



DALE BORD

143

DALE BORD

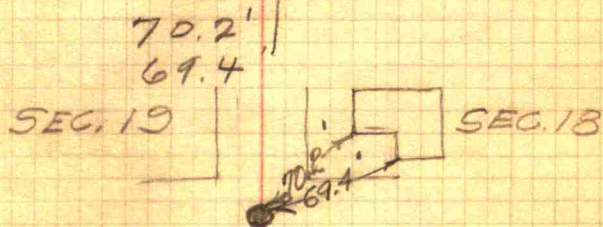
1863 A

Sum C.W.

321.5
293.0
28.5

T17N. R1W.
Corner stones

Section corner between
Sec 19, 20 + 17 + 18



SEC. 20 SEC. 17

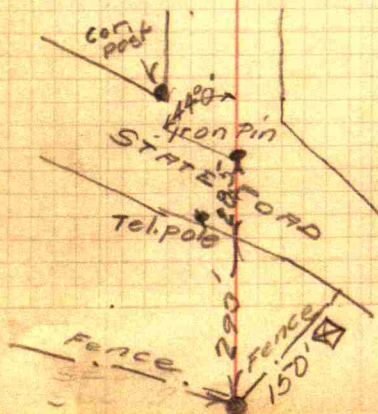
Witness: - Sch. house N45°W - N40°W.

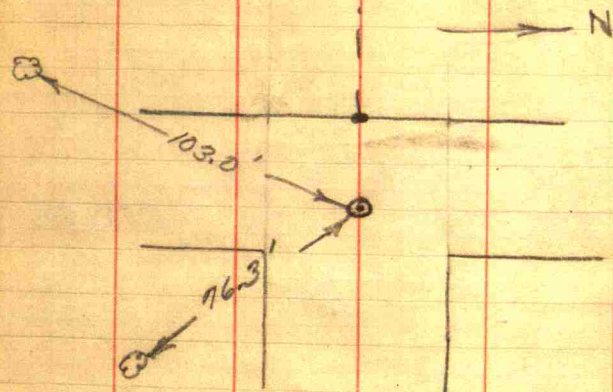
Sta 0+0 - Iron Pin in Center of
State Road is 321.5' N. of SE Cor Sec 19 - E. 114°W

Witnesses - Cone, Cor Post N35°W 47.9'

Tel. Pole - S60°W 7.2'

Barn 150' N of stone





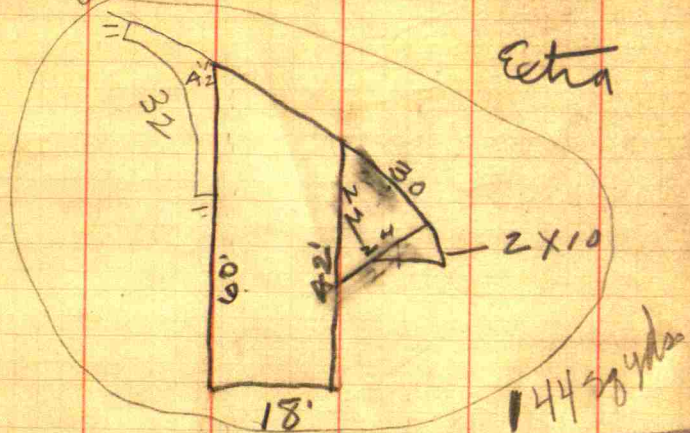
Sta 89+42

Witnesses:

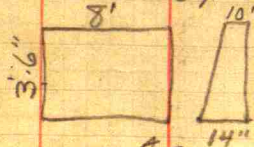
24" Walnut - S. 45° E. 76.3'

14" " - S 10° W. - 103.0'

John Dale Road.



Sta 2+90 - 26' x 12" x 2 ft Headers

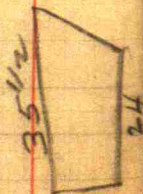
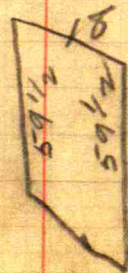
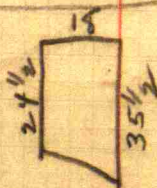


Extra

$$2 \times 1 \times \frac{7}{2} \times \frac{4.8}{2} = 56 = 2.5 \text{ cu yds}$$

5+21 26' x 18" + 9 Headers

Extra



231 sq yds

E.

0+0
1.50'

Iron Pin

W

5

N

1+0

2+0

109'
+ 47.5' x 9'

3+0

4+0

5+0

106 1012'

11.5'

17'

16'

11.0' 15.5'

114.5' 15'

6

Sta 5+12 Fence E

S. Pt of way line R.R.

5+15.5 fence W.S. at way line

STA 5+21 - 14" V.T. - 21'-0"

STA 5+30 Cen of R.R. track

STA 6+19 Cen. T.H. 18E track

STA 6+45 fence 6th Line TH 18E

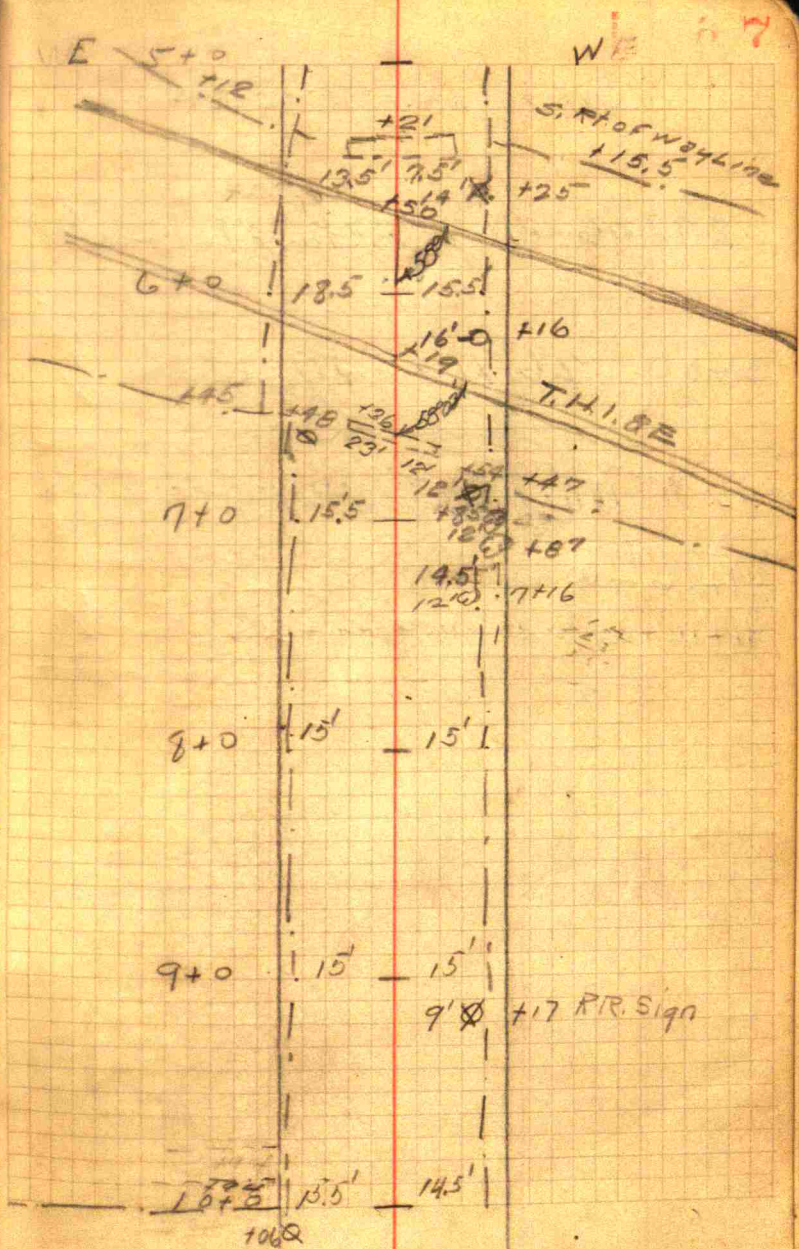
STA 6+47 " W " " "

STA 6+36 - 35' of 10" V.T. towards road

6+36 — 30'x15" and 9 Headers ✓

9+95 — 16' of old 12" relaid + 2 L Headers ✓

10+64 — 26'x15" and 9 Headers ✓

17+24 - 18+00 — 16'x10" old - 2 L Headers
and 60'x8" Dr Tile ✓20+60 - 26'x12" New and 9 Headers
Extra ✓27+60 - 4' old 10" and 12'x8" Dr Tile and
L Headers

Sta 10+64 - 16' of 10" Armo

29+06 - 16' x 10" old and L H dials

31+00 26' x 12" and 9 H dials ✓

34+30 - 38+64 18' x 8" Dr T and 16' x 10" old + 2 L's ✓

41+16 - W. side - 16' of old + L's

41+16 - E side - 16' of old + L's ✓

E. 10+0

W

9

11+0

$\begin{array}{r} +64 \\ 91 \overline{) 145} \\ 71 \end{array}$
15' - 145'

12+0

$\begin{array}{r} +64 \\ 16 \overline{) 15} \\ 15 \end{array}$
15' - 15'

13+0

15'

14+0

$\begin{array}{r} +67 \\ 16 \end{array}$

15'

15+0

145'

155'

E

15+0

11
W

+24

14'

16+0

14.5'

15.5'

+60.5

14'

☒

17+0

14'

+03

+20

+3.4

14.5'

+50

☒



+76 = 60'

+63

17'

18'

+77

+01 18+0

13.5'

15.5'

19+0

13'

15.5'

+10

+06

20+0

13.5'

15.5'

E 20+0

W 13

151 15' 13' 15.5'

21+0 13.5' 16'

+09 14'

22+0 13.5' 16'

23+0 14' 16'

+21 15' 16'

24+0 15.5' 16'

25+0 14.5' 16'

18'

E 25+0

M 15

121

2141

26+0

145

120

16

+72

3151

+48

27+0

15

17

50



+95

121

2151

16

+49

+60 200



28+0

16.5



600

+16

29+0

14.5

16



600

+106

+29

2141

+42

271

+82

30+0

+95

14

14

17

E
30+0

W 17

31+0

14' - 17'

+55

Q14

32+0

14' - 17'

17'

+77

33+0

14.5' - 17'

+12

+64 Q14

34+0

14.5' - 17'

35+0

15' - 16'

E
35+0

+73

36+0

+40

37+0

38+0

39+0

+88

40+0

14'

15'

+49

14'

15'

16'

16'

17'

15'

16'

16'

15'

16'

14'

W

+31

+36

+18'

+37

50'

+80

+25

200'

+49

E
4010

W 121

35' +98

4110

+76

15.5'

14.3'

+12

49' 45'

4210

214'

+72'

4310

4410

+16

14'

15'

