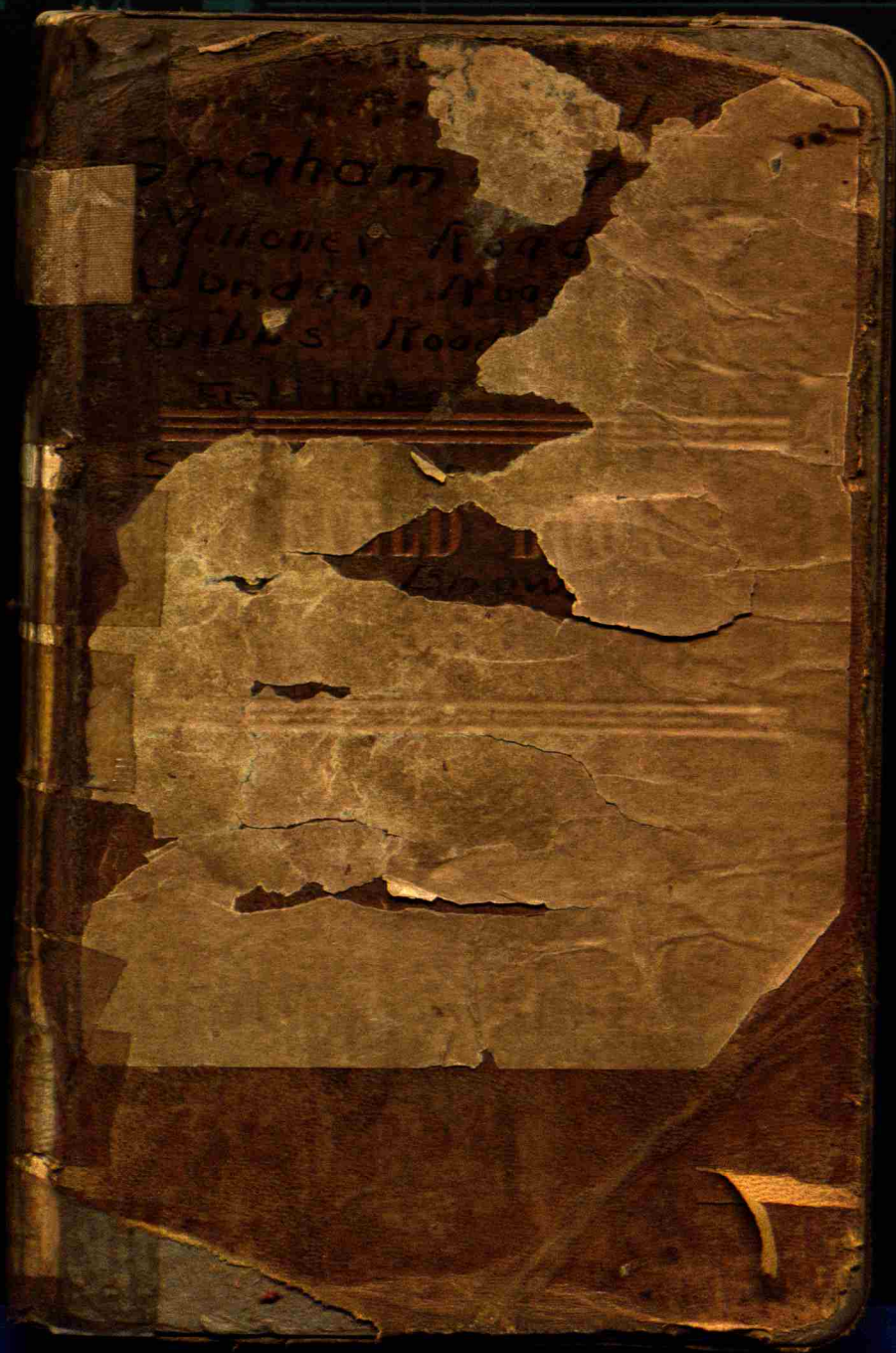


← LETTER →



Synham
Millener Road
London Road
Gibbs Road
5th 1800

1800

Stence - M. O. Stuart Road.

(11) (?) On sec. line bet. 20 & 21
about $\frac{1}{2}$ N. SW. cor. Sec. 21.

2. (?) On N. 15 line thru cen. Sec.
21 about $\frac{1}{8}$ S. Sec. cen. 21

13. Cen. Sec. 21

14. E. $\frac{1}{2}$ mi. Sec. 21. - 22

Jos. Wheeler
Oscar Carter

Stones on C. I. West Road.

✓ 1. East $\frac{1}{2}$ mi. Sec. 21.

✓ 2. NE. cor. Sec. 21.

Andrew Roberts
Rabt Pounds.

On Orien Hadley Road-

✓ 1. NE cor. Sec. 21.

✓ 2. S $\frac{1}{2}$ mi. Sec. 15.

Jr. S. Miller.
Chas. Roberts.

On Alva Stanley Road

1. S. $\frac{1}{2}$ mi. Sec. 15. (22)

2. Cen. S. SE ⁴ sec. 15. (22)

3. S $\frac{1}{2}$ mi. Sec 14. ? (23)

4 SW. cor 13. (14, 23, 24)

5. S $\frac{1}{2}$ mi. Sec. 13. (24)

6. Cen. S. SE ⁴ sec. 13 (24)

6

7. On N 15. line thru ~~Can.~~ NE 9-24

8. On N 15. sec. line bet. 24 ⁽¹⁵¹⁰⁾ & 19

Jos. Miller

Chas. Roberts.

7

8 Conn Road

Sta Mark Azim Bearing
 0+00 X on Concrete
 Crossing $50^{\circ}W$ $52^{\circ}10'W$

$56^{\circ}E$

5+17.0 Stake at P.I. $555^{\circ}20'E$ $557^{\circ}E$ Def L
 $\Delta = 55^{\circ}20'$
 $10 = 6^{\circ}55'$

$$\text{Tan} = \frac{25 \tan 27^{\circ}40'}{2 \sin 6^{\circ}55'} = \frac{1314}{2408} = 54.5$$

$$R = T \times \cot 27^{\circ}40' = 103.8$$

$$\frac{25}{103.8} = \frac{x}{88.8} = \begin{matrix} 21.2 \text{ inside} \\ 28.8 \text{ outside} \end{matrix}$$

8+00 Stake at P.I. $559^{\circ}37'E$

Def L
 $4217'$

Witnesses Curb $12.9'E$
 $112.9'W$

High Point Rock $S35E 9'$

5+17

54.5

4+62.5 = P.C.

5+62.5 = P.T.

Stake $S 15'$
 $N 15'$

30' Cottonwood $S40^{\circ}E 37.5'$

Sta Mark Azim Bear

10+40 Iron
Pillar. S 86° 53' E
P.I.Def L
27° 16'

$$\frac{25 \tan 13^\circ 38'}{2 \sin 3^\circ 24' 30''} = \frac{60435}{1189} = 50.8$$

$$R = \tan \times \cot 13^\circ 38' = 209.5$$

$$\frac{25}{210} = \frac{X}{225} = 26.8 \text{ outside}$$

$$23.2 \text{ inside}$$

16" Post + S10W 21'
24" Cottonwood 45° E 25.1'
Stake 59.0
N 21.1'

$$\frac{10+40}{50.8}$$

$$9 + 89.2 = P.C.$$

$$10 + 89.2 = P.T.$$

12

Graham Road

EI

Constit

100.00 84.27 El. @ Rd Sta
10+00

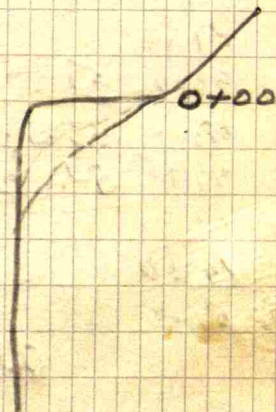
Ditch

0+00	90.80	75.67	30' N of Fence Line Sta 11+50
0+10	93.10	77.37	15' N Fence
0+60	92.85	77.12	
1+80	89.95	74.22	At prop line E 15' N
2+60	89.30	73.57	"
3+10	90.70	74.97	"
3+45	87.10	71.37	
3+60		69.75	Same as Flow Line Culvert Sta 14+90

13

in Bottom Ditch

of Fence



14

Graham.

E1.

BM

104.23

0+00	96.10	54.67	70' H $\frac{1}{2}$ Sta 24+15
0+05	98.00	56.57	
1+00	96.05	54.62	Bed opposite 30' H

Bank is 3' Higher than
present channel is 6' wide

15

E. end S. Rail Sta. 25+33

Bed

Sta 25+15

Levels
+ 3' deep.

0+00 49.45
 0+10 51.00
 0+50 50.35
 1+10 49.04
 1+50 49.75
 1+50 46.80
 53.95
 53.85
 50.26

B.M.
 57.04
 150' W of Culvert. 40'
 30' N \swarrow

"

"

"

Red

40' N \swarrow 50' \swarrow Culvert
 50' " " 75' E " "
 60' " " 100' E " "

N \swarrow

Red Mean

A.P. Meridian Road

Sta 24+00 - Same from 8+90

Sta 24+90 12' x 20' V.
old 24+00. 2x3 Box
30' LongSta 26+48 - Span
20' Roadway No ChangeSta 25
PC 25+93

Sta 26+61 P.I.

Con Rock 22.5' E of
P.I. at 26+83.5

PT. Sta 27+18

Alfie B. Station

London S.

Ernie Habers to G. B.

Al.

Columbus Meridian Road

Stone Cen Meridian T.P. 17 1/4 R 2W

$$\Delta = 72^{\circ} 0'$$

$$T = 68'$$

$$Sma = \frac{a}{2}$$

$$R = \frac{5730}{60} = 95.5$$

$$D.C. = \frac{72 \times 100}{120} = 60^{\circ}$$

$$L = 120.0'$$

$$C = 10'$$

$$\text{Def. for } 10' \text{ chords} = 3^{\circ}$$

Staked

P.C. sta 25+93

P.I. sta 26+61

P.T. sta 27+13 End of Prod

$$\Delta 72^{\circ} 0'$$

$$T 68'$$

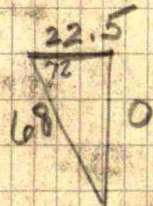
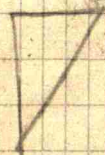
$$L 120$$

$$R. 95.5$$

$$DC 60^{\circ}$$

$$\left\{ C. 10'$$

$$\left\{ \text{Def } 3^{\circ} 00'$$



$$\frac{92}{68} - \frac{22.5}{68}$$

$$.95106$$

$$0 = 64.7$$

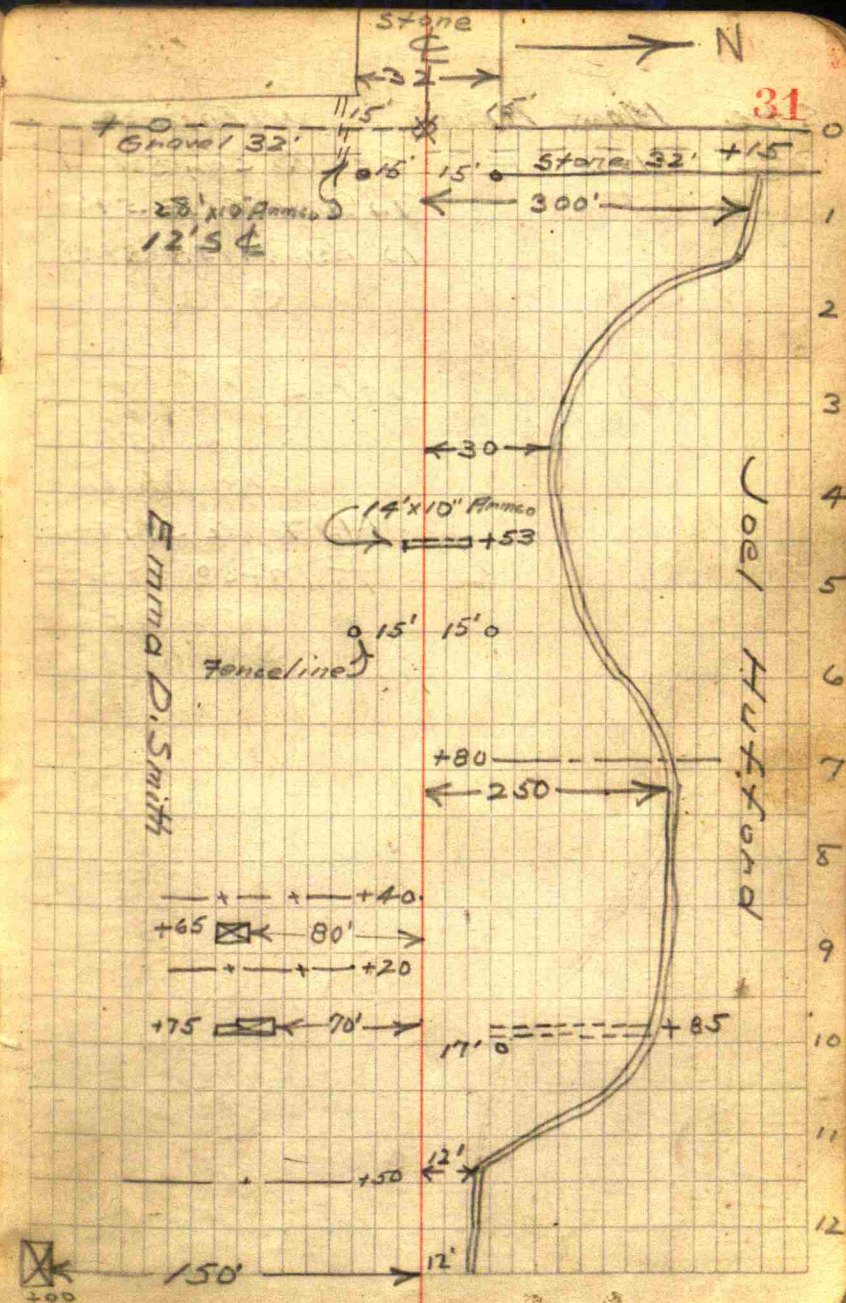
30

Graham Road

Sta.	Mark	Azimuth	Witnesses
0	Stone		W ² Mi Stone Sec 21 10" Walnut N64E51 Con Post S45°W22'

Tel. Poles Both
sides 150' Apart +
14' off \leftarrow To Sta 18 +
No Fence S. Side
9+20 11+40

Tel poles at
Fence Line from
Sta 18 + 0.



