

← A4 →

← LETTER →

BROWN FOR

Henshew & Mary
M. Ward

Book 74

4' Rise
8' Span

6.00
1.00
2.00

BENCH MARKS.

JOHN FLINN ROAD

UNION TWP.

Henry B. Steeg - Level

R. G. Riggan - Rodman.

August 5, 1930.

Weather - Clear + Sunny.

2.
B.M. No

1. S.E. Cor. "L" HEADER AT
N.W. Cor. Intersection of
Flinn & Leathers Roads

ELEVATIONS.

110.00.

2. S. End of W. Rail of
Concrete Bridge.

114.30

3. S. Gate Post of
John Flinn Residence.

122.45

4. High Point on Corner post
on W. side road between
corn field + pasture. App.
1/8 mi. N. of Flinn Res.

125.70

5. High Point on Corner Post
S.W. cor. intersection of
Flinn and Bailey Roads.

130.34

6. Top. S. Rail C. I. & W. R. R.
at E. Flinn Road.

128.96

7. Cement Sill of S. Window
E. Side Brick School.

137.72

B. M. No.

8 N. E. corner of post at
S. W. corner of road at end
of Flint Road

133.75

Elev. S. Flint Road at end

129.36

8

7

BENCH MARKS.

MARION BAILEY ROAD

UNION TWP.

Henry B. Steeg - Levelman.
R. S. Figger - Rodman.

August 5, 1920

Weather - Clear + Sultry.

8

B.M. NY

- | | | |
|----|--|-----------------------------|
| 1. | High Point on Conc. Post
SW cor. intersection of
Flinn & Bailey Roads
Same B.M. as No. 5 on
Flinn Road | 130.34 |
| 2. | N. Post of Small gate to res.
on E. side road 300' above
terr. | 131.06 |
| 3. | N.E. corner of Concrete
Step to Church | 129.92
119.96 |
| 4. | S.W. Corner of Concrete
walk in front of
J.D. Brickert store. | 132.07 |
| 5. | Top Conc. Post 250' N. of
C.I. & W. R. R. tracks. | 134.59 |
| 6. | Brace Rock in SW corner
of road intersection at end
of Alex & Bailey Road at end | 125.36 |
| | | 126.09. |

9

10
TRANSIT NOTES.

John Flinn Road.

George R. Harvey - Chief of Party

Henry B. Steeg - Instrument.

R. G. Biggan - Rodman.

Chas. L. White - Rodman.

Aug., 6, 1920

Weather - Clear + Hot.

12

66+95 End of Flinn Road.

53+53 Sec. Line

47+03.5 Φ of C.I. & W. RR.

40+14 Bay Point M. Bailey Road.

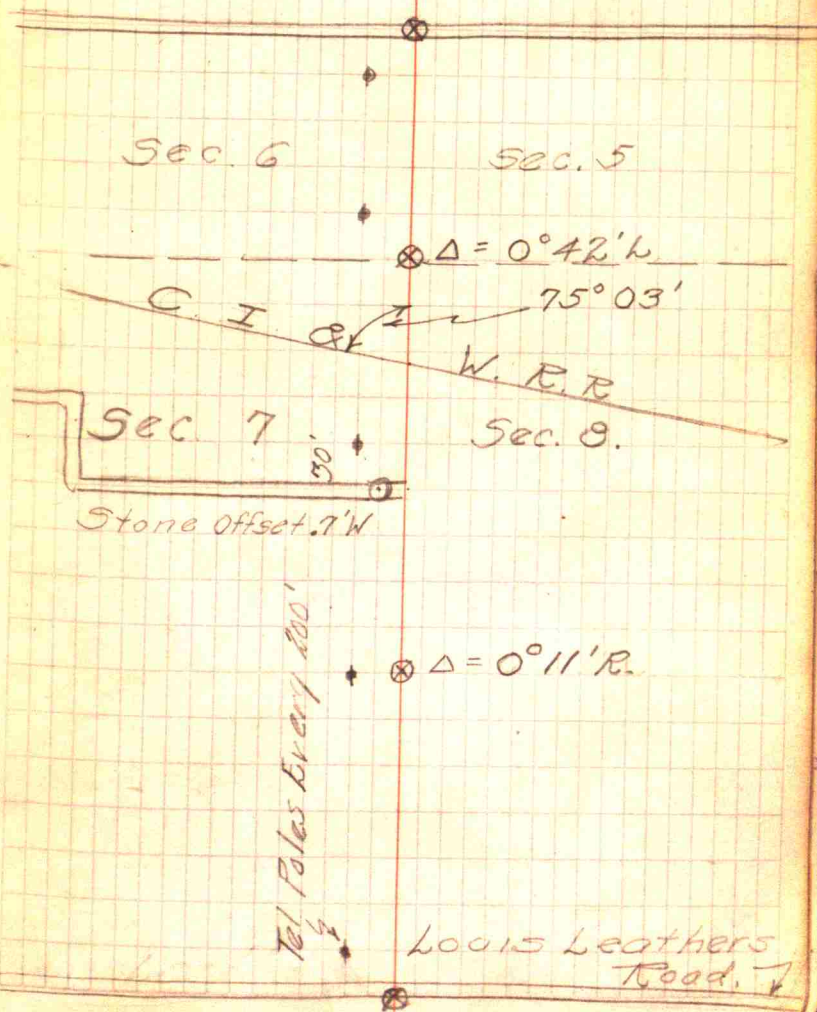
26+79.5 E $\frac{1}{2}$ Mi. Stone Sec. 7

0+00

(Near Montclair)

13

Note: Stakes set every 500'
Offset 15' E. of Φ .



14

15

TRANSIT NOTES.

MARION BAILEY ROAD.

George R. HARVEY - C. of T.
Henry B. Steeg - Transitman.
R. G. Riggan - Rodman.

August 7, 9, 1920.

16

16+76.3 P.T.

16+46.7 Turn North $\Delta = 87^{\circ}34'R$ P.I.

15+96.8 T.C.

13+07.4 T.C.

14+01.2 Turn West $\Delta = 88^{\circ}58'L$ P.I.

14+55.6 P.T.

6+76.3 P.C.

7+69.9 Turn North $\Delta = 88^{\circ}50'R$ P.I.

8+24.37 P.T.

0+00

17

Iron Pin

 $\Delta = 87^{\circ}34'R$

T = 49.92'

L = 79.55'

D = 110°

E = 20.06'

D = 5°30'

C = 10.0'

High Rack

Hub

 $\Delta = 88^{\circ}58'L$

T = 93.79'

L = 148.18'

D = 60°0'

E = 38.36'

D = 3°

C = 10'

Hub

 $\Delta = 88^{\circ}50'R$

T = 93.58'

D = 60° L = 148.05'

E = 38.2'

D = 3°0'

C = 10.0'

John Flinn Road

20

38+10 End of Marion-Bailey Road

25+24.7 P.T.
 24+13.8 Section Line P.I.
 24+22.6 P.C.

21

Stone 15' E of T

Jas. Scott

Scott, Jas.

$\Delta = 7^{\circ} 9' R.$ ($D = 1045'$)
 $T = 51.14'$ ($C = 50'$)
 $L = 102.14'$
 $E = 1.6'$
 $D = 7^{\circ} 00'$

Section Line

Stone 15' E of T

Sta.

$$18 + 28.2$$

$$\Delta 86^\circ 24' L$$

$$T = \frac{53808}{100} = 538.08$$

$$L =$$

$$\frac{100 \times 86.4}{100} = 86.4$$

$$D = 100^\circ$$

$$E =$$

$$43^\circ 12'$$

$$86.4 \left| \begin{array}{r} 2592 \\ 2592 \end{array} \right. \quad \left| \begin{array}{r} 30' \\ \hline \end{array} \right.$$

Def 30' per ft arc,
= 5° for 10'

$$\begin{array}{r} 18 + 28.2 \\ 53.8 \\ \hline \end{array}$$

$$1774.4$$

$$5^\circ 18'$$

$$5^\circ$$

$$\hline 10^\circ 18'$$

$$\begin{array}{r} 78.7 \overline{) 2598} \quad \overline{) 3301} \\ \underline{2361} \\ 2370 \\ \underline{2361} \\ 90 \end{array}$$

$$33.01$$

24

Miller Road

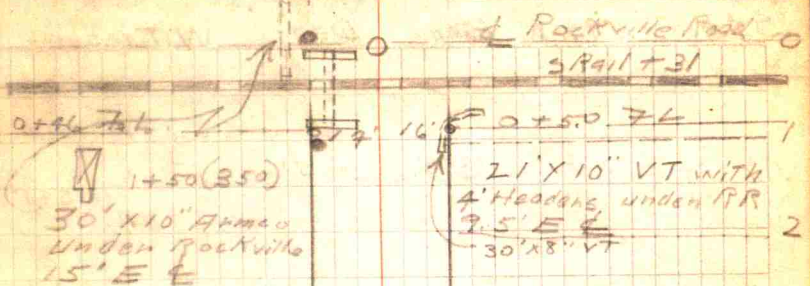
Sta	Mark	Bear	Def	Witnesses
0+00	I. P.	N15°W		SE. cor S. Header Cut Rent under RR N. 20° E. 26'

Cont. Bn	300'S	stap	R.P. Crossing	
"	"	500'W	"	0 Sign N15° E 52.4'

Power Pole E. side 3' W. Fence Line
 spaced 140' - First pole 0+20 - and
 0+60. Then every 140' to 9+80
 Then on W side from 10+20 to End
 2' E of Fence line

P. cen Rockville Road

(25)

+62
-57

+67

Jenny McClain

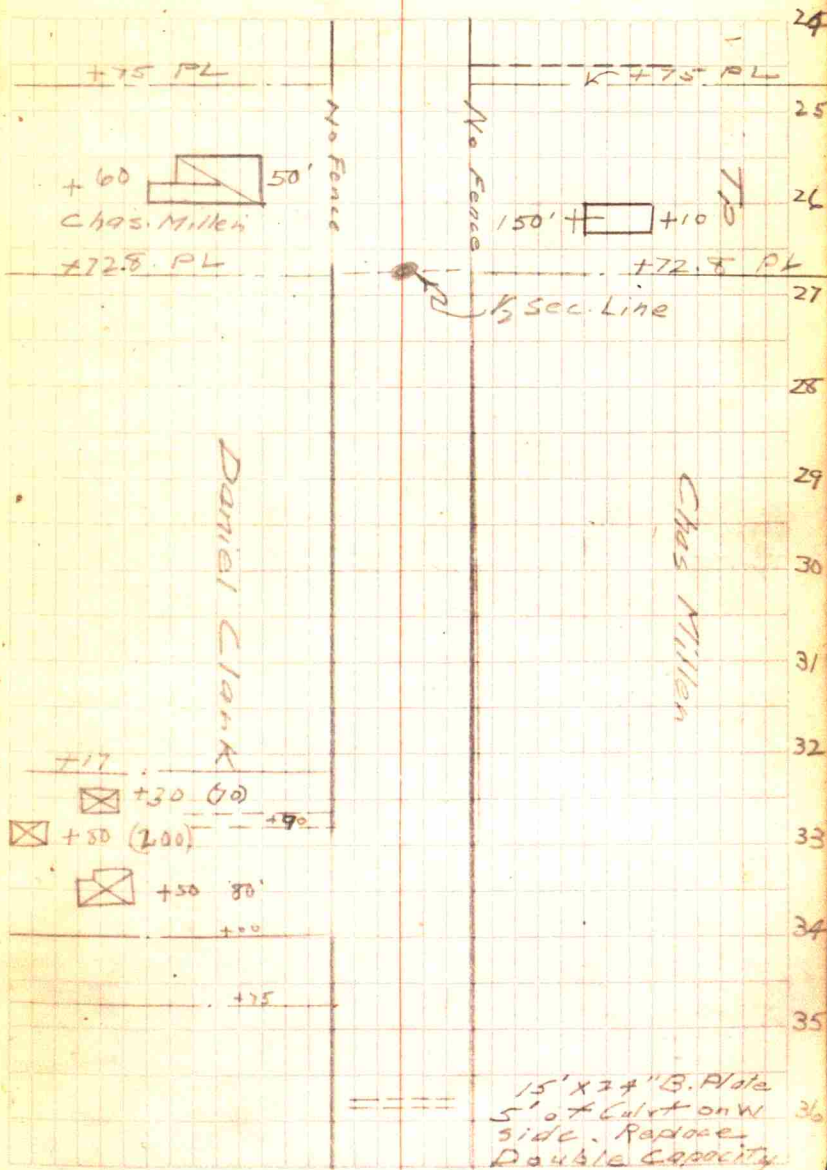
Jenny McClain

+50
+9716' x 15" V.T.
80' W of E to W side

28

Sta	Mark	Bean	Def.	Witnesses
26+72.8	Stone Cen. Sec 5		0°0'	6" Sugg. S 35° E 40.5' Con Post E 17.5'