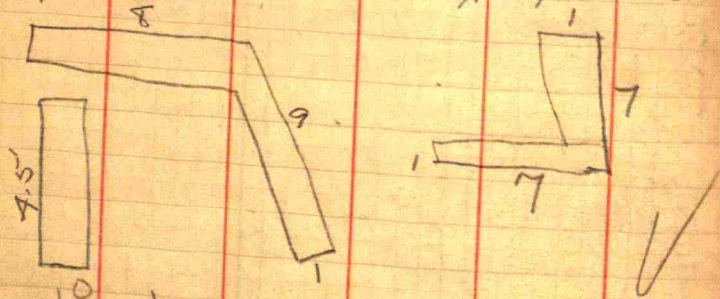
4510

13.5'

15.5'

49+83 E-Side
26'xold 15" and 2 L's

49+83 W side - 36'x24" New



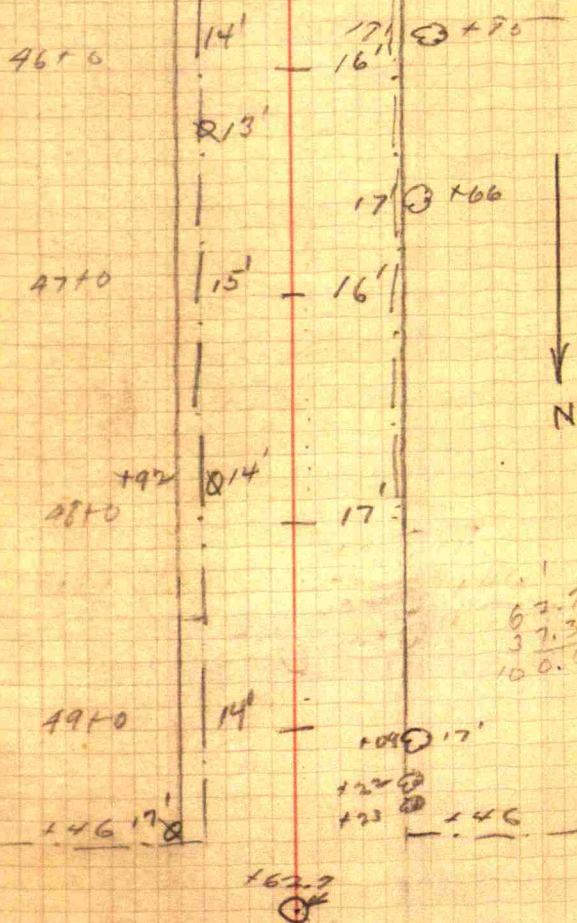
$$30 \times \frac{1}{2} \times \frac{1}{27} = 5 \text{ cu yds conc}$$

66+30 - 16'x10' old and 72'x8" D tile 2 L's

71+90 - 4' of 10' old and 10'x8" D tile - 2 L's

E
95+0

W 23



62.7
32.3
100.0

A hand-drawn surveying diagram on grid paper. A vertical line represents a survey line with points marked from 50+0 at the top to 54+0 at the bottom. To the left of this line, there are several rectangular shapes and measurements. A rectangle at 50+0 has a diagonal line and is labeled with '69.4', '70.2', and '35'. Below it, another rectangle is labeled '51+0' and '13'. Further down, a point is labeled '52+0' and '14'. At 53+0, there is a point labeled '19.5' and '13'. At 54+0, there is a point labeled '14' and '15'. To the right of the vertical line, there are several points and measurements. At the top, a point is labeled '46.27'. Below it, a point is labeled '10' and '16.1'. Further down, a point is labeled '14.5'. At 15, there is a point labeled '15.5'. At 15, there is a point labeled '15.1' and '15.1'. At 16, there is a point labeled '16.7'. The diagram includes various lines, angles, and measurements, suggesting a surveying or engineering project.

N

S

27

5410

+40

5510

15'

15'

5610

15'

13' 72

15'

+31

5710

5810

+56

5910

14' +80

70

59+0

60+0

61+0

62+0

63+0

64+0

16'

16'

15'

16'

14'

15' 8" +85

13' 8" +95

15'

13' 8" +93

S

+5

85

+89

N
6410

S

31

14' - 15' $+23$
 $\textcircled{2} 17'$

6510 14' - 15'

6610 14' - 15' $+84-17'$
 $+90$
 $+18$

$+300$

$+82$

6710

$+16$  50'

$+60.5$ $+49$

6810

$+118$  150'
 $+55$

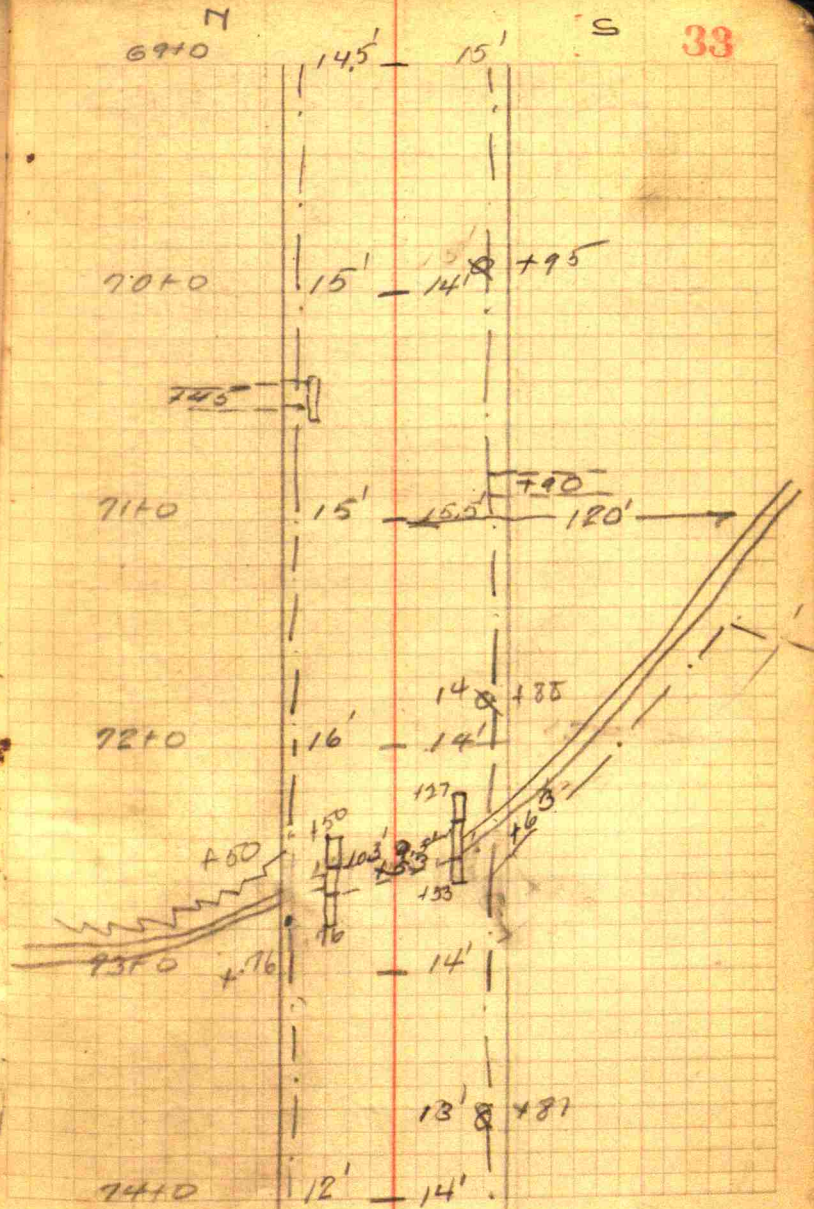
6910

14.5' - 15'

15' $+88$
 15'

Sta 70+45 - 14.5' of 6" drain
tile incased in concrete at
gate way

Sta 72+53 Aborn Bridge



Sta 76+25 - 6" tile down
S. side of road

74+0

12' - 14'

75+0

12' - 14'

74+26

76+0

12' - 14'

+25

77+0

13' - 14'

74+23

78+0

12' - 14'

79+0

12' - 14'

79+0

80+0

13' - 14'

14' 8"
+74

81+0

13' - 14'

82+0

13' - 15'

14' 2" +71

+12

83+0

13' - 14'

106 @ 17'

84+0

13' - 14'

13' 2" +74

84+0
+15 @ 13'

85+0 13' - 15' ~~20+0-18'~~

86+0 13' - 14' 13' ~~+7'~~
15' 18'

87+0 13' - 14'

13' ~~+48'~~

88+0 -

+78 

89+0 -

88+78 Armes -16' x 8"

88+78

26'x15" and a Headers. ✓

89+62 — 26'x15" and 2 a's ✓

~~104+95~~ — 26'x15" and a's ✓
97+65

100+47 = 16' of old 94'x8" Dr Tile
and 2 L's ✓

104+95 — 26'x15" and 2 a's ✓

104+95 — W side 16' of old and
174'x8" Dr Tile and 1 L Header ✓

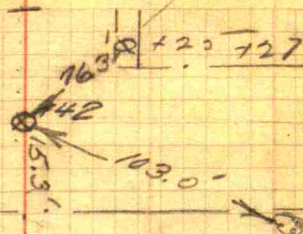
113+48 — 26'x15" and 2 a's ✓

113+85 — 28' old and 2 L's ✓

117+84 — 26'x15" and a's ✓

89+0

+27



Sta 97+65-13' 7 18" N.T.

140+28 N side 16' x old + 2 L's ✓

140+32 S side 14' x 8' D. Tile + 2 L's ✓

142+00 - W side 92' x 8" D. Tile + 2 L's ✓

142+90 - 14' x 8" D. Tile + 2 L's ✓

94+0

+18

+1360

95+0

9'

-15.5'

96+0

9'

-16'

+78

97+0

8'

-16'

$$\frac{2'}{1} = \frac{11'}{3}$$

+65

98+0

+100 8'

-16'