St 9. Mark Azim

13+21 Stone E

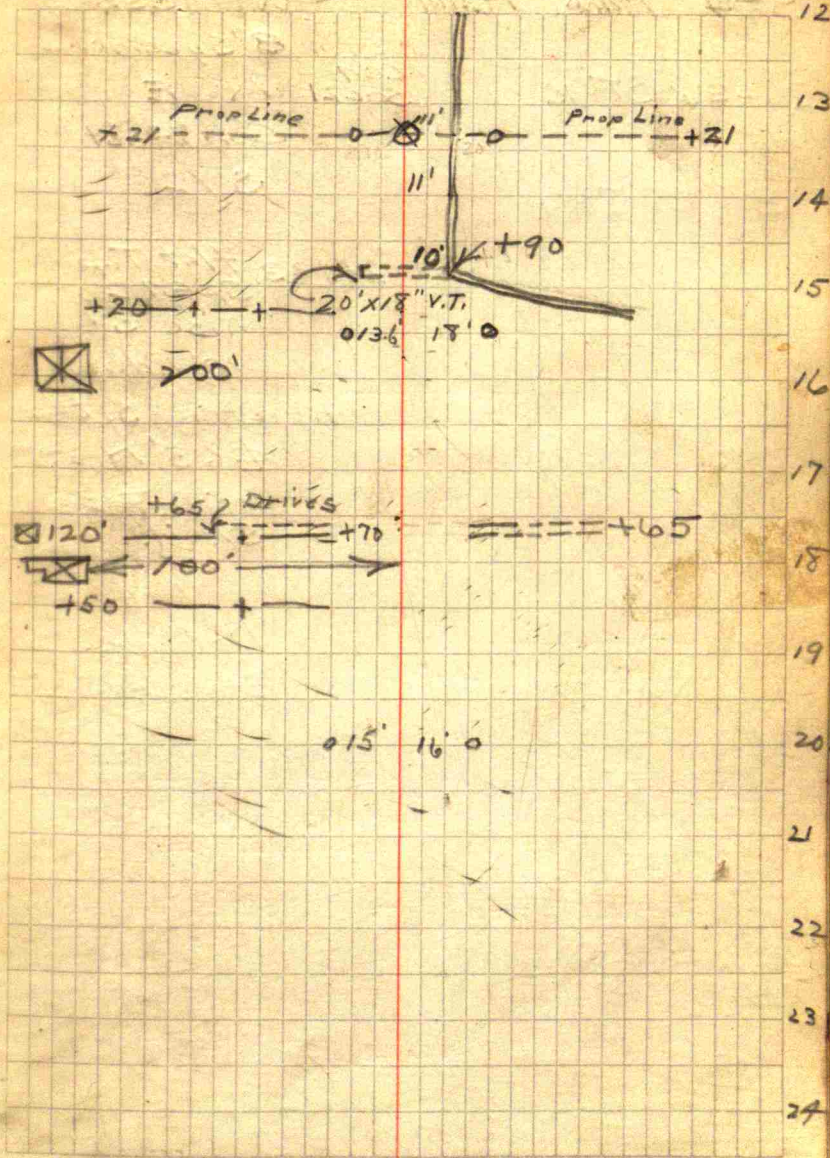
Witnesses
 Cen W. Cen Sec 21
 24" Supn S50E 59'
 10" Fish N15W 21.5'

No Fence S. 17+65
 to 18+50

13 21
 11 50
 17'

1490 E
 1150
 340

→ N 33



34

Sta Mark Azim

26+36 Stone

Cen.
Sec 21

Witnesses

8" Sycamore

N E

Cor Post

S 12'

24+33 Flat Top

Sp 97 20

Rise 5'

18' Rdway

Wings S. Back

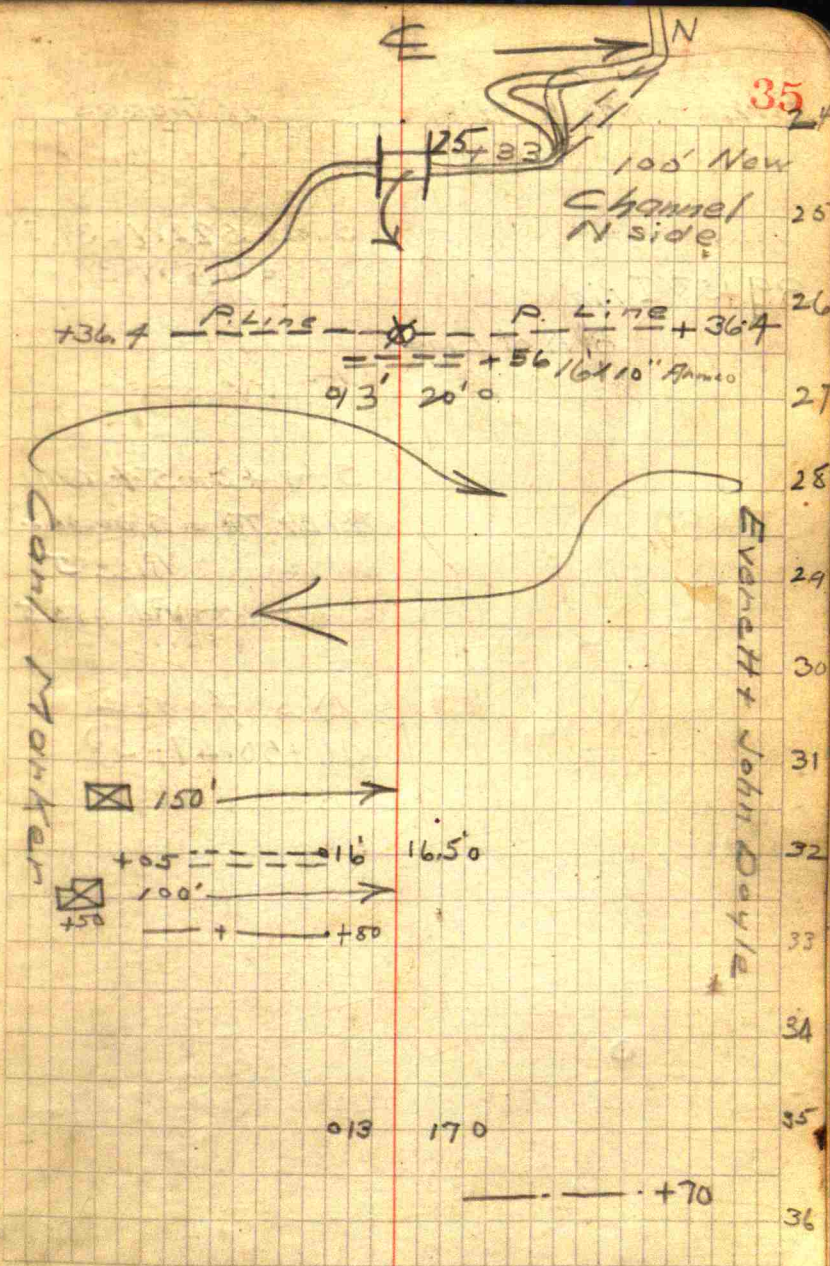
± 6.5' N of

inside face
S rail.

No fence S.

Sta 32+00 to 32+80

35



+36.4 P. Line +36.4

+56 16' 10" Anno
43' 20" 0

Canal Marker

150'

+65 16 16.50

100'

+80

013 170

+70

36

Sta Mark Azim

Witnesses

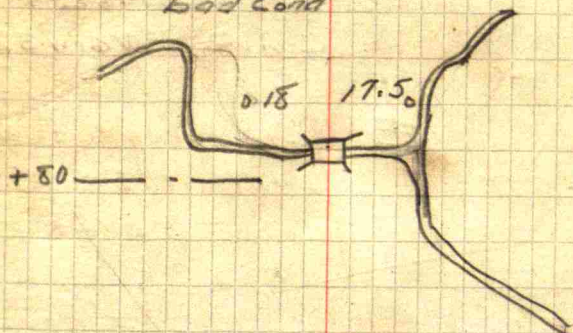
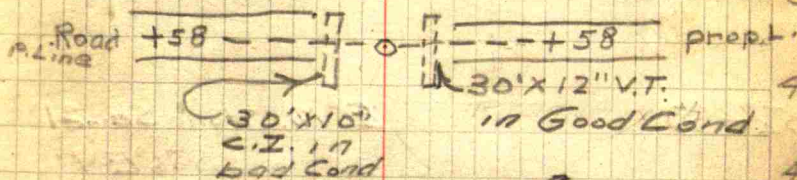
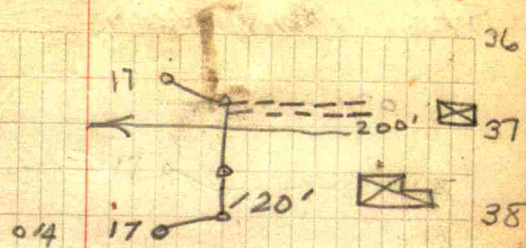
Sugar S22W° 34.5'
Stone N68°W 38.9'

39+58 I. Pin

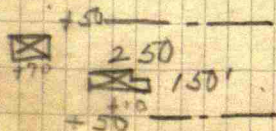
8" N of Line

Sta 42+54. Concl.
Flat Top Span 12
Rise 5
Rdn 413.5No Fence
46+50.47+50

37



013' 16' 0



Margaret Doyle

Jess Winnings

36

37

38

39

40

41

42

43

44

45

46

47

48

57³⁸ Mark Azim

Should Have
Series wider Rd
St 44+40
unless Road
is Graded to
West.

52+80

E² Mi. Stone Sec 21
24" Beech S86°E 9
Con Post N60W32'

E → 39

+44

013.5 165.0

~~+~~+30
E35 24" Beech

014 16°

+33 Prop Line

50'
+57 → +30
013' 16°

48

49

50

51

52

53

54

55

56

57

58

59

60

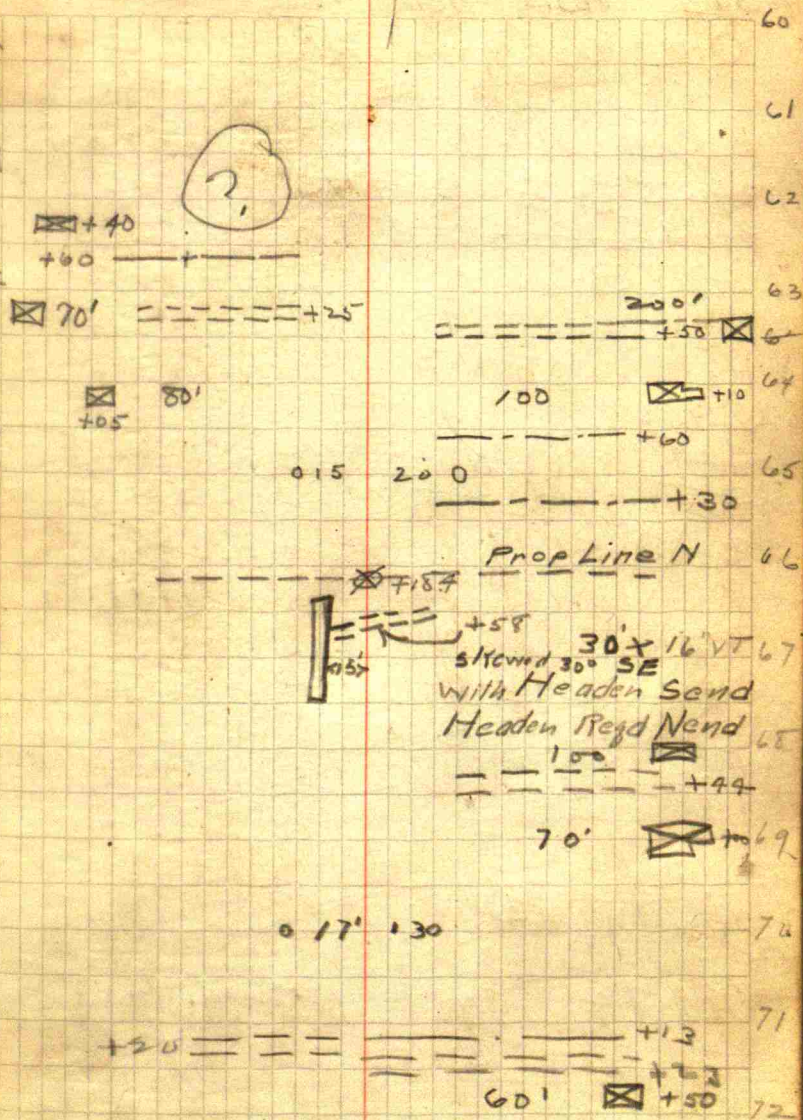
40

Sta No Mark Azim

66 + R. 4 Stone E. Cor W. cen Sec 22.
 24 Elm N 62° E 56'
 Cor Post S 15.8'

41

Lem Everett



44
Sta

0+00

Det

N36°30'E I.P.

N32°40'E

Pl 2+84

3+05.5 L8°^{22'} 3+04.95~~3+69.5~~ L12°10' N24°E I.P.

PT 3+25.90

Pl 6+40.3

6+83 6+82.14

~~6+17~~ R16°37' N40°30'E I.P.

P.T 7+23.38

Pl 7+24.08

7+65.5 7+64.18

7+24.5 R15°54' N57°E I.P.

PT 8+03.58

Pl 8+50.5

9+19.7 R14°35' N71°E I.P. = 9+17.17

PT 9+53.41

Maloney Road

Needle

Bear Mark.

At intersection
with Brown Road

+ Foyette Road

45

Witnesses

Cement Post S61°E 16.9 N32°40'E 47.2

Cen. End of

Bridge Floor N15°W 44' N 91.0'

Cen Post S30°E 25'

Cement Post 62°30'E 13'

White Oak 30" N85°30'W 17'

Cement Post S61°E 14.3'

10" Sycamore N19°W 14'

Cement Post S40°30'E 16'

19" Walnut S65°E 22' 6"

Cement Post S25°E 15.2'

24" Beech N79°W 26' 2"

46

Sta Det Needle
 Bean Mark
 P. 6. 10+12.8
 10+60.0 P 2836 S 88° 30' E I. P. 10+64.85
 PT = 11+15.8

P. 6. 13+72.9
 14+00 R 5° 25' I. P. 14+00
 14+27.06 PT 300 E I. P.

P. 6. 14+81.67
 15+72 R 17° 55' Stake
 PT 16+60.84

P. 6. 16+60.65
 17+46.4 L 23° 15' S 82° 30' E L 17° 42'
 17+46.4 L 23° 45' S 80° 15' E I. P. 17+41
 P. T. 18+14.15

22+15.4 L 0° 55' S 83° 15' E 22+08

P. 6. 29+73.32
 30+62.9 R 83° 4' S 30+54.8
 PT 31+11.76 S 15' E

47

Cement Post S 7° E 15'
 12" Sycamore N 7° E 20.5'

Sugar 24" N 47° W 53.5'
 Walnut 10" N 65° E 72'

Cement Post N 05° E 3.8'

Cement Post S 19° 30' W 15'

Con Post S 1° 30' W 15.2'
 " " N 4° W 16.1'

Con Post N 43° W ~~22.8'~~ 23.3'
 " " S 39° W 23.3'

Def. Needle
Bear. Monk

Plb Sto 31+35

32+29 L 90° 9' E Stone 32+30.76
PT 32+85.26

52+89 L 0° 25' N 89° 40' E Stone 52+58
40
52+18

Plb. 71+29.57 - 40 = 70+89.57

72+52 R 90° 15' ~~S 89° 30' W~~ Stone 72+25.5
40
PT 72+80 S 15' W 71+85.5

40
72+40

Plb 79+25.69 - 40 = 78+85.69

80+22 - 79+82

80+88.5 L 90° 29' ~~N 89° 15' E~~ Stone Cen W of Cen
N 89° 15' E Sec 25 T 17
N R 1 E

PT 80+76.49
40

80+36.49

Con Post S 15.5'
" " N 45 W 23'

Con Post S 15'
W. Cherny S 75 E 88'

Con Post N 15.5'
" " S 45 W 23.5'

Con Post S 15.5'
" " N 45 E 22'

Sta	Def	Needle	Monk
P. 6	92+08		9/16 8

94+125R90°35'	515' E	Stone	93+05
---------------	--------	-------	-------

PT	93+59.49		92+63
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	93+19.49		
--	----------	--	--

100+55.9			
----------	--	--	--

I.P.

99+08.0			
---------	--	--	--

40			
----	--	--	--

98+68.0			
---------	--	--	--

Con Post	N 15.8'		
----------	---------	--	--

" "	E 15'		
-----	-------	--	--

Con Post	N 45 E 25'		
----------	------------	--	--

34" Elm Stump	N 40 E 32'		
---------------	------------	--	--

Maloney Road

Property owners

N. Side

S. Side

Sta. To Sta

Sta To Sta

0+00 22+08 U.G. Arbuckle 0+00 17+80

22+08 30+54.8 Ellison Arbuckle both sides
Except Penn. RR. Rot Way
Sta to Sta

E. Side

W. Side

30+54.8 32+30.76 Hannah Coffman
Estate 30+54.8 32+30.76

N. Side

S. Side

32+30.76 72+255

32+30.76 52+58

52+58 72+255

E side

W. Side

72+25.5 80+22 Steven Maloney 72+255 80+22

N. Side

S. Side

80+22 86+05 " 80+22 93+05

86+05 92+ James Collins

92+ End. John Maloney

W. Side

93+05 99+08

Chas O. Coffman

U. G. Arbuckle

Ellison Arbuckle

Elizabeth Strawn Meyer

Steven Maloney

Steven Maloney

"

"

"

"