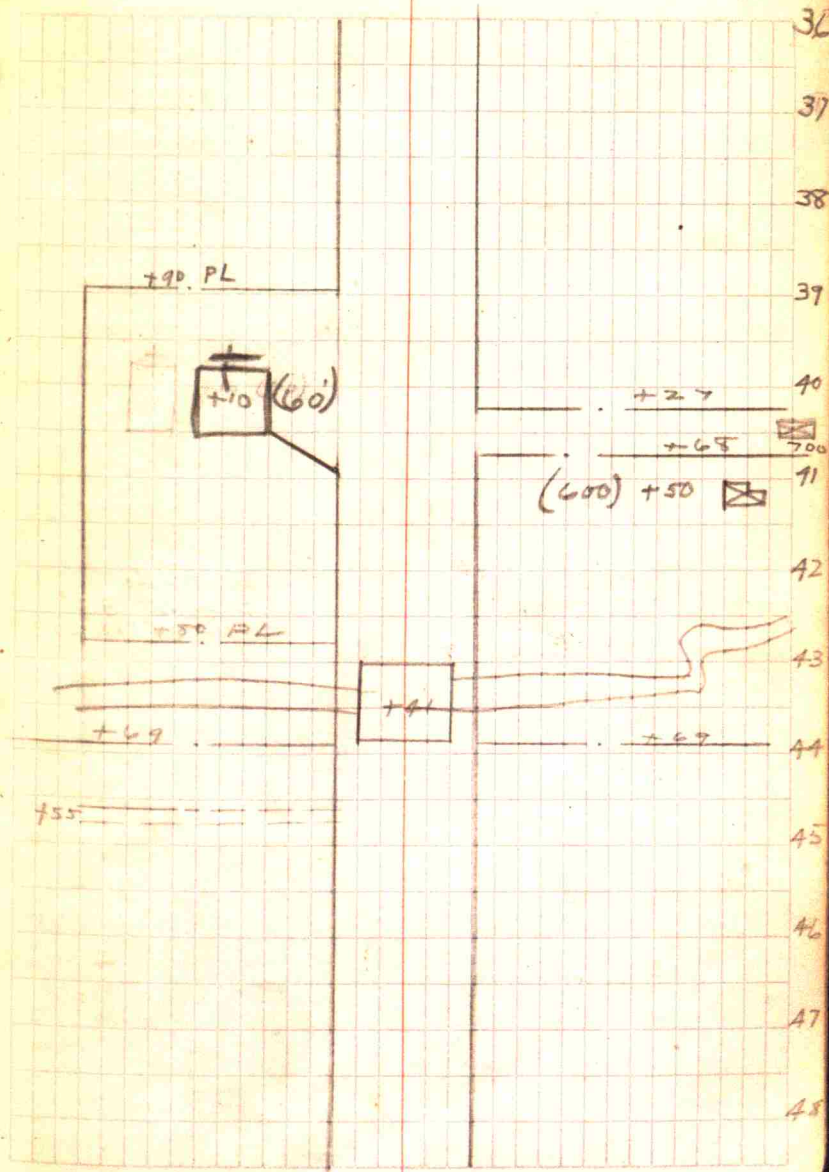
29



30

43+41 Iron Bridge
 Span 28'
 Rdway 14'
 Rise 7'

31



38

W
20

Miller Levels

Sta	A	B	C	D	E
0+00 Cutvt under Rockville Culvt 42' S St 00 Culvt under RR	99.75 7L S 77.95 7L E 53.50 7L N 98.75	96.50 7L N 97.95 7L S 98.20	100'S 200'S 95.60	100'E 100.50	99.95
0+21	99.50 ²¹	101.30 ²²	101.40 ¹³		101.20
0+31	102.15				102.15
0+36	102.15				102.15
0+42	99.70 ²⁰	101.75 ²³	101.80 ¹⁴		101.90
1+00	102.40 ²⁰	102.00 ¹⁶⁷	100.90 ¹³	101.80 ⁹	101.90
2+00	104.00	104.20 ¹⁶⁷	103.80 ¹³	104.50 ⁹	104.70
3+00	103.20	103.00 ¹⁶⁷	103.00 ¹³	104.10 ⁹	104.30
4+00	103.00	103.00 ¹⁶⁷	102.70 ¹⁴	104.00 ⁷	104.10
5+00	103.30	103.20 ¹⁶⁷	103.00 ¹⁴	104.20 ⁶	104.40
6+00	103.80	103.80 ¹⁶⁷	103.50 ¹⁴	104.50 ⁶	104.60
7+00	104.40	104.10 ¹⁵⁷	104.10 ¹²	105.00 ⁷	105.10
8+00	104.30	104.50 ¹⁵⁷	104.30 ¹³	105.10 ⁷	105.40
9+00	104.40	104.60 ¹⁵⁷	104.10 ¹¹	105.30 ⁸	105.40
10+00	105.40	105.50 ¹⁵⁷	104.90 ¹²	105.60 ⁷	105.75
11+00	104.70 ¹⁶⁷	104.90 ¹⁶⁷	103.80 ¹²	105.20 ⁷	105.45
11+17	103.10 ²⁰	102.20 ¹⁶⁷	103.65 ¹³	104.90 ⁶	105.25
12+00	104.00	104.40 ¹⁶⁷	103.60 ¹³	104.90 ⁶	105.30
13+00	104.60	104.90 ¹⁶⁷	104.10 ¹³	105.10 ⁶	105.30
14+00	105.00	105.00 ¹⁷⁷	104.70 ¹¹	104.50 ⁷	105.70
15+00	105.50	105.20 ¹⁷⁷	105.10 ¹⁰	106.10 ⁴	106.30
16+00	106.20	106.00 ¹⁷⁷	105.50 ⁵	106.70 ⁴	106.75

20E.

39

7	6	H	I	Bench Marks
100.80 ^{200'E}	97.45 ^{200'W}	99.20 ^{100'W}	100.00	El. 100.00 S. Headen Culvt. under RR T.H.H.
101.00 ⁵	98.20 ¹⁰	100.00 ¹⁵	100.00 ²⁰	
			102.15	
			102.15	
101.50 ⁵	98.55 ⁵	100.65 ¹⁴	102.05 ¹	
102.00 ³	100.70 ⁵	103.00 ¹¹	103.20 ¹⁵⁷	103.60 ²⁰
104.65 ²	102.70 ⁷	104.15 ¹¹	104.30 ¹⁵⁷	104.30 ²⁰
104.40 ⁰	102.70 ⁹	103.30 ¹⁵⁷	103.30 ²⁰	
104.10 ³	102.50 ²	103.50 ¹⁴⁷	103.00 ²⁰	
104.10 ⁴	103.20 ⁹	103.50 ¹⁴⁷	103.00	
104.30 ⁴	102.20 ⁹	104.15 ¹⁴⁷	103.70	
104.90 ⁴	104.00 ¹¹⁷	104.80 ¹⁴⁷	104.30	
105.10 ⁴	104.30 ⁷	104.60 ¹⁴⁷	104.20	
105.60 ⁵	104.20 ⁸	104.70 ¹⁴⁷	104.50	
105.50 ⁵	104.45 ⁸	105.50 ¹⁴⁷	105.10	
105.35 ⁵	103.90 ⁸	104.60 ¹⁴⁷	104.00	El. 110.70 Top Cement post 16' W I.P. 5413+34.8
105.10 ⁴	103.60 ⁶⁷⁰	102.15 ^{67L}	102.90 ¹⁴⁷	
104.90 ³	103.80 ⁹	104.40 ¹⁴⁷	104.00 ²⁰	
105.00 ⁶	104.40 ⁹	104.90 ¹⁴⁷	104.60	
105.00 ⁶	105.00 ¹⁰	105.00 ¹⁴⁷	104.90	
106.20 ⁵	105.10 ¹⁰	105.80 ¹⁴⁷	105.90	
106.50 ⁵	105.70 ¹⁰	106.60 ¹⁴⁷	106.40	

40

20W

Sta	A	B	C	D	E
17+00	10660	10630	10630	10700	10730
18+00	10740	10730	10670	10750	10770
19+00	10755	10740	10660	10770	10790
20+00	10720	10700	10610	10700	10700
21+00	10575	10570	10490	10600	10650
22+00	10490	10520	10440	10640	10665
22+52	10290	10230	10570	10720	10725
23+00	10560	10560	10510	10700	10710
24+00	10760	10550	10700	10860	10865
25+00	10880	10910	10870	10950	11040
26+00	10970	10990	10960	11050	11060
27+00	11110	11130	11030	11110	11120
28+00	11200	11230	11100	11180	11230
29+00	11250	11270	11210	11270	11275
30+00	11200	11200	11100	11200	11240
31+00	11160	11150	11090	11180	11220
32+00	11200	11180	11060	11230	11236
33+00	11300	11300	11100	11260	11270
34+00	11280	11280	11080	11190	11150
35+00	11060	11070	10930	11050	11060
35+97	10860	10635	10790	10960	10980
36+00	10880	10890	10650	10980	10930
37+00	10950	10930	10840	10950	10975
38+00	10910	10900	10850	10950	10950
39+00	11010	11000	10850	11070	11090

41

F	G	H	I
10730	10660	10660	10650
10750	10650	10720	10700
10765	10700	10740	10740
10650	10650	10680	10690
10620	10520	10591	10650
10660	10420	10460	10500
10700	10530	10260	10260
10700	10560	10650	10650
10840	10720	10920	10940
10990	10910	10960	11010
11050	10970	11020	11020
11110	11030	11070	11040
11180	11100	11130	11140
11270	11140	11210	11230
11230	11100	11160	11190
11230	11120	11120	11080
11260	11270	11270	11260
11170	11120	11250	11260
11020	10940	11065	11040
10990	10750	10600	10650
10970	10710	10670	10650
10950	10860	10910	10900
10950	10860	10890	10850
11010	10940	10950	10950

42

Sta	A	B	C	D	E
40+00	111.00	110.70 177	110.10 10	110.70 4	110.80
41+00	111.70	111.80 177	112.10 10	111.70 4	111.80
42+00	106.20	106.80 167	106.50 11	107.60 4	107.60
43+00	102.50	103.00 167	102.20 11	105.05 3	104.93
43+27	100.70 72	100.70 167	100.35 11	104.50 3	104.50
43+41	97.70				104.72
43+56	100.60	106.60 167	100.40 9	104.00 4	104.80
44+00	102.10	102.20 157	101.60 5	103.70 2	103.50
45+00	104.15	104.10 167	102.50 5	104.10 2	104.20
46+00	108.70	108.40 167	106.80 9	107.50 4	107.50
47+00	115.20	115.20 157	103.40 5	113.20 3	113.70
48+00	117.50	117.40 167	116.20 7	116.60 2	116.20
49+00	115.20	116.50 972	114.20 9 Top	115.00 4	115.20
49+78	114.50	111.40 167	112.90 9	114.60 4	114.90
50+00	114.20	114.50 167	112.40 5	114.90 2	115.00
51+00	116.00	116.10 167	114.20 8	115.52 3	115.50
52+00	117.80	118.10 167	116.20 10	117.30 4	117.30
53+00	119.20	119.00 167	118.20 13	119.00 4	119.50
54+00	119.70	119.90 100 W 20 W	120.20 10		120.20
54+10	121.50	120.50			stone 120.45

43

F	G	H	I
110.60 10		110.90 20	
112.00 6	111.80 14	112.20 157	112.20 20
107.70 7	107.20 9	111.50 187	112.00 20
115.10 7	103.10 11	103.00 187	103.00 20
104.00 8	99.50 12		99.50 20
		7 Low E.	
104.80 9	99.70 12	101.10 177	102.00 20
103.95 10	101.60 15	101.50 177	101.20 20
104.20 8	102.35 14	102.80 177	103.30 20
107.60 9	106.70 12	107.70 177	108.50 20
113.70 9	113.20 11	114.20 157	116.50 20
116.60 10	115.20 13	116.20 167	116.30 20
115.20 9	114.20 14	115.20 167	115.50 157
115.30 9	112.00 11 Top	111.40 1172	111.60 157
115.20 5	113.60 12	113.70 157	
115.30 6	114.50 12	115.50 167	116.30 20
117.10 9	116.40 11	118.10 167	118.60 20
118.20 8	118.30 13	118.40 167	118.80 20
120.10 8			
		20 E	100 E
		120.30	120.10

Bottom Step
N. 71947 Church
Steps.

11245

44

Check B.M.
B.M. No 3. 112.45

⊙ 112.76

⊙ 106.15

B.M. No 2: 110.70 ✓

⊙ 104.55

B.M. No 1. 100.02 ✓

45
Miller

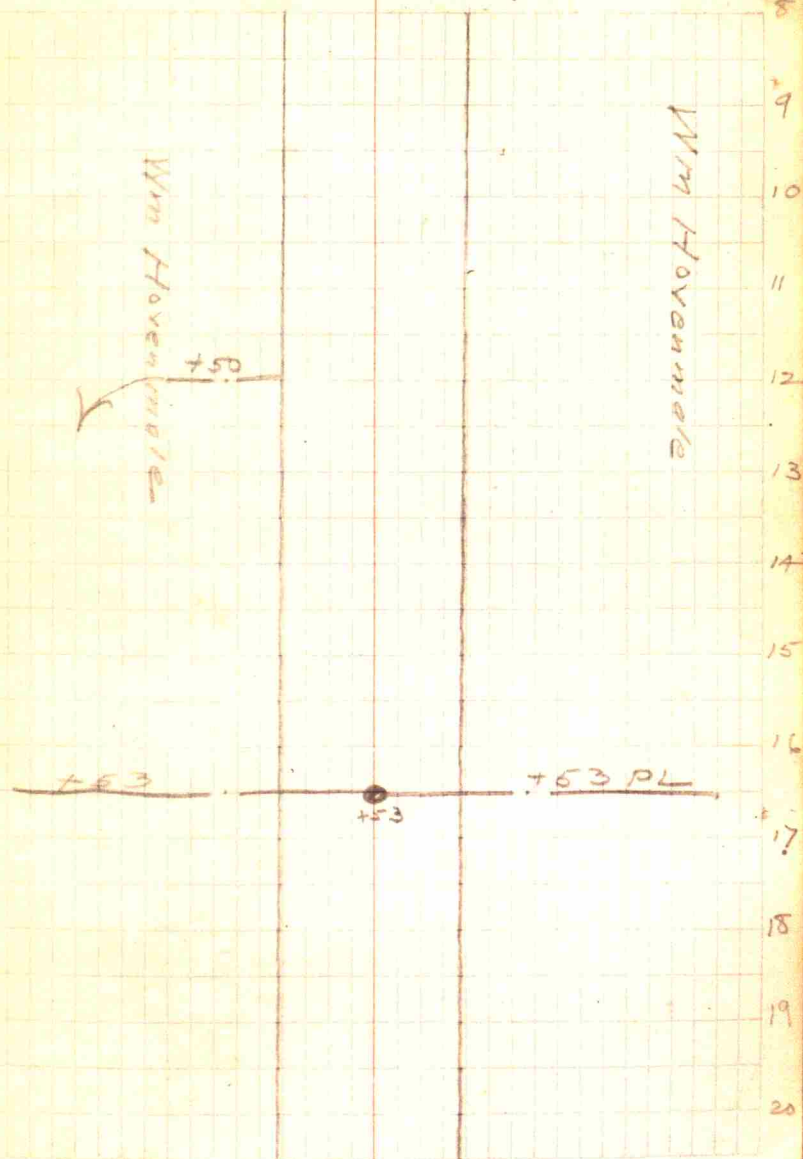
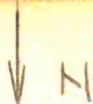
48

