓  
42.50

N

3.87 51.87

93

94

## Arm Dugan

Stat	B.S.	I.L.	F.S.	Elev
15		51.87	2.95	48.92 41.50
				42.90
16			4.10	47.87 41.40
			9.45	42.32
17			4.41	47.46 41.30
			9.80	42.07
18			4.30	47.57 41.20
			9.80	42.07
19			3.70	48.07 41.10
			10.30	41.57
20			3.85	48.02 <del>41.00</del>
			10.20	41.67
21 0			6.43	45.44 40.84
π	6.81	52.25		
22			5.32	46.93 40.68
			10.30	41.95
23			9.53	47.72 40.51
			10.55	41.70

## Drain.

42.00  
41.50

95

20.0  
1

Gore's line

96

Stat.	B.S.	H.I.	F.S.	
			4.30	
24	5225	4.10	47.95	40.34
		<del>15.00</del>	41.25	
25		4.26	47.99	40.17
		11.55	40.70	
26		6.32	45.93	40.00
		11.25	41.00	
27		6.45	45.80	39.83
		11.45	40.80	
28		6.30	45.95	39.66
		11.40	40.85	
29		5.70	46.55	39.49
		11.70	40.55	
30		6.58	45.67	39.32
<del>30</del>		12.00	40.25	
π	4.19	49.86		
31		7.12	42.74	39.15
32		9.60	40.26	

97

Trvo No 28

98

Stat	B.D.	H.I.	F.S.	Elev
32		49.86	3.62	46.24 38.98
			9.90	39.96
33			5.49	44.37 38.81
			10.10	39.76
34			5.65	43.21 38.62
			10.20	39.66
35			5.76	44.10 38.45
B.M.			3.38	46.48
35			11.00	38.86
0			6.10	43.76
$\pi$	4.95	48.71		
36			5.37	43.34 38.28
			9.80	38.91
37			4.89	43.82 38.11
			10.20	38.51
38			4.12	44.59 37.94
			10.47	38.24

99

Top S. parapet bridge at 33+50

100

Stat.	B.S.	H.I.	F.S.	Elev
39		48.71	4.45	44.26
			✓	37.72
				38.20
40			7.70	41.01
			✓	37.60
				38.00

101

$$\begin{array}{r} 40.00 \\ 37.60 \\ \hline 24 \\ .2 \end{array}$$
34°  
17

39 of other ditch.

102

## Barnett Drain

Stat	B.S.	H.I.	F.S.	Elev
13 M R	18.32	58.32		50.00 49.00
	8.85		8.85	49.47
1			6.24	52.08 48.60
			9.50	48.92
2			7.29	51.03 48.20
			10.20	48.12
3			7.80	50.52 47.80
			10.70	47.62
4			8.61	49.71 47.40
			10.80	47.52
5			8.88	49.49 47.00
			11.05	47.27
6			8.90	49.42 46.84
			11.20	47.12
7			7.48	50.84 46.66
			11.30	47.02
8			8.00	50.32 46.50
			11.60	46.72

## Union Township

Baldwin Road  
Carton 103

Cool-Clear

Aug. 23, 1916

47	1.00	Top corner stone in bottom at 0100
	1.26	Began at noon.
22	3.48	
	22	
	1.41	
-	-	
-	2.83	
-	-	
-	2.72	
	1.22	
12	2.31	
	1.68	
27	2.44	
	1.02	
28	2.58	
	1.19	
36	4.18	
	1.05	
22	3.82	



104

9	58.32	8.40	49.92	46.34
		12.00	46.32	
10 ⊙		8.10	50.22	46.18
		12.10	46.22	
π	6.50	56.72		
11		6.63	50.09	46.02
		10.30	46.42	
12		6.86	49.86	45.86
		10.60	46.12	
13		7.12	49.60	45.70
		10.55	46.17	
14		6.92	49.80	45.54
		10.65	46.07	
15		6.01	50.71	45.38
		11.00	45.72	
16 ⊙		5.55	51.17	45.22
		11.40	45.32	
π	3.24	57.41		

105

	1.41	
-		3.48
	.07	
.04		4.04
	.91	
.40		4.07
	1.22	
.26		4.00
	1.80	
.97		3.90
	1.55	
.53		4.26
	1.55	
.34		5.33
	.92	
.10		5.95