Melvin O. Gibbs Levels

54

250' W 0

100' W 0

	A	B	C	D	E
					195.35
0+00	196.90 ²⁰	196.60 ¹⁵⁷	195.72 ¹⁰	196.46 ⁴	196.65
1+00	194.84 ¹⁴	194.50 ¹³⁷	193.70 ⁸	194.50	194.66
1+24	193.50 ²⁰	192.62 ¹²⁷	193.65 ⁷		194.60
2+00	195.16 ²⁰	194.70 ¹²⁷	193.90 ⁷	194.61 ²	194.62
3+00	196.90 ²⁰	196.65 ¹¹⁷	195.70 ⁶	195.72 ²	195.45
4+00	192.90 ²⁰	192.70 ¹¹⁷	191.45 ⁴		191.10
5+00	188.22 ²³	188.35 ¹⁵⁷	187.60 ⁸	188.10 ⁴	188.03
6+00	186.95 ²⁰	186.31 ¹¹⁷	184.66 ⁴		186.65
6+05		186.12 ¹⁵⁷	183.70 ⁸	186.04 ⁴	186.82
7+00	190.10 ²³	189.82 ¹⁵⁷	188.42 ⁹	188.16 ⁴	188.30
8+00	189.25 ²⁰	188.57 ¹⁵⁷	187.42 ¹⁰	187.96 ⁴	187.82
9+00	187.80 ²⁰	187.30 ¹⁵⁷	186.06 ¹⁰	185.95 ⁴	185.82
10+00	184.70 ²⁰	184.38 ¹⁴⁷	184.15 ¹⁰	184.72 ⁹	184.95
10+37			181.15 ¹¹	183.00 ⁹	184.96
11+00	183.70 ²⁰	183.20 ¹²	182.35 ¹⁰	184.70 ⁵	185.02
12+00	185.82 ²⁰	186.76 ¹⁵⁷	186.20 ¹⁰	186.81 ⁶	187.15
13+00	186.97 ²⁰	185.17 ¹⁴	188.00 ⁹	188.57 ⁶	188.70
14+00	190.75 ²⁰	191.05 ¹⁵	189.35 ⁸	189.85 ⁵	190.00
15+00	193.30 ²⁰	193.27 ¹⁵	191.80 ⁷		192.35
16+00	194.10 ²⁰	194.20 ¹⁴	193.80 ⁸	194.00 ⁴	193.80
17+00	196.45 ²⁰	196.25 ¹³	195.42 ⁹	195.95 ³	195.95
18+00	197.70 ²⁰	197.95 ¹⁴	197.10 ⁵	197.70 ⁵	198.04
19+00	198.40 ²⁰	198.60 ¹⁴	198.10 ⁵	198.70 ⁵	199.09
20+00	197.90 ²⁰	198.20 ¹⁴	198.10 ¹	198.60 ⁵	199.02

7 8 9 10 11 12 13 14 15 16 17 18 19 20

	7	8	9	10	11	12	13	14	15	16	17	18	19	20
	196.20 ⁸	195.23 ¹³	195.30 ¹⁵⁷	195.22 ²⁰										
	194.36 ⁸	193.41 ⁷¹	193.87 ¹⁶⁷	193.70 ¹⁶⁷										
	192.67 ⁸	192.57 ⁷¹	191.89 ¹⁶⁷											
	194.37 ⁹	193.98 ¹³	194.60 ¹⁶⁷	194.60 ¹⁶⁷										
	195.12 ¹¹	195.80 ¹⁶		195.50 ¹⁹										
	191.10 ¹¹	192.00 ¹⁶		192.00 ²⁰										
	188.15 ¹²	187.66 ¹⁴	188.37 ¹⁷⁷	188.40 ¹⁹										
	186.53 ¹²	184.23 ¹⁴		183.76 ²⁰										
	185.60 ¹²	183.73 ¹⁴	183.60 ¹⁷⁷											
	188.27 ¹¹	189.68 ¹⁷		189.45 ²⁰										
	187.96 ⁹	186.80 ¹³	187.10 ¹⁷⁷	186.46 ¹⁷										
	185.70 ⁹	185.30 ¹¹	186.70 ¹⁷⁷	186.50 ¹⁷										
	184.65 ⁸	183.33 ¹³	183.33 ¹⁷	183.06 ¹³										
	182.60 ⁸	181.05 ¹³												
	184.75 ¹¹	183.60 ¹⁷	183.90 ¹⁴	184.15 ²⁰										
	186.77 ⁹	185.63 ¹¹	187.70 ¹⁶⁷	188.00 ¹⁶⁷										
	187.63 ⁹	187.20 ¹²	188.72 ¹⁵	189.00 ¹⁵										
	189.83 ⁹	189.60 ¹¹	190.15 ¹⁵	190.30 ²⁰										
	193.55 ⁹	193.60 ¹³	193.85 ¹⁵	193.65 ¹⁵										
	195.75 ⁹	195.56 ¹³	196.10 ¹⁵	196.10 ¹⁵										
	197.35 ⁹	197.12 ¹¹	197.45 ¹⁴	197.40 ¹⁴										
	198.50 ⁹	198.05 ¹¹	198.42 ¹⁴	198.40 ¹⁴										
	198.50 ⁷	197.70 ¹¹	198.15 ¹⁴	198.15 ¹⁴										

55 M.
E. 200. m
COA. Pos
15' S. Sta
0700

Sta	A	B	C	D	E
21+00	197.55	197.85	197.70	198.30	198.75
22+00	197.50	197.60	197.40	197.95	198.30
23+00	196.60	196.65	196.50	197.00	197.50
24+00	196.50	196.45	196.30	196.76	197.20
25+00	196.32	196.60	196.05	196.90	197.10
26+00	196.72	196.90	196.80	196.75	197.20
26+92	197.15				197.00
27+00	196.66	196.80	197.00	197.05	196.95
28+00	196.27	196.45	196.25	196.75	197.11
29+00	196.15	196.10	196.00	196.73	197.15
30+00	196.30	196.50	196.10	196.60	196.95
31+00	195.80	196.10	195.75	196.20	196.40
32+00	194.80	195.00	194.60	194.90	195.35
33+00	193.66	193.70	193.45		193.82
34+00	191.96	192.25	191.80	192.00	192.53
35+00	189.83	190.11	190.16	190.73	191.13
36+00	188.90	189.10	189.03	189.30	189.90
37+00	187.70	187.95	187.50	187.60	188.30
38+00	185.70	185.80	185.75	186.45	186.85
39+00	184.10	184.00	185.00		185.55
40+00	183.00	182.55	183.73		184.32
41+00	181.90	181.90	181.40	182.00	183.15
42+00	182.43	182.25	181.63	182.00	182.30
43+00	182.00	181.00	179.46	181.20	181.33
44+00	180.95	179.85	179.25	179.62	180.00

7	G	H	I	
198.30	197.60	199.00	197.90	✓
197.80	197.40	197.80	197.90	✓
197.30	196.20	196.65	196.76	✓
197.05	196.00	196.20	196.30	
196.65	195.05	196.25	196.00	
196.80	196.00	196.30	195.90	
196.70	196.58	196.80	196.80	⊙
196.70	196.31	196.46	196.46	Stake of Sta 25
196.63	196.10	196.10	195.86	EI. 197.05
196.50	196.35	196.76	196.80	BM. Cont Post
195.95	195.80	196.10	196.20	Cement
195.00	194.83	194.70	195.10	15.5 Sta 26+92
193.60			194.10	EI 201.94
192.20	191.90		192.60	
190.55	190.16	190.25	189.96	
189.40	189.20	189.32	189.85	
187.70	187.55	188.10	188.20	
186.35	186.20	186.30	187.15	
185.10	184.90	185.10	185.60	✓
183.50	183.60		184.30	✓
182.70	182.00	182.30	180.96	✓
182.00	180.90	181.76	181.17	✓
180.90	180.05	180.86	180.50	✓
179.50	178.86	179.80	179.30	✓

51+58

74
66.20 67.20

68.65

Sta	A ₂₀	B ₂₀	C ₂₀	D ₂₀	E ₂₀
45	178.00	177.50	177.40	175.30	175.30
46	170.80	176.05	175.35	176.65	175.20
47	174.95	174.20	173.95	174.53	175.18
48	172.90	172.90	172.06	173.15	170.71
49	171.40	171.40	170.70	171.70	172.13
50	170.30	170.30	169.55	170.27	170.65
51+30	168.20	168.20	167.60	168.75	169.10
52	167.25	167.25	167.13	167.53	168.00
53	166.10	165.70	165.60	166.10	166.42
54	165.10	164.75	164.30	165.07	165.25
55	164.10	163.75	163.15	163.93	164.33
56	162.70	162.52	162.15	162.83	163.21
57	160.93	160.93	160.50	162.00	162.30
58	160.42	160.42	159.83	161.00	161.55
59	159.50	159.50	158.70	159.83	160.30
60	158.40	158.60	157.30	158.21	158.47
60+73	149.40	146.40	150.09	151.97	157.20
61	150.30	55.00	55.70	56.00	157.38
62	56.20	56.60	56.15	55.70	156.88
62+80	52.43	54.65	54.45		154.62
63+00	33.92	33.92	45.67	53.90	154.09
63+26	30.10	28.45	28.45	29.55	151.47
63+64	26.25	24.45	43.90	150.00	153.10
63+80	26.85	24.10	44.20	44.20	144.91
64+00	25.00	22.40	27.20	28.70	135.52
64+39	19.70	35.17			148.06

67.75 66.70

59

F ₂₀	G ₂₀	H ₂₀	I ₂₀	
178.30	177.55	177.95	177.20	←
170.82	176.10	177.70	176.80	←
174.90	174.20	175.10	174.74	←
173.20	172.00	172.90	172.50	✓
171.75	171.20	171.30	171.60	✓ E. Corn Post
170.25	169.43	170.60	170.70	✓ Jones Point Yard
169.10	168.43	168.95	169.16	✓ 7.00
167.25	167.30	167.30	167.40	✓ E1170.25 ✓
166.25	166.06	166.45	166.50	✓
164.57	164.30	164.50	164.50	✓
164.10	163.30	163.95	163.80	✓
162.74	162.10	162.65	162.45	✓
161.70	161.15	161.20	161.60	✓
161.22	160.63	161.00	161.50	✓
159.61	159.56	160.19	160.00	✓
158.05	157.90	159.00	159.40	✓
157.06	153.50	153.30	156.00	✓
157.16	56.70	167.70	158.30	✓
56.50	56.35	57.20	57.40	
54.30	54.47	56.00		
53.82	53.76	55.80		7.00
53.57	53.43	55.20	55.50	35.20
51.09	52.75	52.30	51.10	
52.52	51.76	50.30		
52.17	51.33	50.00	50.50	
53.32	53.23	53.00	53.60	59 N 64 N

Sta	A	B	C	D	E
64+80	27 49.25	52.54		27 54.66	154.46
65+00	25 53.86	54.80		27 55.00	155.30
66+00	20 54.70		7 54.17		154.09
67+00	20 52.10	10 52.05			152.50
65+00	20 50.70	10 50.30			150.35

out

62+00	20 56.23	16 56.87	7 56.50		156.36
63+00	37 45.67	21 53.80	4 53.85		154.76
63+26	63 28.45	59 29.55	15 52.46		153.20
63+64	31 43.90	21 53.10	9 51.09	4 52.75	152.60
64+00	66 122.40	58 127.26	48 128.70	23 35.52	152.17
64+39	80 19.70	57 35.17	27 48.06	19 53.32	153.20
64+65	30 54.66	23 53.30	15 54.52	8 54.26	154.20
65+00	29 55.05	12 54.00	15 55.35	8 55.55	154.97
66+00	28 54.25	17 53.85	11 54.60		154.86
67+00	29 52.00	16 53.30			153.73
68+00	14 150.45	14 150.10	3 151.00		151.25
69+00	22 147.10	14 146.40	5 147.35		147.69
70+00	21 43.83	13 44.35	8 44.93		145.22
71+00	20 142.60	16 142.60	12 142.40	6 143.12	143.12
72+00	19 141.16	17 141.45	10 138.20	3 139.10	139.20
73+00	25 131.85	15 129.78	10 130.82		130.80
74+00	25 112.30	11 121.70	7 120.86		121.10
75+00	20 106.45	17 107.15	11 108.89	5 112.00	112.51

F	G	H	I
5 53.53	13 55.18	24 54.80	40 55.95
7 54.65	11 55.50	20 55.50	37 56.10
53 53.60	21 54.00	29 54.40	33 55.20
53 53.40	22 54.00	33 53.90	
53 53.50	22 54.00	33 52.50	

B.M. E/35.32
 Section
 Pump. 7/1000
 Sch. H. Yd

77 57.35	17 57.45	23 57.33	
9 56.70	15 55.73	28 55.53	
13 55.20		25 52.30	
11 52.30	12 51.33	25 51.20	
7 53.20	8 52.90	25 54.55	
4 55.40	15 55.52	28 55.25	
6 55.80		22 55.50	
5 54.30	12 55.15	28 55.05	
10 53.70	13 52.16	18 53.66	21 153.85
8 147.54	26 151.21	7 152.40	
5 44.50	16 44.51	20 45.20	
7 42.70	10 41.90	20 42.20	
13 139.01	13 137.92	19 142.35	25 142.91
5 129.70	13 134.00	22 140.00	26 140.00
11 121.17	14 120.43	20 123.80	26 126.50
12 112.26	17 110.65	20 108.93	25 105.20

Sta	A	B	C	D	E
76+00	106.27	106.20	106.40		106.89
76+51	107.30		106.58		106.07
77+00	105.75	104.96	105.45		105.62
78+00	104.70	104.20	104.75		104.85
79+00	104.05	103.95	104.15		104.27
79+41	104.20	103.83	103.75		103.85
80+41	103.71	103.20			102.84
81+41	102.76	103.10	103.00		103.20
82+00	102.90	102.60	102.40	102.95	103.35
83+00	103.70	103.60	103.70	103.85	104.10
84+00	102.82	103.40	103.10	103.65	103.95
85+00	102.12	102.81	102.60	103.21	103.45
86+00	102.50	102.55	102.90	102.96	103.39
87+00	101.85	102.20	101.50	102.50	102.73
88+00	101.63	102.30	101.95	102.50	102.65
88+69	99.35	99.62	101.10		103.10
89+00	101.95	101.85	102.05	103.05	103.32
90+00	106.45	105.90	105.65	106.55	106.72
91+00	105.30	105.83	105.40	106.50	107.00
92+00	105.20	105.65	105.32	106.50	106.92
93+00	105.69	105.95	105.78	106.66	107.20
94+00	105.53	106.04	105.75	106.76	107.11
95+00	105.93	106.15	105.76	106.70	107.00
96+00	106.50	106.53	106.13	107.01	107.41
97+00	106.30	106.70	106.45	107.40	107.57

F	G	H	I	
106.97	106.31	105.55		
105.80	105.30	105.80	105.50	No fence N side from Rd
104.95	104.40	104.30	104.20	N to Sta 80 + rd
104.55	104.20	104.55	104.20	+ rd
103.50	103.52	104.05	103.40	Tel. poles on R hand side of
102.95	103.00	102.25	102.51	✓ F line 175' Apart
102.90	102.20	102.60	102.20	✓ Sta 73 to 100
103.77	103.15	103.70	103.30	✓
103.65	102.85	103.37	102.80	✓
103.30	102.50	102.90	103.10	✓
103.00	101.43	103.10	102.70	✓
102.65	101.10	102.50	102.30	✓
102.72	101.06	102.46	102.30	✓
101.32	99.75	100.86		✓ Replace
103.21	102.00	102.50	102.60	✓
106.53	105.15	106.05	105.40	✓
106.65	105.30	106.10	105.48	✓
106.85	105.50	106.01	106.00	✓
106.97	105.66	106.26	106.03	✓
107.04	105.83	106.27	106.20	✓
106.79	105.90	106.36	106.23	✓
106.28	106.45	106.90	107.00	✓
107.40	106.50	107.40	106.80	✓

Sta	F	F	C	D	E
98+00	10741	10710	10640	10724	10733
99+00	10750	10710	10655	10680	10655
99+35	10576	10563	10530	10710	10750
99+54	10413	10410	10760		10786
99+947	10396	10526	10618		10670
100+23.7	10422	10450	10535	10590	10615
101+26.6	10530	10522	10530	10520	10485
101+44	10505	10520	10516	10506	10463
101+99.86	10475	10450	10470		10420
102+67.26	10370	10390	10340		10340
103+11.09	10347	10340	10326	10290	10300
104+00	10230	10200	10210	10180	10180
105+00	10063	10065	10060	10075	10003
106+00	9920	9930	9932	9945	9946
107+00	9956	9956	9965		9981
107+64	9940	9915	9936	9970	9950
(P) 108.66	9760	9770	9946	9894	9763
P. 109+67		9736		9668	9676
110+00	9760	9687		9710	9700
110+95	9615	9622	9655	9670	9640
111+77	9570	9640	9600		9560
112+48	9616	9630	9680	9660	9616
113+00	9565	9637	9590	9550	9510
114+00	9723	9670	9675	9720	9700
115+00	9650	9636	9632		9630

F	S	H	I	J
10636	10630	10683	10700	
10695	10630	10683	10680	BME 1108.69
10734	10574	10590	10680	Top E. Gate
10745	10412	10410		Post Sta 102
10662	10692	10695		+67
10620	10625	10670		
10495	10550	10596	10750	
10440	10600	10750	10882	
10420	10610	10710	10870	
10360	10376	10425		
10345	10340	10380		
10190	10225	10240	10290	
10085	10060	10070	10050	
9990	9930	9930	9950	
9973	9955	9930	9900	
9930	9910	9915	9885	
9670	9636	9585		
9620	9645			
	9700			
9530	9660			
9510	9555	9555		
9485	9510			
9420	9460			
9655	9560	9655		

20' to E old rd
60' to Creek Bank
17' to 3-27' E old rd
45' to Cr. Bank
5-15-30'
49' to Cr. Bank
56' to " "
46' " "
88' " "
Creek Turn SE
97 114+00

