

MS Cort Road

Lowder

195

MINING
TRANSIT BOOK

368 A

John M. McCord

Sta	West	20'	East	20'
0+00	100.39		100.00	
0+20	101.04		101.02	
1+00	102.70		102.66	
2+00	103.66		103.56	
2+75	104.88		104.78	
3+00	102.92		103.30	
4+00	99.02		99.00	
5+00	97.08		97.61	
6+00	95.11		95.35	
6+75	93.85		93.97	
7+50	93.80	17'	92.32	
8+00	94.69	17	92.95	
9+00	94.56	17	92.51	
9+70	94.17	17	92.35	
10+00	98.51		96.07	
10+50	95.08	10'	91.21	
11+00	89.55		89.34	
11+35	89.90		90.30	
11+40	91.56		92.02	
11+50			86.84	
11+55			85.90	
11+58			86.70	
11+68	92.78		91.32	
11+80	92.72		91.78	
12+00	91.04		92.17	
13+00	91.45		91.50	
14+00	94.16		95.31	

North

719
down 30'

Relocation

Sta	20'	East
0+00	100.05	100.00
1+00	101.12	
2+00	102.72	
3+00	102.98	
4+00	103.56	9772
5+00	102.34	
6+00	99.20	
7+00	98.75	
8+00	97.50	
9+00	92.78	D=60°
10+00	91.85	
11+00	92.35	
12+00	92.92	
13+00	94.67	
14+00	94.06	
15+00	90.15	
16+00	89.13	
17+00	90.77	
18+00	91.78	
19+00	91.32	
20+00	90.92	
21+00	91.03	728
22+00	92.67	727
23+00	95.16	726

96.30

D=60°

17
91.87

92.3
5.66
95.90

ap 15
from
house

Sta
 0+00
 0+20
 1+00
 2+00
 2+75
 3+00
 4+00
 5+00
 6+00
 6+75
 7+50
 8+00
 9+00
 9+70
 10+00
 10+50
 11+00
 11+35
 11+40
 11+50
 11+55
 11+58
 11+68
 11+80
 12+00
 13+00
 14+00

Stone—
 Sta 0+15 - 30" Walnut hole
 Fence E+W - -

Drive way 0+00 - 0+15 East
 0+33 Pole 3' E of E
 0+60 6" Pole 16' E of E
 1+20 18" " 16' E of E

P.C.
 P.I. - Sta 6+96 -
 P.T.

9+00 Fence 6" N N B

E. Bank 11+40 - 1154
 E edge water
 & Stream
 W edge water
 W Bank
 E edge old road
 12+20 Pole 18" N - Brass wire
 Pole 14+10 - 18' N
 Tree 14+50 - 17' N Remains

(N²M: 3417-1E) BM Cl 100.00
 Top of Stone

removal
 Fence 0+20 - P.S.
 2+10 - Fence E
 4+40 " W
 6+04 " W

0+00
 Cen Rd 100 - N -
 98.76

Stone at 6+76 $\angle 90^\circ - D = 60^\circ$
 $\angle = 150^\circ$
 Tan = 96'

Gate N

Gravel S of very old Top Bank
 at 93.45 - 10' N of E 11+68
 11+55 Fence 11+68

removal 6'

North

15+00	⁷ 20 93.20	¹⁰ 97.16	
16+00	⁷ 20 97.84	⁸ 96.55	
16+93	⁷ 21 92.64	²⁰ 94.43	¹⁵ 93.82
17+43	²⁰ 92.64	⁷ 25 94.17	¹⁰ 94.17
17+93		²⁰ 92.36	¹² 92.05
18+43	91.25		
18+93	91.80		
19+18	91.95		
19+43	92.13		
19+93	92.01		
20+43	²⁰ 91.99		
20+93	95.39		
21+43	96.15		
22+43			

34
95.79

98.32
97.00
94.5
93.60
93.94
91.30
91.43
91.80
91.91
91.50
92.41
94.56
96.37
97.93

98.90	⁵ 97.43	²⁰ 98.10	726 up 95
		²⁴ 96.86	hmm do.
		⁷ 20 94.61	²⁴ 97.74
		²⁰ 94.28	715
			²⁰ 93.49
			91.65
			91.41
			91.55
			91.70
			91.82
¹⁰ 94.51	⁵ 95.86	²⁰ 95.12	306 added
	²⁰ 95.69	²⁰ 95.69	327
⁴ 95.45	⁸ 96.55	¹⁵ 96.72	2020 T
			96.6

500

15+00
16+00
16+93
17+43
17+93
18+43
18+93
19+18
19+43
19+93
20+43
20+93
21+43
22+43

15+05 pole 20' N

PC Pole 12' N of Φ

Fence 12' due East of 17+93

PE

20+50 Pole 15' E of Φ
20+65 Pole 10' W of Φ
20+43 Fence at Rdway N+S.

P.T.

16+93 - Brace to 116'

centerline

215 280
21+40

50¢

Sagle Bridge

Bedstead 13'-6" x 22'-0"

Bed to Crown 6.6' —

7 lines 8" I's —

All wings @ 45°

34
Omer Button Rd.
Brown Tp.

Corner Stones:

010 - Stone - Cen E. Cen
✓ Sec. 6

Wit.

18" Elm: $N 40^{\circ} E - 29.4'$

N. end of W. rail of Culvt.

on Martin Hart Rd.

$S. 4^{\circ} W - 198'$

✓ - Stone: E² mi stone, Sec 6

Wit: Concrete post.

$N 1^{\circ} W - 23.4'$

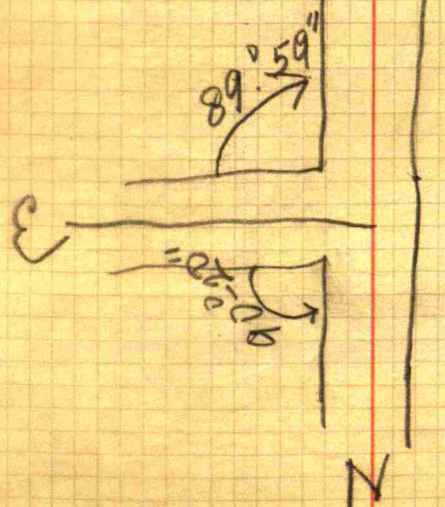
Concrete post

$N 9^{\circ} E - 26'$

✓ - Stone - Cen W Cen. Sec 5

24" Elm $N. 45^{\circ} W - 34.4'$

12" Elm $N. 10^{\circ} W - 65.6'$






0+18

elm 12" South 25'

19

1+0

House 
tree 
telephone P 

0+00 Cent. Cen. stoul

← 16' — 1+0 →
16'