106

17	54.41	2.61	51.80	45.06
		9.10	45.31	
18		3.25	51.16	44.90
		9.35	45.06	
19		4.35	50.06	44.74
		9.60	44.81	
		9.95	44.46	
20		5.55	48.86	44.58
			44.61	
0		6.40	48.01	
π	5.68	53.69		
21		5.36	49.05	44.42
			44.90	
220		5.00	48.69	44.26
*		9.90	45.29	
π	4.06	52.75		
230		4.60	48.15	44.10
*		8.60	44.15	

107

	.60
25	6.74
	.76
.16	6.26
	.43
.07	5.32
	.37
E. end sewer on road at 19+80	
.03	4.28
	.95
.48	4.63
	2.80
1.03	4.43
	2.00
.05	4.05

108

$\pi$	5.03	53.18	48.15
240			5.83 47.35 43.94
$\pi$	5.45	52.80	
			5.25 43.70
25			5.25 47.55 43.78
			9.00 43.80
0			5.44 47.36
$\pi$	5.27	52.63	
26			5.32 47.31 43.62
			8.80 43.83
270			5.15 47.48 43.46
$\pi$	7.40	54.88	
A			11.10 43.78
28			8.75 46.13 43.30
			11.20 43.68
13.14			8.14 46.74
			12.60 42.28

.04  
~~40~~

109

	.02	3.41
	.02	3.77
	.43	
	.21	3.69
	.94	
	.32	4.02
	1.30	
	.38	2.85
	1.02	
Top boiler sheet	End on Higgins	
Bottom	" "	

110

29 54.88 8.40 46.48 43.14

11.30 43.58

30 8.40 46.48 42.98

11.50 43.38

31 7.65 47.23 42.82

11.60 43.28

0 8.51 46.37

32 11.60 43.28 42.66

7 4.50 50.87

32 3.75 47.12

33 3.96 46.91 42.50

3 43.15

34 4.06 46.81 42.34

7.85 43.02

35 4.45 46.42 42.18

7.85 43.02

36 0 4.50 46.37 42.02

7 4.69 51.06

.44 3.34

1.66

.40 3.50

1.09

.46 4.41

2.50

.62 4.56

62

2.35

.65 4.41

2.50

.68 4.47

2.52

.84 4.24

2.82

.68 4.35

111

LETTER

112

37	51.06		4.90	46.16	41.88	.43	4.28	2.02
			8.75	42.31				
0			6.10	49.96				1.87
$\pi$	6.35	51.31						
38			5.26	46.05	41.72	.58	4.33	
				42.20				1.55
39 0			4.49	46.82	41.56	.42	5.26	
$\pi$	4.06	50.88						
39			8.90	41.98				<del>2.75</del> 2.50
40 0			5.22	45.66	41.40	-	4.26	
			9.50	41.38				.29
$\pi$	6.15	51.81						
41 0			5.19	46.62	41.24	.16	5.38	
$\pi$	5.51	52.13						2.32
42 0			4.71	47.42	41.06	1.05	6.34	
			11.00	42.13				
$\pi$	5.13	52.55 47.26						

113

114

430	3	52.55	6.03	46.52	40.92
$\pi$	5.01	51.53			
43			10.40	41.13	
44			5.86	45.67	40.76
			10.60	40.93	
45			5.57	45.98	40.60
			10.70	40.83	
460			6.05	45.48	40.44
			10.75	40.78	
$\pi$	5.42	50.90			
47			5.22	45.68	40.28
			10.50	40.40	
48			9.80	46.10	40.12
				40.30	
49			5.38	45.52	39.96
			10.60	40.30	
50			8.05	42.85	39.80
			10.45	40.45	

2.83

.21

5.60

.72

.17

4.91

.74

.23

5.36

1.00

.34

5.04

.85

.12

5.40

.55

.18

5.78

.96

.34

5.56

1.58

.63

3.05

115

116

51

50.90 6.58 44.32 39.64

10.70 40.20

52

5.65 45.25 39.48

10.90 40.00

11.45 39.45

0

5.75 45.15

π

3.32 48.47

53

3.79 44.68 39.32

39.40

54

3.86 44.61 39.16

39.35

55

3.95 44.52 39.00

8.70 39.77

56

4.65 43.82 38.85

8.80 39.67

57

4.60 43.87 38.88

8.80 39.67

39.45

2.22

.56 4.68

2.00

.52 5.77

1.11

Bottom W. end sewer in road

.08 5.36

150

.19 4.45

1.78

.77 5.52

2.77

.72 4.87

2.80

.79 4.99

117

500  
16

118

58		48.47	4.39	44.08	38.81
			9.00	39.47	
59			4.57	43.90	38.72
			9.75	38.72	
60	⊙		6.42	42.05	38.63
π	5.15	47.20			
				38.80	
61			3.60	43.60	38.55
			8.20	39.00	
62			4.41	42.79	38.46
			7.75	39.45	
63	⊙		4.15	43.05	38.37
			8.30	38.90	
π	5.19	48.24			
64			5.09	43.15	38.28
			9.60	38.64	
65			5.58	42.66	38.20
			9.80	38.44	