S+68

	A	B	C	D	E
116	95.30	94.80	94.85		94.70
116+62.8	95.95	95.70	95.50		95.00
117+12.8	95.55	96.15	94.50	95.500	95.500
118+00	94.00	94.23	93.55	94.30	94.85
119+00	93.85	94.65	93.80	94.50	94.69
120+00	93.70	94.70	94.00		94.24
121+00	92.90	92.80	92.76	93.40	93.68
122+00	93.38	93.50	92.83	93.17	93.28
123+00	92.20	92.86	92.95		93.22
124	93.00	93.45	93.30	93.45	93.66
124+88	92.63	93.10	93.62		93.17
125+41	93.84	92.76			92.72
126+00	93.20	92.33			92.60
127+00	92.60		91.45		92.15
127+40	557	25			90.45
128+00	91.20	90.12			92.85
129+00.8	3587 10300	26 10175		14 10180	92.85
130+00	92.91	93.90	92.90	92.93	93.11
131+00	92.73	92.86	93.00	93.04	93.30
132+00	92.40	92.60	92.90	93.20	93.37
133+00	93.00	93.05	92.33	92.93	93.10
134+00	92.10	92.40	92.08	92.70	92.88
135+00	92.16	92.46	91.90	92.30	92.97
136+00	91.32	92.10	91.80	92.20	92.40
137+00	92.52	93.40	91.68	92.32	92.63

69

F	G	H	I	
94.90	95.15	94.10		
95.10	95.60	94.80		Con Stone 176'W And line 7.W. of stone
95.28	95.36	95.80	95.80	
94.50	93.80	94.00	94.00	
94.30	93.60	94.00	94.00	0 Stake at 122+00
93.73	92.85	93.70	94.00	94.11
93.52	93.00	92.74	92.60	
93.12	92.75	92.73	91.33	
93.04	92.85	92.60	92.80	
93.20	92.75	93.60	93.50	
93.33	93.00	92.90		Ret W 60 - CB 46 C 30 RW 10 CB 57 C 40 RT 5 - CB 63 C 56
92.90	93.10			
92.68	92.70			
92.05	91.92			
90.70	90.90			Bed. Stream 7812 Top Ret. B 9.6 2 Wall. 88R 75CB C 64 CB 50 C 14
107.62	102.70			
92.80	92.72	93.36	93.70	
92.92	92.54	92.74	93.20	
93.11	92.16	93.10	92.80	
92.91	92.30	93.26	93.00	
92.66	91.96	92.50	92.10	
92.16	91.60	92.37	92.26	
92.22	91.46	92.20	92.10	
92.26	91.63	92.40	91.70	

Sta	A	B	C	D	E
138+00	91.65	92.20 ¹⁴⁷	91.68 ¹¹	91.80 ⁶	91.86
139+00	89.70	90.60 ¹⁴⁷	91.05 ¹²	91.25 ⁶	91.40
140+00	91.60	91.60 ¹⁵⁷	90.90 ¹¹	91.10 ⁷	91.30
141+00	91.43	91.62 ¹⁴⁷	90.72 ⁹	90.86 ⁶	90.94
142+00	91.00	90.90 ¹⁴⁷	90.46 ¹²	90.90 ⁷	90.93
143+00	90.86	90.52 ¹⁴⁷	89.93 ¹²	90.70 ⁷	91.00
144+00	90.65	90.63 ¹⁴⁷	89.25 ¹⁰	90.10 ⁷	90.48
144+49	86.25 ¹⁴⁷	86.00 ^{97.1}	89.10 ⁹	90.36 ⁵	T
145+00	88.86	89.40 ¹⁵⁷	89.70 ¹¹	90.50 ⁵	90.80
146+00	90.13	90.35 ¹⁴⁷	90.13 ¹²	91.00 ⁷	91.10
147+00	89.25	90.20 ¹⁴⁷	91.52 ⁹	91.30 ⁸	→
148+00	94.00	93.45 ¹³⁷	92.80 ¹¹	92.80 ⁸	92.70
149+00	94.00	94.35 ¹⁴⁷	94.64 ¹¹	95.04 ⁷	94.98
150+00	94.56	95.26 ¹⁴⁷	95.00 ¹¹	95.40 ⁷	95.70
151+00	93.70	94.30 ¹⁵⁷	94.05 ¹¹	95.00 ⁶	95.19
152+00	93.50	93.55 ¹⁵⁷	92.76 ¹¹	93.76 ¹⁰	94.00
153+04	95.20 ^{250' But wand}	93.10 ¹⁰⁰	93.05 ²⁰	93.15 ¹⁰	93.35 ²

100'S 94.05
200'S 94.50
300'S 92.50
400'S 95.00

F	G	H	I	
91.80 ²	90.90 ¹¹	91.70 ¹⁵⁷	90.80 ²⁰	
91.30 ³	90.26 ¹¹	91.60 ¹⁵⁷	90.90	
91.05 ²	89.60 ¹⁰	91.20 ¹⁵⁷	90.80	
90.71 ²	90.70 ³	88.70 ¹¹	91.00 ¹⁵⁷	20 90.80
90.30 ⁶	88.32 ⁷	90.07 ¹⁵⁷	90.25	
90.00 ⁷	87.63 ¹²	89.84 ¹⁷⁷	89.93	
89.36 ⁸	87.10 ¹²	90.00 ²⁰⁷		
89.06 ⁸	86.00 ⁷⁴	86.20 ¹⁰	89.50	Flow E
90.20 ¹⁰	86.50 ¹⁴	89.42 ²²⁷		Sta 146 to end Tel poles 1' W of E. fence
90.40 ⁶	88.80 ⁹	90.35 ¹⁶⁷	89.95	9070
91.16 ²	90.62 ⁵	90.22 ⁹⁷		
92.80 ²	93.22 ⁹⁷	90.22	96.20 ¹⁸	
94.97 ³	94.60 ⁷	95.05 ¹⁰⁷	95.40 ¹³	22 97.46
95.46 ³	94.80 ⁹	94.84 ¹¹⁷	95.00	BM Cor Stone El 93.13
95.10 ⁴	94.90 ¹⁶⁷	95.10 ¹⁵		
93.83 ⁶	93.52 ¹⁰	93.60 ¹²⁷	93.50 ²⁰	
92.96 ¹⁰	93.16 ¹³	93.05 ²⁰		

Eraction Road

Sta MK Det Con Post E 154
 " " " " " 25'

73+60.8 I.P. R 91°10' $D = 60^\circ$

$$\tan = \frac{5847.5}{60} = 97.46$$

P.C. 72+62.34

PT. 74+4.3 Ext = $\frac{24571}{60} = 40.95$

$$L = \frac{91.66 \times 100}{60 \times} = 151.95$$

1724
 11
 46
 35
 53
 7

Con Post W 15
 Tel 580 E 16.4

80+60.9 I.P. L 94°15' $D = 45^\circ$

$$\tan = \frac{2329.6}{45} = 51.77$$

P.C. 80+09.13

PT. 81+87.44 Ext = $\frac{455.6}{45} = 10.12$

$$L = \frac{44.25}{45} = 98.33$$

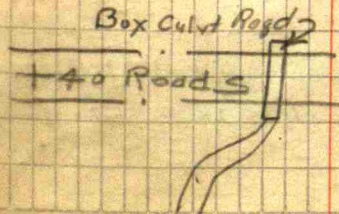
80+60.9
 247.7
 247.7
 650

73+60.8 7E and N. Drive E • 73+60.8 PL E and S

Lern
 E
 V
 E
 N
 E
 T

Joel T Hufford

From Bridge
 Tel poles on
 N side only of
 Fence Line



74

Sta MK Det

83+80.6 I.P. $\angle 27^{\circ} 58'$

D 10'

$$L = \frac{27.967}{10} = 279.7 \text{ Mail Box } 595 \text{ V. } 19'$$

$$\text{Tan} = \frac{1425}{10} = 142.5'$$

$$\frac{175}{10} = 17.5'$$

P.C. 82+37.8

P.T. 85+17.5

86+77.5 I.P. $\angle 4^{\circ} 14'$ D 4'

$$L = 4 \cdot \frac{2333}{4} = 105.83$$

P.C. 86+24.6

P.T. 97+29.4

$$\text{Tan} = \frac{211.63}{4} = 52.91$$

$$\text{Ext} = \frac{3.91}{4} = .98$$

16" Elm N45' W 37.5'

10" Walnut N45E 32.4'

83
074
13.2

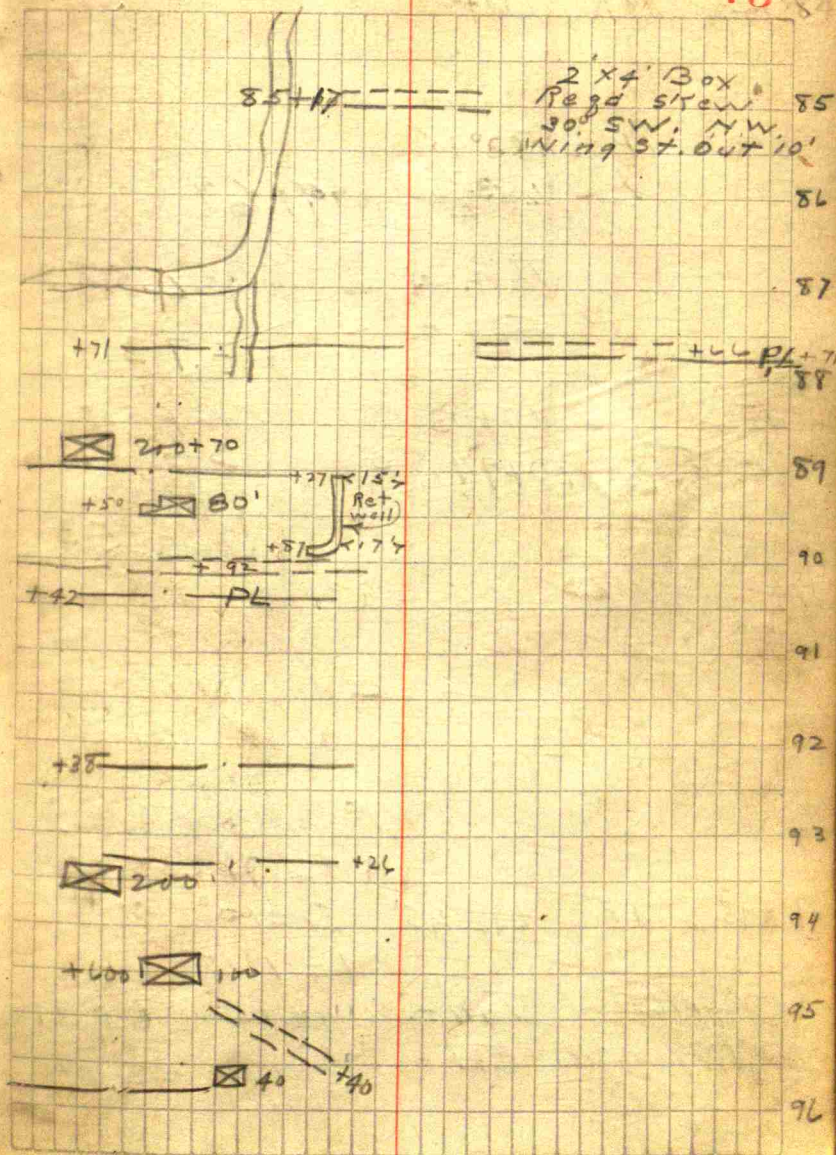
16" Syc N35°W

20'

595 V.

19'

75



76

Sta MK Def

90+49 I.P. R 3°40'

$$L = \frac{3.6667}{4} = 91.67$$

$$\text{Tan.} = \frac{183.00}{4} = 45.82$$

$$\text{Ext.} = \frac{2.93}{4} = .73$$

$$\text{P.C.} = 90+03.18$$

$$\text{P.T.} = 90+94.85$$

Cor Post
S - 17'8" Walnut
N 85° E 538" Maple 31.5
N 40° W
10" Apple S 50° W

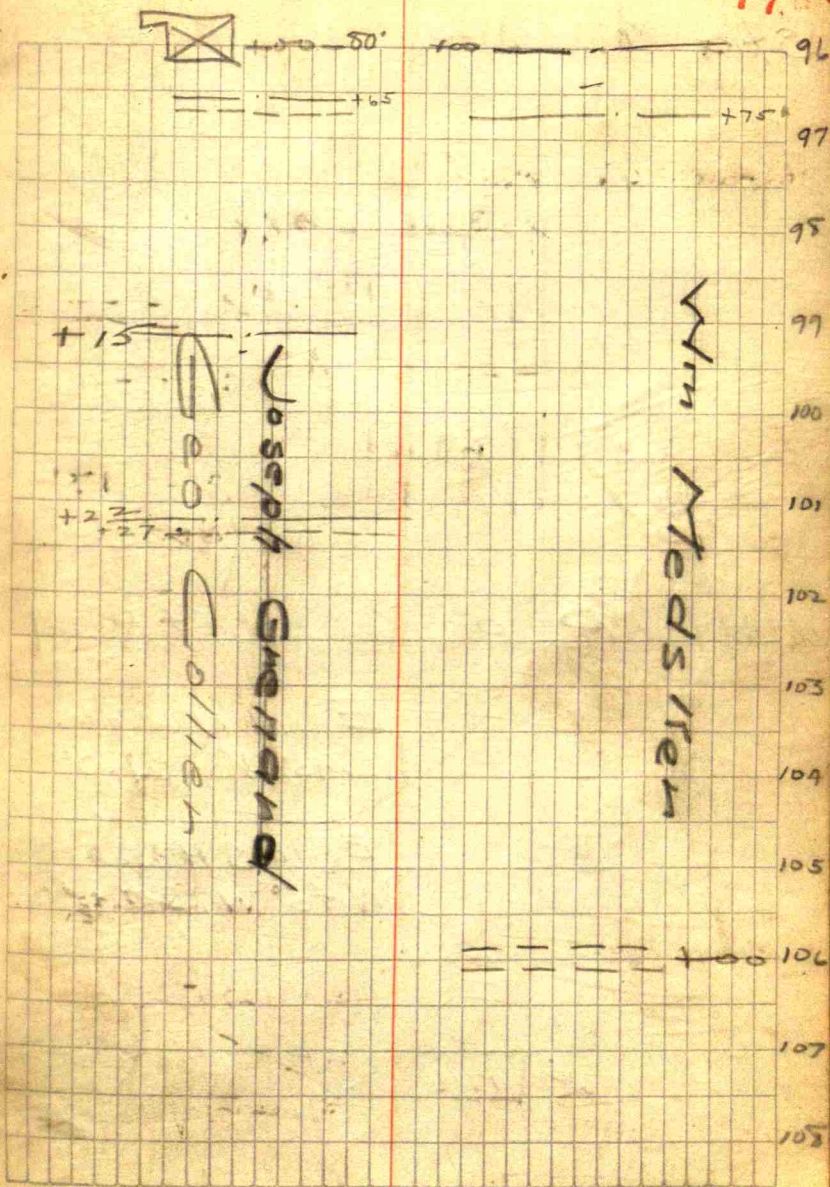
96+75.2 I.P. L 12°45' D = 10° 41.2'

$$L = 127.5$$

$$\text{P.L. } 96+15.1 \text{ Tan} = \frac{640.15}{10} = 60.01$$

$$\text{P.T. } 97+42.6 \text{ Ext} = \frac{356.5}{10} = 35.6$$

77

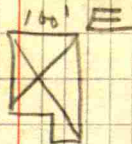


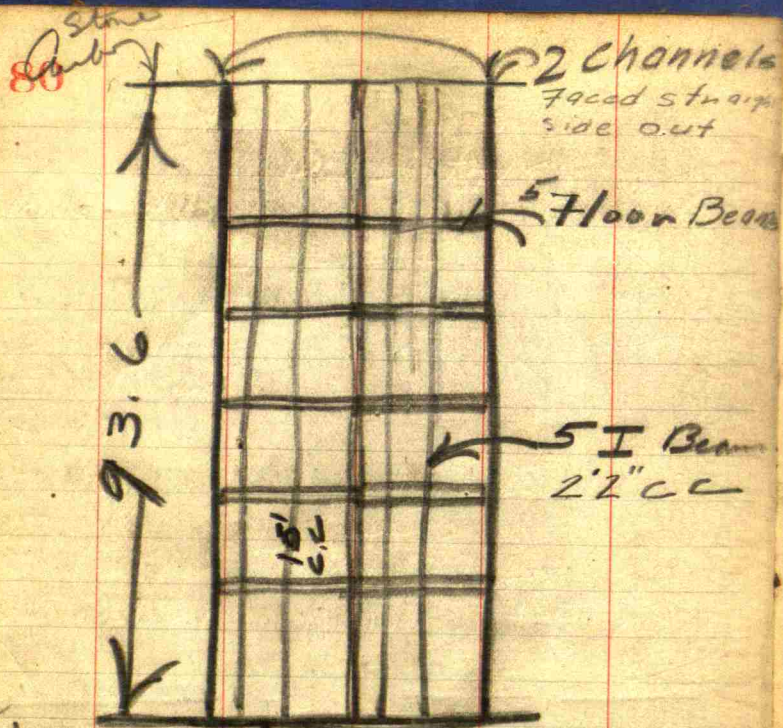
Sta Mark Def.