Sta MK Det Witnesses

16+53 Stone 0°00'

Con post
W 1"

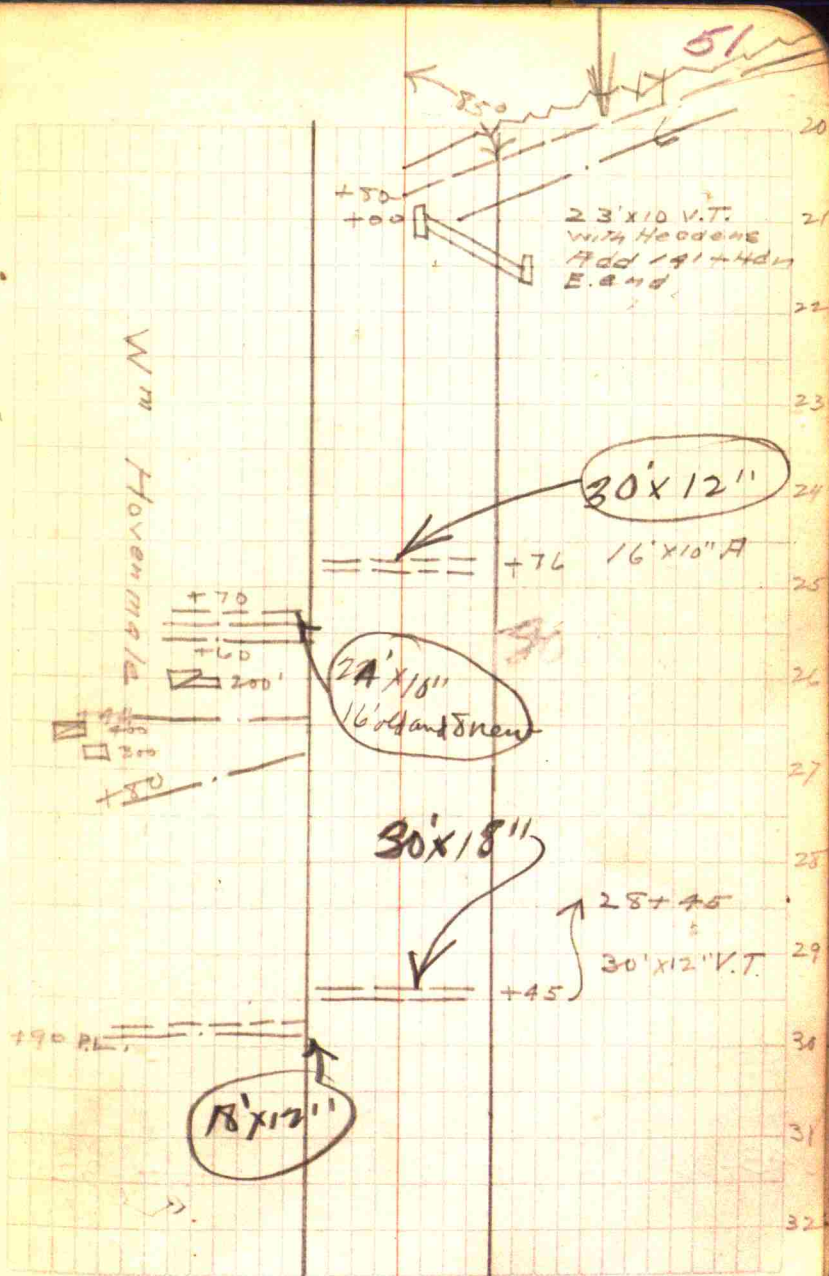
49



50
Sta MK Det Witnesses

Tel Poles E side Sta
2/1+00 to end at 7 line
150' apart.

Rail Fence on E Sta 12+50
to Sta 9 20+65



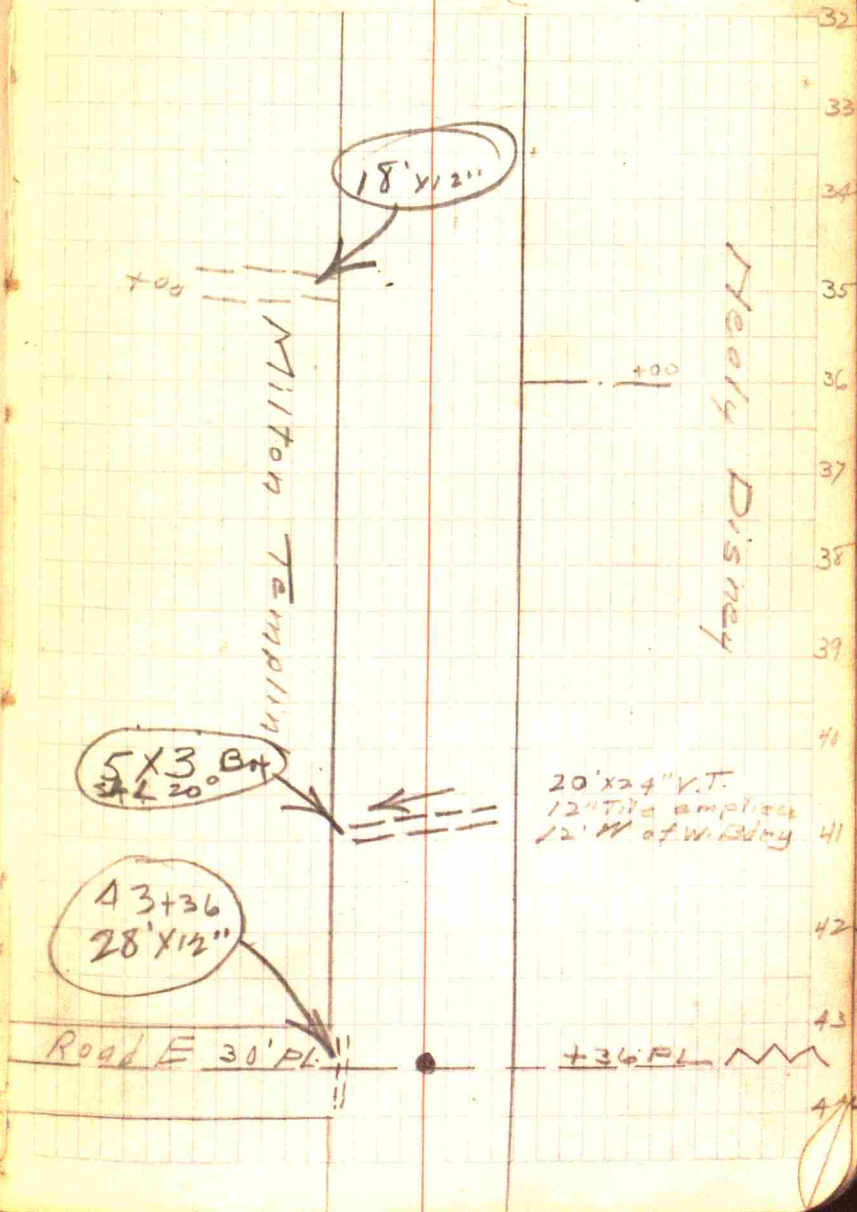
52
Sta MK Det Witnesses

43+36 Stone 0°00'

18" Apple N45°E
32'
Cor Post W
16.8'

53

YH



54
Sta MK Det Witnesses

Y.H

55

18' x 10"

Hedge fence 43+36 to 54+78
James BOON

John Ridpath

39+

44

45

46

47

48

49

50

51

52

53

54

55

56

56

Sta MK Det

Witness
Coh Post E 19'

56+78 Stone 0°00' S gate post 53°0'W33'

60+10

Flat Top

22' Span

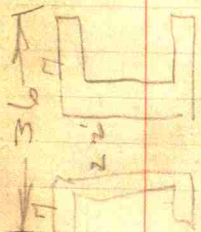
16' Rdway

5' Rise

Skewed 15° NE

Wings St. back

± Bh 1' E ± Rd



63+37

Steel Bridge
14' Rdway

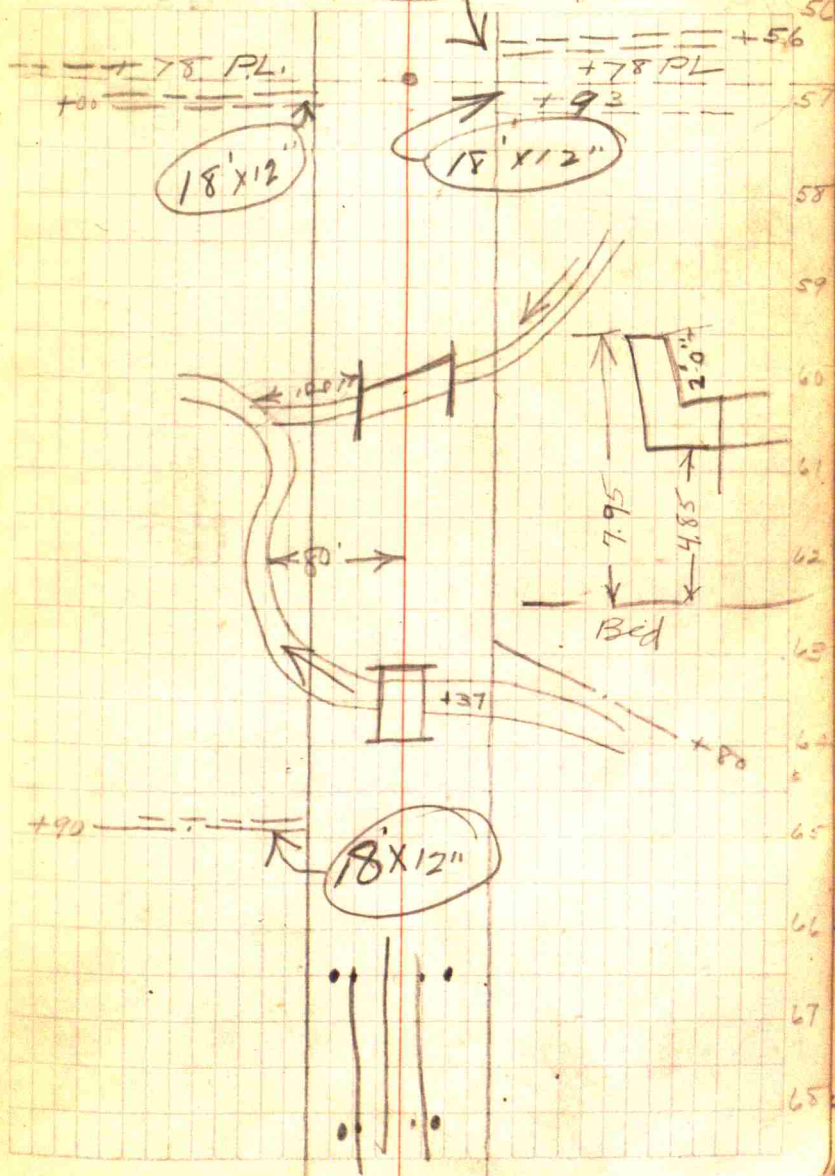
± ± Bh 2' W ± Road

Shift Bridge to Center of Rd - New Abuts - paint and blk floor
 All wings at 45°
 Clear N side of channel 50' each way and S side of channel 100' E at angle of 45° with ± of Road