+41

99+0

+72

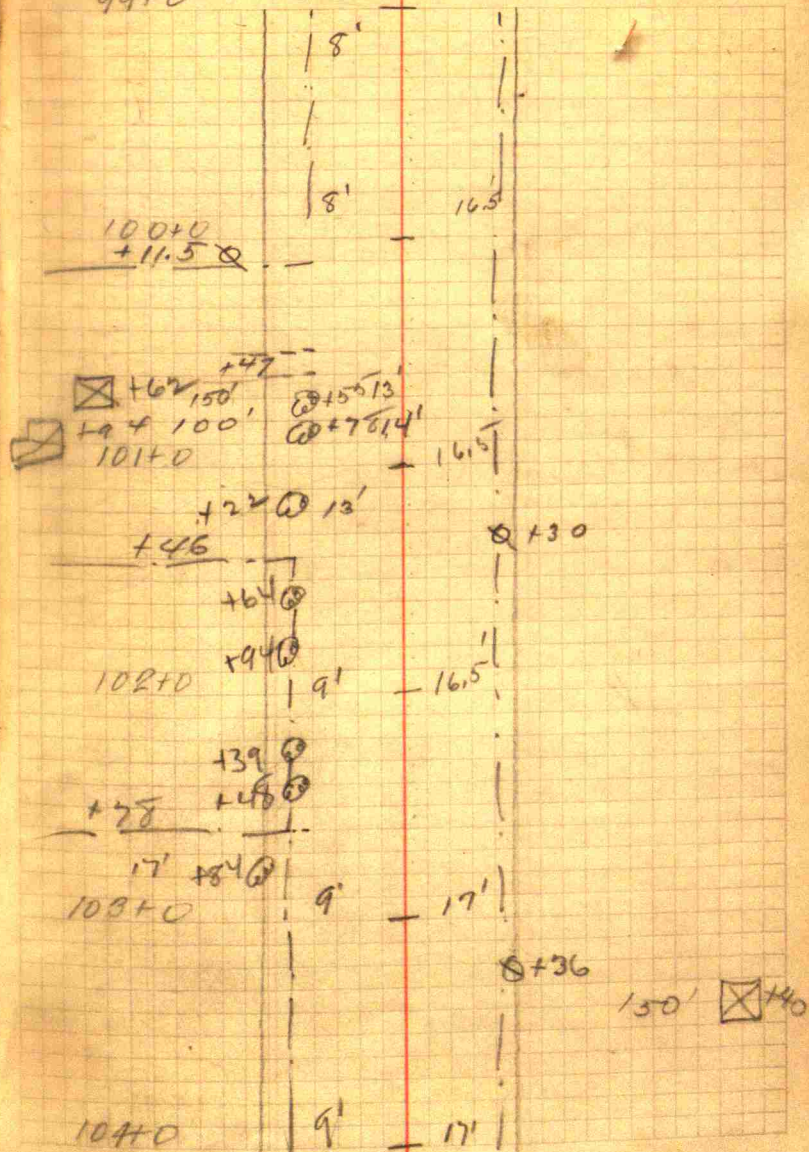
8'

-16.5'

Sta 1025 F

E
99+0

W 47



Sta 104+95/6' 7/2" Armo

104+0

W 49

105+0

9' - 17'

8+04

+21

+380 @ 15'

106+0

9' - 15'

+9540'

+21

+2

200'

+14

107+0

8' - 17'

+94

8+06

+31

108+0

8' - 17'

14' @ +76

109+0

11' - 16'

Sta 110+58 - 6" tile from
field in side ditch E side

Sta 113+40 - 16' of 12" diameter

E
109+0

W 51

110+0 9' - 16' 15' 8+78

110+0

110+0

111+0 13' 8' -

8+44

112+0 12' - 16'

113+0 10' - 16'

13' 8' +10

140
6' 10'

114+0 10' - 16'

Corner Stone
Wit.!

C
N



Note

concrete post W. 16.2'

11

N. 45° W 18.6'

114+0

+04 @ 15'

115+0 12'

16'

+77

12'

+20

12'

+56

+91

+90 @ 14'

116+0

14'

-783 +91
-+97

no fence → +57 @ 16'

117+0

-12'

118+0

-12'

+05

+67 @ 16'
119+0 10' 12'

Culvert +84
V.T. 16"

Sta	3' ant	Stk	Ditch	Berm	℄
0+00		96.63	96.77	7.0'	96.40
1+00	94.32	94.54	94.64	94.87	94.91
2+00	93.89	94.03	94.20	94.91	95.10
3+00	93.90	94.17	93.94	94.83	95.27
4+00	94.57	94.82	94.56	95.25	95.70
5+00	94.61	94.80	94.76	95.90	96.08
5+21	93.40	93.45	93.31	96.36	96.44
5+50	BM.	S. rail	R.R.	98.04	
6+0	94.80	95.80	96.84	96.73	96.85
6+36			94.04	97.05	96.75
7+0	94.71	94.70	95.04	95.51	95.30
8+0	94.96	95.09	94.76	95.73	95.98
9+0	93.95	94.29	93.92	95.29	95.60
10+0	94.21	94.52	94.60	95.20	95.28
10+64		94.15	"	94.32	95.15
11+0	93.85	94.20	94.61	95.11	95.53
12+0	94.78	95.30	94.74	95.33	95.85
13+0	94.40	94.55	94.81	95.40	95.49
14+0	94.63	94.92	95.02	95.70	95.61
15+0	95.72	95.52	95.33	96.12	96.28
16+0	97.14	97.21	"	96.51	97.20
17+0	99.11	99.04	97.89	98.43	98.78
18+0	101.12	101.06	"	101.03	100.85
19+0	99.74	99.85	99.74	100.70	100.61

Berm	Ditch	Stk	3' ant w	
	96.00	96.25		B.M.
95.19	94.37	94.91	94.79	Top of
94.70	94.17	94.42	94.30	Concrete
94.80	93.86	94.33	94.29	Post.
95.29	94.38	95.65	95.60	E.I.
96.15	94.81	95.45	95.52	100.00
96.52	93.53	93.80		
6+19	S. rail J.N.	I+E. section	97.07	
96.85	96.68	95.00	94.57	0
97.00	94.15	94.19		99.58
95.40	94.95	95.35	95.17	
95.81	95.20	95.57	95.62	
95.34	94.60	94.75	94.70	
95.12	94.35	94.82	94.75	
94.30		95.00		
94.95	94.75	94.95	94.96	
95.40	94.85	95.40	95.41	95.59
95.48	94.86	95.35	95.39	
95.69	94.77	95.53	95.40	
96.14	95.29	95.90	95.78	
96.94	96.13	97.15	97.03	99.03
98.25	97.57	99.23	99.21	
100.90	98.95	100.75	100.73	
100.35	99.44	99.83	99.72	

Sta	3' ant E	Stk	Ditch	Run	4	Run	Ditch	Stk	3' ant W
20+0	99.84	99.94	99.89	100.49	100.50	100.61	99.43	99.85	99.87
21+0	100.35	100.32	100.39	100.65	100.50	100.74	99.65	100.06	100.12
22+0	100.43	100.60	100.45	101.23	100.91	101.20	100.14	100.66	100.58
23+0	101.05	101.15	101.05	101.81	101.66	101.95	100.95	101.51	101.36
24+0	102.35	102.30	102.06	102.72	102.90	102.35	101.17	102.94	102.52
25+0	104.49	104.68	103.72	103.92	104.14	103.75	103.40	104.60	104.53
26+0	106.01	106.05	105.45	105.88	106.11	105.76	105.30	106.10	105.80
27+0	105.81	106.00	104.74	104.92	105.40	104.84	105.21	105.59	105.28
28+0	102.90	102.94	102.95	103.64	103.85	103.39	103.18	104.03	104.08
29+0	103.01	103.10	103.13	103.26	103.56	103.02	102.60	102.39	102.38
30+0	103.50	103.23	103.12	103.33	103.64	103.03	102.39	102.38	101.80
31+0	104.59	104.44	103.68	104.04	104.40	103.85	102.45	103.02	102.64
32+0	108.25	108.34	107.37	106.12	106.19	106.15	105.80	106.10	105.68
33+0	107.74	107.66	106.54	107.12	107.25	106.76	106.54	106.47	106.00
34+0	106.54	106.35	105.98	106.73	106.89	106.61	106.20	106.39	105.99
35+0	105.93	105.72	105.26	106.54	106.84	106.47	105.51	105.50	105.41
36+0	105.71	105.38	105.37	106.63	106.75	106.40	105.55	105.38	105.47
37+0	107.01	106.91	106.40	106.83	107.06	106.80	106.33	106.63	106.65
38+0	107.55	107.60		107.82	107.48	107.80	107.55	108.09	107.55
39+0	107.82	107.97	108.18	109.08	109.01	109.06	109.40	109.39	111.15
40+0	108.45	108.70	107.75	108.57	109.09	108.80	108.16	109.25	109.28
41+0	106.44	106.54	105.57	105.85	106.26	105.76		106.25	106.24
42+0	103.87	103.81	103.21	103.75	104.10	103.79	103.65	103.77	103.70

107.50

BM on rock in yard at Sta 39+0

El. 114.86

102.95

58

Sta	3' out E	Set	Ditch	Burn	E
43+0	102.10	102.70	101.97	102.95	103.33
44+0	101.36	101.51	101.42	102.16	102.70
45+0	101.60	101.60	101.18	101.89	102.33
46+0	101.76	101.42	101.60	101.84	102.12
47+0	101.78	101.80	101.43	102.05	102.34
48+0	101.75	101.80	100.89	101.75	102.11
49+0	100.21	100.41	99.62	100.17	100.34
49+623	50' N, -	99.51			

Sta	3' out N	Set	Ditch	Burn	E
49+83		98.73	98.70		99.45
50+0	99.28	99.37	99.20	99.60	99.63
51+0	99.65	100.01	99.12	99.94	100.01
52+0	99.97	99.93	99.76	100.67	100.92
53+0	100.02	101.01	101.07	101.30	101.56
54+0	101.77	101.75	102.10	102.57	102.65
55+0	103.76	104.21	103.40	103.70	104.12
56+0	107.07	107.18	106.42	105.23	106.10
57+0	107.33	107.65	107.41	107.43	107.60
58+0	108.25	108.68	108.25	108.21	109.11
59+0	109.93	110.20	109.10	109.99	110.19
60+0	110.77	111.52	110.78	111.55	111.41
61+0	106.59	106.96	106.85	107.20	107.21
62+0	105.03	104.84	104.15	104.78	104.73
0	105.30				

105.00

79

Burn W	Ditch W	Set W	3' out W
102.90	102.44	102.33	101.95
102.12	101.62	101.66	101.44
101.70	101.43	101.75	101.85
101.51	101.36	101.39	101.30
101.75	101.74	101.60	101.59
101.41	100.84	102.12	102.10
99.92	99.77	101.02	101.05
50'E -	100.40		

Burn S	Ditch S	Set S	3' out S
99.64	98.65	99.56	0104.27
99.77	98.80	100.11	100.18
100.84	99.80	100.64	100.72
101.66	101.21	100.63	100.72
102.73	102.27	102.98	103.05
103.79	102.94	104.70	104.70
105.31	104.76	107.90	107.81
108.55	109.15	108.20	108.34
109.14	108.46	109.53	109.61
109.60	109.33	110.15	110.18
111.19	111.00	112.62	112.45
107.24	106.93	109.63	109.60
104.65	104.17	106.70	106.56
B.M. - Sch. Window			Sta 49+623
EI. -	103.43		

Sta	3rd H.	N	N	N	E
63+0	102.90	103.0	102.80	103.41	103.25
64+0	101.99	101.80	101.80	102.26	103.11
65+0	102.13	102.06	101.71	102.41	102.90
66+0	103.14	102.88	101.91	102.71	103.03
67+0	102.50	102.26	101.75	101.98	102.31
67+16	B. M. on bridge over creek				
68+0	101.35	101.64	100.15	100.99	100.99
69+0	100.18	99.99	97.78	97.26	97.50
70+0	98.59	98.47	97.40	97.04	98.22
71+0	97.57	97.58	96.19	95.13	97.59
72+0	96.77	96.95	94.77	93.26	97.04
72+53	B. M. on S. rail bridge				
72+53	Bed of stream lower spring				
73+0	95.90	95.53	96.13	96.66	97.04
74+0	97.19	97.38	96.10	96.90	97.07
75+0	97.71	97.98	97.20	97.0	97.27
76+0	96.50	96.97	97.36	97.55	97.31
76+25	95.606" in S. side of cut corner				
77+0	97.75	98.07	97.02	98.77	97.60
78+0	99.32	99.58	98.91	97.36	97.77
79+0	100.50	100.97	100.15	100.61	101.11
80+0	102.31	102.29	101.84	102.10	102.45
81+0	105.30	105.66	104.30	104.47	104.88
82+0	107.68	107.71	107.61	108.66	107.05
83+0	107.15	106.90	106.63	107.23	107.64