114+74 1P 0° End of Road

E end N Header
S45W 21.0'E end S Header
N45°W 20.6'

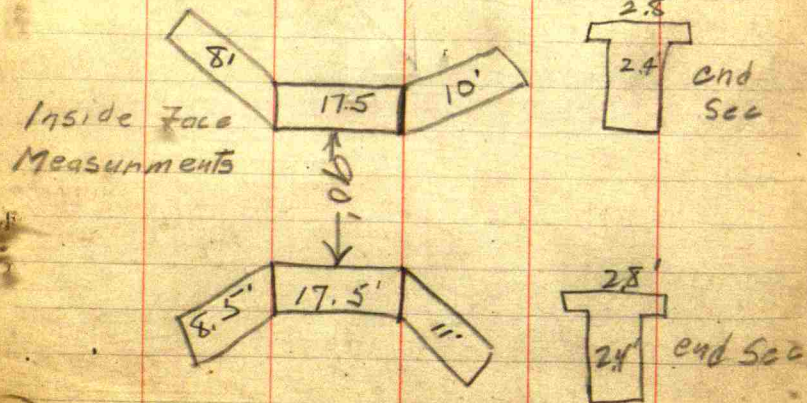
Sta 114+74 Road X+S





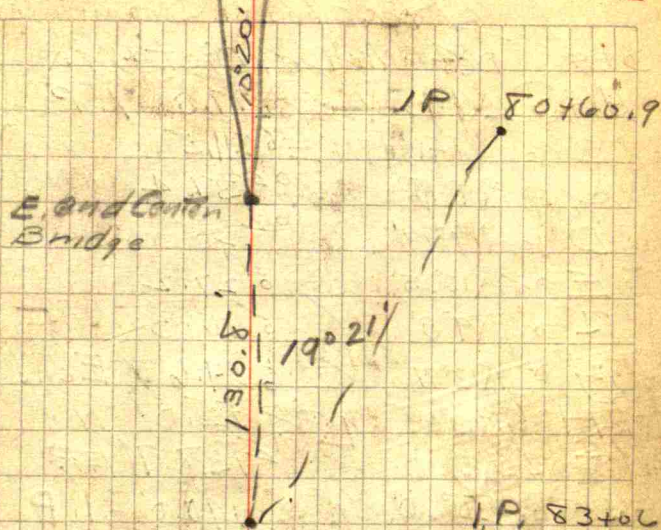
Stone
Curb

Maximum width
Floor 13.8'

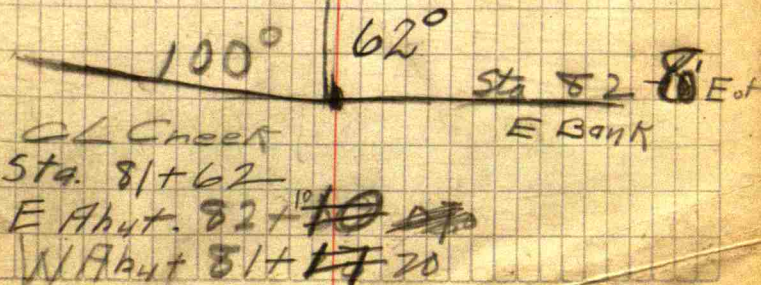


Wend Center
Bridge

31



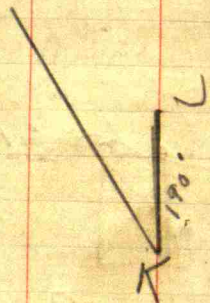
E Bank 81+92
W " 81+32
Width Water 60
way on E



Location Springtown

Sta	Def	Needle B.	Dist	MK
A+000	L 6°	N 20° 45'	79.8	I. P
B	L 6° 41'	N 14° E	211.5	
C	R 11° 18'		37.4	
D	1/2 R 17° 17'		40.0	
E	1/4 R 15° 25'		27.2	
F	1/2 R 9° 8'		16.3	✓
G	1/2 R 12° 11'		24.6	End Bridge
H	1/2 R 13° 35'		55.0	W "
I	1/2 R 5° 20'		138.7	
J	L 8° 20'		190.0	I. P
K	0° 00'			

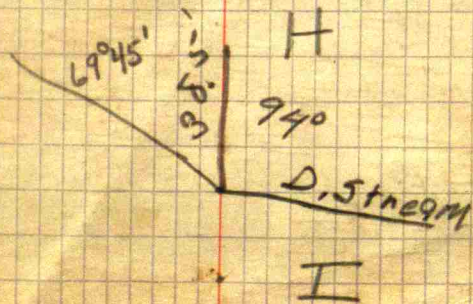
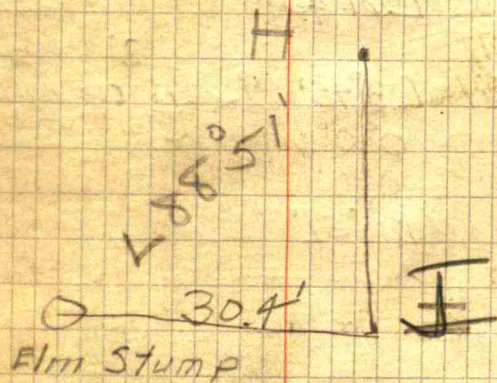
con post
N 10° W 17'
30mc
5134'



Bridge



Center



New Location

Sta	Mark	Def	Dist
0+00	A (J)	IP	
0+75	stake	E	0° 0'
1+44	stake	E	0° 0'
2+04	stake	E	0° 0'
2+24	"	E	0° 0'
2+34	"	E	
Pl. 2+44	"	E	0° 0'
Pl. 2+89	B spike	L	61° 43'
Pl. 3+25	21 Nail		
Pl. 3+80	21 Nail	L	3° 45'
4+50			0° 0'
5+00			0° 0'
5+95	9 (A)	R	10° 52'

Stake N 25° 90°
 11' N Cen Elm Stump
 inside face
 W Abutment

inside face
 E. Abutment
 at E

About 2' W &
 old Road

3' W & old Rd

← 10' Cedar N 30° E
 31' St W 25°

Stake N 90°

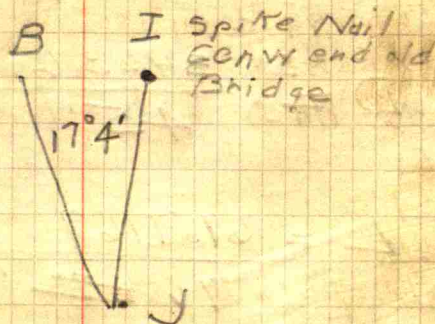
Stake N 90°

St E on E 33'

St 25° W 90°

"

"



Sta

2+89

$$\Delta = 61^{\circ}43'$$

$$\tan = 45'$$

$$D = \frac{3423.6}{45'} = 76^{\circ} \overline{175}''$$

$$L = \frac{61.7167}{76. \overline{08}} \times 100 = 81.21$$

$$\text{Ext} = \frac{944.9}{76} = 12.43'$$

Chords 10'

Dist 22.8' per 1' of Arc -

per 10' Arc = 3°48'

10' 3°48'

20' 7°36'

30' 11°24'

40' 15°12'

50' 19°0'

60' 22°48'

70' 26°36'

81.2 30°52'

$$R = \frac{5730}{76} = 75.4'$$

Sta

200' W 0

100' W 0

0+00	²⁵ 94.10	²⁰ 94.95	¹³ 95.73	⁸ 97.14	99.65
0+75	¹⁵ 95.85	¹⁵ 96.02	⁵ 95.45	¹ 95.29	98.00
1+44	¹⁹ 94.50	¹⁹ 89.05	¹² 91.70	⁶ 92.46	97.46
1+51					91.31
1+59					86.90
1+69					85.22
1+80					85.95
1+85					88.40
2+04	²⁵ 89.40	¹⁵ 91.15	¹⁰ 91.20		91.92
2+24	¹⁵ 93.00	¹⁵ 93.48	⁹ 93		93.50
2+34	¹⁵ 94.90	¹⁵ 94.88		⁴ 99.90	103.15
2+44	²³ 96.34	¹⁷	¹⁶		109.25
2+54	²⁵ 96.70			⁶ 112.29	110.29
2+64	³² 96.75			⁹ 113.87	111.68
2+74	⁴³ 95.55			¹⁵ 114.46	111.20
2+84	⁴⁸ 96.35	²⁰ 114.39			110.01
2+94	⁵⁰ 96.75	³⁰ 119.33	²⁵ 116.06		109.03
3+04	⁵³ 95.35	³⁵ 117.47	²⁰ 115.66		110.05
3+14	⁵⁶ 96.40	³² 118.90	²⁷ 115.50	⁵ 110.40	110.86
3+25.21	⁶⁰ 95.55	²⁵ 116.85	²⁴ 115.50	⁷ 111.02	111.65
3+80.21	⁵⁵ 116.65	²⁵ 115.61	¹⁵ 113.67		114.43
4+50	⁵⁰ 92.00	²⁶ 114.75	²⁵ 113.60	¹⁵ 112.05	112.56
5	⁵⁰ 92.00	²⁵ 110.50	²⁰ 110.85	¹⁵ 111.32	110.80
5+75.1		²⁰ 110.05	¹⁵ 108.90		109.45

±

09

BM

E1.100.00

AT \textcircled{I}

9	¹³ 97.22	²⁰ 96.65	¹⁸ 96.18		
93.71	¹³ 96.35	¹⁸ 97.70	²⁵⁴ 98.04	³⁵ 97.69	
91.37	¹⁵ 91.15	²⁰ 90.03			87.85
W Bank					
Wedge Creek					
C. Creek, Bed St					
E. edge Creek					
E Bank					
¹⁰ 92.15	²⁰ 91.50		²⁵ 91.39		
¹⁰ 98.70	¹⁵ 101.30		²⁵ 101.00		
¹⁰ 102.00	¹⁵ 102.95	²⁰ 102.20	²⁵ 103.50		
¹⁰ 106.50	¹⁵ 105.15	²⁵ 103.29			
¹⁰ 109.50	¹⁴ 106.60	²¹ 104.60	²⁵⁴ 104.69		
¹⁴ 105.34	²⁵⁴ 105.67				
¹⁰ 106.61	²⁰ 106.86	²⁵⁴ 106.66			
⁶ 107.83	¹⁵⁴ 108.11	²⁵ 106.80			
¹²⁴ 109.20	²⁰ 108.26	²⁵ 108.61			
⁷⁶ 110.12	¹⁸ 109.94	²⁵ 109.80			
⁴² 110.44	¹⁰ 109.55	²⁵ 111.70			
³⁴ 111.70	¹⁷ 110.10	²⁵ 112.55			
¹⁵ 113.76	¹⁵ 117.56	²⁰ 119.60			
¹ 112.65	¹⁵ 111.60	²⁵ 111.00			
¹⁰ 110.35	¹⁵ 109.10	²⁵ 108.00			
¹⁰ 107.95		²⁰ 106.00			

① Elm St

74x55

094.24

0103.46

BM

ET

I.P. \textcircled{A}

Sta ϕ

A+100 110.20

A+200 111.00

~~2nd alternate Route~~

a. (J)

B. 15 S. rail

5+10

inside face

5+21

W. Bank

560

E. Bank

5+70

inside face

6+12

P.L.

6+65.6

I.P.

D&L 70 old ϕ

32.07

7+19.2

P.T. on Tan
and on ϕ old
LocationPt. 7' S of
at A orig
location - on
 ϕ old locationP.I. Sta
3+80. old
location

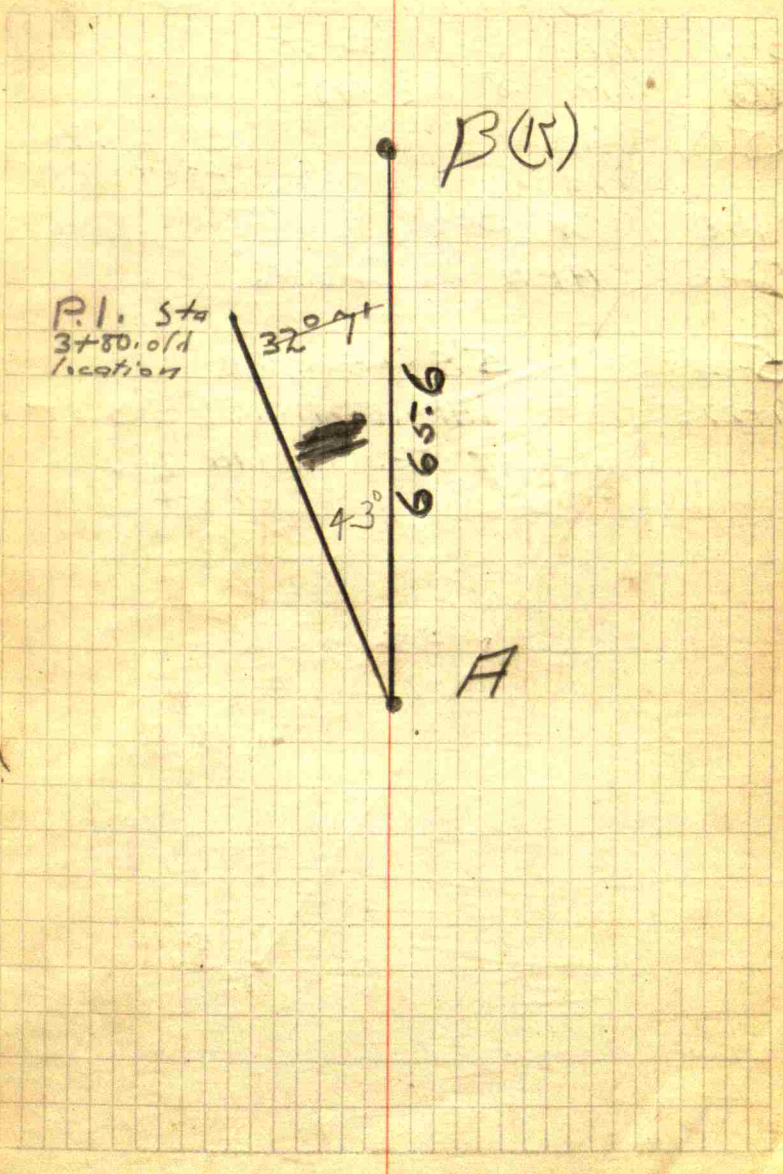
32° 47'

9.599

43°

A

B(15)



Alternate Location.

Springtown Bridge

Sta MK. Def Dist
 A① I.P. 8° 20' 190'

(B)(K) Spike

Beq pt. New
 Location

4+95 W. Bank.

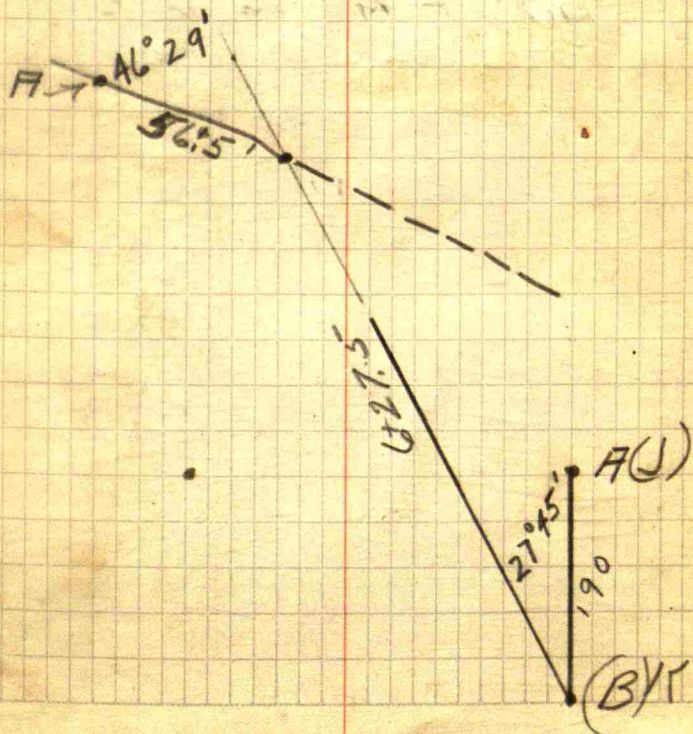
5+00 A+W edge Creek.