← 15½ — 2+0 →
16½

← 15½ — 3+0 →
16

← 15½ — 4+0 →
16

9+25 Peach trees 16½ feet from $\frac{1}{2}$
 10+0 Peach trees 17 " " $\frac{1}{2}$
 10+43 " " 19 " " $\frac{1}{2}$
 10+70 Fence on north

$\leftarrow 15'3'' \quad 16'3'' \rightarrow$
 $-5+0$

$\leftarrow 15' \quad 16' \rightarrow$
 $-6+0$

$\leftarrow 15' \quad 15'9'' \rightarrow$
 $-7+0$

$\leftarrow 14'6'' \quad 16' \rightarrow$
 $-8+0$

$\leftarrow 14\frac{1}{2}' \quad 16' \rightarrow$
 $-9+0$

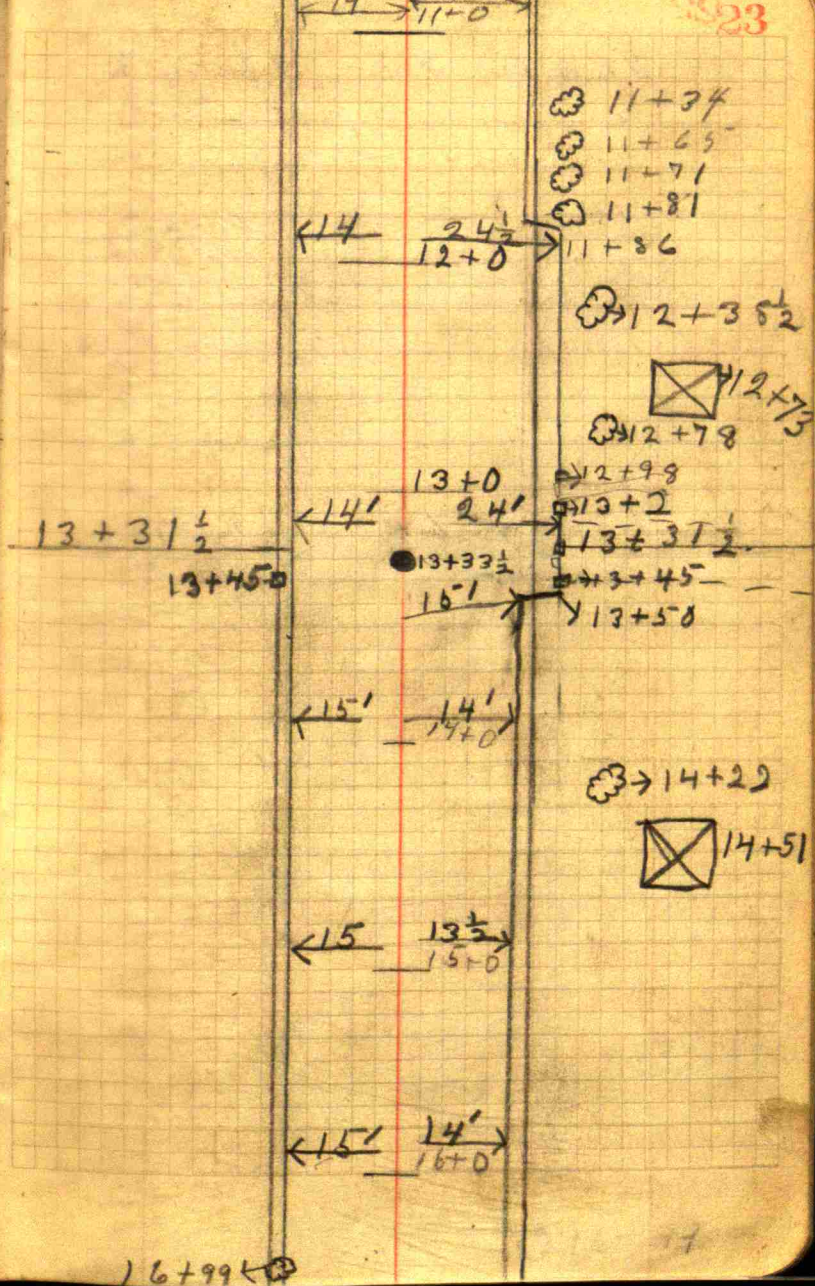
$\leftarrow 14\frac{1}{2}' \quad 15\frac{1}{2}' \rightarrow$
 $-10+0$

9+25

10+0

10+43
 +70

11+34 Peach trees 17 ft. from \ominus
 11+65 Peach trees 17 ft. " \ominus
 11+71 Peach trees 19 ft. " \ominus
 11+81 Peach trees 19 ft. " \ominus
 11+86 Fence on N - 24 $\frac{1}{2}$ ft. from \ominus
 12+38 $\frac{1}{2}$ Mulberry trees 36" 31 ft. from \ominus
 12+73 House 95 ft. " \ominus
 12+78 Rear tree 24" 40 ft. " \ominus
 12+98 Cement gate post 24 ft. " \ominus
 13+2 Cement gate post 24 ft. " \ominus
 13+31 $\frac{1}{2}$ Cement gate post & fence N - 24' \ominus
 13+31 $\frac{1}{2}$ Fence S. 15' \ominus
 13+33 $\frac{1}{2}$ \ominus^2 mile stone sec 6
 13+45 Cement gate post on N. 24' \ominus
 13+45 Gate post on S 15' \ominus
 14+22 Lydn tree 18" 18' from \ominus
 14+51 Barn 30' " \ominus
 16+99 Walnut tree 6" 16' " \ominus



21+24 Oak tree 36" 30' from R

$\leftarrow 15' \quad \begin{array}{r} 14 \\ - 17+0 \end{array} \rightarrow$

$\leftarrow 15' \quad \begin{array}{r} 14'6'' \\ - 18+0 \end{array} \rightarrow$

$\leftarrow 15' \quad \begin{array}{r} 15' \\ - 19+0 \end{array} \rightarrow$

$\leftarrow 15' \quad \begin{array}{r} 15' \\ - 20+0 \end{array} \rightarrow$

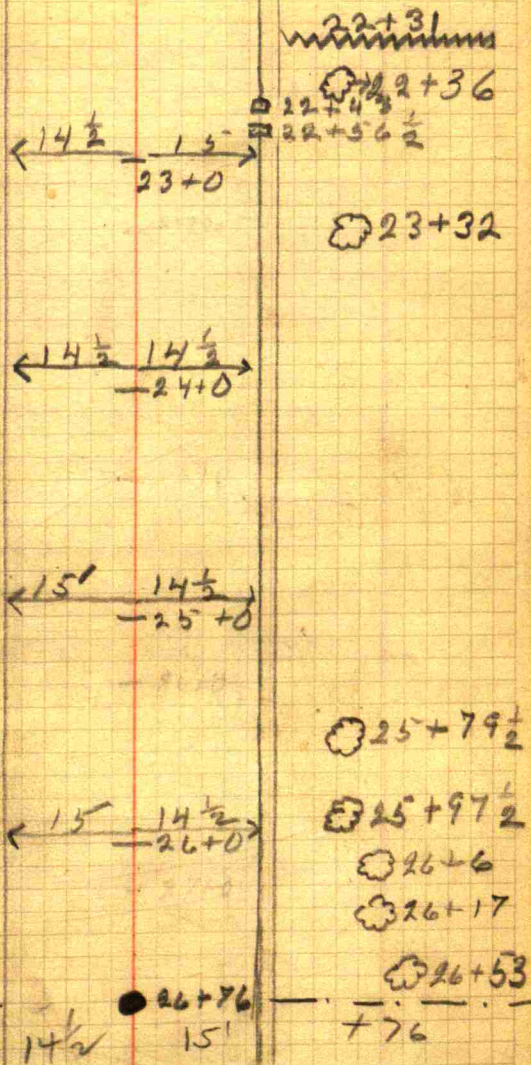
$\leftarrow 15' \quad \begin{array}{r} 15' \\ - 21+0 \end{array} \rightarrow$