5 0 97.71 S	5 0 104.05 S		
Reum	10.12	10.12	3rd H.
103.37	102.80	103.08	103.17
102.85	101.80	101.83	101.77
102.55	101.81	101.73	101.62
102.61	101.84	102.80	102.67
101.48	100.97	101.11	101.09
stop, E.L.	103.96		
100.41	99.89	100.85	100.89
98.90	97.44	99.86	100.10
96.97	97.23	97.21	97.20
97.43	96.62	97.08	97.02
97.34	96.00	96.51	96.48
E. End EL 99.89		E. End Bridge	
Lower spring	Bed of stream	6" Tile in N. Ditch	
97.42	91.93	92.10	92.10
96.67	95.18	96.16	96.09
97.05	95.26	97.46	97.43
97.96	97.13	98.51	98.56
97.18	97.50	97.93	97.91
road and bridge cut into di. from N. side of			93+20
98.55	97.73	98.25	98.23
99.50	99.00	99.96	99.98
100.81	100.00	101.12	101.50
102.35	101.35	103.39	103.42
104.56	104.22	106.85	106.89
108.12	107.23	109.08	109.15
107.21	106.24	106.81	106.83

Sta 52	N	N	N	N	E
	3 out	Set	Set	Set	
84+0	106.51	106.47	106.50	106.28	107.37
85+0	106.52	107.26	106.86	107.74	108.00
86+0	106.71	106.67	106.40	107.06	107.35
87+0	106.96	106.65	106.30	106.54	106.94
88+0	107.30	107.05	106.25	106.59	106.25
88+78	Arrived at road				16'
17'	F.L.H. 4 Top				E
106.45	105.04	105.64		106.67	
89+0	106.35	106.29	104.98	106.45	106.70
B.M. on Corp post S. side road					
89+62	106.32	106.28	105.21	Fl. 8	106.92
90+0	106.56	106.25	105.52	106.24	106.85
91+0	107.72	107.88	106.23	107.63	107.34
92+0	107.36	107.62	106.60	107.49	107.67
93+0	106.73	107.09	106.30	107.16	107.51
94+0	106.87	107.03	106.66	107.45	107.69
95+0	106.31	106.34	106.21	106.92	107.20
96+0	105.79	105.67	105.51	106.76	106.15
97+0	104.18	104.25	103.51	104.40	104.36
97+65		103.05	101.63	102.43	104.03
98+0	103.52	103.55	102.33	103.43	103.81
99+0	103.67	103.89	102.92	103.42	103.92
100+0	104.63	104.56	103.00	103.70	103.76
101+0	102.48	102.45	101.11	no ditch	100.44
102+0	99.25	97.95	97.34	97.64	97.55
555	B.M. on NW corner				
100					

Baym	Adch S	Set S	South 53
106.65	105.91	106.12	106.02
107.65	106.95	108.15	108.13
106.67	106.40	107.21	107.20
106.47	105.74	105.19	105.14
106.56	105.50	106.19	106.21
	F.L. 5	Top	17'
	104.95	105.75	105.85
106.50	105.60	105.82	105.82
EL. 111.20	W.	107.79 - 50' 5 on E	
106.42	Fl. 7.5	105.15	105.77
106.45	105.76	105.50	105.52
107.00	106.76	106.01	106.00
107.63	107.09	107.00	106.82
107.21	106.38	106.35	106.34
107.60	106.65	107.17	107.32
107.03	106.32	106.75	106.81
106.24	106.03	106.60	106.52
104.46	104.12	104.55	104.50
102.63	Fl. 30	101.24	
103.55	102.56	102.91	102.70
103.60	102.92	103.12	102.97
103.66	103.61	103.80	103.91
100.30	100.10	100.64	100.42
97.54	97.33	97.35	97.50
Concrete fly of house at Sta 100+50			
EL.	104.34		

64 3' out sta E 097.50
 103+0 95.61 95.55 95.32⁵ 95.65 95.64
 104+0 93.12 93.03 93.46 94.11 94.40
 104+46 91.69 92.80⁴ 92.02 93.69 93.95
 105+0 91.66 91.79 91.74⁴ 93.64 93.77
 106+0 92.36 92.52 92.85⁷ 93.24 93.78
 107+0 91.22 91.26 90.94⁷ 91.10⁴ 91.41
 108+0 89.83 89.81 89.60⁷ 90.08 90.20
 109+0 89.03 89.01 88.08^{7.5} 88.26⁵ 88.53
 110+0 85.96 86.10 86.36⁸ 86.82 86.78
 111+0 85.69 85.87 84.16⁸ 85.63 85.49
 112+0 83.01 83.53 83.96^{9.5} 84.68 84.78
 110+58 Flow line 83.86 6' W. from E
 113+0 82.50 82.53 82.20¹⁰ 84.06 84.04
 113+40 82.46 82.25^{7.5} 82.30^{7.5} 82.98 94.11
 114+0 92.54 93.14 81.95¹¹ 83.04 83.75
 115+0 81.90 82.02 81.37 82.16 82.56
 116+0 81.14 80.43 79.80¹⁴ 81.50⁸ 81.74
 117+0 80.91 80.48 80.19¹⁴ 80.85¹⁰ 80.90
 118+0 80.00 79.68 79.47¹⁵ 80.55¹⁰ 80.50
 118+84 79.00¹⁵ 78.86^{7.2} 80.52¹⁰ 90.90 80.22
 119+0 79.65 79.75 79.60¹⁵ 81.16⁵ 80.50
 119+77 83.06 83.22
 Bed of S. - E. 74.25
 Bed of S. - W. 75.00
 Flow line 18" tile 75.23
 Flow line tile from on E side 74.55
 Stream flows W + S

Beam Hatch Sta W 3' out
 10.5 13.5
 95.61 95.35 95.75 95.76
 94.19 93.45 93.90 93.71
 93.49 93.06¹⁰ 92.18¹⁰ 92.40¹⁰
 93.50 92.22 92.21 92.24
 93.34 93.46 94.25 94.36
 91.30 91.35 91.30 91.32
 89.91 89.26¹⁰ 89.73 89.79
 88.18 87.86¹⁰ 88.42 87.92
 86.65 86.00 86.60 86.41
 85.23 84.79 85.20 85.00
 84.19 83.68 83.97 83.98
 83.90 82.90¹³ 83.04 82.83
 83.63 83.19¹⁰ 82.23 82.53¹⁴ 82.86¹⁴
 83.30 82.86⁹ 83.32 83.75
 82.26 82.12¹⁰ 81.81 81.94
 81.43 80.96¹⁰ 80.70 80.62
 80.89 80.25⁹ 80.32 80.23
 79.25 78.72¹⁰ 79.46
 79.25 78.71¹⁰ 78.91¹⁰ 79.03
 78.90 78.90 79.00
 82.93 and W side 84.51

65 B.M. on SE corner of concrete
 station 105.50
 E1. 95.45
 89.32
 Top of fence post
 by telephone post
 on W.
 E1. 87.79
 84.50
 N. end E rail
 B.M. on
 NE corner of
 rail of bridge
 Sta 119+77
 E1. 84.63

44.95
66

	10' ant	3' ant	sta	ditch	Berm	old road	new road	W	Bottom ditch	sta	3' ant
120+0	8072	8076	8048		8225 ⁴	8285 ⁴	8250	8235 ⁸	7956 ¹⁰	8162	8165
121+0	8159	8185	8189		8204 ¹⁴	8267 ⁸	8234	8149 ⁴	7935 ¹⁰	8220	8211
122+0	8317	8305	8316		8309 ¹³	8351 ⁸	8374		7873 ¹⁰	8235	8292
123+0	8376	8391	8392		8413 ¹⁴	8447 ⁸	8455	838	7921 ¹⁰	8355	8397
124+0	8511	8470	8445		8469 ¹⁴	8520 ⁸	8427	8506	7955 ⁹	8460	8470
125+0	8460	8409	8350		8389 ¹³	8435 ⁷	8391		7992 ⁹	8385	8388
126+0	8361	8334	8303		8306 ¹³	8328 ⁷	8306		8013 ⁷	8300	8290
127+0	8230	8199	8214		8268 ¹³	8290 ⁷	8220		7969 ⁷	8170	8175
128+0	8119	8119	8134		8209 ¹²	8246 ⁷	8134	25E 8186	8000 ⁵	8134-0 8106*	8109
129+0	8154	8172	8190	20 21' 8076	8260 ¹²	8269 ⁸	8175		8080 ⁸	8180 8148	8126
129+12+11						8290 ⁸	8171	7970 ⁷			
130+0	8221	8223	8270		8352 ¹²	8364 ⁷	8285	Bottom ditch 8343E	8245 ⁴	8301	8298
131+0	8427	8455	8500	14 8503	8526 ¹¹	8539 ⁷	8506	8501 ³	8616 ⁴	8568	8582
132+0	8780	8815	8825	8743		8794 ⁷	8825	8814 ³	8833 ⁴	8865	8892
133+0	8941	8970	8928		8909 ⁷	8957 ⁵	8974		8955 ⁴	9030	9032
134+0	9166	9159	9164		9085 ¹³	9119 ⁵	9116		9095 ⁵	9152	9128
135+0	8910	8906	8940	13 8920	8961 ¹³	9006 ⁵	8972	8954 ³	8901 ⁸	8902	8900
135+77		8844 ^{7-3W}	8863 ^N	8842 ⁷	8985 ¹⁰	8991 ⁹	8902	8796 ¹⁰ 2E 8826 ²⁰	8940 ¹³	8913	8907
136+23			8849 ^{7E}	8860 ^{2-10S}	8922 ¹³	9002	8975 ⁵	8995 ³	8841 ^{7E}	8840	
137+0		8875	8903	8918 ¹³	9010 ¹⁴	9075	9075 ³	8995 ⁸	8878 ⁹	8917	8915
138+0		9028	9043	9010 ¹⁴	9076 ¹⁴	9200	9195 ⁴	9130 ¹²	9130 ¹²	9236	9251
139+0		9120	9127	9121 ¹¹	9195 ⁷	9282	9263 ⁴	9195 ⁹	9195 ⁹	9195	9216
140+0		9187	9185	9214	9271						

John J.
Concrete
Foot W.
8642
to 129+20
side road.