5+40 S.E. + E. Bank

6+27.5 Pt. intesection 56.5'S of
 I.P. at A. on old $\frac{1}{2}$

See p. 118

Vine covered
 pole N30E31
 Stakes A + Δ New
 Location N20' A+7.
 S12' A+7.



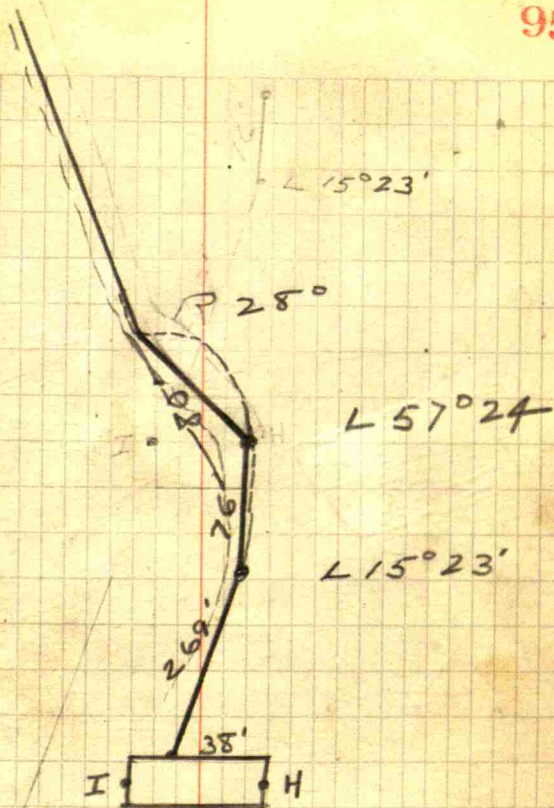
Springtown Buds

Sta.

Cen. L.

1+00	97.22
2+00	97.59
3+00	98.46
3+50	99.43
4+00	99.88
4+30	99.91

100.88 Hub Guard at Crown
 100.02 Arch at Crown



Survey for Streets Park + Lincoln Ave Extensions
Brownsville

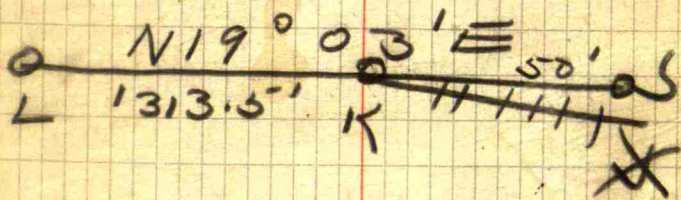
Sta Def

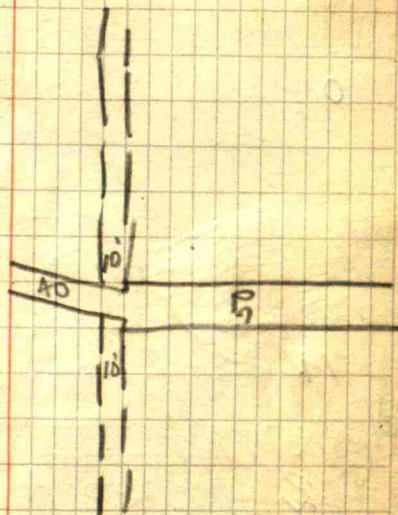
0+00 L7°29'

J Manks in line on Walk

K " " " " "

L 12" Sugar N70°E 23'
20" Elm S50°E 27.8'





100

S Bdry

Sta

0+00

0+10

3+30

8+80.4

N Bdry

Sta

0+00

0+146

St

5+81.5

8+68

S Bdry intersects @ Green St
42.7' Not J. Δ intersection $114^{\circ}26'$

Park Ave.

Brownsburg

114

Fence line

" "

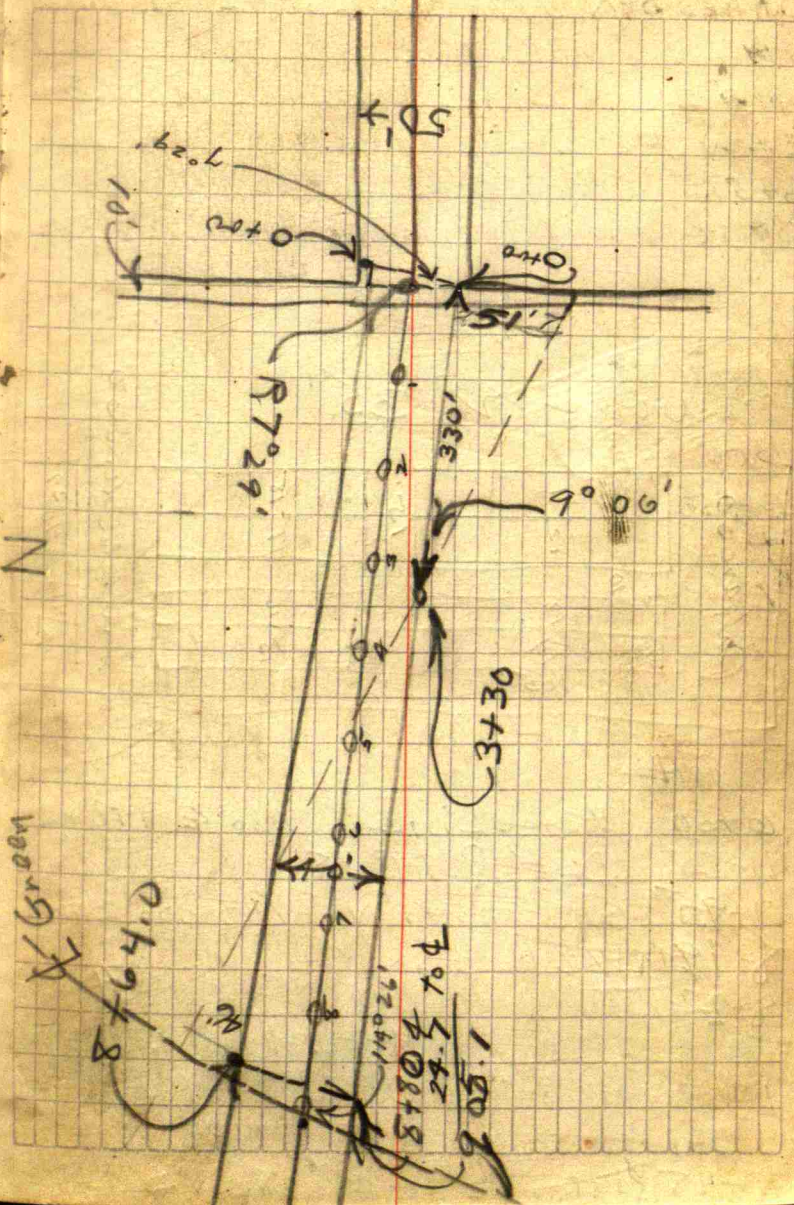
Side walk and Prop
Line

Fence Line

" "

SWK.

101



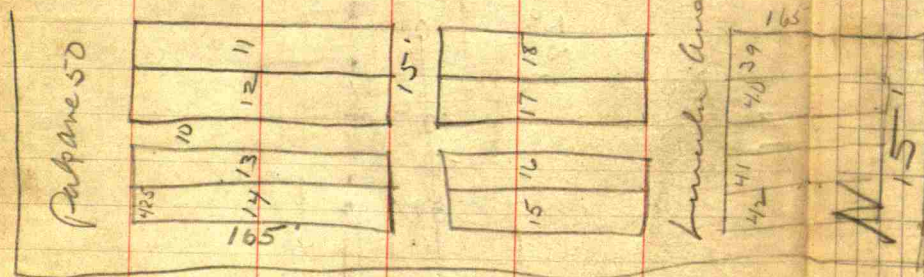
103 Lincoln Ave
Boundary

0+00 S'N NW Con Lot 42 Johnson
+ Hughes Addition.

0+13 Fence Line which is 16.5' S of
E+W Fence

6+57.5 N+S Fence on Tan which
pt is 22' N of Line Fence E+W

work at 35'



⊕

6+50 Fence Line. Also ⊕ at 6+50

6+50 Def R. $19^{\circ}38'$

7+95 Gate at pt 1' N of NE con Barn

8+17 NW Edge Barn

8+25 Stakes 9+27 NE end House 4' SE

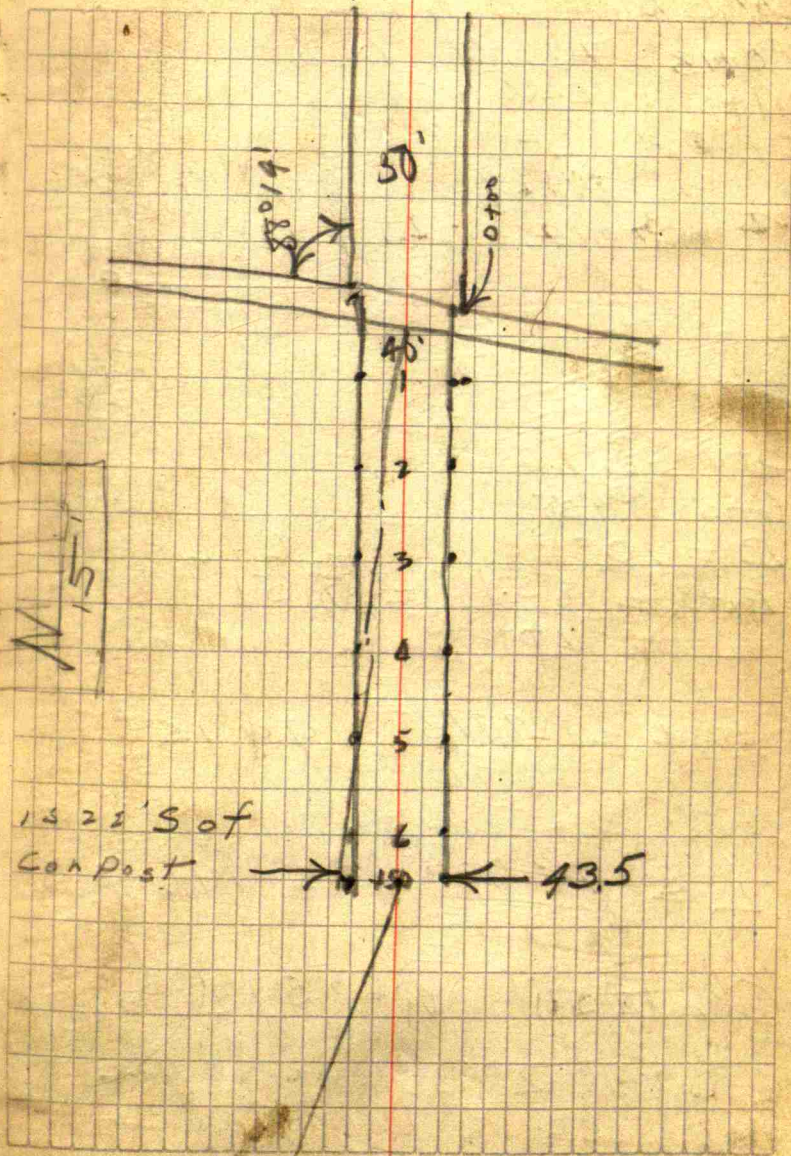
9+25 Stakes 9+41 NW end H. 11' S of ⊕

10+00 Stakes 9+37 House 11' S of ⊕

10+27.7 " at E Edge EWR

10+48 Inter. ⊕ Green 283.7' S of K

103



N Bdry

0+13 Fence line

7+01 E+W Fence

Sta

6+50 R19°38'

D = 10°

$$\text{Ext} = \frac{85.1}{10} = 8.51$$

$$\text{Tan} = \frac{99.15}{10} = 9.915$$

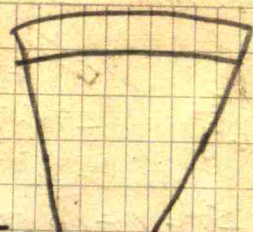
$$L = \frac{19.633}{10} \times 110 = 196.33$$

Chords 50' R = 573'

Def = 2°30' per 50' arc
or 3' per Ft arc

PI 6+50

$$\begin{array}{r} 99.15 \\ \text{PC } 5+50.85 \\ 1 \quad 96.33 \\ \hline \text{PT } 7+47.18 \end{array}$$



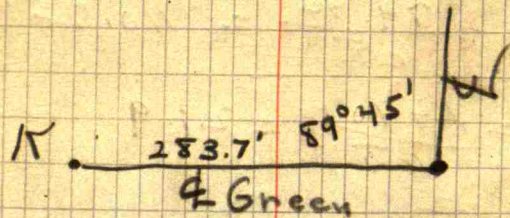
$$573 = 50 = 593' X$$

$$573X = \frac{29650}{3500} = 51.75 \text{ O}$$

48.25 I

$$573 = 60 - 593' X$$

$$573X = \frac{6211}{57.9} \text{ O}$$



106

H. C. Jordan

Sta. Mark. Det. Dist.

P₆ 8700O+64.6 Stone L74°57'
at. P.I.

PT = Sta 91 + 10.2

Δ 74°57'
Tan 65' Approximated

$$D = \frac{4392.8}{65} = 68^\circ$$

$$\text{Tan} = \frac{4392.8}{68} = 64.6$$

$$L = \frac{74.95}{68} = 110.2$$

$$\text{Ext.} = \frac{1490.1}{68} = 21.9$$

Con Post

S 64° E

35'

Con Post

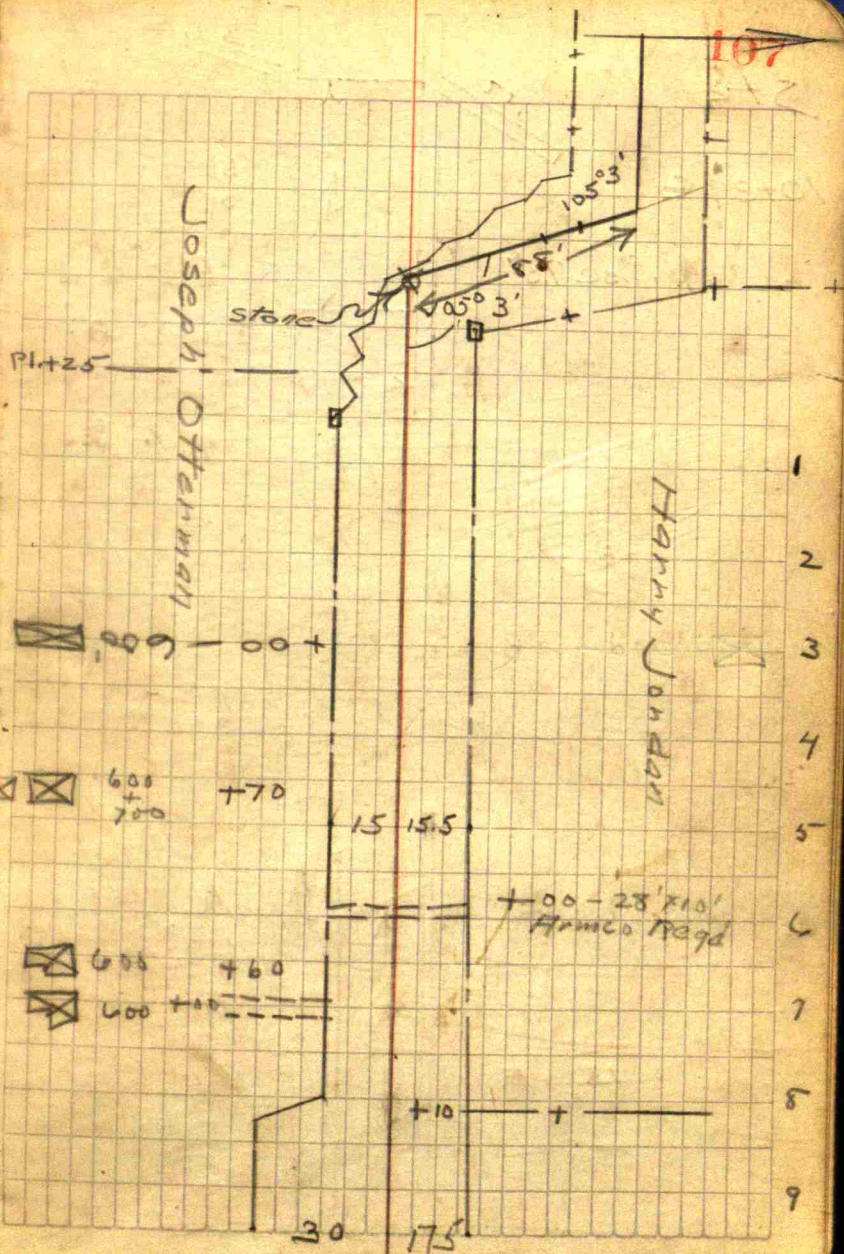
N 39° E

19.5'