		2.69	
66			5.27
		1.22	
-			5.18
		.29	
17			3.42
		1.10	
			5.05
45		2.67	
			4.33
99		2.82	
			4.68
53		off end private bridge	
		1.65	
36			4.87
		1.11	
29			4.46

119



120

66 48.24 5.65 42.59 38.11

10.00 38.24

67 4.90 43.34 38.02

38.20

68 0 4.90 43.34 37.93

10.30 37.94

π 2.99 46.33

69 3.15 43.18 37.84

8.10 38.23

70 4.09 42.24 37.75

8.10 38.23

71 3.21 43.12 37.66

8.40 37.93

72 0 3.22 43.11 37.57

π 3.79 46.90

8.50 38.40

73 4.57 42.33 37.50

8.60 38.30

.65

13 4 4.48

.57

18 5.32

.36

61 5.41

.74

39 5.34

1.61

48 4.49

1.39

27 5.56

2.02

81 5.52

2.98

80 4.83

121

122

74	46.90	4.80	42.10	37.41
		0.55	38.35	
750		4.23	42.67	37.32
π	4.68	47.35		
		9.20	38.15	
760		4.73	42.62	37.23
		9.46	37.95	
π	5.14	47.76		
770		5.55	42.21	37.15
		10.15	37.61	
π	9.63	46.84		
78		5.05	41.79	37.06
		9.35	37.19	
790		4.56	42.28	36.97
		9.50	37.34	
π	4.81	47.09		
80		5.40	41.69	36.88
		9.65	37.44	

3.22

123

94	4.69
	3.26
83	5.35
	2.89
72	5.30
	2.18
46	5.06
	1.65
43	4.73
	1.48
37	5.31
	1.72
56	4.81

0		47.09	6.10	40.99
π	5.93	46.92		
810			4.50	42.42 36.80
				37.40
π	4.35	46.77		
820			4.78	41.99 36.71
				37.45
π	5.33	47.32		
830			4.80	42.52 36.62
				37.48
π	4.08	46.60		
84			5.43	41.17 36.53
			9.10	37.50
850			9.46	37.14 36.44
π	9.33	46.47		
85			5.61	40.86
860			5.13	41.31 36.35
			9.50	36.97

		2.14	
80	2.92	5.62	
74		5.28	
	2.89		
86		5.90	
	3.20		
87		4.64	
	2.90		
70		4.42	
		70	
	2.28		
62		9.99	

126

$\pi$	5.17	46.51		41.39	
870			5.20	41.31	36.27
1	5.18		9.70	36.85	
$\pi$	5.18	46.49			
880			5.07	41.42	36.18
				36.75	
$\pi$	4.80	46.22			
89			4.91	41.31	36.09
			9.50	36.72	
900			5.17	41.05	36.00
$\pi$	4.12	45.17			
				36.70	
91			4.30	40.87	35.91
			8.50	36.67	
92			3.98	41.19	35.83
			8.75	36.42	
93			3.95	41.22	35.74
			8.65	36.42	

LETTER

127

					2.22
				.58	5.04
				2.13	
				57	5.24
				2.33	
				69	5.22
				2.56	
					5.05
				70	
				2.70	
					4.96
				76	2.50
					5.36
				59	
				2.35	5.98
				69	

128

94 45.17 4.26 40.91 35.65

9.20 35.97

95 4.10 41.07 35.56

✓  
35.98

96 0 4.93 40.24 35.35

✓  
9.10 35.99

π 4.05 45.09

97 4.68 40.91 35.29

9.35 35.74

98 3.68 41.41 35.20

✓  
35.80

99 4.18 40.91 35.11

9.20 35.89

100 0 4.09 41.00 35.03

π 4.00 45.00

9.50 35.50

10 0 0 9.83 35.17 34.94

π 11.10 40.27

129

185

32 4.26

1.87

5.51

42 1.91

4.06

61

1.96

5.12

45 1.94

6.21

60 2.26

5.88

78 2.32

5.97

1.29

47

5.18

23

23

130

101	46.27	6.15	40.12	
102		6.69	39.58	34.86
		11.10	35.17	
103		5.58	40.69	34.76
		10.80	35.47	
104		5.79	40.98	39.65
		11.25	35.02	
105		5.71	40.56	34.59
		11.00	35.22	
106 0		5.81	40.46	34.50
π	4.50	44.96	35.20	
107		4.15	40.81	34.42
		9.30	35.66	
108		9.80	40.16	34.33
		9.05	35.91	
109		9.89	40.07	34.24
		9.25	35.71	