09036

09176

68

3' out

Sta

Natch

Rem

E

Rem

Natch

Sta 5 3' out

69

141+0	9352	9353	930 ⁹ ₈	935 ⁷ ₄	9369
142+0	9506	9517	945 ⁹ ₅	948 ⁶ ₄	9501
143+0	9787	9759		9610 ⁸	9644
144+0	10105	10083	9900 ⁸	9913 ⁴	9905
145+0	9874	9886	9579 ⁴	960 ⁴ ₆	9616
146+0	9442	9434	940 ⁴ ₆	947 ⁴ ₃	9482
147+0	9503	9521	936 ⁴ ₄	938 ³ ₂	9417
148+0	9285	9283	9181 ⁸	921 ⁵ ₅	9240
149+97	9100	9155	9184	916 ¹⁰ ₅	9105

9375 ⁴	9342 ⁹	9466	9467
9476 ⁶	945 ⁵ ₀	9488	9469
9619 ⁷	9612 ⁹	9600	9569
9844 ⁶	9885 ¹¹	9909	9900
9616 ⁶	9573 ¹²	9557	9509
9431 ⁶	9306 ¹²	9295	9282
9421 ⁵	9436 ¹⁰	9421	9359
9240 ⁶	9187 ¹⁰	9186	9141
9075 ¹⁰			

B.M. at
Sta 142+50
on rock at
base of bridge
fence

E1.96.62

© 98.95

72

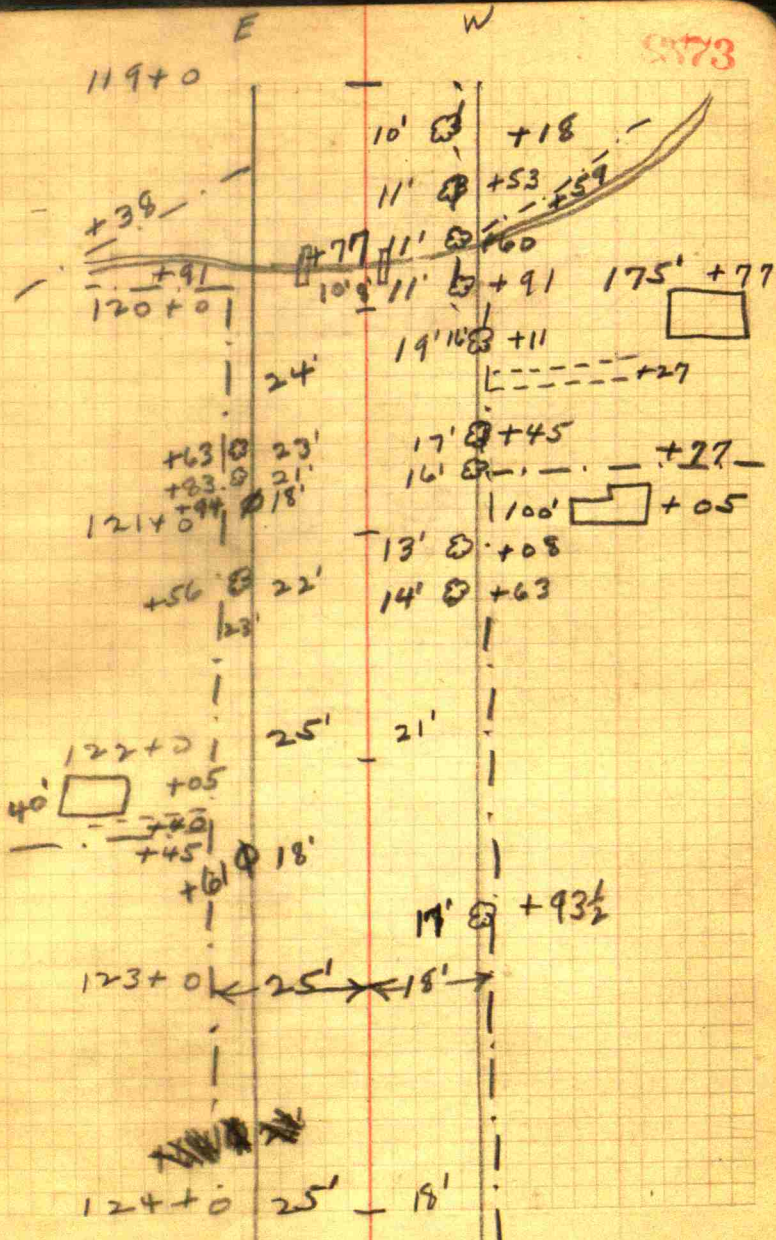
119+77 Concrete Bridge



16½' span
9' Rise
22' Rails

18" Net. tile from N. along
W side of road. 14' from E

573



124+0

+64

P

23'

125+0

25' - 16'

126+0

24'

- 14½'

+28

Q

18'

127+0

22'

- 14'

+05

Q

17'

128+0

21'

- 13'

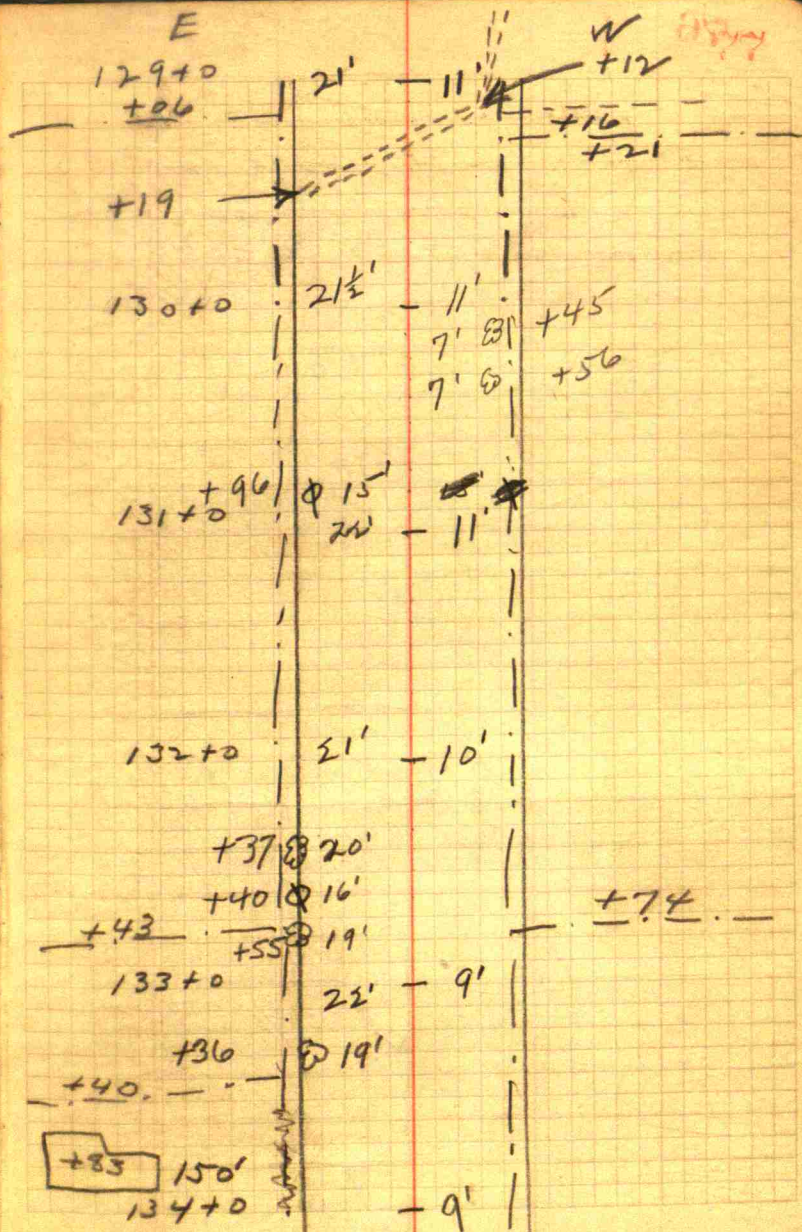
129+0

+18

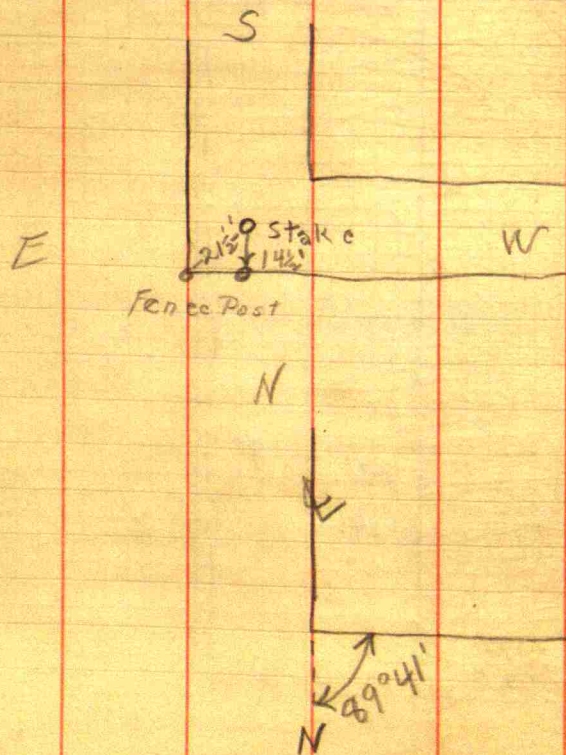
Q

17'

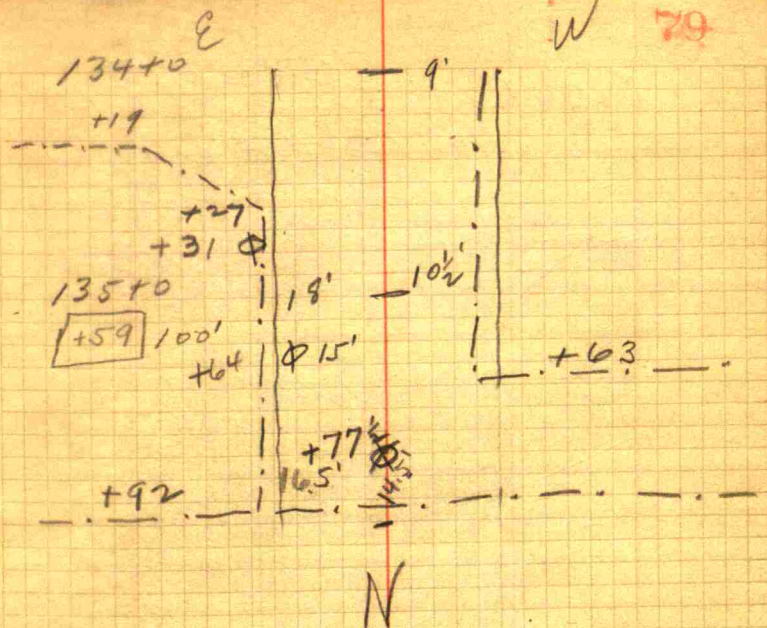
129+12 - 14" Vit. Tile
crosses road from E. and
runs So. along W side ditch -
to bridge at Sta 119+77