Tel. poles

13' 5 1/2"

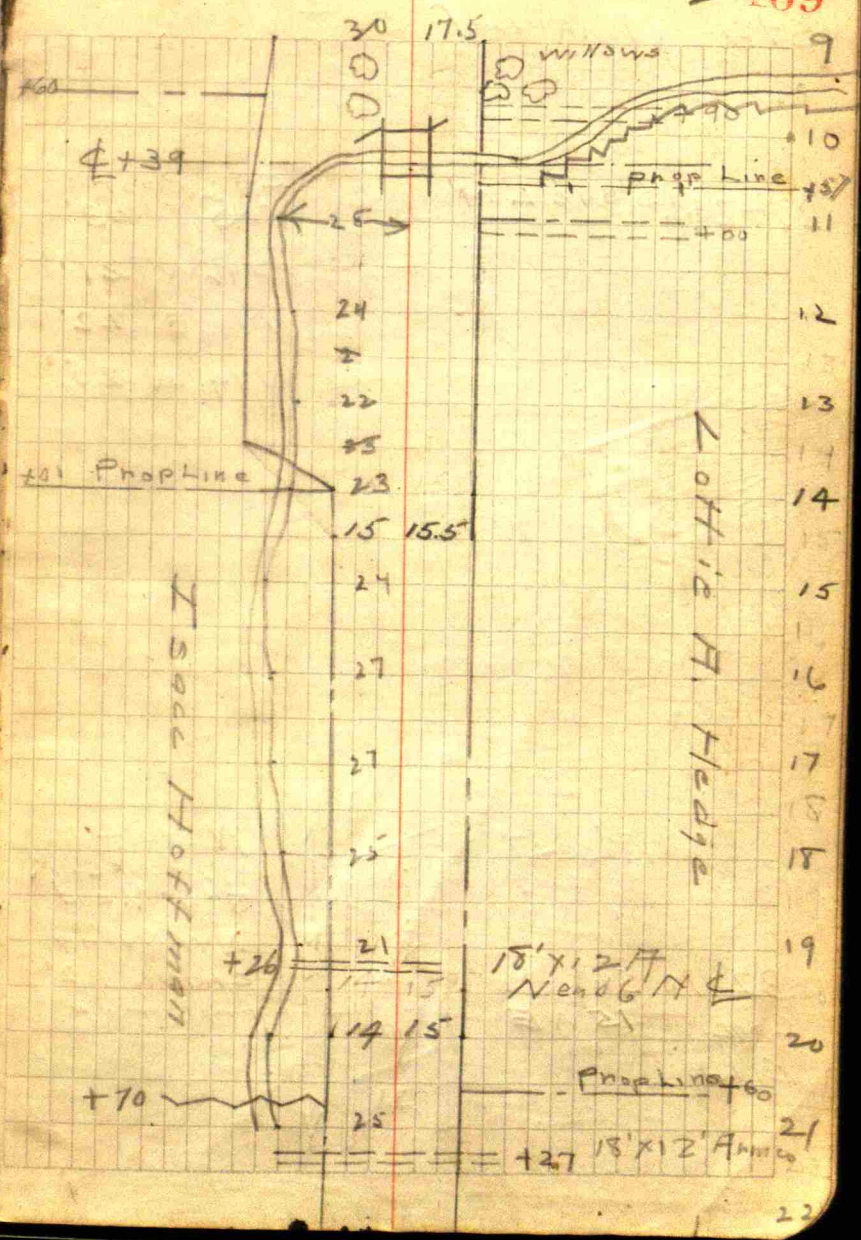
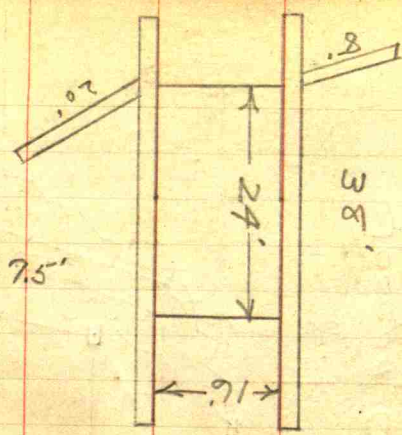
Spaced 200'



Sta

10+39

Rise 7.5'



110

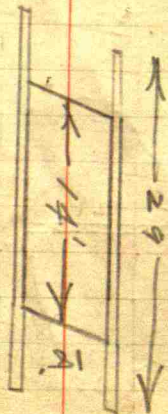
Sta Mark Def Dist

27+24.4 Stone L 19'

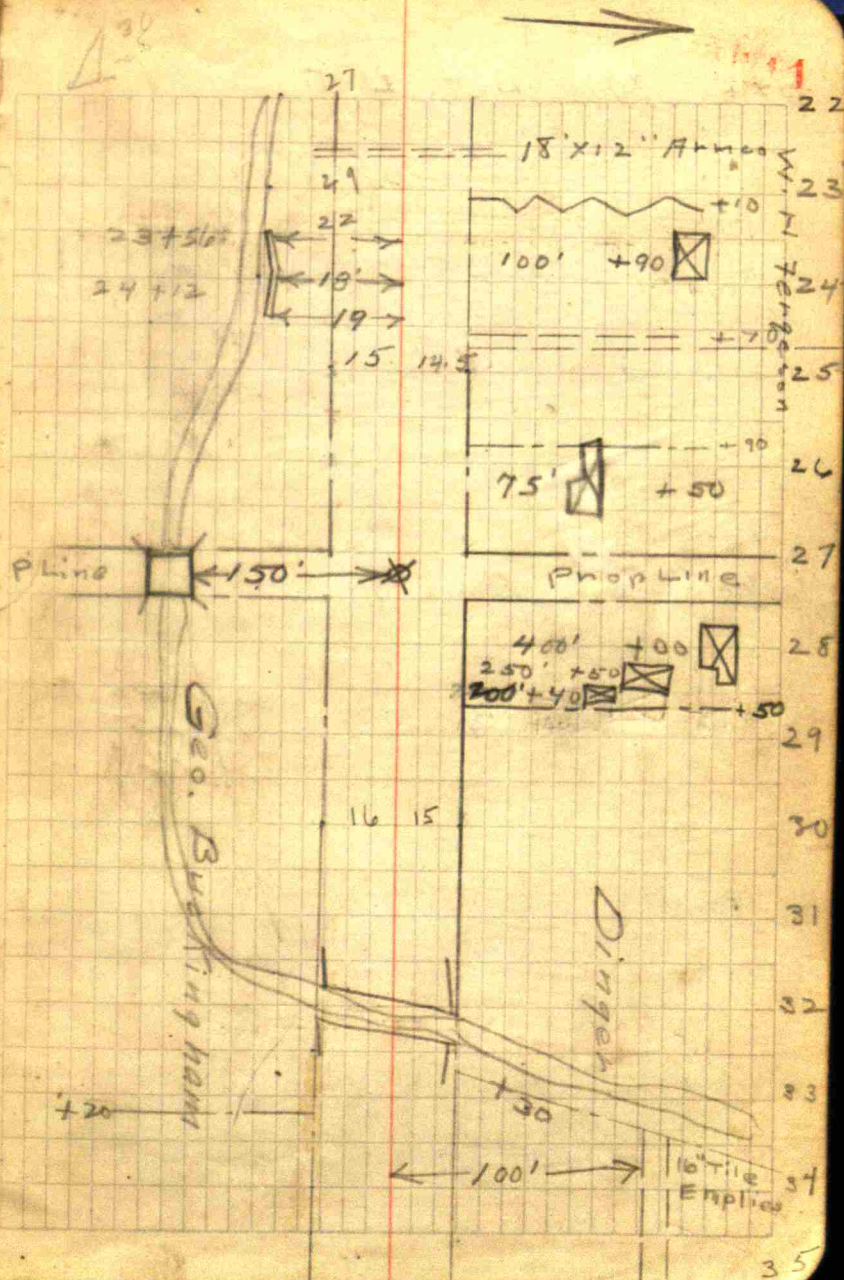
Cor Post
 S45°E 23'
 S46°W 21'
 N46°E 22'
 N41°W 25'

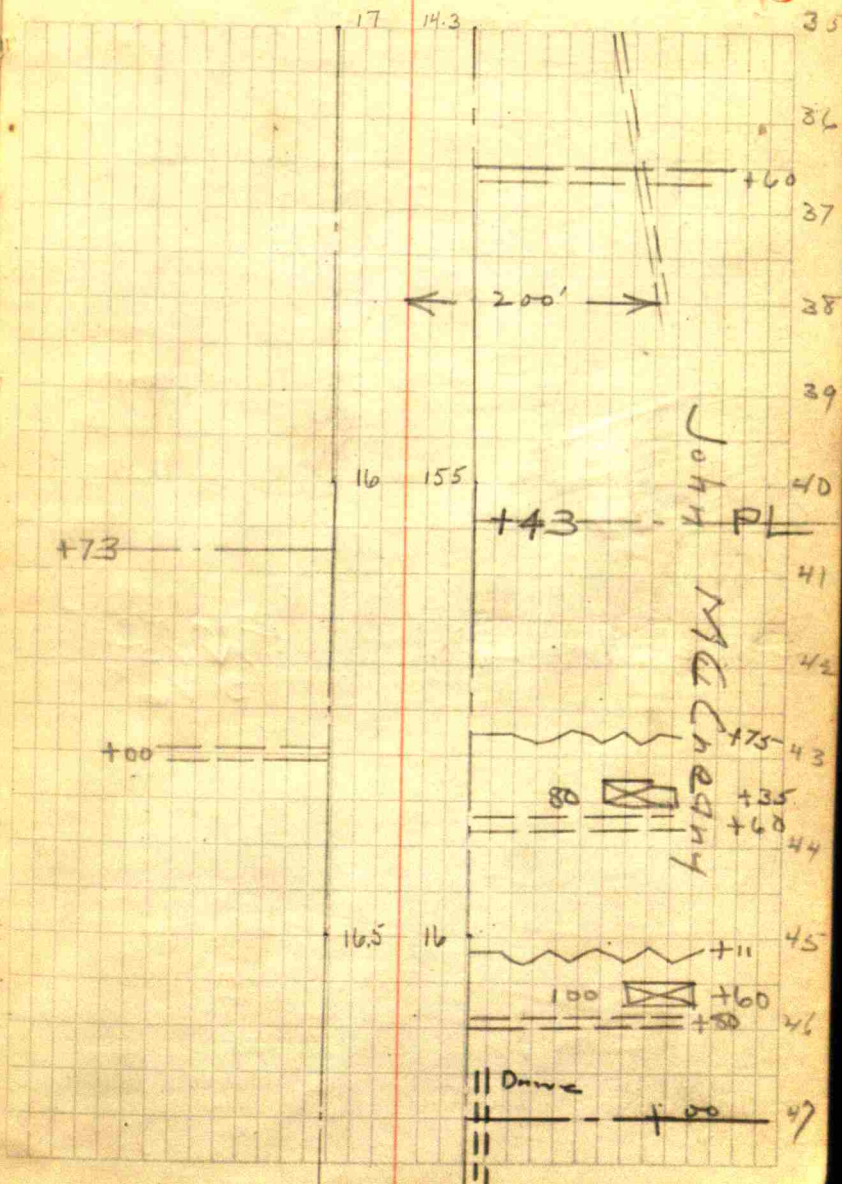
Rises'

32+10 Skewed
 Cork. 15°NE
 Culvert



N Half
 W. Abut sunk
 8" at N. end
 NW wing
 Chacked 2'
 from top





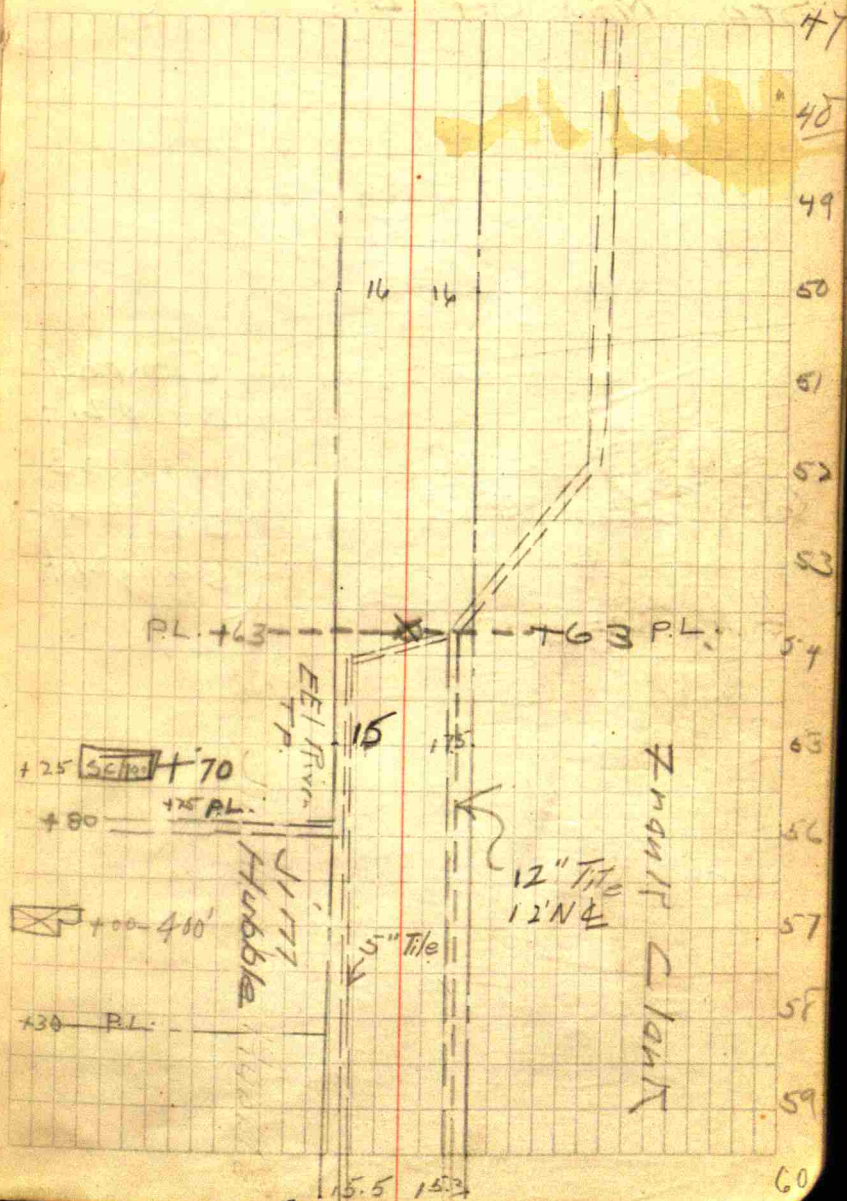
114

Sta Mark Det Dist

53+63 Stone L'06'

Cor Post
N 15'
S 16'