$\leftarrow 14\frac{1}{2}' \quad \begin{array}{r} 15\frac{1}{2}' \\ - 22+0 \end{array} \rightarrow$

21+24

22+31 rail fence on North
 22+36 Oak tree 36" 30' ♀
 22+43 Gate post on N. 15' from ♀
 22+56 " " " N. 15' from ♀
 23+32 Oak tree 48" N 28' " ♀
 25+79½ Oak tree 24" N 28' " ♀
 25+97½ " " 24" N 24' " ♀
 26+6 " " 12" 24' " ♀
 26+17 " " 24" 26' " ♀
 26+53 " " 24" 20' " ♀
 26+76 Stone e.w.e. Sec 5

Stone Sta 26+76
 Ref R. 0°-11'



S 26

N 29

26+76

27

15 1/2 - 16'

28

15 1/2 - 16'

29

15' - 16'

4' Elm
+ 58

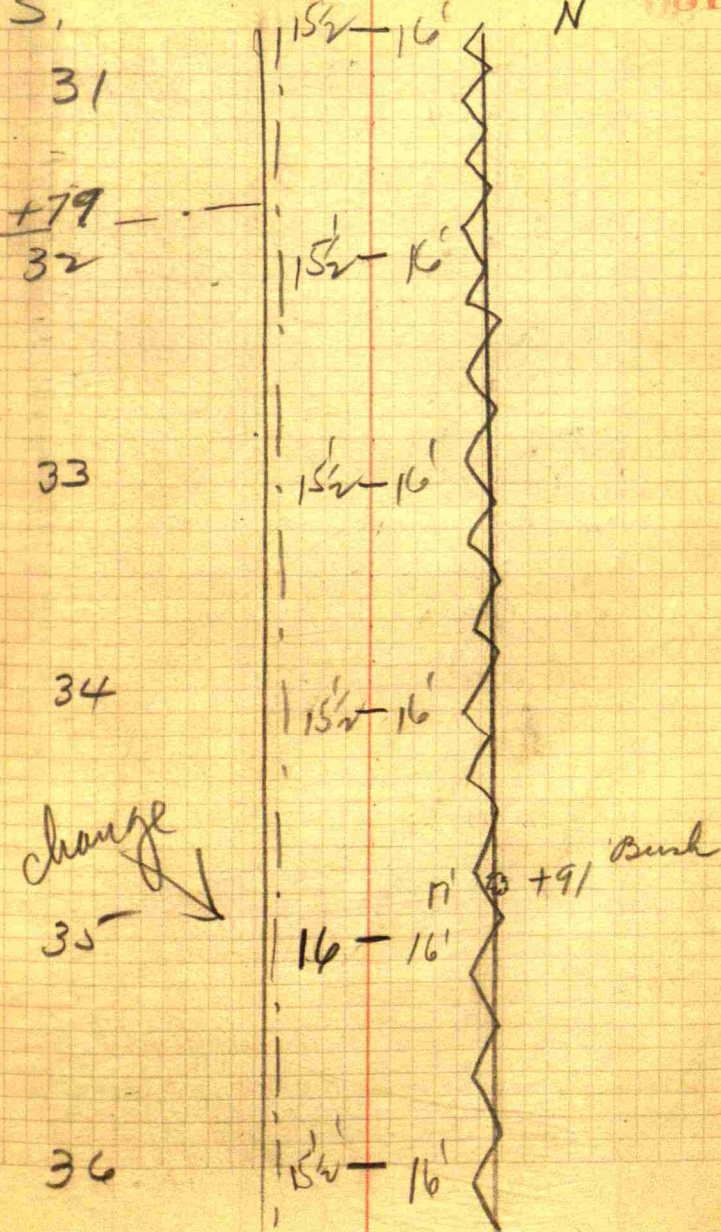
15'

30

15 1/2 - 16'

31

15 1/2 - 16'



36

+29

$15\frac{1}{2}$ - 16'

37

$15\frac{1}{2}$ - 16'

38

$15\frac{1}{2}$ - 16'

39

16' - 15'

40

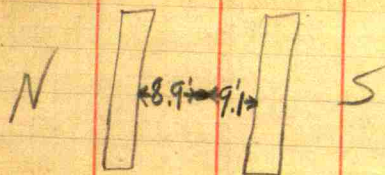
$17\frac{1}{2}$ - 15'

+0.5

+0.5

41

17' - 14'