1.40

131

				4.73
32	1.16			
				5.93
31	1.20			
				5.80
34	1.37			
				5.97
68	2.00			
				5.96
70	3.59			
				6.39
1.24	5.22			
				5.83
1.59	5.14			
				5.83
1.47				

132

B.M  
140

44.96 5.79 39.17

10.00 34.96

110

4.29 40.67 34.15

9.55 35.41

111

5.34 39.62 34.06

9.90 35.06

112 0

9.18 40.78 33.97

✓  
35.10

π

4.61 45.39 46.17

113

5.70 39.69 33.88

10.55 34.84 3

114

5.15 40.24 33.79

10.60 34.79

115

4.27

4.27 41.12 33.71

10.90 34.48

116 0

5.73 39.66 <sup>33.46</sup><sub>32.78</sub>

π

4.50 44.16

✓  
37.50

7.56

~~5.03~~

133

Top concrete header to 16" tile

at 109+40

6.52  
Bottom of file

1.28

~~6.28~~  
~~7.18~~

5.56

1.00

5.92  
~~3.92~~

6.81

1.13

~~5.92~~  
~~3.96~~

5.81

96

5.45  
~~3.64~~

6.45

1.00

4.95

7.42

.79

4.70

6.05

.89

134

117	44.16	4.56	39.60	<del>32.24</del> 33.52 35.30
118		4.26	39.90	<del>32.00</del> 33.43
		9.80	35.36	
119		4.90	39.26	<del>32.74</del> 33.34
		10.05	34.11	
0		9.80	39.28	
$\pi$	4.31	43.59		
120		5.33	38.26	<del>31.84</del> 33.25
			34.20	
121		5.35	38.24	<del>31.84</del> 33.16
			34.30	
122		5.26	38.33	<del>31.74</del> 32.07
		9.65	33.94	
123		5.03	38.56	<del>31.72</del> 32.19
		9.85	33.74	
124		5.65	37.94	<del>31.66</del> 32.80
		10.10	33.49	

135

	7.68			
	1.88	6.18		
	10.60			
	1.93	6.57		
	7.00			
	.77	5.92		
	4.78			
	95	5.01		
	6.80			
	1.14	5.08		
	8.84			
	1.87	5.26		
	7.28			
	76	5.58		
	3.79			
	68	5.05		



136

125	43.59	9.90	38.69	<del>32.81</del> 31.60
		10.55	33.04	
126		5.00	38.59	<del>32.71</del> 31.64
		10.25	33.34	
127		5.21	38.38	<del>32.62</del> 31.48
		10.20	33.39	
128		6.23	37.36	<del>32.53</del> 31.44
		10.40	33.19	
129		6.00	37.59	<del>32.44</del> 31.40
		10.20	33.39	
B.M.O		1.73	41.86	
K	1.70	43.56		
130		6.05	37.51	<del>32.35</del> 31.39
		9.95	33.61	
		5.70		<del>32.26</del> 31.29
131		<del>10.40</del>	37.86	
		10.40	33.16	
132		5.48	38.08	<del>32.14</del> 31.22
		10.25	33.31	