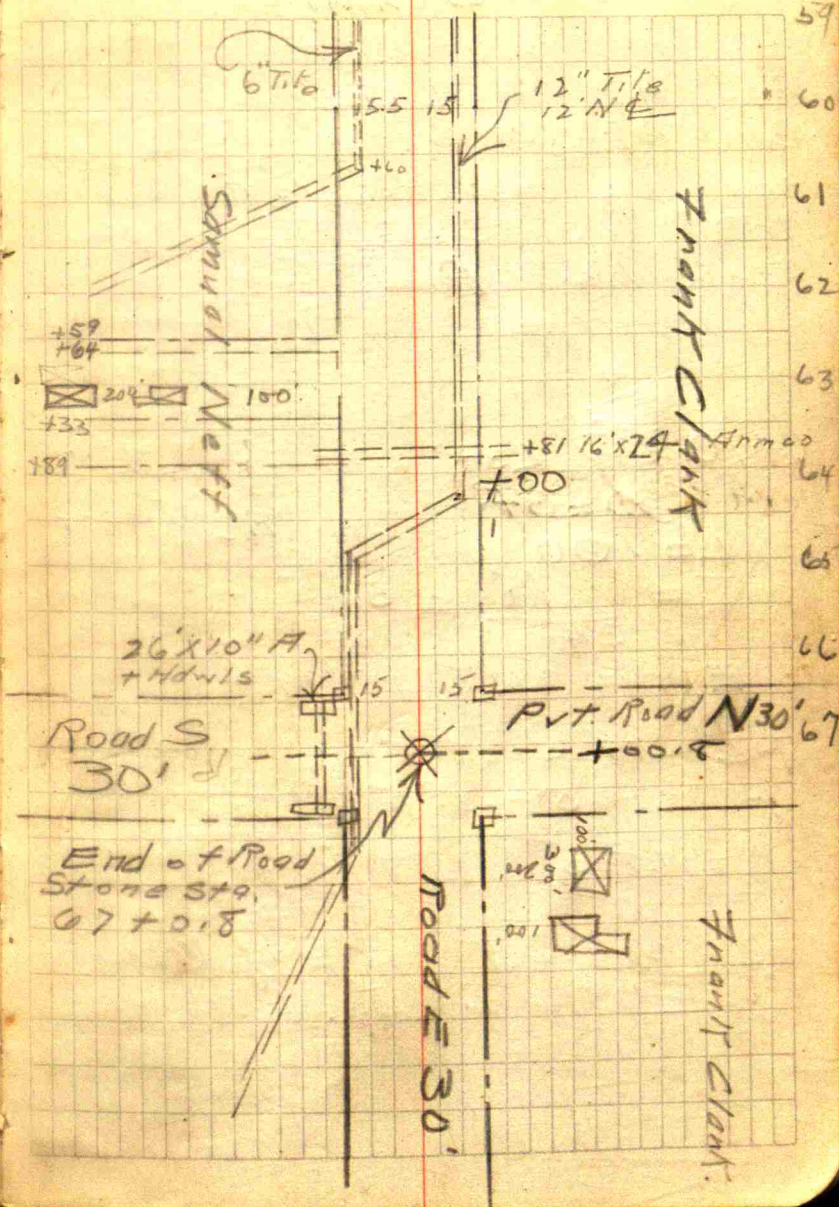
115



Sta	Mark	Def	Dist
-----	------	-----	------

67+0.8 Stone End

Cor Post
N45W 21.4
N45E 23
S45E 22
S45W 21.4



Final Relocation

Spring Town

M/K Det Dist
 A(J) l.p 8°20' L 152.6'
 B(K) Spike L 31°12' St at L 514' at
 4+61 Inside face W Abt. 1's of fence. Fence
 4+70 W. Bank Creek Tel. pole at L 119
 5+21 Inside face

6+10 P.T.
 spike L 34°
 D = 34°

$$L = 100$$

$$T = \frac{175.8}{34} = 51.5$$

$$Ext = \frac{261.8}{34} = 7.99+$$

PL Sta 5+58.5

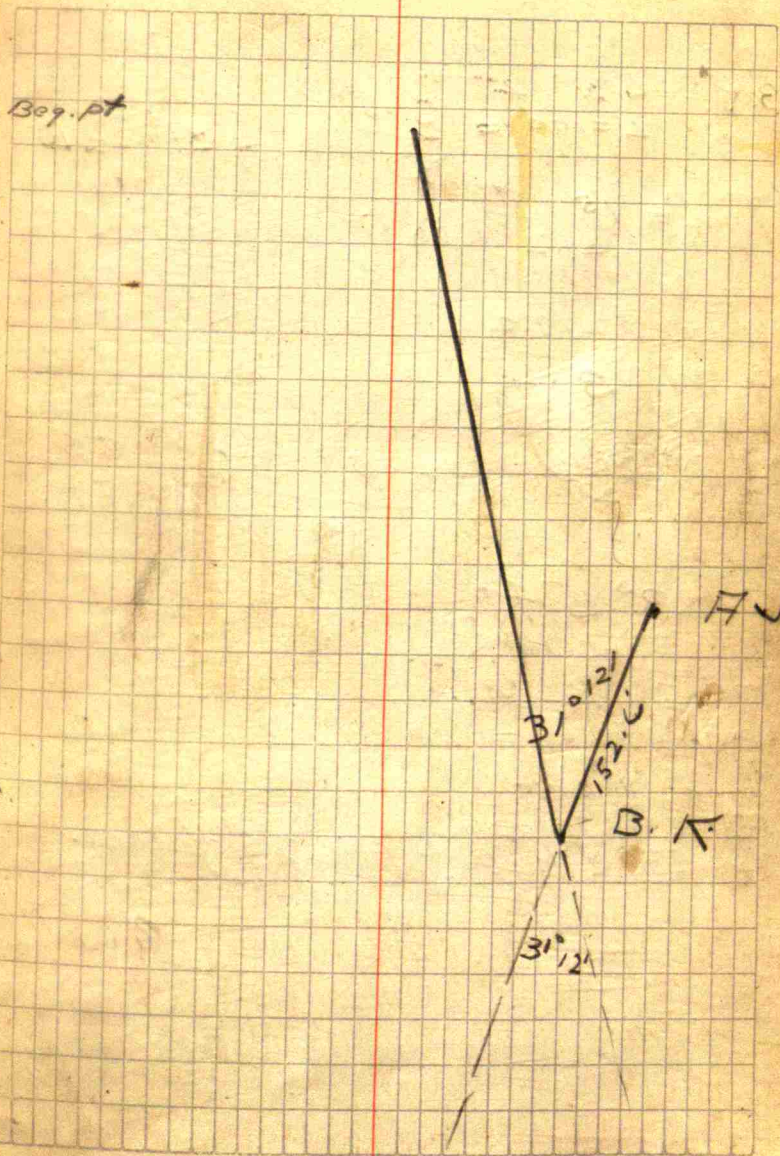
PT Sta 6+58.5

$$R = 168.5$$

(B) is 612.7 feet E of l.cen
W of NW 4 Sec 35.

Stakes on Radius
 28' W + 14' E
 These stakes
 are on boundary
 lines

190
 37.4
 152.6



$$BK \quad \Delta 31^{\circ}12'$$

$$L=100 = \frac{31.2}{D} \times 100 = 31^{\circ}12' = D$$

$$\text{Tan} = \frac{1599.8}{31.2} = 51.3$$

$$E_x = \frac{219.2}{31.2}$$

$$\frac{31.12}{2} = 15^{\circ} 36' \quad 4 \overline{) 216} \begin{array}{r} 180 \\ 36 \\ 54 \end{array}$$

$$3^{\circ} 54'$$

$$\frac{12^{\circ} 60'}{4} = \frac{216}{36} = 3$$

$3^{\circ} 54'$ def per 25' of arc.

122
Sta

Levels

±

0+00	20 97.20			98.65
1+00	20 N 96.10			96.20
2+00	20 96.00			95.85
3+00	20 96.00			96.05
4+00	20 95.55			94.33
4+61	20 93.36			93.45
4+80	10 of stream 86.10			86.46
5+05	← Stream			85.00
5+13	20			89.73
5+21	20 86.00	10 91.63		92.76
5+40	20 94.53		13 96.51	95.30
5+50	30 94.16	20 96.40	18 96.51	100.39
PL 5+58.5	40 97.95		5+70 101.30	104.97
5+80	Edge Bank 40 112.40	22 112.06	8 109.30	112.50 111.20
PI	20 111.20	12 110.93	109.30	109.85
PT	40 110.40		109.30	109.26
7+00	20 110.40		109.70	109.52
8+00	20 111.70		111.20	110.60
9+00	40 111.90		111.40	111.05
				111.60

94.88

105.59

123

BMEI
100.00
Bridge
Floor.

	20 98.65			98.65	✓
	20 96.10			96.10	✓
	20 95.80			95.80	✓
	20 95.90			95.90	✓
	20 94.50			94.50	✓
91.78	16 86.16	←		94.46	✓
92.00	20 92.46			92.46	✓
					✓
	15 92.97			22.5 96.30	✓
				101.76	✓
				20 107.95	✓
				30 109.50	✓
				40 112.10	✓
	16 112.72			25 110.36	✓
	12 110.45			40 111.35	✓
	8 109.76			20 110.86	✓
	20 109.90			30 110.30	✓
	106.20			40 106.16	✓
				40 107.70	✓
	20 107.60			40 104.10	✓
	20 106.30			40 105.00	✓
	20 105.30			40 103.60	✓
				40 103.00	✓
					3M 109.46

Exc 3877 Cu Yds @ 25 = 969.25
 1036 " " Borrow = 259.00
 Gravel 2233 Cu Yds @ 3.00 = 6699.00

Culverts
 New

26' X 10" @ 1.25 = 32.50
 40' X 12" @ 1.40 = 56.00
 10' X 18" @ 2.00 = 20.00
 Old pipe Reland

26' X 10" @ 20¢ = 5.20
 30' X 12" @ 20¢ = 18.00
 16' X 18" @ 25¢ = 4.00

Cu Yds Concrete / Hdrnk

31.1 @ 9.00 = 279.90

Tile drains

8661' X 6" in place = 787.50
 @ = 525 Rds @ 1.50

Sub Total 9130.15

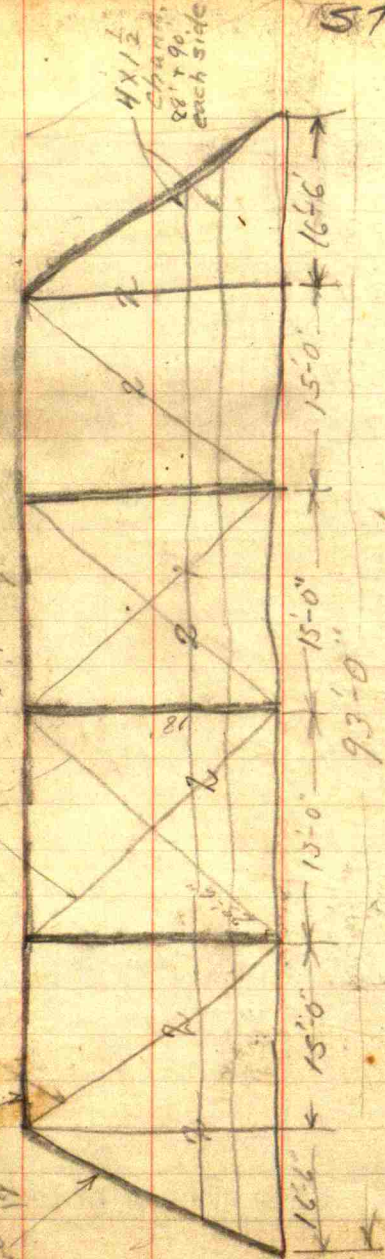
Profit including 1869.85

Cont, Ins, Foreman \$11000.00

\$10,500

67
 50
 3350
 223340
 5
 2/67
 22

Steel Bridge

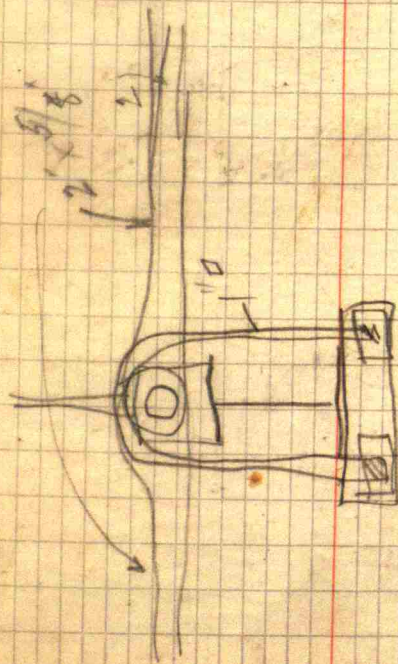


Cover all width 16'-0"
width of roadway 14'-0"

at Sta. 80+20 (approx)

Graham Rd.

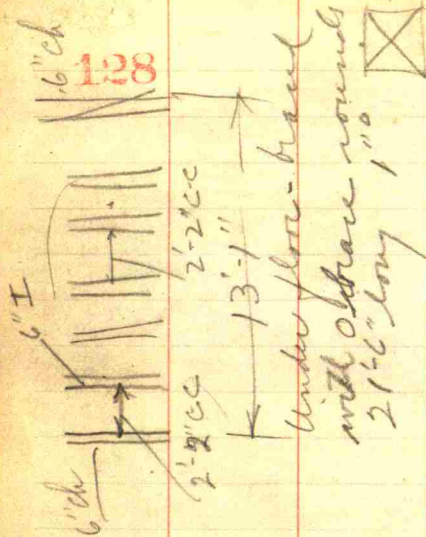
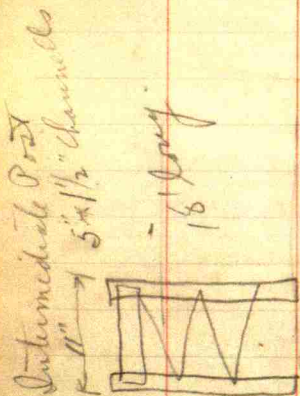
notes for reconstruction.



Present Steel Bridge

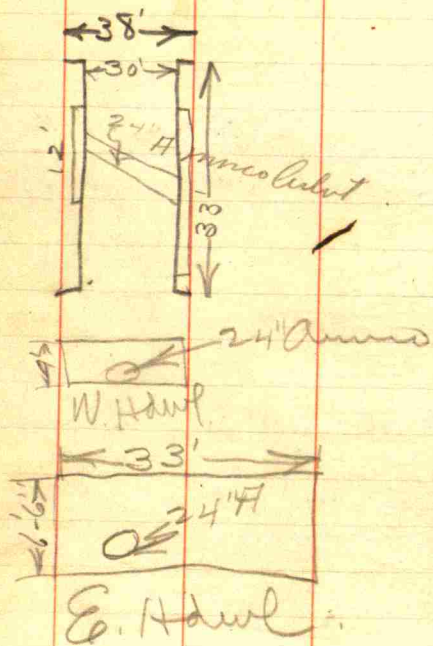
3 Tq. 80 res - Graham Rd

129



I-beams
 1-0 x 16-0





132

STILESVILLE BRIDGE

Clear Span 85'

Overall Length 91'

Clear Roadway 13'-8"

5' Floor Beams 6" x 18" ~~Plank.~~

6 spans 15' c-c.

8 Floor Joists 12" x 3" Lap 2'-0"

2 Handrails each side 8" x 2" Plank.

Floor Joists - 2 outside ones

2' c-c Others 1'-9" c-c

Abutments 3' Thick.

For Block Floor

$$\begin{array}{r} 60 \\ 32 \\ \hline 92 \end{array}$$
 Road # 60 - Sec. 7

$$\begin{array}{r} 31 \\ 60 \\ \hline 91 \end{array}$$

134

Baker Bridge on

W. Fork Whick Creek

Clear Span 75'

Overall Length 79'

6 spans 13' c-c.

5 Floor Beams 13' c-c. (12" x 6")

9 Floor Joists Lap 2' (3" x 10")

1 Hand Rail each side 2" x 4"

Width of Clear Roadway 15'-4"

(at intermediate posts)

Width at end posts 15'-10"

Pittboro-Danville Rd. at
ne cor. of Danville.

135

Rd. # 4 - Sec. 14.
For block floor.

136

Pecksburg BRIDGE

July 9, 1921

Clear Span 86'

Overall Length 90'

Clear Roadway 16'

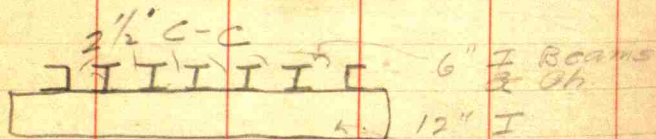
6 chords 15' each

5 Floor Beams - 12" I Beams

Handrails OK 4" channels

Floor Joists made up of

5" I Beams & 2" channels

just west of Pecksburg on
Clayton - Amos Rd. - Top. Rd. 137

JULY 13, 1921

5 chords 15'-0" c-c

4 floor beams 15" I's

6 f I's 2'-2" c-c

2 channels 2'-0" c-c

channels to be reversed

Nailing strips to be on

outside of channels

Clear Span 71'-0"

Overall 76'-0"

Clear Roadway 15'-8"

2-4" channels each side for
handrails - one new section
reqd. 4" channel 15'-0"

Maximum width of roadway 15'-11"

142

LIZTON BRIDGE

JULY 13, 1921

HARRY
STEARNS

PONY TRATT TRUSS Stowel
 about 30° 0'
 5 I-Beams Floor Joists 27'-6"-C
 7 Floor Beams 8" x 15" E-I
 2 channels 7'-0" C-C
 3 chords - "A-B" 17'-0"-C" + 2 - 16'-0" + 2 - 9' 11"
 Maximum width 13'-8"
 Clear Roadway
 Handrails 2-2 1/2" laticed 10' apart
 Stone curbs 52'-0" apart
 Clear Span 47'-0"
 Overall length 50'-0"
 Handrails O.K.

8 | 44.15'

40

4

60

255

2 | 98.33

24.6'

5° 32'

143

5° 32'

5° 32'

11° 04'

5° 32'

16° 36'

5° 32'

22° 07'