41

17 - 14

42

17 - 14

43

17 - 14

44

17 - 14

45

17 - 14

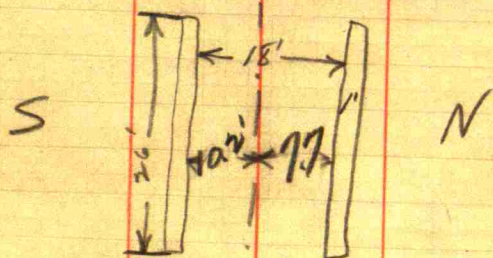
24' eye
 ← 17 - 13 + 58

46

17 - 14

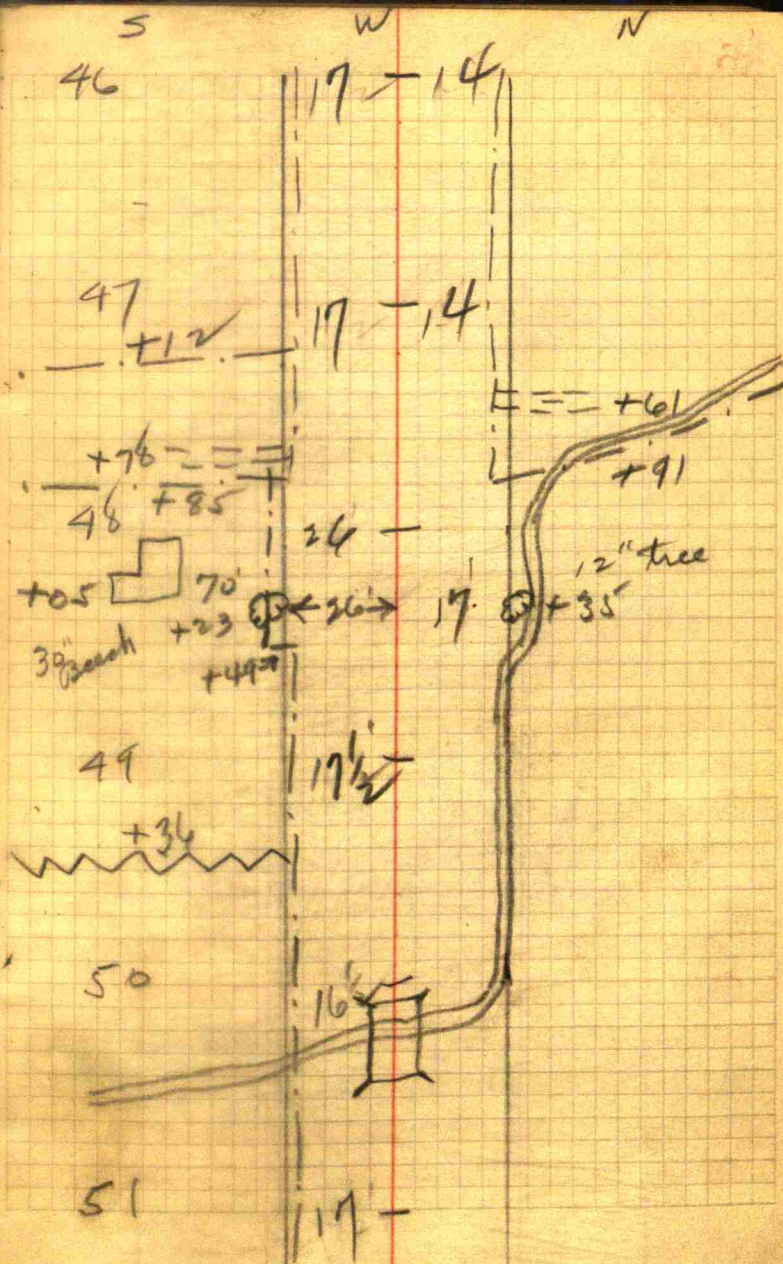
no fence along N side
from Sta 47+91 to

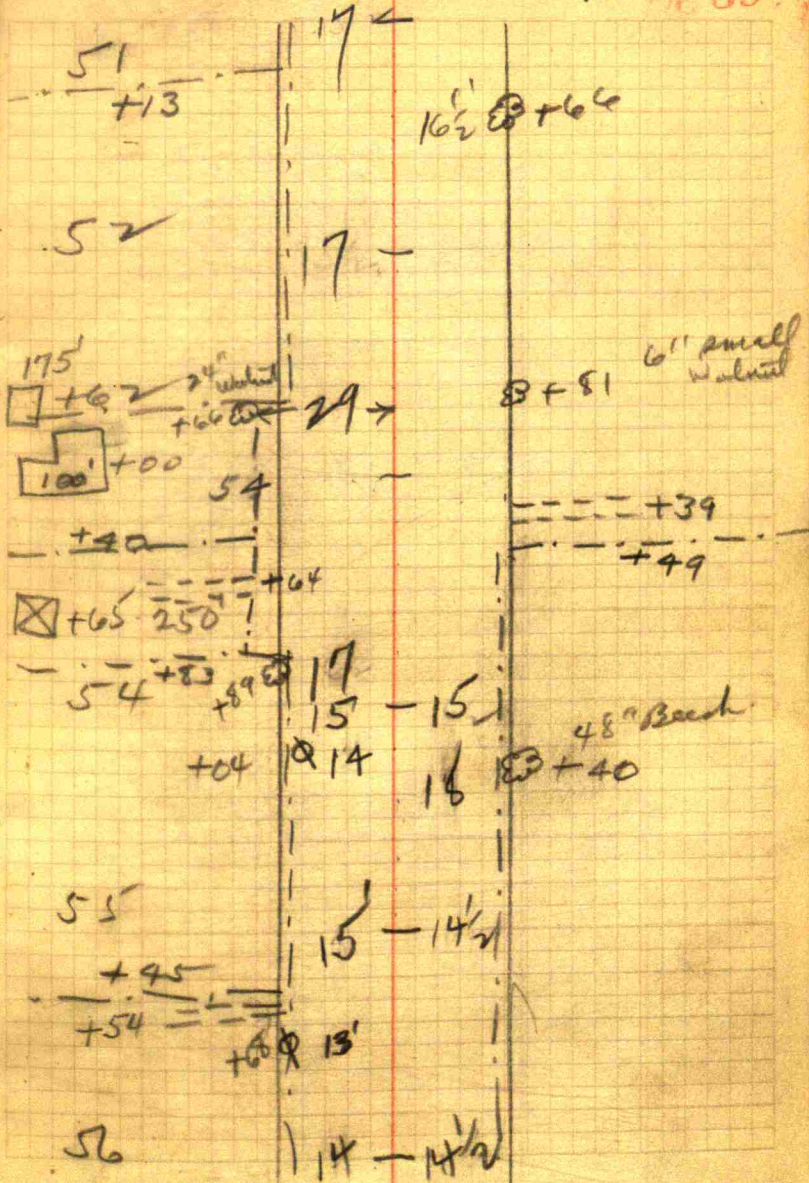
Concrete flat top
Cen. Sta. 50+07.5



12' Span
4 1/2' Rise

Center of Bridge is
Sta 50+07.5





56

14 — 14 1/2

57

14 1/2 — 14 1/2

+46 ~~14~~

58

no pencil
found

→ 13 1/2 — 14 1/2

59

+28

+25 ~~14~~

14 — 15 1/2

60

14 — 15 1/2

61

14 — 15 1/2

5

61

$\frac{11}{12}$ W $15\frac{1}{2}$ N
 $+12$ \otimes $13\frac{1}{2}$

62

$\frac{11}{12}$ - 10

63

$+90$ \otimes 4
 $\frac{11}{12}$ - $16\frac{1}{2}$

64

$\frac{11}{12}$ - $16\frac{1}{2}$

65

$+60$ \otimes 4
 $\frac{11}{12}$ - $16\frac{1}{2}$

66

$\frac{11}{12}$ - $16\frac{1}{2}$

Stone.