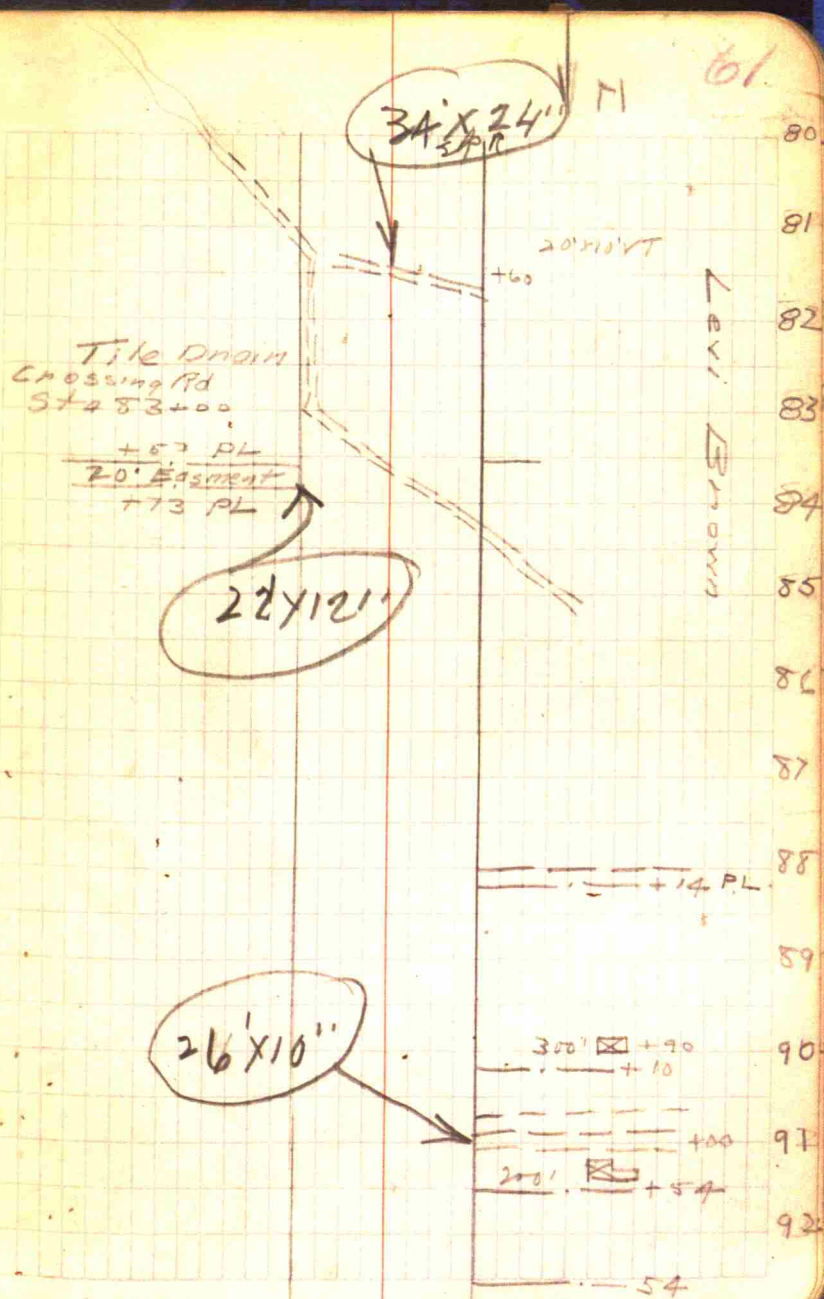
Widen to 24' Rdway
 and clear channel
 on S side
 100' E - to creek

18' x 12"

57



60
Sta MK Det Witnesses



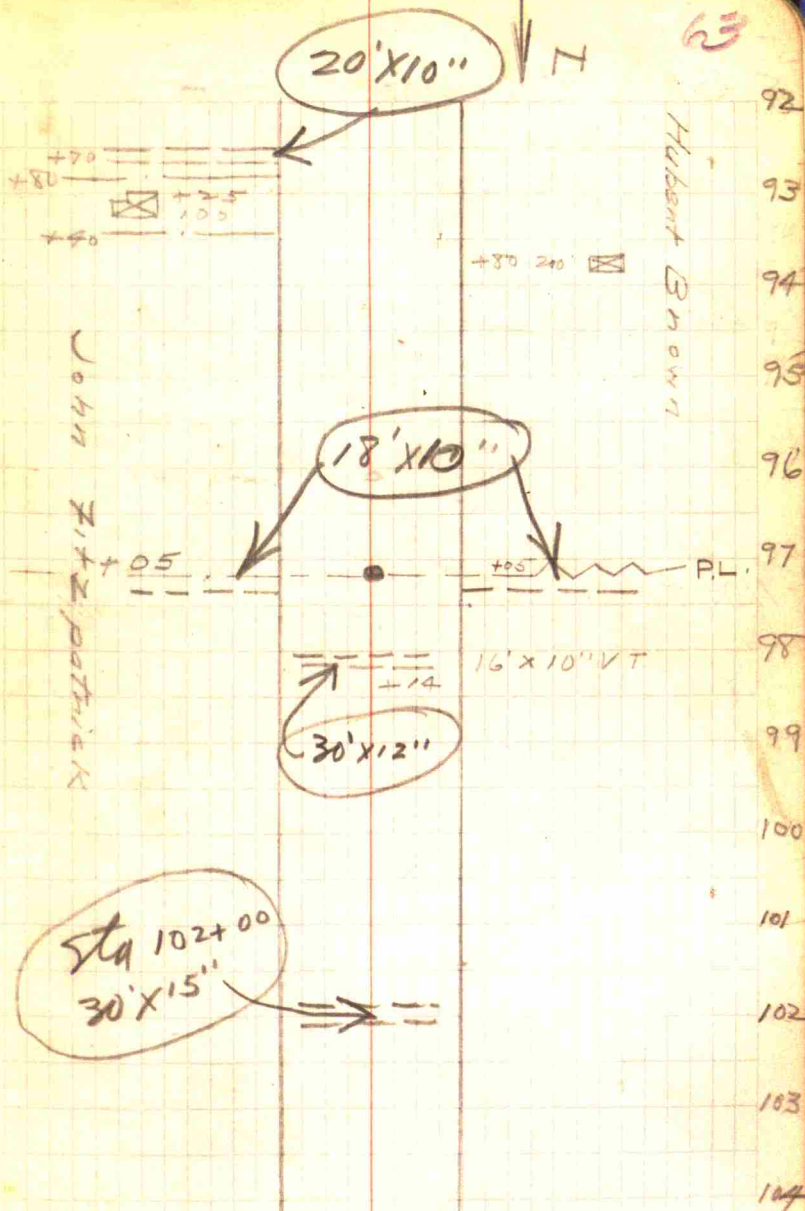
62

Sta MK Det. Witnesses

97+05 Stone

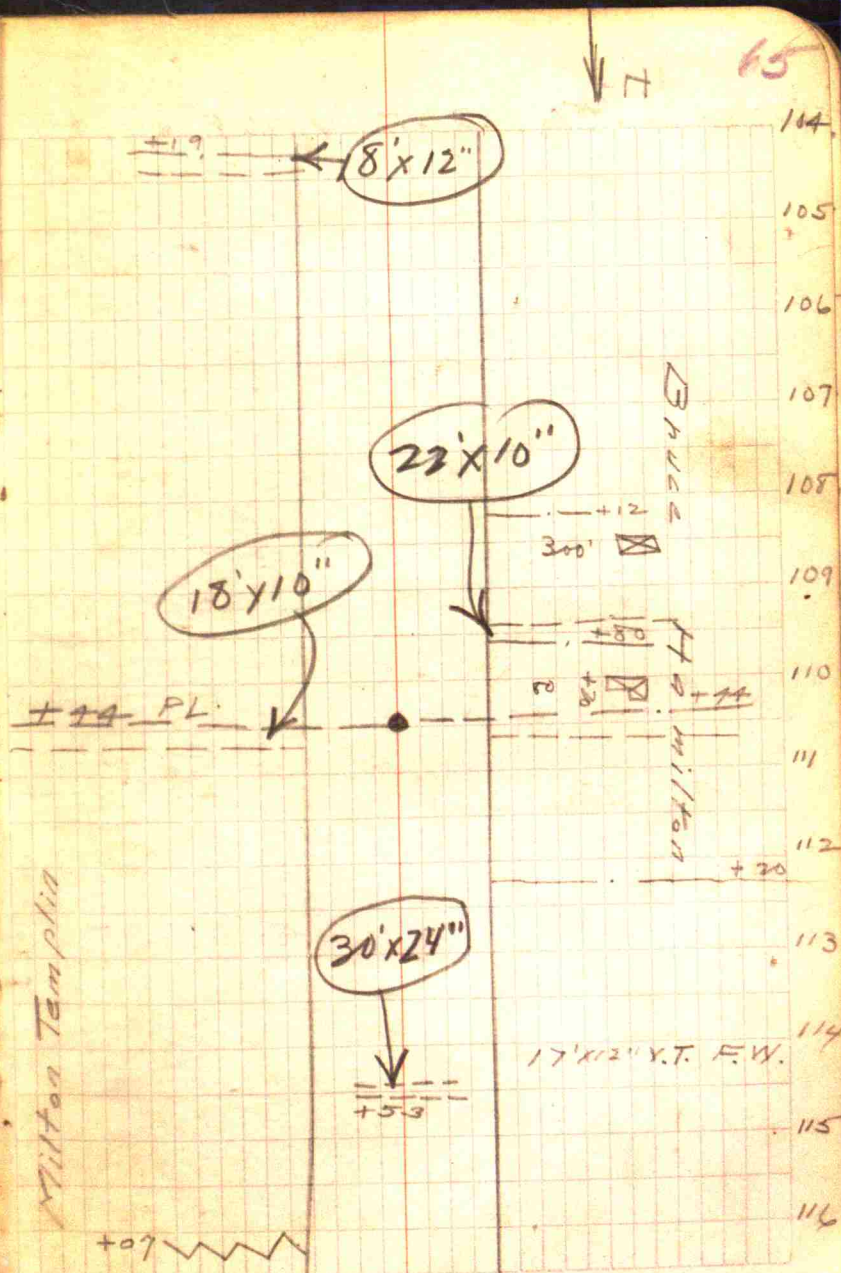
Con Post W 15'
" " E 15.8'

63



64
Sta 14K det Witnesses

110+44 Stone 0°00' Coh Post E 1A
16" Hickory S45°W 35'

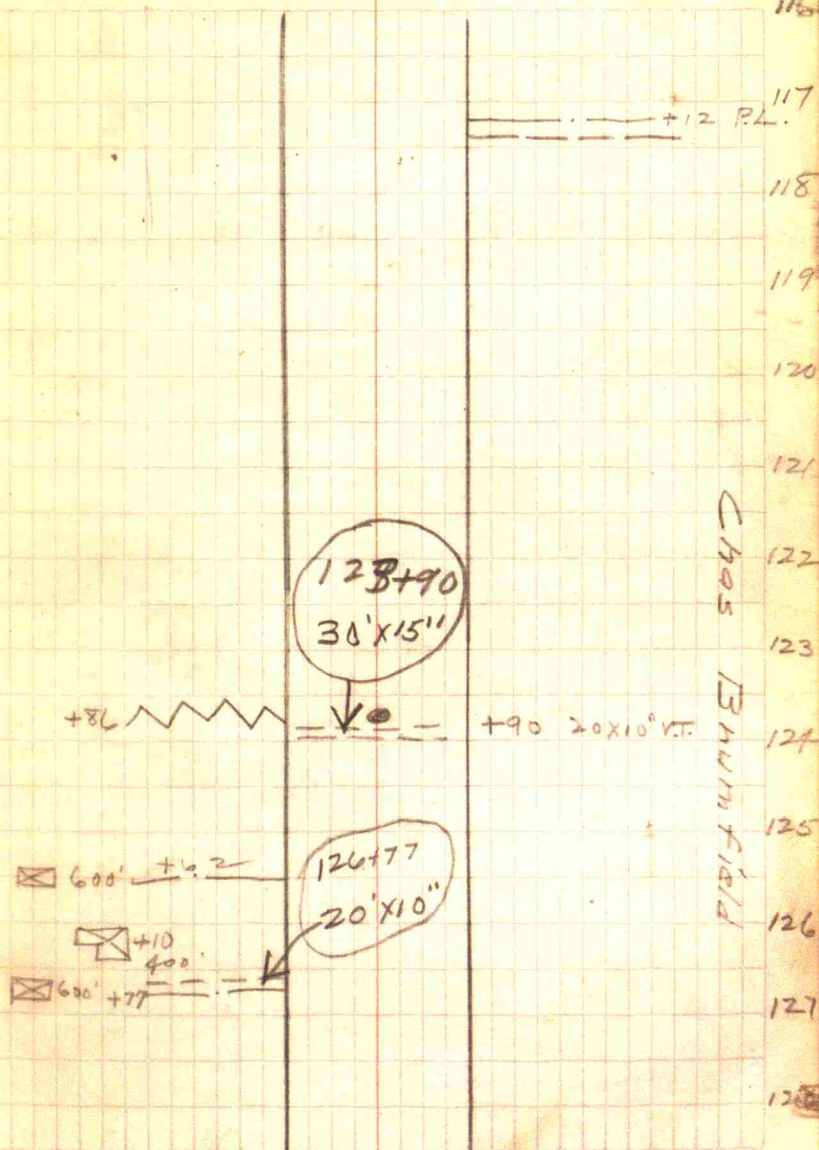


66

Sta MK Def Witnesses

123+86 Stone 0°00

67



68
Sta MK Det Witnesses

130+58 Stone End NW Con. S Headens 45E 16.5
SW " " " 45E 17.5

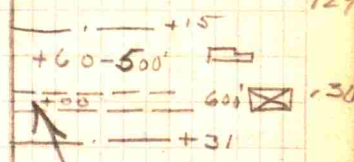
Road E 30'

26' x 18" V T with
L Headens
15' E E

John Ridpath

H

69



128

129

130

131

132

133

134

135

70

Prop Owens

E. Side - John Call. to Sta

Wm Hoozen Mail to Sta

Milton Templin to Road E

Boen to (40A)

Joe Faulkner to Lane

Fitzpatrick to 110744

Milton Templin to end

W. Side

Hoozen mail

Disney

J. Ridpath 40A

W. Thoup Heins 70A

~~Henry O. Deibel 40A~~~~Chas Rutledge 1~~

Edgar Star

Levi Brown

Hubert Brown

Bruce Hampton

Chas Brumfield

71

72 L. H. BROWN ROAD

Sta	A	B	C	D	E
0+0	200' E 93.75	100' E 94.20	20 94.85		95.60
1+00			25 94.80		96.40
1+20			92.40		94.40
1+70			25 77.50	5 80.00	81.60
2+00			25 79.00	5 77.16	78.50
2+40			26 78.80		78.70
3+00			25 80.72		81.00
3+65			25 85.50		85.00
4+00			23 92.80		92.20
5+00			99.00		98.00
6+00			101.70		103.80
7+00			104.00		105.20
8+00			108.60		107.40
9+00			106.80		105.20
10+00			103.00		102.50
11+00			102.60		102.15
12+00			94.60		94.70
12+ 65			83.50		88.00
13+00			89.50		91.60
14+00			93.00		92.50
14+80			83.10		83.20
15+00			81.00		83.00
16+00			94.10		94.70
17+00			91.50		94.75
17+20			91.00		92.90