78

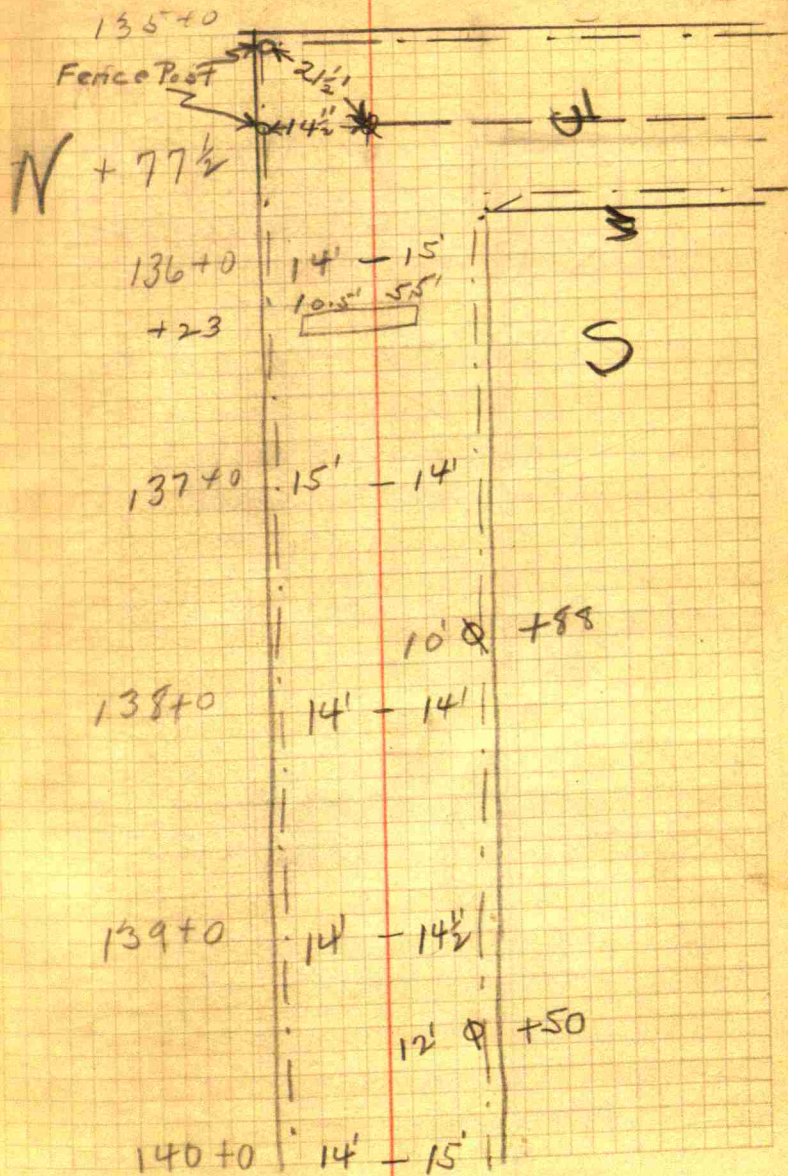


79



136 + 23

16' x 10" Armeo



140 to N

+32

141 to

+22 125'

142 to

+13

+61 160'

143 to

+00

144 to

145 to

14' - 15'

+22

+38

14' - 14' 40' +00

13' +41

14' - 14'

+03

30' →

+84

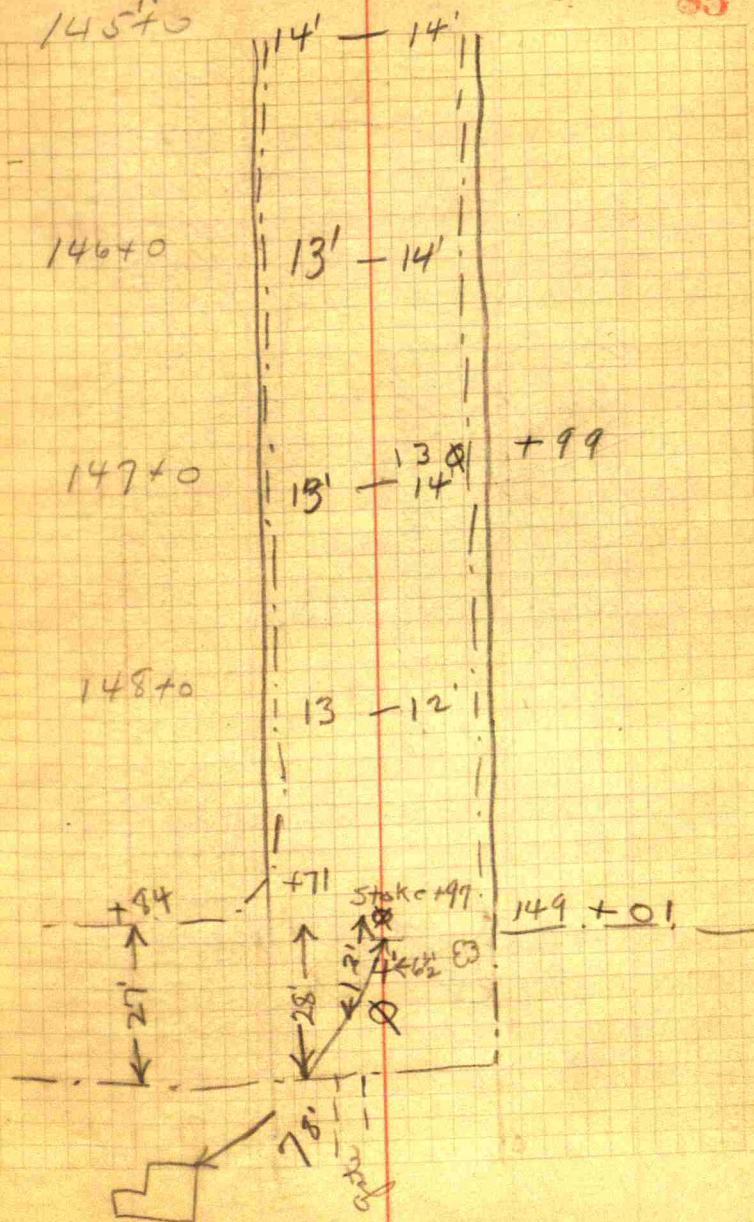
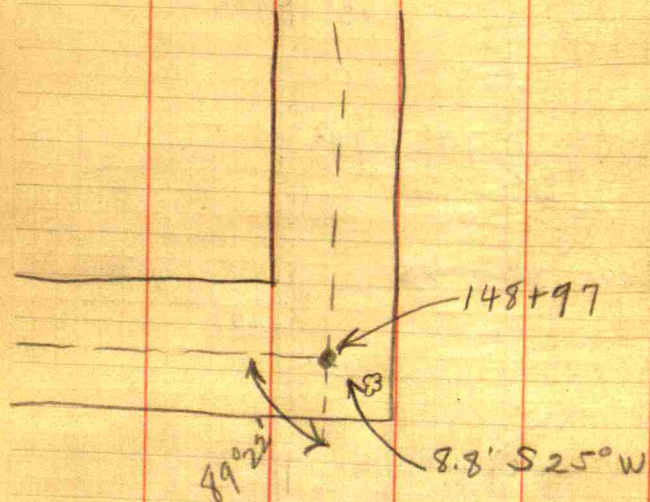
+90

- 14'

+04 14'

14' - 14'

14' - 13' +97



	℄	0
0+0	107.91	105.93
1+0	110.16	
2+0	112.61	
3+0	112.12	
4+0	109.50	
5+0	106.55	105.80 - 106.06
6+0	103.12	102.77
7+0	100.91	100.46
8+0	99.65	99.39
9+0	98.42	98.32
10+0	97.25	96.98
11+0	96.32	96.15
12+0	95.03	95.51 - 102.15
13+0	93.48	92.51
14+0	91.29	91.03
15+0		99.98
16+0		
17+0		

culvert at B.M. on West Head of
 9+00
 99.28

① 105.96
 ② 96.52
 ③ 93.37

9.25
 10.02

.77

103.25

45.2
 9.06

9.06

9.06

9.33

9.01

9.50

10.50

10.02

10.46

9.25

9.17

4.04

4.04

4.04

4.04

4.04

4.04

4.04

4.04

4.04

4.04

4.04

4.04

4.04

4.04

4.04

4.04

4.04

4.04

10.02

9.25

.77

10.02

9.08

9.08

9.08

9.08

9.08

9.08

9.08

9.08

9.08

9.08

9.08

9.08

9.08

9.08

9.08

9.08

88
Cement

175.

30

30

235

36

199

122

77

305 feet two
Inte.

Oct 15.

37
45 $\overline{) 1,670}$
135
320

122

20 $\overline{) 305.0 \times 2.2}$
27
35
27
80

89
305
.37
2135
915
11285

Notre Dame + Penn State
 Purdue + Wisconsin
 Indiana + North Western
 Wabash + Fred. Normal
 Butler + Franklin
 DePaul + Earlham
 Rose Poly + Evansville
 Hanover + Oakland City

80
 80
 80
 80
 80
 40
 30

 470
 259

27/ ^{On 59} 700 feet
 24
 160
 135

 250

Oct 16

160
 30
 80
 80

 40

6.00
 .17 28

 5.83

1.67 27

$2 \times \frac{7}{12} = \frac{14}{12} = 1.17$
~~1.50~~
 2.67

1.67 | 270 | 16.2

 1030
 1002

 28

1 Sack 2.7 lin ft. Base
 10 Sacks 27 lin ft Base
 1 Sack 12 1/2 lin ft Top —

280 216
 $2 \times \frac{14}{3} = 1.17$
 272

6.00
 6.29
 33

5.96

 5.83

1.13 2.6

 6

16.2

6/16.2
 2.7

2.7 | 700 | 260

 54
 160

Intersection 1.3 Sack 5g yd

$$\frac{1}{28} \times 3 \times \frac{1}{9} =$$

$$\frac{1}{21} \times 3 \times \frac{1}{9} =$$

$$.12 \quad 27 \quad \overline{1200}$$

$$18$$

Q

0+0

0+12.5

0+50

1+0

1+50

2+0

2+50

15.5

107.63

15.5

104.79

15.5

96.20

101.95

105.14

103.61

98.75

95.81

93.77

91.98

15.5

103.83

15.5

101.78

15.5

95.02

Hewb.

0+25

102.50

at.

92.00

D

104.04

D

97.25

4.66% Gd.

96

Sta South East St.
El.