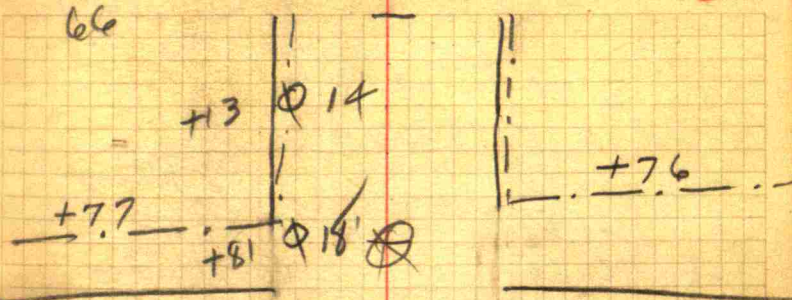
Elm. S 10° E 90'

Fence post N 45° E 26.7'

S

W

N



Road N+5 32' wide
~~66+95~~

End of Project
 66+95

66+79

28' x 12" annex in W side
 ditch of road N+5.

11' 5 of Φ
 17' 2 of Φ

Levels Over Button Rd.

Sta.	± El.	cen Rd. Rd. 50's	cen Rd. North 50'		
0+00	99.95	99.77	100.50		
1+00	101.95			N.S. ditch	S.S. ditch
2+00	101.93			14'	12'
3+00	101.60				
4+00	101.20				
5+00	100.95				
6+00	100.36				
7+00	100.15				
8+00	100.32				
9+00	100.69	8+65		12' N.S. ditch	12' S.S. ditch
10+00	101.10			99.30	100.36
11+00	101.78				99.28
12+00	102.82				
13+00	103.53				
14+00	109.70				
15+00	103.45				
16+00	102.27				
17+00	101.45				
18+00	100.99				
19+00	100.70				
20+00	100.82				
21+00	100.73	21+50		11½' N.S. ditch	12½' S.S. ditch
22+00	100.80			99.64	100.87
					99.60

B.M. on N. end of E. rail of
Culvt. 200' S. of 0+00
E.L. 100.00

100.15

○

○ 100.21

○ 100.68

B.M. on S.E. corner of concrete
pavement E.L. 104.41

Sta ϕ E1.

23+0 101.15
 24+0 102.19
 25+0 101.73
 26+0 101.15
 27+0 101.30
 28+0 101.58
 29+0 101.50
 30+0 101.46
 31+0 101.48
 32+0 101.19
 33+0 101.88
 34+0 101.84
 35+0 101.73
 36+0 102.38
 37+0 102.28
 38+0 101.77
 39+0 100.60
 40+0 100.50
 41+0 100.56
 42+0 99.96
 43+0 99.31
 44+0 99.25
 45+0 99.19
 46+0 98.34
 47+0 97.04

11 $\frac{1}{2}$ ' 12 $\frac{1}{2}$ '
 N.S. ~~101.47~~ 88 ~~100.89~~ ~~101.47~~
 99.67 99.63

⊙ 101.47
 100.89

50
Sta & El.
48+0 94.52
49+0 92.10
50+0 93.81
51+0 94.50
52+0 97.44
53+0 98.45
54+0 98.29
55+0 97.14
56+0 96.45
57+0 96.22
58+0 97.65
59+0 97.55
60+0 97.75
61+0 97.60
62+0 96.83
63+0 96.98
64+0 96.83
65+0 96.25
66+0 95.71
66+79 95.56
66+95 95.81
50' N. 95.75
50' S. 95.00
50' E. 96.00

FI. S	FI. N
11	
50'	50'
Cent Rd S	Cent Rd N
93.60	93.95
Top	Top
94.49	94.80

B.M. on W. end N. rail of 51
bridge Sta. 50+07.5
El. — 95.70

Bridge El.
Bed of stream — 87.92
Top of Slab — 93.69
& 50+07.5 — 94.02

⊙ 97.60 BM 99.92
⊙ 95.26
⊙ 95.70

B.M. on top of NE corner post
El 99.92
20' NE of station 66+95.

0+20	100.00	101.21	Frst	7 ill
1+20	101.00	103.30	2-3 1/4	
2+20	101.72	103.85	2-1 1/4	
2+0	100.80	103.13	2-3 3/4	
4+0	99.60	99.29		0-4
5+0	98.40	97.62		0-9
6+0	97.20	95.40		1-9 3/4
6+75	96.30	94.34		1-11 1/2
8+0	95.20	94.94		0-3
9+0	94.40	95.09	0-8	
10+0	93.60	100.02	6-4 3/4	
11+0	92.80	90.14		2-8
12+0	92.80	92.11		0-8
13+0	93.15	91.70		1-5
14+0	93.50	93.46		0-1 1/2
15+0	93.85	93.32		0-6
16+0	94.20	96.96	2-9	
16+93	94.54	94.53		Id
17+43	94.71	92.91		1-9 1/2
18+43	95.05	91.52		3-6 1/2
19+43	95.39	92.35		3-0 1/2
20+43	95.73	92.34		3-4 3/4
21+43	96.10	96.27	0-2	

53

97.20

90

95.46

900

75

9000

9014

99.73

93.15

266

99.90

91.90

93.85

98.40

93.90

1.40

1.72

97.60

95.10

95.73

2.13

92.34

78

93.60

80

94.67

3.39

6.40

53

103.13

96.96

80

95.20

94.94

94.20

1.33

95.26

95.09

94.40

92.76

92.80

92.11

95.05

69

91.54

94.71

3.53

92.91

1.80

304

B.M. on N.W. Rail of Bridge

Cl. 96.13

From B run East 1187' to corner
Boyd Rd at ①. Continue E 103' to ②
Then N 554 to Hicks N line. Then E on
Hicks N line 407' to ④ Def L 108° 26'
Def R —

From ② Continue E 1025'
556 to Hicks N. line at ⑦ Cont
Continue N 18° W 379' to ⑨ —
Cory Ann Rd at ⑩ — Continue
Cont W 317' to ⑬ at NE cor old
Cem ⑭ Def L 48°-53' — and Run
Def R 29°-43' — and run S
street — Cont 570°-17' W — 1446
570°-17' W — 770' to Cem Rd
① Def L 70°-25' to I

④ is 279' W of McClelland SW cor
and run N 18°-26' W — 488' to ⑤

to ⑥ Def L 90°-18' Run N 18° W
to old 1126' to E Wal Rd at ⑧
Def L 90°-15' ^{589°-27'} Run W 332' to
W to NE Cor Cem at ⑪ 197' —
at Cem. Cont W 715' to N W cor
540°-34' W 349' to Cor Cem ⑮
70°-17' W — 330' to Cem Main VHS
to A. Roberts E line fence ⑫ Cont
⑬ — Cont 570°-17' W — 350' to

$$\begin{array}{r} 103 \\ 688 \\ \hline 791 \end{array}$$

$$\begin{array}{r} 103 \\ 907 \\ 279 \\ \hline 789 \end{array}$$

(10) is 77' N of NE cor Wilson
Cen N Rd is 418'

(11) is 139' N of N line st -
Cen N of N line st

(18) is 477' N of NW cor

(18) is 646' N of N line Nat

Add at (12) - (12) 5 to (3) at
(8) W to (3) = 354'

(15) is 278' N of SW cor

Rebards add in Cen Rd
Road.