LEVELS

73

F	G	H	I	B.M.
25 75.66	200 97.68	100' W 97.60	200' W 95.50	100.00 Can
	25 97.85			Post 36' NW
	96.50			Sta 0+00
15 73.90	17 93.00	25 94.50		✓
	24 75.40			
	24 77.70			
	25 81.45			Culvt Read
	25 86.00			Sta 10+00
	25 89.80			150'
	99.30			99.47 0
	104.70			
	105.30			
	105.90			102.
	104.00			10.2.35 0
	101.60			
	101.30			
	94.35			
	88.60			15' An. 50
	92.70			Regd. on Box
	92.00			Box Regd 214
	84.90			Slew 15' NE
	85.60			
	96.20			BM E/100.95
	97.10			Com Post Sta
	92.80			16+53
				V 100.90

Sta	A	B	C	D	E
17+70			^{25 E} 74.10		65.00
18+00			66.30		65.00
18+15					66.60
18+60			66.90		67.70
19+00			74.50		79.15
20+00			84.85		88.00
21+00	²⁰ 90.10			2 F	93.30
22+00	93.20			4 F	94.55
23+00	93.50			4 F	95.40
24+00	93.50			5 F	93.45
24+76					7 LE 88.70
25+00	89.40			6 F	91.30
26+00	92.30			6 F	93.30
27+00	94.60	⁶ 96.00	⁴ 94.30	6 F	94.20
28+00	89.00			8 F	88.10
28+45	²⁵ 80.00			13	79.50
29+00	87.25			9 F	85.90
30+00			²⁰ 93.45	8 F	94.12
31+00	²⁰ 91.80			9 F	92.10
32+00		²⁰ 88.60		10 F	92.10
33+00	²⁰ 88.65			11 F	89.40
34+00	²⁰ 87.10			11 F	89.20
35+00	²⁰ 88.20			13 F	87.40
36+00	^{20 F} 86.90	^{13 F} 86.20	⁷ 83.90	4 F	87.20
37+00	82.05	^{12 F} 82.40	⁵ 80.15	3	84.35
					80.74
					80.75

F	G	H	I	B.M.
	^{25 M} 69.00			
	68.70			
	69.58			Culvt Paqd About 12' Spall.
	81.40			
	89.00			
⁷ 95.20	¹⁴ 95.10	21	237	BMEI. 95.25
² 94.70	⁶ 94.90	²⁰ 94.60		W. Headen
⁵ 96.00	¹⁷ 94.80	^{21 F} 95.20	237	Culvt. 6+2
⁶ 93.50	¹⁶ 92.50	^{21 F} 96.90		21+00
^{11 TOP} 90.00	^{17 TOP} 88.10	^{17 F} 94.50		95.25 ✓
⁷ 92.00	¹¹ 91.10	^{20 F} 89.00		
⁵ 93.30	¹⁵ 92.70	^{20 F} 91.60		
⁴ 94.20	¹⁴ 93.80	^{20 F} 94.20		
⁶ 89.30	¹⁶ 88.30	^{20 F} 97.30		
¹⁰ 89.00	¹⁷ 87.10	^{20 F} 88.80		
⁵ 89.60	¹⁵ 87.70	^{20 F} 85.50		
³ 92.70	¹⁴ 92.00	^{18 F} 87.55		
¹⁰ 91.60	¹⁰ 91.80	¹⁴ 94.30	²⁰ 94.20	
⁹ 90.00	¹² 89.60	^{17 F} 90.70	^{18 F} 91.50	
¹² 89.00	¹² 87.90	^{17 F} 90.20	²⁰ 90.70	
¹² 87.60	¹³ 87.00	^{17 F} 89.00	²⁰ 89.00	
⁵ 87.20	¹¹ 86.10	^{17 F} 88.10	²⁰ 87.90	BMEI. 92.72:
⁴ 84.60	¹¹ 85.70	^{15 F} 87.30	²⁰ 87.30	N. Gate Post
⁴ 80.82	¹¹ 79.44	¹⁶ 86.45	²⁰ 87.00	5+35+00
		¹⁶ 82.44	²⁰ 83.42	92.35 ✓

76

Sta

	A	B	C	D	E
38+00	77.97 ²⁰	70.46 ¹²	76.19 ⁶	76.94 ⁴	77.02
39+00	75.10 ²⁰	75.40 ¹⁴	72.95 ⁸	73.27 ⁴	73.5
40+00	71.46 ²⁰	70.65 ¹⁴	68.60 ⁹	70.00 ²	70.07
41+93	20			63.50 ¹¹	67.23
42+00	66.10 ²⁰	61.10 ¹⁵	62.30 ¹¹	67.60 ⁴	67.35
42+00	66.80 ²⁰	66.10 ¹⁴	65.30 ¹⁰	66.90 ⁶	66.80
43+00	70.00 ²⁰	67.40 ¹⁶	65.30 ¹¹	65.90 ⁵	68.98
44+00	72.05 ²⁰	71.40 ¹⁵	70.30 ¹⁰	71.50 ⁵	71.50
45+00	70.00 ²⁰	70.75 ¹⁴	69.60 ⁹	70.70 ⁶	70.90
46+00	70.50 ²⁰	70.40 ¹⁴	69.55 ¹⁵	70.20 ⁶	70.40
47+00	67.00 ²⁰	67.20 ¹⁵	67.50 ¹⁰	67.90 ⁶	67.9
48+00	68.60 ²⁰	68.20 ¹⁶	66.40 ⁹	67.10 ⁵	67.20
49+00	66.80 ²⁰	66.90 ¹⁶	65.40 ¹¹	64.90 ⁵	64.30
50+00	62.60 ²⁰	62.20 ¹⁵	60.40 ¹⁰	61.70 ⁵	61.70
51+00	57.90 ²⁰	57.40 ¹⁵	56.30 ¹¹	57.30 ⁶	59.3
52+00	57.50 ²⁰	57.10 ¹⁶	56.50 ¹¹	56.20 ⁶	56.3
53+00	53.70 ²⁰	53.80 ¹⁶	52.60 ¹¹	53.30 ⁶	53.00
54+00	51.60 ²⁰	51.40 ¹⁶	50.20 ¹⁰	50.90 ⁶	50.8
55+00	47.70 ²⁰	47.50 ¹⁶	48.00 ¹⁰	48.70 ⁵	48.30
56+00	46.70 ²⁰	46.80 ¹⁷	46.30 ¹⁰	46.30 ⁵	46.10
57+00	45.20 ²⁰	45.10 ¹⁷	45.10 ¹⁰	45.20 ⁵	45.2
58+00	44.80 ²⁰	44.70 ¹⁷	43.20 ¹⁰	44.20 ⁵	44.80
59+00	43.90 ²⁰	43.70 ¹⁷	43.30 ¹⁰		43.40
60+10	42.60 ²⁰	42.40 ¹⁷	41.30 ¹⁰	43.30	43.60
			39.90		43.90

77

F	G	H	I	B M
76.80 ⁷	76.12 ¹⁰	77.95 ¹⁵	78.50 ²⁰	
73.42 ⁵	72.60 ¹⁰	75.22 ¹⁶	75.80 ²⁰	0.81.15
69.65 ⁴	68.20 ¹⁰	67.90 ¹⁵	71.80 ²⁰	
64.30 ⁵	63.29 ¹⁰	63.50 ¹⁵		
67.40 ⁴	63.50 ¹⁰	67.90 ¹⁵	65.10 ²⁰	
66.20 ⁵	65.30 ¹⁰	67.20 ¹⁵	65.00 ²⁰	
69.10 ⁴	67.70 ¹⁰	70.20 ¹⁵	70.20 ²⁰	
71.10 ⁵	70.20 ¹⁰	71.20 ¹⁵	71.20 ²⁰	0.71.65
70.60 ⁴	69.00 ¹⁰	69.70 ¹⁵	69.30 ²⁰	
70.00 ⁵	67.10 ¹⁰	67.30 ¹⁵	67.10 ²⁰	
68.40 ⁴	67.80 ¹⁰	68.90 ¹⁵	68.80 ²⁰	
67.40 ⁵	66.30 ¹⁰	67.50 ¹⁵	67.10 ²⁰	
67.20 ⁴	63.90 ¹⁰	65.70 ¹⁵	65.20 ²⁰	
61.90 ⁵	60.20 ¹⁰	62.20 ¹⁵	62.10 ²⁰	
57.20 ⁴	56.60 ¹⁰	60.40 ¹⁵	60.10 ²⁰	
56.10 ⁵	55.10 ¹⁰	56.20 ¹⁵	56.90 ²⁰	5.60
53.30 ⁴	52.40 ¹⁰	52.60 ¹⁵	53.10 ²⁰	0.60.82
50.50 ⁵	50.10 ¹⁰	51.90 ¹⁵	50.60 ²⁰	
48.40 ⁴	47.50 ¹⁰	48.40 ¹⁵	48.00 ²⁰	0.49.80
46.70 ⁵	46.00 ¹⁰	46.50 ¹⁵	46.00 ²⁰	
45.00 ⁴	44.20 ¹⁰	44.60 ¹⁵	45.60 ²⁰	
43.00 ⁵	42.50 ¹⁰	42.85 ¹⁵	44.60 ²⁰	S.E. E. Hill
43.39 ⁴	42.20 ¹⁰	42.70 ¹⁵	42.70 ²⁰	60+10.5.29
40.00 ⁵	39.70 ¹⁰	42.40 ¹⁵	42.10 ²⁰	
	38.60	38.80		

Sta	A	B	C	D	E
60+35	41.80	42.10	42.00	42.40	43.60
61+01	41.80	42.40	40.70	41.90	42.20
62+10	40.80	42.10	41.30	42.20	42.60
63+00	40.80	41.90	42.00	44.80	45.50
63+38		42.30	"	"	45.50
63+71	40.20	40.30	41.00	44.40	45.00
64+00	42.20	42.10	42.20	44.80	44.50
65+00	45.80	45.60	"	45.40	45.10
66+10	51.50	51.60	48.00	48.70	48.80
67+00	50.00	50.30	50.00	51.30	51.30
67+00	50.50	50.60	50.30	51.20	51.20
69+00	57.20	57.50	57.00	52.20	52.50
70+00	52.00	52.10	49.00	50.30	51.00
71+00	48.70	48.50	48.00	49.50	49.20
71+30	47.90	48.10	48.20	49.20	50.70
71+42	Bed	45.00	"	"	50.20
71+51	46.70	47.10	48.00	50.40	50.80
72+00	48.30	47.50	47.00	50.40	51.00
73+00	52.50	52.50	52.50	52.30	52.10
74+00	56.80	56.70	55.30	55.00	55.90
75+00	61.40	61.50	59.00	59.50	60.10
76+00	66.40	66.40	63.50	64.30	64.60
77+00	66.80	66.70	66.70	66.80	66.80
78+00	66.60	66.60	66.00	66.80	67.00

					79
F	G	H	I	B.M.	
42.20	41.40	42.50	42.00		
42.00	40.80	42.00	42.00	0 49.15	
42.00	41.80	42.50	42.00	Bridge	
45.20	45.00	45.00	43.10	63.15	
45.65		Red	42.40		
45.40	41.70		40.70		
44.75	41.90		41.50		
44.90	43.90	44.00	43.30		
47.00	47.10	48.30	47.20		
57.00	55.45	57.00	57.20		
57.00	55.10	57.50	57.80		
57.30	57.40	57.20	57.30		
57.20	57.60	57.10	57.20		
57.80	58.15	57.10	56.90	91.42	
57.40	47.10	46.30	45.95	B.M. 54.10	
57.50				50.31	
57.10	57.10	47.20	47.20		
50.00	49.00	49.00	47.40		
57.20	57.50	57.80	57.30	0 60.90	
57.00	57.10	56.70	56.80		
57.90	57.00	61.30	61.30		
61.30	61.40	61.50	61.50		
61.70	61.70	62.20	62.00		
61.70	65.70	66.30	66.30		

Sta	A	B	C	D	E
101+00	72.30	73.40	72.00	73.00	74.00
102+00	71.80	71.50	71.50	72.10	73.00
103+00	73.00	73.00	73.00	74.00	74.60
104+00	73.50	75.50	74.70	75.50	76.00
105+00	76.00	77.20	76.80	77.50	78.00
106+00	77.10	77.50	77.90	78.00	78.8
107+00	78.40	78.40	80.00	81.00	81.90
108+00	83.40	83.60	82.80	83.60	84.00
109+00	86.10	86.10	89.90	89.80	86.00
110+00	87.10	87.10	88.30	89.20	89.20
111+00	91.20	91.20	91.00	91.90	91.90
112+00	91.20	91.20	90.20	90.90	91.20
113+00	89.50	89.20	89.90	89.10	89.20
114+00		84.50	83.80	83.60	85.20
114+53		82.30	9 Bottom	84.20	85.10
115+00	84.60	84.10	83.10	84.90	85.30
116+00	85.20	84.00	85.60		85.90
117+00	84.80	84.80	84.60	86.00	86.34
118+00		86.20	86.20	86.50	88.50
119+00	92.50	92.60	92.00	93.00	92.50
120+00	100.150	100.20	98.00	98.70	98.90
121+00	97.00	95.20	96.20	97.20	97.20
122+00	93.50	93.40	92.00	93.20	93.30
123+00	90.60	90.60	89.70	90.70	91.00

					83
F	G	H	I	B.M.	
74.00	73.30	74.00	74.50		
73.90	72.50	72.50	71.60		
74.00	73.20	73.20	73.50		
74.00	75.00	75.00	75.00		
74.00	76.00	76.00	77.50		073.90
74.00	77.00	77.00	78.50		
74.00	80.00	80.00	81.00		
83.00	83.00	85.00	83.70		
86.00	86.00	86.00	85.70		
88.00	89.00	89.00	90.90		
91.00	91.00	92.00	92.80		084.96
94.00	90.20	91.40	91.90		
97.20	86.00	86.70	86.90		
85.10	85.00	84.50	84.30		78.90
	Bottom	81.70	Top	82.40	Culvert
85.00	84.30	83.70	83.40		Cement Post
84.70	84.60	84.60	84.00		117+17-89.45
86.00	84.70	84.50	84.50		
88.20	86.30	86.70	85.70		
92.50	91.00	91.30	92.50		51.97
92.35	91.80	99.60	104.00		
97.10	96.00	99.90	98.70		
93.10	94.20	91.70	91.30		
90.60	88.90	89.00	88.00		

84

Sta

	A	B	C	D	E
123+90	87.00	87.00	87.00	87.00	87.00
124+00	88.50	88.50	88.50	88.50	88.50
125+00	89.50	89.50	89.50	89.50	89.50
126+00	91.60	91.60	91.60	91.60	91.60
127+00	92.50	92.50	92.50	92.50	92.50
128+00	97.25	97.25	97.25	97.25	97.25
129+00	96.40	96.40	96.40	96.40	96.40
130+00	92.50	92.50	92.50	92.50	92.50
130+58	88.50	88.50	88.50	88.50	88.50

E

85

F G H I B.M.