10+37.1 94.24 P.C.	12+70 93.20
10+47.1 94.24	12+80 93.15 L
10+57.1 94.20	12+90 93.11 ✓
10+67.1 94.15	13+0 93.06 ✓
10+77.1 94.10	13+10 93.01 ✓
10+87.1 94.06	13+20 92.97 ✓
10+92.1 94.03 P.T.	13+30 92.92 ✓
11+0 94.00	13+40 92.87 ✓
11+10 93.95	13+50 92.83 ✓
11+20 93.91	13+60 92.78 ✓
11+30 93.86	13+70 92.73 ✓
11+40 93.81	13+80 92.68 ✓
11+50 93.77	13+90 92.64 ✓
11+60 93.72 ①	14+0 92.60 ✓
11+70 93.67	14+10 92.59 ✓
11+80 93.62	14+20 92.58 ✓
11+90 93.58	14+30 92.57 ✓
12+0 93.53	14+40 92.61 ✓
12+10 93.48	14+50 92.65 ✓
12+20 93.44	14+60 92.79 ✓
12+30 93.39	14+70 92.80 ✓
12+40 93.34	14+80 92.95 ✓
12+50 93.30	14+90 93.12 ✓
12+60 93.25	15+0 93.29 ✓

93⁵²₄₆ 13 07 B.M. Sta. 12+62
95.04

94.00	94.29
047	047
93.953	94.243
047	047
93.906	94.196
93.906	92.59
047	46
93.859	92.13
047	49
93.812	94.149
047	047
93.765	94.102
047	047
93.718	94.056
047	047
93.671	94.024
047	047
93.624	94.031
047	047
93.577	94.000
047	46
93.53	93.54

B.M. Sta. 14+25
94.10

~~15+10~~ 93.50 X
 15+20 93.70 X
 15+25 93.90
~~15+30~~ 94.07 X
 15+40 94.42 X
 15+50 94.77 X ✓
 15+60 95.12 X ✓
 15+70 95.47 X ✓
 15+80 95.81 X ✓
 15+90 96.16 X ✓
 16+00 96.51 X ✓
 16+10 96.86 X ✓
 16+20 97.21 X ✓
 16+30 97.55 X ✓
 16+40 97.90 X ✓
 16+50 98.25 X ✓
 16+60 98.60 X ✓
 16+70 98.95 X ✓
 16+80 99.29 X ✓
 16+90 99.64 X ✓
 17+00 99.99 X ✓
 17+10 100.34 X ✓
 17+20 100.69 X ✓
 17+30 101.03 X ✓
 17+40 101.38 X ✓
 17+50 101.73 X ✓

17+60 102.08 X ✓
 17+70 102.43 X ✓
 17+80 102.77 X ✓
 17+90 103.12 X ✓
 18+0 103.47 X ✓
 18+10
 18+25 104.17 ✓
 18+30
 18+40
 18+50 104.54 X ✓
 18+60
 18+75 104.57 X ✓
 18+80
 18+90
 19+0 104.26 X ✓
 19+10 104.07 X ✓
 19+20 103.88 X ✓
 19+30 103.69 X ✓
 19+40 103.50 X ✓
 19+50 103.31 X ✓
 19+60 103.12 X ✓
 19+70 102.93 X ✓
 19+80 102.74 X ✓
 19+90 102.55 X ✓
 20+0 102.36 X ✓
 20+10 102.17 X ✓

93.53
 047
 93.483
 047
 93.436
 047
 93.389
 047
 93.342
 047
 93.295
 047
 43.248
 047
 93.201
 047
 93.154
 047
 93.107
 047
 93.06

93.06
 047
 93.013
 047
 92.966
 047
 92.919
 047
 92.872
 047
 92.825
 047
 92.778
 047
 92.731
 047
 92.684
 047
 92.637
 047
 92.590

100.91

20+20	101.98	X	✓
20+30	101.79	X	✓
20+40	101.60	X	✓
20+50	101.41	X	✓
20+60	101.22	X	✓
20+70	101.03	X	✓
20+75	100.94	X	✓
20+85	100.68	X	✓
21+0	100.38	X	✓
21+15	100.07	X	✓
21+25	99.71	X	✓
21+30	99.56	X	✓
21+40	99.26	X	✓
21+50	98.96	X	✓
21+60	98.66	X	✓
21+70	98.36	X	✓
21+80	98.06	X	✓
21+90	97.76	X	✓
22+0	97.46	X	✓
22+10	97.16	X	✓
22+20	96.86	X	✓
22+30	96.56	X	✓
22+40	96.26	X	✓
22+50	95.96	X	✓
22+60	95.66	X	✓
22+70	95.36	X	✓
22+80	95.06	X	✓
22+90	94.76	X	✓
23+0	94.46	X	✓
23+10	94.16	X	✓
23+20	93.86	X	✓
23+30	93.56	X	✓
23+40	93.26	X	✓
23+50	92.96	X	✓
23+60	92.66	X	✓
23+70	92.36	X	✓
23+80	92.06	X	✓
23+90	91.76	X	✓
24+0	91.46	X	✓
24+10	91.16	X	✓
24+20	90.86	X	✓
24+30	90.56	X	✓
24+40	90.26	X	✓
24+50	89.96	X	✓
24+56	89.78	X	

① 99.24

96.30
67
96.97
67
96.69
67
96.31

B.M.

~~on curb in Negro~~

~~gate~~

El. 108.10

on walk of
Negro.

97.48

97.12
67
97.79
67
97.46
67
97.13

Cement on Cart & Yunter

Oct. 15	199 Sacks	305 feet
Oct. 16	470 "	700 "
Oct. 18	514 Sacks	790 "
Oct. 19	40 Sacks	60 "
Dec. 10	22 Sacks	20'
Oct. 22	416	495 feet
" "	105	140 "
Oct. 23	187	230 "
Nov. 23	354 Sacks	560 feet
Nov. 24	415 "	725 feet
Nov. 25	200 "	370 "
Dec. 3	1243	
Dec. 4	347	105 "
Dec. 8	130 Sacks	
Dec. 9	474 "	140'
Dec. 10	268	85

South East St.

two Lts. West Side
 3 Lts. + a part. West Side
 2 Lts. on East Side

four Lts. on West side South of East.
 One Lts. on East South of East.
 one Lts. on East South of East
 three Lts. on East side of Street
 South of Sta 15+00.
 three Lts. on West side South of 15+00

36° - 10:30 - 38° - 12:00 - 36° - 3:30 - quit
 36° - 9:15 to 12:00

$$\begin{array}{r} 176 \\ 30-19 \\ \hline 187 \end{array}$$

Oct. 25

936

30

30

30

30

30

30

30

30

30

1205

30

30

30

30

30

30

$$\begin{array}{r} 1385 \\ 78 \\ \hline 1307 \end{array} - 78$$

1307

385
put

38

31

38

114

34

1307

1178

129

34

30

8

4

1020

180

5

1205

75

1130

750

180

5

935

69

868

14

3

42

32

74

Oct 26.

704 bags used
220 Fwt.

$$\begin{array}{r} 310 \\ 310 \\ \hline 620 \\ 62 \\ \hline 682 \end{array}$$

$$\begin{array}{r} 310 \\ 310 \\ \hline 620 \end{array}$$

$$\begin{array}{r} 704 \\ 682 \\ \hline 22 \end{array}$$

110 Center Pavement
on South East St.
Date Cement Feet
Oct 25 13 07 3 85
Oct 26 7 04 2 20

111

112
240

92

30

30

30

30

30

482

30

30

30

30

30

30

30

30

30

752

30

30

30

30

30

30

30

30

30

30

Top
NHNgrows in
one wood

7000

Top

NHNHNHN

30

9

270

482

752

(37)

2800

(210)

310

2

610

31

641

Bottom 113

NHNHNHN

30

9

270

482

752

40

88

56

27

10

72

74

288

31

64

9

256

50

256

289

256

545

480

1025

800

200 Barrels

Row 28
High 7
Long 28
Wide 4
Center 16

13701370
241394

1394

69
1325

28
6

21
4

168
196
21
28
13

430
28
7

19628
13

top

~~XXXXXXXXXX~~~~XXXXX~~18

64

79 800

430

370

952

704

171

151

25

30

30

30

115

30

160

28

17

196

28

476

54

530

800

530

270

430 in car

$$\begin{array}{r} 69 \\ 499 \end{array}$$
499
36

Car gone 463
36 gotten by Kurtly

1000 not car
1000 bags

23 gotten by Kurtly

243 used out of
1000 lot car

Morning total

706 sacks

$$\begin{array}{r} 14 \\ 8 \\ 112 \end{array}$$

$$\begin{array}{r} 448 \end{array}$$

$$\begin{array}{r} 984 \\ 409 \\ 575 \end{array}$$

56
55

$\begin{array}{c} 11 \\ 9 \end{array} \times 4$

$$\begin{array}{r} 99 \\ 4 \\ 396 \\ 352 \end{array}$$

$$\begin{array}{r} 748 \\ 23 \end{array}$$

$$\begin{array}{r} 771 \\ 30 \\ 741 \end{array}$$

$$\begin{array}{r} 13 \\ 9 \\ 117 \end{array}$$

$$\begin{array}{r} 984 \\ 741 \\ 4 \\ 468 \end{array}$$

$$\begin{array}{r} 18 \\ 76 \end{array}$$

$$\begin{array}{r} 463 \\ 243 \\ 706 \end{array}$$

$\begin{array}{c} 11 \\ 8 \end{array} \times 4$

$$\begin{array}{r} 28 \\ 4 \\ 352 \end{array}$$

$$\begin{array}{r} 1000 \\ 741 \end{array}$$

259

$$\begin{array}{r} 45 \\ 5 \\ \hline 225 \end{array}$$

$$\begin{array}{r} 32 \\ 5 \\ \hline 160 \end{array}$$

$$\begin{array}{r} 12 \\ 237 \\ 172 \\ \hline 409 \end{array}$$

$$\begin{array}{r} 12 \\ 172 \end{array}$$

1160

$$\begin{array}{r} 262 \\ 25 \end{array}$$

287 left over

$$\begin{array}{r} 463 \\ 575 \\ \hline 1038 \end{array}$$

$$\begin{array}{r} 463 \\ 697 \\ \hline 1160 \end{array}$$

$$\begin{array}{r} 45 \\ 3 \end{array}$$

$$\begin{array}{r} 32 \\ 3 \end{array}$$

$$\begin{array}{r} 96 \\ 12 \\ \hline 108 \end{array}$$

$$\begin{array}{r} 135 \\ 19 \end{array}$$

$$\begin{array}{r} 154 \\ 108 \\ \hline 262 \end{array}$$

$$984$$

$$262$$

$$\begin{array}{r} 722 \\ 25 \\ \hline 697 \end{array}$$

South East St.

Sta	Sub. Hd.	Sub. Hd.	Sub. Hd.
16+0	96.05	99.03	2'-11 $\frac{1}{2}$ "
17+0	99.53	101.34	1'-10"
18+0	103.01	107.92	4'-8 $\frac{1}{2}$ "
18+50	104.08	107.75	3'-7 $\frac{1}{2}$ "
19+0	103.80	104.22	0'-5"
20+0	101.90	103.39	1'-6"
21+0	99.92	104.83	4'-11"
22+0	97.00	102.71	5'-8 $\frac{1}{2}$ "
23+0	94.00	88.50	
24+0	91.00	87.94	
24+56	89.32	90.31	1'-0"

5'-6"
3'-0 $\frac{1}{2}$ "

B.M. Sta 14+25
Sop of House. El. 94.10

103.73

92.26

81.64

103.39
101.92
1.49

107.75
104.08
3.63

99.03
98.05

104.22
103.90

2.98

4701.34

99.53

90.31
89.32
1.81

104.83
99.92
4.91

99107.72

103.01

471

102.71
97.00
5.71

94.00

88.50

5.50

91.00
87.94
3.06

W

E.