68

Curb + Gutter on N. Wash.

*

	Top Sta	2' W.	5' W. <small>on curb</small>	E
0+0	15.09	15.09	14.89	14.95
0+50	12.69	12.11	12.11	12.13
1+0	9.64	9.12	9.36	9.54
1+50	7.83	7.44	7.30	7.41
1+95	5.61	5.21	5.26	5.49

E Lawton Ave - 5.10

B.M. on West end 69
 of Howell on W. side of
 Rd. west of Sta 0+85
 E.L. 10.00

A - B	63.8'	} 275.6'
B - D	15.8'	
D - E	58'	
E - F	138'	

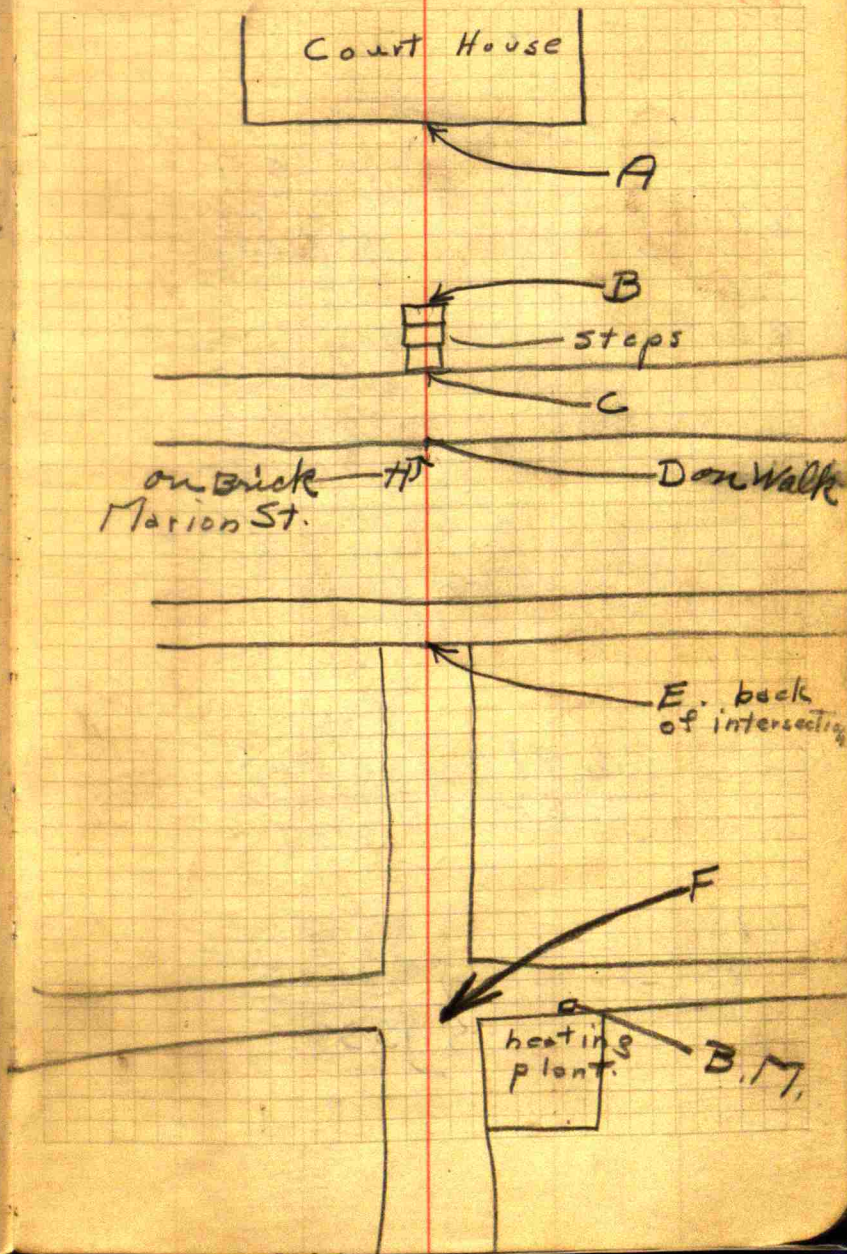
B.M. on sidewalk at edge of Courthouse

El. 100.00

A.	100.00
B.	95.45
C.	93.64
D.	93.44
H.	92.77
E.	93.50
F.	87.58

○ 95.94

B.M. on concrete ledge
East side of double doors
of Heating plant.
El. 91.02



Tile -
Stk Gd. Cut.

0+00	103.05	100.00	3'-8 $\frac{1}{2}$ "
1+00	104.58	100.50	4'-1"
2+00	105.62	101.00	5'-8"
3+00	106.30	101.50	4'-9 $\frac{1}{2}$ "
4+00	107.08	102.00	5'-1"
5+00	107.34	102.50	4'-10"
5+50	107.32	102.75	4'-7"
6+00	107.12	103.00	4'-1 $\frac{1}{2}$ "
6+50	107.22	103.16	4'-0 $\frac{3}{4}$ "
7+00	107.40	103.32	4'-1"
7+50	107.45	103.48	3'-11 $\frac{1}{2}$ "
8+0	107.45	103.64	3'-11"
8+50	107.70	103.80	3'-10 $\frac{1}{2}$ "
9+0	107.25	103.96	3'-3 $\frac{1}{2}$ "
9+50	107.20	104.12	3'-1"
10+0	107.58	104.28	3'-3 $\frac{1}{2}$ "
10+50	108.00	104.44	3'-7"
11+0	108.25	104.60	3'-4 $\frac{1}{2}$ "
11+50	108.29	104.76	3'-6 $\frac{1}{2}$ "
12+0	108.31	104.92	3'-4 $\frac{3}{4}$ "
12+50	108.10	105.08	3'-0 $\frac{1}{4}$ "