	F	G	H	I	B.M.
Bottom	85.00	85.00	85.00	85.00	85.00
Top	89.00	89.00	89.00	89.00	89.00
10	87.10	87.10	87.10	87.10	87.10
15	92.10	92.10	92.10	92.10	92.10
20	96.00	96.00	96.00	96.00	96.00
25	94.40	94.40	94.40	94.40	94.40
30	94.40	94.40	94.40	94.40	94.40
35	91.70	91.70	91.70	91.70	91.70
40	90.30	90.30	90.30	90.30	90.30
				91.50	100' East
				85.50	100' North
				91.60	Rm N. End
					North Header

86	E. St.	2' W	2' E	W.
Sta	E. St	W. St	Stake	
0+00	110.09	109.70	109.42	110.00
1+00	110.25	109.90	109.70	109.85
2+00	110.56	110.15	109.96	110.52
3+00	111.95	111.31	111.36	111.86
4+00	112.80	112.70	112.46	112.65
5+00	112.48	112.27	112.45	112.63
6+00	112.56	112.23	112.19	112.35
7+00	111.58	111.36	111.66	111.82
8+00	112.30	← SE		112.30
8+20	112.22	← HE		SW
9+00	111.72	111.42		Wing
10+00	113.62	113.83		
11+00	114.39	113.81		
12+00	114.35	113.88		
13+00	114.34	114.15		
14+00	115.05	114.68		
15+00	115.90	115.30		
16+00	116.73	116.16		
17+00	117.42	117.15		
18+00	118.43	118.12		
19+00	116.85	116.65		
20+00	116.29	116.40		
21+00	117.25	117.10		
22+00	118.54	117.98		
23+00	118.37	118.29		
24+00	119.00	118.42		

Flinn Road

87

7L Culvert
E. end
108.32

7L Culvert
W. end
108.00

BM No. 1

110.00

BM No. 2

114.30

Bed Stream 8+10

107.50

BM No. 3

122.40

Ditch
Levels

Sta	E. Stake	2' W E Stake
25+00	119.25	119.00
26+00	120.00	119.85
27+00	120.61	120.36
28+00	120.45	120.40
29+00	120.06	120.25
30+00	120.07	119.97
31+00	120.17	119.61
32+00	119.21	119.20
33+00	119.89	119.58
34+00	120.58	120.45
35+00	121.59	121.25
36+00	123.05	122.63
37+00	123.10	123.04
38+00	123.83	123.83
39+00	124.25	124.25
40+00	125.52	125.16
41+00	125.23	124.93
42+00	124.61	124.47
43+00	125.21	124.75
44+00	124.89	124.35
45+00	125.40	124.19
46+00	124.37	124.02
47+00	128.26	128.17
48+00	125.20	125.18
49+00	125.70	124.20
50+00	125.50	124.80

89

BM No. 5
130.24

BM No. 6

128.92

125.25

122.56

FL. Staff - 121.50

119.75

90 Sta	E. Stake	2' N. E. Stake	2' E. W. Stake	W Stake
51+00	125.11	124.46		
52+00	125.22	124.53		
53+00	125.22	124.71		
54+00	124.98	124.81		
55+00	126.76	126.51		
56+00	128.48	127.66		
57+00	128.22	127.70	127.96	128.12
58+00	128.23	131.57	131.29	131.60
59+00	132.04	131.76	131.39	131.25
60+00	131.77	131.56	131.15	131.75
61+00	131.20	131.60	130.80	131.36
62+00	130.45	130.25	130.52	130.85
63+00	131.11	131.65	130.86	131.34
64+00	131.93	131.56	131.13	131.51
65+00	131.60	131.31	131.22	131.56

~~125.31~~

~~122.10~~

91

B.M. No. 7

137.18

Sta 56+15 end 8"
tile W. side FL 124.52

B.M. No. 8

133.19

	1.60	Conet	Grade	
0+00	108.93	108.32	108.33	+0.01
0+50	109.13	108.40	108.50	+0.10
1+00	109.23	108.49	108.63	+0.14
1+50	109.28	108.56	108.68	+0.12
2+00	109.28	108.66	108.68	+0.03
2+50	109.30	108.73	108.70	
3+00	109.40	108.83	108.80	-0.03
3+50	109.52	109.17	108.92	-0.26
4+00	110.09	109.50	109.49	-0.01
4+50	110.04	109.37	109.44	+0.07
5+00	109.97	109.25	109.37	+0.12
5+50	109.84	109.13	109.24	+0.11
6+00	109.56	109.00	108.96	-0.04
6+50	109.28	108.75	108.68	-0.07
7+00	109.15	108.50	108.55	+0.05
7+50	108.90	108.25	108.30	+0.05
8+00	108.17	108.00	—	Ext. Data
9	110.03	109.00	109.20	+0.20
9+50	110.23	109.33	109.40	+0.07
10	110.58	109.67	109.75	+0.08
10+50	110.91	110.00	110.08	+0.08
11	111.25	110.33	110.42	+0.09
11+50	111.66	110.67	110.83	+0.16
12	111.97	111.00	111.14	+0.14
12+50	112.15	111.21	111.32	+0.11
13+00	112.37	111.42	111.54	+0.12
13+50	112.39	111.63	111.79	+0.10

		+0.13	+0.11	+0.05	93
14+00	112.56	111.83			+111.96
14+50	112.75	112.04			+111.15
15+00	112.92	112.25			+111.30

7+50	108.75	108.25	108.15
7+00	109.15	108.50	108.35
6+50	109.42	108.75	108.82
6+00	109.69	109.00	109.09
5+50	109.83	109.13	109.23
5+00	109.93	109.25	109.33
4+50	110.03	109.38	109.43
4+00	110.10	109.50	109.50
3+50	109.66	109.16	109.06
3+00	109.28	108.83	108.68
2+50	109.18	108.75	108.58
2+00	108.88	108.66	108.22
1+50	108.66	108.56	108.06
1+00	108.31	108.49	107.71
0+50	107.95	108.41	107.35
0+20	107.76		
0+00		108.32	

94

Bailey Road

Levels	for tile from			
Running Sta	Stake	NW to Ground	to Sta 7+70	4's
0+00	119.69			
1+00	120.02	119.95		
2+00	120.25	120.08		
3+00	121.40	121.16		
4+00	123.03	122.85		
5+00	124.21	124.16		
6+00	123.62	123.49		
7+00	123.66	123.58		
8+00	124.24	124.16		
9+00	124.94	124.89		
10+00	125.17	125.11		
11+00	125.10	125.35		
7+9	17.57	2'S	217.55	5.57
7+50				2'S
6+73	125.54	125.00	125.32	125.47
6+00	125.70	125.12	125.47	125.55
5+00	127.14	126.30	126.42	126.62
4+00	128.29	127.58	127.19	127.55
3+00	127.00	126.67	126.50	126.82
2+00	126.48	126.05	125.90	126.40
1+00	125.72	125.32	125.44	125.57
0+15				125.19

119.43
 11
 95
 BM
 on Bailey Road Hub Stake
 E. side Sta 34+00
 120.58
 176.38 7L 12" Tile
 Flinn Road Sta 32+70

BM No 1
 130.23

118.33 7L 12" Tile W
 side Flinn Road. Sta
 0+15 S. side Bailey Road

96	W				
sta	sta	2'E			
8+24	12530	12513			
9+00	12554	12544			
10+00	12585	12599			
11+00	12636	12638			
12+00	12656	12656			
13+00	12683	12680	EST	2'W	
13+75	12718	12704	12709	12693	

18+20	131.02	Stake at W. Bdry		
	130.69	" " E "		
	129.33	Stake Sta 1+00		
	127.73	" Sta 1+10		
	126.86	RR side ditch		
		or Flow line tile		

	EST	2'W	2'E W	W ST.
20+40	130.70		ST.	
21+00			131.61	131.61
		131.29	131.50	131.32
22+00	130.68	129.96	129.95	130.12
23+00	129.05	128.90	129.40	129.36
24+00	130.36	130.32	129.40	129.49
25+00	129.70	129.78	129.66	129.98
26+00	131.15	131.26	130.54	130.57
27+00	130.64	130.86	130.56	130.70
28+00	131.67	131.88	132.13	132.51

B.M. No 3
Bailey Road
129.90

B.M. No 4
132.05

B.M. No 5.

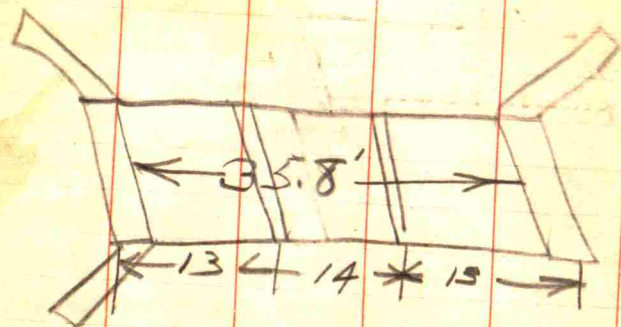
	EST	2'W	2'E W	W ST.
29+00	131.72	132.18	132.03	132.38
30+00	130.80	131.10	130.56	130.90
31+00	130.11	130.31	130.12	130.41
32+00	129.00	129.19	128.39	128.89

98

Stake	W. side	Ground
0+0		415
23+00	129.36	
0+20	129.05	12880
1+00	128.33	12820
2+00	128.26	12819
3+00	126.35	12641
3+50	128.32	12860
3+75	125.55	12555
4+25		10500

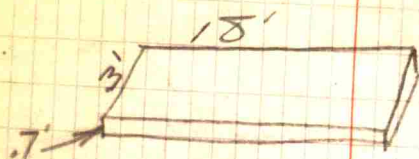
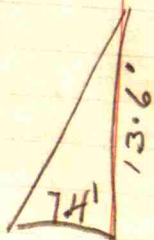
99

Downland Road Bn



Clear span 35.8'
 overall length 40.0'
 Max. width 13.6'
 outside channels to be reset.

5 lines Is 2-2" cc
 2 Floor Beams 5 as shown
 Hand Rails 1 1/2 x 4" channels
 No. change



102 Crit Clay Bridge

Sta

Shank
S. Line
Center

0+00					89.73
0+08	²⁵ 91.20	¹⁶ 92.75	¹² 93.33	⁶ 96.10	96.36
1+00	²⁶ 93.24		¹⁵ 95.00	⁷ 97.36	97.52
2+00	²⁵ ←	¹⁴ 107.74	⁹ 104.02	⁵ 103.97	104.63
2+65	²⁵ 107.60		¹⁴ 107.60	⁶ 107.30	107.75
3+00	107.50	¹⁴ 106.90	¹⁰ 104.66	⁶ 104.60	105.25
West				<u>3+00</u>	E. 98.35
0+06	²⁵ 93.00	¹⁷ 93.16	¹¹ 93.88	⁶ 96.50	96.60
1+00	²⁵ 95.90	²⁰ 96.10	¹⁴ 96.15	⁷ 97.70	98.09
2+00	²⁰ 107.00	¹³ 102.75	⁸ 98.90	⁶ 99.83	100.20
2+85	←		¹³ 94.40	¹¹ 100.00	100.20

BM. E. 100.00
12" Round post 15' S. E
Shank 100' W. of Culvert

103

⁶ 96.02	¹³ 93.65		
97.50	¹⁵ 97.05		
⁶ 103.90	¹⁰ 103.70	¹⁷ 96.23	²⁵ 96.70
⁷ 107.20	¹⁵ 107.60		
104.40	¹³ 103.37	¹⁶ 109.50	²⁵ 108.00
			²⁵ 107.75
⁶ 96.30	¹³ 92.85	¹⁹ 93.08	²⁵ 93.10
⁷ 97.95	¹⁰ 95.75	²⁰ 94.45	²⁵ 94.14
¹¹ 99.55	¹¹ 97.65	¹⁵ 97.75	²⁵ 96.61
¹¹ 100.00	¹³ 94.60		