2.33

24

5.89

2.42

63

5.88

8.39

77

5.76

4.20

66

4.83

6

95

5.15

8.30

Top center N. parapet to bridge at  
road at 1294.30

126 Began Noon Aug 28

8.95

90

5.60

7.53

1.13

5.90

137

138

133

43.56

5.85

37.71

~~32.09~~  
31.16

10.65

32.91

134

6.17

37.39

~~32.00~~  
31.70

10.20

33.36

135

5.64

37.92

~~31.91~~  
31.44

10.80

32.76

136

6.07

37.49

~~31.82~~  
31.00

10.45

33.11

1370

6.36

37.20

~~31.73~~  
30.44

11.00

32.56

π

5.25

42.45

138

4.67

37.78

~~31.44~~  
30.48

10.00

32.45

139

5.29

37.16

~~31.58~~  
30.72

9.70

32.75

140

5.89

36.61

~~31.47~~  
30.76

9.50

32.95

7.14

82

5.02

7.85

1.36

5.39

8.17

85

6.01

7.92

1.29

5.67

7.85

83

5.47

6.07

81

6.19

7.40

1.19

5.50

9.90

1.98

5.14

139

140

141

42.45

5.50

36.95

31.39  
~~30.70~~

1.36

10.00

5.56

9.70

32.75

31.31  
~~30.44~~

11.75

142 0

5.06

37.39

31.31  
~~30.44~~

1.79

6.08

9.35

33.10

π

5.75

43.14

10.60

143

4.89

38.25

31.22  
~~30.78~~

1.07

7.03

10.85

32.29

7.76

144

5.35

37.79

31.14  
~~30.72~~

1.00

6.65

11.00

32.14

6.95

145 0

6.99

36.15

31.04  
~~30.46~~

88

5.09

11.20

31.94

π

6.40

42.55

6.66

146

4.30

38.25

30.98  
~~30.40~~

.92

7.26

10.65

31.90

7.15

147

5.00

37.55

30.89  
~~30.34~~

1.01

6.66

10.70

31.85

7.40

148

9.94

37.61

30.81  
~~30.28~~

99

6.80

31.80

141

142

0		42.55	10.69	31.86	
$\pi$	10.28	42.14			
149			4.43	37.71	<del>30.73</del> <del>30.92</del>
				31.75	
150 0			5.14	37.00	<del>30.63</del> <del>30.18</del>
	5.33	42.33			
150			10.85	31.48	
151 0			5.27	37.06	<del>30.55</del> <del>30.12</del>
				31.40	
$\pi$	5.20	42.26			
152			5.00	37.26	<del>30.47</del> <del>30.06</del>
			10.70	31.56	
153 0			10.70	41.56	
$\pi$	10.49	42.05			
153			5.75	36.30	<del>30.89</del> <del>30.41</del>
			10.70	31.35	
154 0			6.05	36.00	<del>30.31</del> <del>29.74</del>
			10.90	31.15	

143

				7.43	
					6.98
			1.82		
				6.91	
			85		6.37
				6.66	
			95		6.51
				7.36	
			1.09		6.79
				7.58	
			96		5.91
				6.66	
			84		5.69

144

	$\pi$	5.29	41.29 <del>42.05</del>	5.29	36.00	
155			8	5.23	36.06	<sup>30.23</sup> <del>29.86</del>
				10.05	31.24	
D				10.12	31.17	
$\pi$	10.15	41.32				
156				4.60	36.72	<sup>30.15</sup> <del>29.82</del>
				10.00	31.32	
1570				4.49	36.84	<sup>30.06</sup> <del>29.74</del>
				10.20	31.12	
$\pi$	4.78	41.62				
158				4.23	37.39	<sup>29.98</sup> <del>29.70</del>
				10.55	31.07	
159				4.90	36.72	<sup>29.90</sup> <del>29.64</del>
				10.65	30.97	
D				6.47	35.15	
$\pi$	5.21	40.36				
160				3.73	36.63	<sup>29.91</sup> <del>29.60</del>
				9.60	30.76	

145

					6.75	
						5.83
				1.01		
					8.08	
						6.57
				1.17		
					8.22	
				1.06		6.78
					7.96	
				1.09		7.41
					8.50	
				1.07		6.82
					785	
				.95		6.82

146

1610	40.36	4.73	35.63	<del>29.73</del> 29.71
		9.66	30.70	
$\pi$	6.63	42.26		
162		4.87	37.39	<del>29.65</del> 29.60
		11.80	30.46	
163		5.54	36.72	<del>29.57</del> 29.42
		11.85	30.41	
1640		5.73	36.53	<del>29.48</del> 29.36
	5.40	41.93		
161			30.40	
165		4.98	36.95	<del>29.41</del> 29.30
		11.90	30.05	
1660		6.15	35.78	<del>29.33</del> 29.29
		11.80	30.13	
$\pi$	6.33	42.11		
167		5.31	36.80	<del>29.24</del> 29.11
		12.20	39.91	