10396
16
17

10732
10275
457

10745
10364
381

10492
16
08

Fl. of Fl. 100.00

107.08

10630
10150
480

10800
10444
356

10730
10230
500

650
200.00
1450
500

10745
10348
397

10800
10400
400

108.10

108.29
10476
353

16.5
40
660.0

108.10
10508
302

12.50
5.00.0
5000

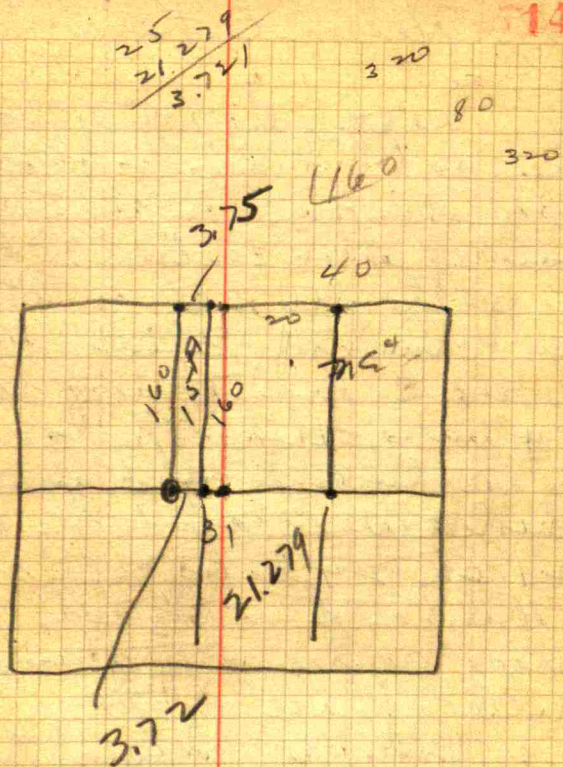
10734
10250
484

10725
10396
329

10831
10492
339

Pt of the E² of the NW⁴
 31-17-2 E. and bounded
 as follows. Commencing at
 a point 25 ch W of the
 NE corner of the W² of the
 NE⁴. and running thence
 S 160 R.A. to the half section
 line thence E on the half
 section line to a point
 21.279 ch W of the SE
 corner of the W² of the NE⁴
 thence N running parallel
 with the 1st line being 160 R.A.
 to the Sec. line thence W
 on Sec line 3.75 ch to
 to place of beg.

15 a. more or less



Case.

a pt. of the NW⁺ of Sec 31-17-
 2E. and bounded as follows - to wit
 Beg. at a point on the S line of
 said quarter section 15 ch 22 links
 E of the SW corner thereof
 and running thence East
 on the S line thereof 20 ch
 34 links; thence N 40 ch to
 the N line of said quarter sec.
 thence W on said N line
 21 ch 24 links to a stone
 thence S 5 3/8 rods to a
 stone continuing thence S,
 to the place of beg.

Est. to contain 83.71 a
 more or less.

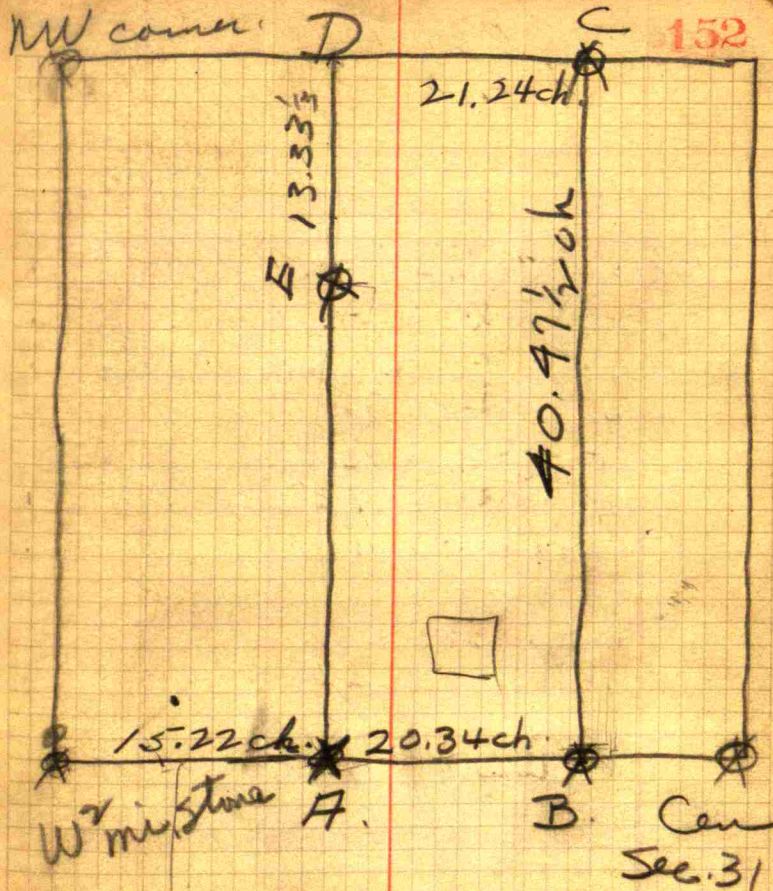
Nelson E. Kern,
Pt. NW⁴ Sec 31-17-2E.

A. - Set stone at SW
corner of N.E. Kern 83 a.
Wit. Stone - N^o - 40 links
B - Set stone at SE
corner of N.E. Kern's 83 a.
between Kern + S. Ennis
Wit. Stone. - N^o E. 30 links

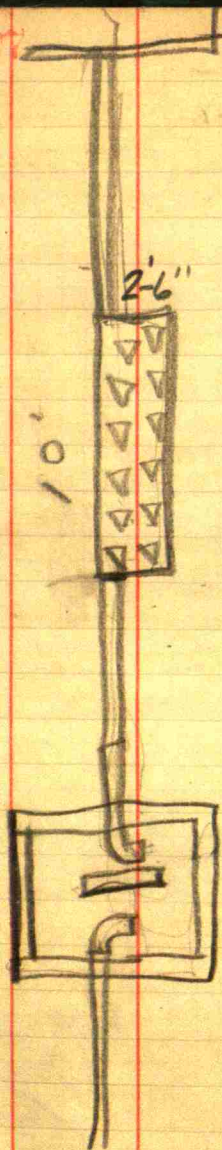
C - Stone
B to C - 40.47½ ch.

C to D. - 21.24 ch.
Set stone

Found two stones at
the W² mile of Sec 31-17-
2E. - W² mi. stone of
31-17-2C is 10' N of
the E² mi stone of sec
36-17-1E.



157



Brownburg - 158
 Green St.
 Height of curb - W. side

0+0 - 9½"

0+25 - 11"

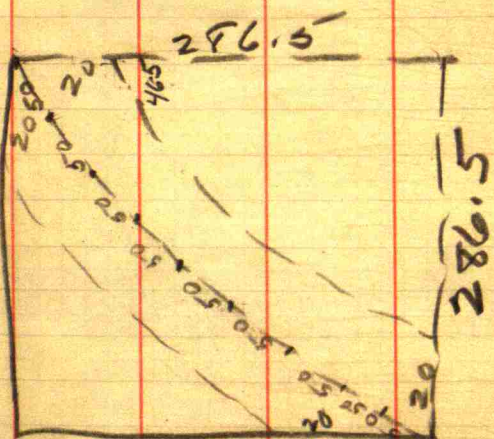
0+50 - 12½"