30' to stream
120' to Sta

19+00	114.34	11370	11374
19+50	114.55	11380	113.95
20+00	114.62	11390	114.02
20+50	114.72	11400	114.12
21+00	114.76	11410	114.16
21+50	114.82	11420	114.22
22+00	114.93	11430	114.33
22+50	115.02	11440	114.42
23+00	115.29	11450	114.69
23+50	115.37	11460	114.77
24+00	115.41	11471	114.81
+25.	115.41	11476	114.81
+50	115.41	11481	114.81
+75	115.50	11486	114.90
25+00	115.50	11492	114.90
25+25	115.55	11497	114.95
25+50	115.69	115.02	115.09
25+75	116.05	115.07	
26+00	115.49	115.13	
26+25	115.69	115.18	
26+50	115.89	115.23	
26+75	116.07	115.28	
27+00	116.10	115.33	
27+25	115.88	115.38	
27+50	115.96	115.42	

Flinn Road
Levels

8	15	11310	112.25-112.27	✓
8	15+50	11332	112.46	112.49 ✓
8	16+00	11365	112.66	112.62 ✓
8	16+50	11377	112.87	112.94 ✓
6	17+00	113.77	113.08	113.17 ✓
6	17+50	113.23	113.29	113.23 ✓
6	18+00	113.50	113.50	113.50 ✓
6	18+50	114.14	113.60	113.54 ✓

106

Levels for Clay

Sta	State	Ground 4' S
0+00		
1+00	124.24	124.16
2+00	125.36	125.21
3+00	126.02	125.88
4+00	125.64	125.43
5+00	125.63	125.43
6+00	125.96	125.77
7+00	125.98	125.89
8+00	126.87	126.84
9+00	129.61	129.45
10+00	129.68	129.52
11+00	129.10	128.91
12+00	128.43	128.39
13+00	127.83	127.72
14+00	127.95	127.80
15+00	129.06	128.92
16+00	128.46	128.41
17+00	128.72	128.11
18+00	128.41	128.30
19+00	129.15	129.03
20+00	130.00	129.93
21+00	129.92	129.79
22+00	129.50	129.37

126.88 Low

128.02 100'

126.50 Low

107

Place on Ground 12+50

M. Sta 17+00

place 20' S. Sta 16+50

110
level on Flum Feb 7/23-21 Johnson

Sta.	26+6	stake	Elev. Tile -	stake
26	115.73	120.03	116.00	
27	115.93	120.61	116.38	
28	116.13	120.15	116.40	
29	116.34	120.06	116.53	116.53
30	116.55	120.07	116.55	119.3
31	116.76	120.17	116.74	
32	116.97	119.21	117.17	
33	117.18	119.89	117.34	119.15 slope stake
34	117.39	120.58	117.54	
35	117.60	121.59	117.66	
36	118.27	123.05	118.40	123.06
37	118.93	123.10	118.52	11
38	119.60	123.83	119.15	123.81
39	119.85	124.75		
40	120.10	125.57		

26+50	-116.40
27+50	-116.40
28+50	-116.35
29+50	-116.60
30+50	-116.62

OK. to Sta. 35 but lake out ~~three~~ inches fall from 26+50 to 28+50-

J. Johnson - 9-23-21

Top tile
37+50 - 119.50

112

Back on Fleun Rd. 700

Flo.	Grade +0	Stake	Clear Pd	Stake Clear Pd
35				
36				
37				
38	107.16			
39	106.63	227		
40	<u>1.53</u>	22		

106.56
106.80
107.56

333 76

334 176.00
608

107.37
54
106.63

100228
50
11400

226
9220
9065
2520

100228
37
9147
65
0775

9/00

113

10680 0+00
714

106914 0+50 ✓
114

107.028 1+00 L
114

107.142 1+50 L
114

107.256 2+00 L
114

107.370 2+50
114

107.484 3+00
077

107561 3+34

114 John Buckert Tile Drain

Sta.	El. Stake	El. ground
B.M.	10.00 tile	
0+00	14.50	14.65
1+00	15.60	15.05
2+00	17.60	17.15
3+00	18.00	17.60
4+00	18.24	17.83
5+00	16.40	16.03
6+00	16.20	15.80
7+00	16.10	15.75
8+00		
9+00	15.70	15.10
10+00	16.80	15.90

Sta.	Stake	Ground	Tile
8+24 or 0+30	12580	(121.12)	12+00 12805 127.96
1+00	12506	12500	13+00 127.90 127.75
2+00	12608	12600	14+00 12842 128.35
3+00	12619	12665	15+00 127.70 128.06
4+00	12641	12632	16+00 12815 128.00
5+00	12668	12660	17+00 12844 128.30
6+00	12663	126.53	18+00 128.68 128.50
7+00	12755	12746	19+00 13075 130.50
8+00	12869	12865	
9+00	12760	12743	
10+00	12795	12786	
11+00	12526	128.18	

9/27-21 J.P.G.

115

Top of 4" tile near red post. In outlet.

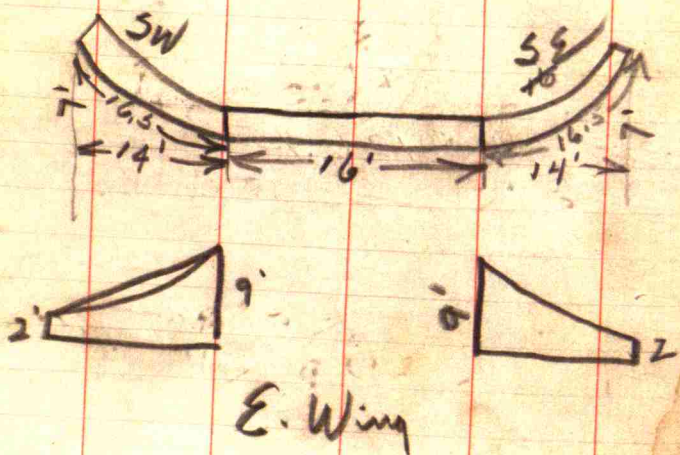
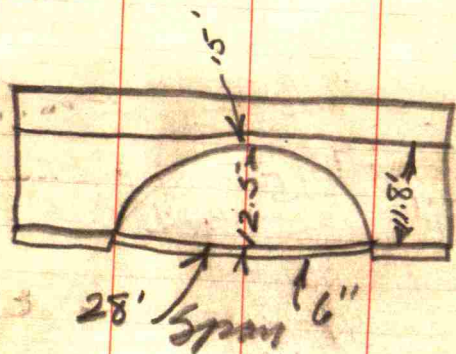
35' E into pond.
 E. Edge of pond
 7+65 - water level in pond = 15.20
 stake 8 in 1.88 ft. of water
 no reading taken directly on Sta. 8+00

Bot Pond 126.45

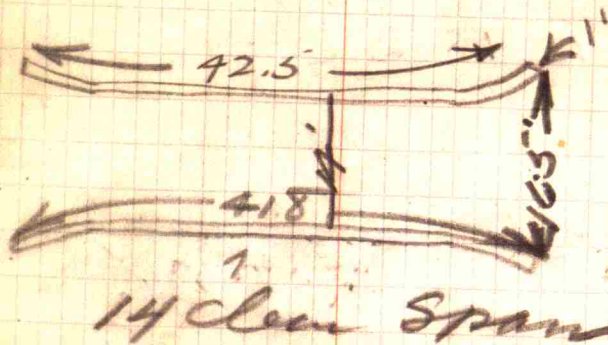
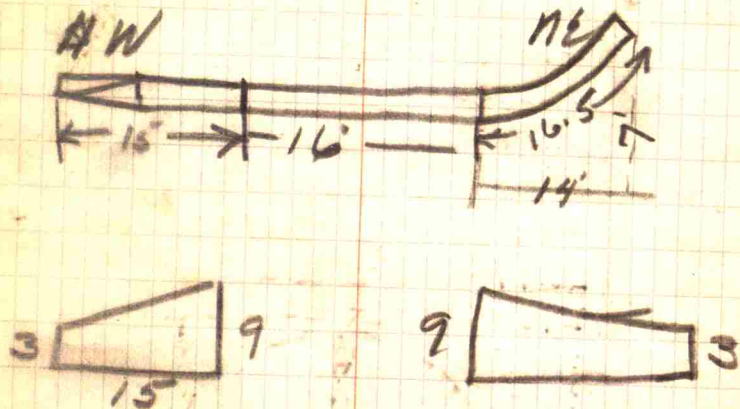
122.28
 60
 121.68

116

White Bridge Center



117



Stream face of wings
potted 1" to foot.

118
Sta

Additional Tile
Bailey Road

Grade St.	Top 5" Tile at 100
0+00	127.20
0+25	127.18
0+40	127.26
0+70	127.44
0+85	127.31
1+00	127.41
1+50	128.77
2+00	129.62
2+50	130.15
3+00	130.54
3+50	
4+00	130.67

124.06
0.60

123.46

BM
No 3
NE cor
chuck
step
El.
129.92

131.20
131.20

119

Tile from 13+75 to

123.46	3.74	127.64.9
123.65	3.53	
123.76	3.50	
123.99	3.45	
124.11	3.20	
124.21	3.20	
124.58	4.19	
124.96	4.66	
125.33	4.82	
125.71	4.83	
126.46	4.21	

75
4
35

750
30
325

19.

75
15
375
1125

124.96

37

12533

123.46
75

124.21
75

124.96
75

125.71
75

126.46

120

Miller Road Ditch Levels

Sta	A	B	C	D
0+0.0	100			99.07
	<small>FL. N 98.2%</small>	<small>F.L.S.</small>		
0+50	10230	101.05	101.75	101.62
1+00	104.08	102.80	101.96	103.45
2+00	104.63	104.10	104.46	103.91
3+00	103.51	102.81	103.87	103.07
4+00	103.55	102.94	103.67	103.16
5+00	103.73	103.34	103.75	103.67
6+00	104.00	103.17	103.98	104.10
7+00	104.80	104.15	104.58	104.13
8+00	104.42	104.38	104.50	104.22
9+00	104.76	104.34	104.77	104.76
10+00	105.14	105.35	105.32	105.52
11+00	104.13	104.48	104.52	105.19
11+17	<small>FL. E 102.34</small>	<small>FL. W 103.25</small>	<small>FL. W 103.79</small>	<small>FL. W 102.19</small>
12+00	103.73	103.89	104.41	104.40
13+00	104.66	104.57	104.45	104.84
14+00	104.99	104.95	105.01	104.97
15+00	105.98	105.31	105.13	105.65
16+00	106.85	106.17	105.87	106.25
17+00	106.85	106.61	106.32	106.87
18+00	107.37	106.47	106.93	107.24
19+00	107.65	106.87	107.02	107.70
20+00	107.12	106.79	106.70	107.18

121

July 31. Aug.

Clear & Hot

K.T. Sollust, Farmer

C.O. Gossett, Levelman

B.M. E.A. 100.00

S. Head, Tree
Culvert

B.M. E. 103.72

18' W. I.B. Sta. 131.32

122

Sta	A ²	B	C	D ³
21+00	106.29	105.13	105.45	106.71
22+00	105.04	104.13	104.77	105.29
23+52	<small>FL 102.34</small>	<small>TOP 103.13</small>	<small>FL 103.10</small>	<small>FL 102.12</small>
23+00	106.55	103.93	105.25	105.61
24+00	109.15	107.04	108.26	108.66
25+00	109.70	109.00	108.63	108.97
26+00	110.04	109.81	109.37	109.85
27+00	110.56	110.38	110.22	111.15
28+00	111.53	111.20	110.53	112.17
29+00	112.07	112.17	111.97	112.82
30+00	111.52	112.21	110.94	112.14
31+00	111.04	111.98	110.82	111.54
32+00	111.08	111.91	110.79	111.87
33+00	112.82	112.68	111.10	113.10
34+00	111.91	111.60	110.72	112.53
35+00	110.16	109.85	109.30	110.73
35+97	<small>TOP 107.55</small>	105.94	<small>FL 106.00</small>	<small>TOP 107.80</small>
36+00	106.95	109.24	107.21	108.80
37+00	109.00	109.54	108.40	109.25
38+00	108.85	109.80	108.51	109.04
39+00	109.65	110.07	108.73	110.13
40+00	110.90	110.56	110.10	110.73
41+00	112.01	111.87	111.92	111.87
42+00	111.41	106.58	107.87	106.95
43+00	103.22	103.10	103.04	102.74

112.45

123

EL. 112.40 BM. Bottom step
N. flight church
steps.