7.10

97 5.90

6.60

81 7.74

6.10

89 7.15

6.52

92 7.05

5.70

62 7.59

5.75

80 6.45

5.37

67 7.56

147

148

168	42.11	5.78	36.33	29.16 29.12	95
		12.00	30.11		
1690		5.74	36.37	29.09 29.04	92
$\pi$	4.24	40.61			
		10.60	30.01		
170		5.41	35.20	29.00	1.21
		10.40	30.21		
171		4.38	36.23	28.91	.62
		10.85	29.73		
170		11.02	29.59		
$\pi$	12.21	41.80			
172		5.13	36.67	28.82	1.38
		11.60	30.20		
1730		5.24	36.56	28.73	1.47
$\pi$	4.04	40.60			
		10.50	30.10		
1740		3.39	37.21	28.65	1.30
		10.65	29.95		

6.00

692

39.00  
 170 - 29.00  
 1000  
 1020  
 850  
 1500  
 1360  
 1530  
 87  
 261  
 351  
 27.37

7.28

795

6.20

6.77

7.32  
82

710

7.85

10.50

7.83

11.20

8.56

149

30.63  
 29.00  
 1.63  
 27.37

150

$\pi$	3.84	41.05		37.21		
175			4.45	36.60	28.56	
			11.45	29.60		
170			11.27	29.78		
$\pi$	10.42	40.20				
176			4.85	35.35	28.97	
			10.50	29.70		
1770			4.97	35.23	28.38	
$\pi$	4.55	39.58				
			10.20	29.38		
1780			4.84	34.74	28.80	
			10.10	29.48		
$\pi$	6.00	35.48				
179			5.18	35.56	28.21	
				29.40		
10	5.88		5.88	34.86		
$\pi$	4.95	39.81				

8.35

151

1.04 8.04

7.75

1.23 6.88

8.22

1.00 6.85

8.00

1.18 6.34

8.75

1.19 7.35

8.46



152

180 39.81 3.50 36.31 28.12

10.60 29.21

0 3.80 36.01

π 3.48 39.49

1810 9.34 35.15 28.04

10.60 28.89

π 4.01 39.96

0 5.28 34.68

10.18 44.86

182 10.10 34.76 27.93

71. 28.80

183 11.64 33.22 27.84

✓ 28.60

184 11.24 33.62 27.75

✓ 28.40

1850 12.00 32.56 27.67

✓ 28.20

π 11.71 44.57

153

1.09 8.19

7.29

85 7.11

6.36

87 6.83

6.04 P.A. at 183

76 5.38

5.22

65 5.87

4.87

53 5.19

154

186 44.57 11.69 32.88 27.58

28.10

187 10.00 34.57 27.49

28.00

188 11.08 33.49 27.41

27.80

189 10.69 33.88 27.33

27.60

B.M 10.81 33.76

190 10.80 33.77 27.37<sup>25</sup>

27.250

191 10.25 44.32 27.17

27.40

1920 10.68 33.89 27.09

27.90

π 5.21 38.10

192 10.70 27.90 27.01

1

3.89

62 5.30

3.81

51 7.08

3.34

39 6.08

2.44

27 6.55  
189+70 leaves R.R.

1.92

25 42 Top bottom step S side E wing

6.72

1.33

13 7.05

1.63

31 6.80

39 39

155

156

193	38.10	4.80	33.30	26.93
		11.15	26.95	
194		5.08	33.82	26.85
		10.35	27.75	
195		4.95	33.15	26.76
		11.10	27.00	
196		4.30	33.80	26.67
			27.00	
197		4.35	33.75	26.59
X	3.81	37.56		
		10.15	27.41	
198		4.84	32.72	26.50
			27.30	
199		4.15	33.91	26.41
		10.55	27.01	
200		3.95	33.61	26.32
		10.20	27.36	

157

	1.22	
.02		6.37
	3.02	
90		6.17
	4.22	
24		6.39
	1.74	
33		7.13
	4.26	
82		6.16
	6.00	
80		6.22
	5.69	
60		7.00
	6.07	
1.04		7.29

158

201	37.56	4.04	33.52	26.24
		10.70	26.86	
2020		5.18	32.38	26.75
$\pi$	6.46	38.89		
		12.10	26.74	
203		5.65	33.19	26.07
			26.60	
204		4.50	34.34	25.99
		12.30	26.54	
205		5.05	33.79	25.91
			26.50	
206		4.74	34.06	25.83
			26.40	
206775		12.40	26.44	25.77

159

	6.15	
62		7.28
	2.29	
-		5.63
	1.96	
53		7.12
	4.00	
55		8.35
	4.22	
.59		7.88
	4.30	
.57		8.23
	3.44	
.67		
	Temp. line	.67

160

~~Thompson~~  
T Eggers -  
sold 30 acres of  
east 70 a piece.  
layband describe  
plat.

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