4"

15+50	94.10	93.77	
16+0	95.84	96.10	
16+50	97.58	97.88	
17+0	99.32	99.90	
17+50	101.06	102.19	102.04
18+0	102.80	103.61	103.50
18+50	103.87	104.17	104.32
19+0	103.59	103.10	103.20
19+50	102.64	102.20	102.45
20+0	101.69	101.95	101.85
20+50	100.74	101.50	101.40
21+0	99.71	100.65	100.80
21+50	98.21	99.50	99.87
22+0	96.79	98.50	98.80
22+50	95.29	96.79	96.80
23+0	93.79	93.95	94.33
23+50	92.29	92.10	92.30
24+0	91.79	91.60	90.92
24+50	90.29	89.40	89.00

$$\begin{array}{r}
 9410 \quad 9257 \\
 1.74 \quad 170 \\
 \hline
 9584 \quad 94.31 \\
 174 \quad 21 \\
 \hline
 9758 \quad 9432 \\
 174 \quad 21 \\
 \hline
 10106 \\
 10350 \\
 21 \\
 \hline
 10359 \\
 195 \\
 \hline
 10264
 \end{array}$$

$$\textcircled{100.32}$$

$$\textcircled{98.92}$$

$$\begin{array}{r}
 9410 \\
 9850 \\
 9679 \\
 \hline
 171
 \end{array}$$

$$\begin{array}{r}
 9805 \\
 9257 \\
 \hline
 348
 \end{array}$$

$$\begin{array}{r}
 174 \quad 9605 \\
 21 \quad 21 \\
 \hline
 9953 \quad 103.01 \\
 21 \quad 21 \\
 \hline
 104.08 \quad 102.80 \\
 21 \quad 21 \\
 \hline
 103.87 \quad 101.90 \\
 21 \quad 21 \\
 \hline
 99.92 \quad 101.69 \\
 21 \quad 95
 \end{array}$$

$$\begin{array}{r}
 99.71 \\
 150 \\
 \hline
 98.21 \quad 9700 \\
 150 \quad 21 \\
 \hline
 96.71 \quad 9679 \\
 150
 \end{array}$$

$$\begin{array}{r}
 9529 \\
 150 \\
 \hline
 9379 \\
 150 \\
 \hline
 9229
 \end{array}$$

Morn. 250 sacks.
 aft. 74
 30

(354)
 bag

Feet 560

(24)
 (13)

(35)

Nov. 23.

Morn. Lem. 35 at 10:00
 noon 40 at 12:00
 Eve. 42 3:00 at 4:30
 " 40 4:00

Nov. 24
 Morn. Lem. 38 at 8:30
 noon 36 at 4:00

Nov 25

Morn. 36° Lem. at 10:00
 noon
 Eve. 40 Lem. at 4:00

Dec. 3

Lem. Morn. 38
 noon 52
 Eve.

Nov. 24
180 sacks.

$$\begin{array}{r}
 2:60 \\
 6:30 \\
 \hline
 90
 \end{array}
 \begin{array}{r}
 120 \\
 180 \\
 90 \\
 \hline
 390 \\
 50 \\
 \hline
 440 \\
 425 \\
 \hline
 415
 \end{array}$$

725 Feet

Nov. 25
80 sacks.

220 feet
on west side
In Morning

150
Feet
East side
In aft

$$\begin{array}{r} 800 \\ 82 \\ \hline \end{array}$$

$$\checkmark 718$$

$$\checkmark 400$$

$$120$$

$$1258$$

$$20$$

$$\hline 1258$$

$$15$$

$$\hline 1243$$

$$75$$

$$31$$

$$75$$

$$225$$

$$\hline 2325$$

$$310$$

$$300$$

$$310$$

$$233$$

$$\hline 1163$$

Dec. 3

Lacks.

1243

Dec 9,

Sacks. $351 - 4 = 347$

347 sacks used

$$\begin{array}{r} 57 \\ 120 \\ \hline 177 \end{array}$$

$$\begin{array}{r} 528 \\ 199 \\ \hline \end{array}$$

$$\begin{array}{r} 351 \\ \hline \end{array}$$

120

57

4

181

528

181

347

135

300

Dale Road Est

✓ 8469 Cu. Yds Exc + Fill @ 35
 3058 Cu Yds Gravel @ 1.55
 3057 Tons W.B.M @ 2.90 -

✓ 212' x 15" C.M.P. @ 2.00

✓ 26' x 12" C.M.P. @ 1.50

✓ 78' x 18" C.M.P. @ 2.50

✓ 26' x 24" C.M.P. @ 3.50

2 Std. Inlets @ 25.00

76 Cu. Yds Conc. @ 12.00

✓ 198' 6" Pipe Reins @ 25.00

= 2964.45 ✓

= 4739.90 ✓

= 8865.30 ✓

= 424.00

= 39.00

= 195.00

= 91.00

= 50.00

= 912.00

= 49.50

18329.85

	Q. & R.	North	Cut	Fall
0				
1	9553	9564		0'-1½"
2	9492	9539		0'-5½"
3	9510	9514		0'-½"
4	9638	9489	1'-6"	
5	9638	9649		0'-1½"
6	9527	9659		0'-4"
7	9584	9579	0'-8"	
8	9620	9504	1'-2"	
9	9540	9489	0'-6"	
10	9549	9474	0'-9"	
11	9555	9474	0'-10"	
12	9605	9489	1'-2"	
13	9600	9504	0'-11½"	
14	9616	9519	0'-11½"	
15	9655	9551	1'-½"	
16	9780	9684	0'-11½"	
17	9972	9834	1'-4½"	
18	10022	9968	0'-6½"	
19	10031	10006	0'-3"	
20	10024	10028		Ed.
21	10039	10050		0'-1½"
22	10103	10072	0'-3½"	
23	10169	10111	0'-7"	
24	10301	10254	0'-4½"	
25	10481	10414	0'-8"	

B.M.
on School House
Window

10393

B.M. on E
where S & S. side Rd.
and E of Concrete
intersect East other
Sta 0+0

El. 97.96

Elk 7/22. Cut Fill.

26	10624	10550	0'-9"
27	10594	10548	0'-5½"
28	10446	10522	0'-9"
29	10271	10496	2'-3"
30	10227	10470	2'-5"
31	10287	10444	1'-7"
32	10606	10490	1'-2"
33	10637	10536	1'-0"
34	10629	10582	0'-5½"
35	10562	10628	0'-8"
36	10563	10674	0'-11"
37	10705	10720	0'-2"
38	10799	10766	0'-4"
39	11162	10812	3'-6"
40	10860	10829	1'-3½"
41	10687	10678	0'-5"
42	10430	10498	0'-8"
43	10266	10358	0'-11"
44	10223	10287	0'-8"
45	10290	10256	0'-2"
46	10194	10225	2'-3½"
47	10220	10194	0'-3"
48	10305	10163	1'-5"
49	10123	10132	0'-1"
50	10056	10101	0'-5½"
51	10119	10119	0'-0"

0106.27

52	12097	10137	0'-5"
53	10246	10187	0'-7"
54	10350	10304	0'-5½"
55	10509	10453	0'-6¾"
56	10820	10602	2'-8"
57	10924	10751	1'-9"
58	11000	10850	1'-6"
59	11069	10850	2'-2¼"
60	11261	10800	4'-7½"
61	10980	10738	2'-5"
62	10698	10602	0'-11½"
63	10357	10455	1'-½"
64	10226	10347	1'-2½"
65	10184	10278	0'-11½"
66	10287	10284	0'-½"
67	10145	10218	0'-9"
68	10127	10128	282
69	10049	9978	0'-8½"
70	9845	9843	282
71	9745	9798	0'-6¼"
72	9687	9768	0'-10"
73	9656	9738	0'-10"
74	9775	9720	0'-6¼"
75	9880	9780	1'-0"
76	9830	9852	0'-2¾"
77	9871	9924	0'-6¼"

Pl. 2th. New Rd Cut Füll

78	10029	9996	0'-4"
79	10130	10102	0'-6"
80	10388	10298	1'-1 $\frac{3}{4}$ "
81	10762	10488	2'-9"
82	10963	10712	2'-6"
83	10704	10808	1'- $\frac{1}{2}$ "
84	10646	10778	1'-4"
85	10834	10761	0'-9"
86	10748	10744	0'- $\frac{1}{2}$ "
87	not set	10727	—
88	10630	10726	0'-11 $\frac{1}{2}$ "
89	10600	10725	1'-3"
90	10670	10724	0'-6 $\frac{1}{2}$ "
91	10798	10723	0'-9"
92	10743	10722	0'-2 $\frac{1}{2}$ "
93	10706	10721	0'-2"
94	10695	10720	0'-3"
95	10599	10635	0'-4"
96	10607	10549	0'-7"
97	10434	10436	set
98	10353	10371	0'-3"
99	10389	10296	0'-11 $\frac{3}{4}$ "
100	10482	10140	3'-5"
101	10274	9989	2'-10 $\frac{1}{4}$ "
102	9845	9838	0'-1"
103	9571	9687	1'-2"

Sta 100+50 B.M. 104.34

check 104.36

109	9332	9536		2'- $\frac{1}{2}$ "
105	9206	9385		1'-9 $\frac{1}{2}$ "
106	9272	9234	0'-4 $\frac{1}{2}$ "	
107	9143	9083	0'-7 $\frac{1}{2}$ "	
108	8997	8932	0'-8"	
109	8921	8781	1'-5"	
110	8610	8630		0'-2 $\frac{1}{2}$ "
111	8572	8479	0'-11"	
112	8346	8437		0'-11"
113	8261	8395		1'-4"
114	8284	8338		2'-6 $\frac{1}{2}$ "
115	8226	8266		0'-5"
116	8146	8194		0'-6"
117	8104	8122		0'-2'
118	8021	8075		0'-6 $\frac{1}{2}$ "
119	8000	8175		1'-9"
120	8112	8300		1'-11"
121	8214	8255		0'-5"
122	8349	8210	1'-4 $\frac{1}{2}$ "	
123	8418	8230	1'-9 $\frac{1}{2}$ "	
124	8500	8250	2'-6"	
125	8445	8270	1'-9"	
126	8374	8290	0'-10"	
127	8240	8310		0'-8 $\frac{1}{2}$ "
128	8149	8330		1'-10"
129	8204	8387		1'-10"

130	8260	8470	2'-1"
131	8492	8590	1'-0"
132	8823	8710	1'-1½"
133	8981	8830	1'-6"
134	9180	8950	1'-3½"
135	8922	9000	0'-9½"
136	8860	9050	1'-10½"
137	8918	9100	0'-12"
138	9062	9150	0'-10¾"
139	9192	9200	0'-1"
140	9233	9307	0'-9"
141	9446	9414	0'-4"
142	9613	9521	0'-11"
143	9962	9628	3'-4"
144	10163	9672	4'-11"
145	9976	9593	3'-10"
146	9519	9451	0'-8½"
147	9568	9309	2'-7"
148	9335	9167	1'-8"
148+97	9216	9025	1'-11"

① 8945-

Sta 133+30
 Rock on East side
 of Road in cliffs
 front yard
 El. 9237

B.M. at end
 of Rd at Base
 of first Pine tree
 El. 9256