124

	Station	Point	Point	Station	
	A ^E	B	C	D ^W	
43+41		97.75			
44+00	101.49	103.25	101.65	102.12	
45+00	103.21	103.93	102.60	103.95	
46+00	108.40	107.00	106.88	108.52	109.00
47+00	114.85	113.54	114.27	115.55	106.00
48+00	116.18 ²⁵	116.59	116.67	117.63	108.00
49+00	115.24	115.41	115.04	115.95	110.00
49+79		115.20	115.30		110.90
50+00	113.95	115.21	113.79	114.70	111.20
51+00	115.30	117.43	114.72	116.24	112.40
52+00	118.51	116.60	116.85	118.43	113.60
53+00	118.97	118.84	118.29	119.37	114.80
54+00	121.15	119.91	119.61	120.47	116.00

Stone
120.91

127

<u>108.40</u> →		Top W. Sta 45+60 103.59
Top W. 645+80	Can Rd at Bridge	
104.19	106.25	
SE 1'	Can Rd	St. W 1'
107.59	107.65	107.60
112.47	111.95	112.37
114.62	114.50	114.95
at St		at St
116.16	115.60	115.65
		114.19
114.20		114.92
116.12		116.40
118.70		118.58
119.15		119.50

7.4.49.78
w. side
111.46

128

BM
 A50-00
 A150-00
 A250-00

Stream

Sta	Stake	Tire
23	100	9924
24	10259	9890
25	10314	9959
26	10349	10110
27	10403	10163
28	10498	10250
29	10551	10314
30	10495	10284
31	10448	10252
32	10449	10240
33	10617	10192
34	10531	10125

129

134

Sta. 20+11.5

 $\Delta 81^{\circ} 22'$

Ext = 10.4'

$$D = \frac{18261}{10.4}$$

D = 1750

$$L = 100 \times \frac{81.35}{175} = 46.5$$

$$T = \frac{4925.7}{175} = 28.1$$

P.L. 19+834

Def = 52.5' per 77'

$$Def_{10'} = \frac{525}{60} = 8^{\circ} 45'$$

R = 3274

1003

15.27

$$\frac{2011.5}{28.1}$$

$$\frac{1983.4}{46.5}$$

2129.9

135

90

$$\frac{183.4}{6.4}$$

6.4

52.5

6.4

2100

$$\frac{3150}{60}$$

$$\frac{336.00}{300}$$

$$\frac{5^{\circ} 36'}{36}$$

.36'

5^o 36'8^o 45'
$$\frac{13^{\circ} 81' = 14^{\circ} 21'}{8^{\circ} 45'}$$

$$\frac{23^{\circ} 06' = 22^{\circ} 66'}{8^{\circ} 45'}$$
8^o 45'31^o 51'8^o 45'40^o 36'

140

$$\Delta 86^\circ 35'$$

$$T \frac{5398.1}{110} = 49.1$$

$$L = \frac{100 \times 86.58}{110} \quad \frac{8658}{11}$$

$$L = 78.7$$

$$D = 110^\circ$$

$$D 10' \text{ an} = 5^\circ 30' \quad 43^\circ 18'$$

$$\text{Def } 1' \text{ " } = 33'$$

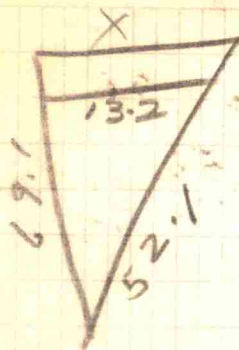
$$\begin{array}{r} 18 + 28.2 \\ 49.1 \end{array}$$

$$\begin{array}{r} 17 + 79.1 \end{array}$$

$$\begin{array}{r} 38.07 \\ 4 \\ \hline 60 \overline{) 152.28} \quad \angle 2^\circ \\ \underline{120} \\ 320 \end{array}$$

$$\begin{array}{r} 78.7 \\ 33 \\ \hline 2361 \\ \underline{2361} \\ 71 \\ \hline 60 \overline{) 2597} \quad \angle 43 \\ \underline{240} \\ 197 \\ \underline{180} \\ 17 \end{array}$$

$$\begin{array}{r} 11 \overline{) 865.8} \quad \angle 78.7 \\ \underline{77} \\ 95 \\ \underline{88} \\ 78 \end{array}$$



$$\begin{array}{r} 110 \overline{) 5398.1} \quad \angle 49.1 \\ \underline{440} \\ 998 \\ \underline{9} \end{array}$$

$$521 : 13.2 \times 69.1 : X$$

$$\frac{35}{60} = \frac{7}{12}$$

$$\begin{array}{r} 12 \overline{) 70} \quad \angle 583 \\ \underline{60} \\ 1006 \end{array}$$

$$\begin{array}{r} 1382 \\ 1973 \\ 691 \end{array}$$

$$\begin{array}{r} 1382 \\ 1973 \\ 691 \end{array}$$

$$\begin{array}{r} 1382 \\ 1973 \\ 691 \end{array}$$

$$\begin{array}{r} 902.12 \\ 521 \end{array}$$

$$\angle 17.3$$

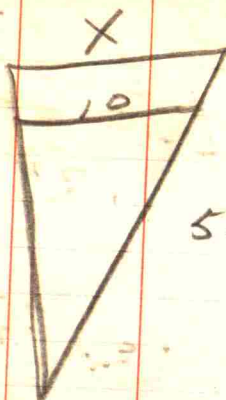
$$43 \ 18$$

$$\begin{array}{r} 60 \\ \hline 2580 \end{array}$$

$$330$$

$$\begin{array}{r} 902.12 \\ 521 \\ \hline 3811 \\ 3647 \\ \hline 1640 \end{array}$$

142



$$52.1 : 13.2 = 69.1 : X$$

$$\begin{array}{r} 13.2 \\ \times 69.1 \\ \hline 1382 \\ 1973 \\ 691 \\ \hline \end{array}$$

$$10 : 52.1 = X : 59.1 \quad \left(\frac{59.1 \times 10}{52.1} \right)$$

$$52.1$$

$$52.1 : 59.1 = 10 : X$$

$$\begin{array}{r} 52.1 \overline{) 59.1} \\ \underline{52.1} \\ 700 \\ \underline{521} \\ 1790 \\ \underline{1563} \\ 2270 \end{array}$$

$$52.1 : 10 : 69.1 : X$$

$$52.1 \overline{) 69.1} \quad \left(13.26 \right)$$

$$\begin{array}{r} 52.1 \overline{) 69.1} \\ \underline{52.1} \\ 1700 \\ \underline{1563} \\ 1370 \\ \underline{1042} \\ 3280 \end{array}$$

13.26

17.3

143

$$\begin{array}{r} 110 \overline{) 5730} \\ \underline{550} \\ 230 \\ \underline{220} \\ 10 \end{array}$$

$$5.21$$

$$1.34$$

$$\begin{array}{r} .134 \\ \times 3 \\ \hline .402 \end{array}$$

$$10 : 52.1 : X : 59.1$$

$$15.4 \quad 52.1 X = 59.1$$

$$5.21 \overline{) 59.1} \quad \left(11.34 \right)$$

$$\begin{array}{r} 5.21 \overline{) 59.1} \\ \underline{521} \\ 700 \\ \underline{521} \\ 1790 \\ \underline{1563} \\ 2270 \end{array}$$

$$\begin{array}{r} 4.72 \\ \times 3647 \\ \hline 4250 \end{array}$$

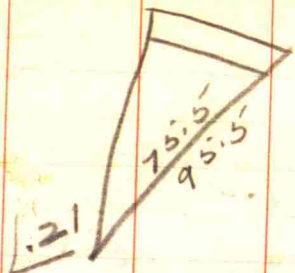
$$13.2 : 52.1 X 69.1$$

$$\begin{array}{r} 13.2 \\ \times 69.1 \\ \hline 1182 \\ 1673 \\ 591 \\ \hline \end{array}$$

$$52.1 \overline{) 77012} \quad \left(14.78 \right)$$

$$\begin{array}{r} 52.1 \overline{) 77012} \\ \underline{521} \\ 2491 \\ \underline{2084} \\ 4072 \end{array}$$

144



19.76

$$\begin{array}{r} 25 \overline{) 5.24} \\ \underline{50} \\ 24 \end{array}$$

$$25 : 95.5 = x = 75.5$$

$$95.5x = 75.5 \times 25$$

$$\begin{array}{r} 75.5 \times 25 \\ \underline{95.5} \\ 19.1 \end{array}$$

19.1

$$\begin{array}{r} 191 \overline{) 3775} \\ \underline{191} \\ 1865 \end{array}$$

1865

1719

1469

1339

1230



$$\begin{array}{r} 17.6 \\ .21 \\ \hline 176 \\ 352 \\ \hline 3.696 \end{array}$$

$$\begin{array}{r} 25 \overline{) 3.7} \\ \underline{21} \\ 37 \end{array}$$

$$\begin{array}{r} 17.6 \\ 13.9 \\ \hline 13.9 \end{array}$$

145

$$\begin{array}{r} 17.6 \\ 3.7 \\ \hline 21.3 \end{array}$$

$$\begin{array}{r} 25.00 \\ 5.25 \\ \hline 30.25 \end{array}$$

$$\begin{array}{r} 29^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 34^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 40^{\circ} 16' \end{array}$$

$$\begin{array}{r} 29^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 34^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 40^{\circ} 16' \end{array}$$

$$\begin{array}{r} 10^{\circ} 45.6' \\ 5^{\circ} 30' \\ \hline 6^{\circ} 75.6' \\ 7^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 12^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 18^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 23^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 29^{\circ} 16' \end{array}$$

$$\begin{array}{r} 10^{\circ} 45.6' \\ 5^{\circ} 30' \\ \hline 6^{\circ} 75.6' \\ 7^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 12^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 18^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 23^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 29^{\circ} 16' \end{array}$$

$$\begin{array}{r} 18^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 23^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 29^{\circ} 16' \end{array}$$

$$\begin{array}{r} 12^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 18^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 23^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 29^{\circ} 16' \end{array}$$

$$\begin{array}{r} 6^{\circ} 75.6' \\ 7^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 12^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 18^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 23^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 29^{\circ} 16' \end{array}$$

$$\begin{array}{r} 7^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 12^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 18^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 23^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 29^{\circ} 16' \end{array}$$

$$\begin{array}{r} 5^{\circ} 30' \\ \hline 12^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 18^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 23^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 29^{\circ} 16' \end{array}$$

$$\begin{array}{r} 5^{\circ} 30' \\ \hline 12^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 18^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 23^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 29^{\circ} 16' \end{array}$$

$$\begin{array}{r} 5^{\circ} 30' \\ \hline 12^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 18^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 23^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 29^{\circ} 16' \end{array}$$

$$\begin{array}{r} 5^{\circ} 30' \\ \hline 12^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 18^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 23^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 29^{\circ} 16' \end{array}$$

$$\begin{array}{r} 5^{\circ} 30' \\ \hline 12^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 18^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 23^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 29^{\circ} 16' \end{array}$$

$$\begin{array}{r} 5^{\circ} 30' \\ \hline 12^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 18^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 23^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 29^{\circ} 16' \end{array}$$

$$\begin{array}{r} 5^{\circ} 30' \\ \hline 12^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 18^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 23^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 29^{\circ} 16' \end{array}$$

$$\begin{array}{r} 5^{\circ} 30' \\ \hline 12^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 18^{\circ} 16' \\ 5^{\circ} 30' \\ \hline 23^{\circ} 46' \\ 5^{\circ} 30' \\ \hline 29^{\circ} 16' \end{array}$$

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Stones ON BAILEY Road

1. Same as No. 3 on Flinn road.

Distance 1 to 2 769.9

2. Hub Stake + Tack.
W. on line from No 1
Cor. Post $12^{\circ} W. 15'$
Plumb Tree $4^{\circ} N 10^{\circ} W. 69'$

3. Hub stake + Tack
N. on line from No 2 671.3'
14" Apple $S 45^{\circ} E 38'$
S.E. Cor Chas. Clay Barn $N 1^{\circ} W 15'$

4. N.E. Cor Blacksmith Shop
 $S. 50^{\circ} W 17'$
14" Maple $N 45^{\circ} W 42.0'$

5. 18" Maple $N 50^{\circ} W 32.0'$
24" Maple $S 20^{\circ} W 62.0'$

149

150

6. I. P. 10" Color. $1750^{\circ}W$ 26.5'
S.W. Cor. Stone No. 20 E. 345.

7. Iron Pin at P.I. 15' W. of Stone
and 17' E. of Cor. Post 18' S.

8. Iron Pin 15' W of Cor Stone
Cor. Post. $545^{\circ}W$ 21.5'

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STONES ON FLINN ROAD

1. S.E. Cor. Sec. 7 Sta. 0100
S.W. Cor. 1/4 Header N45°E 19'
S.E. " " " N45°W 17'
N.E. " 12 Sq. Conc. Post S45°W 22'
2. E 1/2 Mi. S. E. 7 14" WALNUT
S 87°W 36.5'
Cor Post 12" Sq. W 15'
" " 8" " E 10'
3. C.E.N. E. N.E. 1/4 Sec. 7
15" Walnut N45°W 42.5'
10" Sq. Cor Post S45°W 22.5'
4. N.E. Cor. Sec. 7.
10" Cherry S 35°W 54'
12" Sq. Post (Conc) W 15'

$$4 \overline{) .25} \quad \underline{61}$$

$$\frac{3}{5} \times$$

$$\begin{array}{r} 121.54 \\ 121.07 \\ \hline 160 \overline{) 470000294} \\ \underline{320} \\ 1500 \\ \underline{1440} \\ 600 \end{array}$$

$$\begin{array}{r} .00294 \\ 25 \\ \hline \end{array}$$

$$\begin{array}{r} 1470 \\ 588 \\ \hline \end{array}$$

$$.07350$$

153

154

5. N.E. Cor. S.E. 1/4 S.E. 1/4 Sec. 6.
 8" Arch N45°E 28'
 Cor. Post N45°E 22'
 Cor. " N45W 21'

$$\begin{array}{r} 35.17 \\ 7.30 \\ \hline 42.47 \end{array}$$

$$\begin{array}{r} 60 \overline{) 5730} \\ \underline{540} \\ 330 \end{array}$$

$$\begin{array}{r} 60 \overline{) 330.1} \\ \underline{300} \\ 30.1 \end{array}$$

5° 30'

95.5

$$\begin{array}{r} 5.17' \\ 7.30 \\ \hline 12.47' \\ 7.30 \\ \hline 19.77' \end{array}$$

$$\begin{array}{r} 19.77' \\ 20.17' \\ 7.30 \\ \hline 27.47' \end{array}$$

$$\begin{array}{r} 27.47' \\ 7.30 \\ \hline 34.77' \\ 35.17' \end{array}$$

$$\begin{array}{r} 6 \\ 1.5 \\ \hline \end{array}$$

44.29'

155

$$\begin{array}{r} 148.5 \overline{) 44.500} \\ \underline{44454} \\ 3 \end{array}$$

$$\begin{array}{r} 10 \overline{) 180} \\ \underline{18} \text{ per pt} \end{array}$$

$$\begin{array}{r} 113 + 07.4 \\ 325 \\ \hline 307.4 \end{array}$$

$$\begin{array}{r} 17.6 \\ 18.1 \\ \hline 5.17' \end{array}$$

$$\begin{array}{r} 1408 \\ 1776 \\ \hline 60 \overline{) 3168} \\ \underline{3000} \\ 16.8 \end{array}$$