$\Delta 90^\circ$
 $L 450'$
 $D = 20'$

$$T = \frac{5730}{20} = 286.5'$$

$$E = \frac{2373.4}{20} = 118.67'$$

$$R = 286.5$$



PI

$$286.5 : 266.5 = 50 : X$$

Angle.	Sine.	Tan.	Sec.	Cosec.	Cotg.	Cosin.	Angle.	Sine.	Tan.	Sec.	Cosec.	Cotg.	Cosin.
0	0	0	1.	∞	∞	1.	90	1.	0	0	∞	0	0
10	.0029	.0029		343.8	343.8	1.	50	.1392	.1405	1.0098	7.185	7.115	.99027
20	.0058	.0058		171.9	171.9	.99998	40	.1421	.1435	1.0102	7.040	6.968	.98988
30	.0087	.0087		114.6	114.6	.99996	30	.1449	.1465	1.0107	6.900	6.827	.98944
40	.0116	.0116	1.0001	85.94	85.94	.99993	20	.1478	.1495	1.0111	6.768	6.691	.98902
50	.0145	.0145	1.0001	68.76	68.75	.99989	10	.1507	.1524	1.0115	6.636	6.561	.98858
1	.0175	.0175	1.0002	57.30	57.29	.99985	80	.1536	.1554	1.0120	6.512	6.435	.98814
10	.0204	.0204	1.0002	49.11	49.10	.99979	50	.1564	.1584	1.0125	6.394	6.314	.98769
20	.0233	.0233	1.0003	42.98	42.96	.99973	40	.1593	.1614	1.0129	6.277	6.197	.98723
30	.0262	.0262	1.0003	38.20	38.19	.99966	30	.1622	.1644	1.0134	6.166	6.084	.98676
40	.0291	.0291	1.0004	34.38	34.37	.99958	20	.1650	.1673	1.0139	6.059	5.976	.98629
50	.0320	.0320	1.0005	31.28	31.24	.99949	10	.1679	.1703	1.0144	5.955	5.871	.98580
2	.0349	.0349	1.0006	28.85	28.84	.99939	88	.1708	.1733	1.0149	5.855	5.769	.98531
10	.0378	.0378	1.0007	26.45	26.43	.99929	50	.1736	.1763	1.0154	5.759	5.671	.98481
20	.0407	.0407	1.0008	24.56	24.54	.99917	40	.1765	.1793	1.0160	5.665	5.576	.98430
30	.0436	.0437	1.0010	22.93	22.90	.99905	30	.1794	.1823	1.0165	5.575	5.485	.98378
40	.0465	.0466	1.0011	21.49	21.47	.99892	20	.1822	.1853	1.0170	5.488	5.396	.98325
50	.0494	.0495	1.0012	20.23	20.21	.99878	10	.1851	.1883	1.0176	5.403	5.309	.98272
3	.0523	.0524	1.0014	19.11	19.08	.99863	87	.1880	.1914	1.0181	5.320	5.226	.98218
10	.0552	.0553	1.0015	18.10	18.07	.99847	50	.1908	.1944	1.0187	5.241	5.145	.98163
20	.0581	.0582	1.0017	17.20	17.17	.99831	40	.1937	.1974	1.0193	5.164	5.066	.98107
30	.0610	.0612	1.0019	16.38	16.35	.99813	30	.1965	.2004	1.0199	5.089	4.989	.98050
40	.0640	.0641	1.0020	15.64	15.60	.99795	20	.1994	.2035	1.0205	5.016	4.915	.97992
50	.0669	.0670	1.0022	14.96	14.92	.99776	10	.2022	.2065	1.0211	4.945	4.843	.97934
4	.0698	.0699	1.0024	14.34	14.30	.99756	86	.2051	.2095	1.0217	4.877	4.773	.97875
10	.0727	.0729	1.0027	13.76	13.73	.99736	50	.2079	.2126	1.0223	4.810	4.705	.97815
20	.0756	.0758	1.0029	13.23	13.20	.99714	40	.2108	.2156	1.0230	4.745	4.638	.97754
30	.0785	.0787	1.0031	12.75	12.71	.99692	30	.2136	.2186	1.0236	4.682	4.574	.97692
40	.0814	.0816	1.0033	12.29	12.25	.99668	20	.2164	.2217	1.0243	4.620	4.511	.97630
50	.0843	.0846	1.0036	11.87	11.83	.99644	10	.2193	.2247	1.0249	4.560	4.449	.97566
5	.0872	.0875	1.0038	11.47	11.43	.99619	85	.2221	.2278	1.0256	4.502	4.390	.97502
10	.0901	.0904	1.0041	11.10	11.06	.99594	50	.2250	.2309	1.0263	4.445	4.331	.97437
20	.0929	.0934	1.0043	10.76	10.71	.99567	40	.2278	.2339	1.0270	4.390	4.275	.97371
30	.0958	.0963	1.0046	10.43	10.39	.99540	30	.2306	.2370	1.0277	4.336	4.219	.97304
40	.0987	.0992	1.0049	10.13	10.08	.99511	20	.2334	.2401	1.0284	4.284	4.165	.97237
50	.1016	.1022	1.0052	9.839	9.788	.99482	10	.2363	.2432	1.0291	4.232	4.113	.97169
6	.1045	.1051	1.0055	9.567	9.514	.99452	84	.2391	.2462	1.0299	4.182	4.061	.97100
10	.1074	.1080	1.0058	9.308	9.255	.99421	50	.2419	.2493	1.0306	4.133	4.011	.97030
20	.1103	.1110	1.0061	9.065	9.010	.99390	40	.2447	.2524	1.0314	4.086	3.962	.96959
30	.1132	.1139	1.0065	8.834	8.777	.99357	30	.2476	.2555	1.0321	4.039	3.914	.96887
40	.1161	.1169	1.0068	8.614	8.556	.99324	20	.2504	.2586	1.0329	3.994	3.867	.96815
50	.1190	.1198	1.0072	8.405	8.345	.99290	10	.2532	.2617	1.0337	3.949	3.821	.96742
7	.1219	.1228	1.0075	8.206	8.144	.99255	88	.2560	.2648	1.0345	3.906	3.778	.96667
10	.1248	.1257	1.0079	8.016	7.953	.99219	50	.2588	.2679	1.0353	3.864	3.732	.96593
20	.1276	.1287	1.0082	7.834	7.770	.99182	40	.2616	.2711	1.0361	3.822	3.689	.96517
30	.1305	.1317	1.0086	7.661	7.596	.99144	30	.2644	.2742	1.0369	3.782	3.647	.96440
40	.1334	.1346	1.0090	7.496	7.429	.99106	20	.2672	.2773	1.0377	3.742	3.606	.96363
50	.1363	.1376	1.0094	7.337	7.269	.99067	10	.2700	.2805	1.0386	3.703	3.566	.96285
							82	.2728	.2838	1.0394	3.665	3.526	.96208
							74						

Cosin. Cotg. Cosec. Sec. Tan. Sine. Angle.

Cosin. Cotg. Cosec. Sec. Tan. Sine. Angle.