

STANLEY J.
Cook.
R.D.

146

6

STANLEY J.

COOK

May 18, 1926

Stanley Cook Rd.

Stone - 0+00

Wit. - Tel. pole N15°E 28.5
Car post S45°W 22'

Stone - 26+66

Wit:

NE cor. house 68 link

NW cor House 73½ link

Stone - 53+32.5 (26, 27, 34, 5)

Wit:

Fire plug S30°W 62.0

SW cor of brick

foundation of house E-47.0'

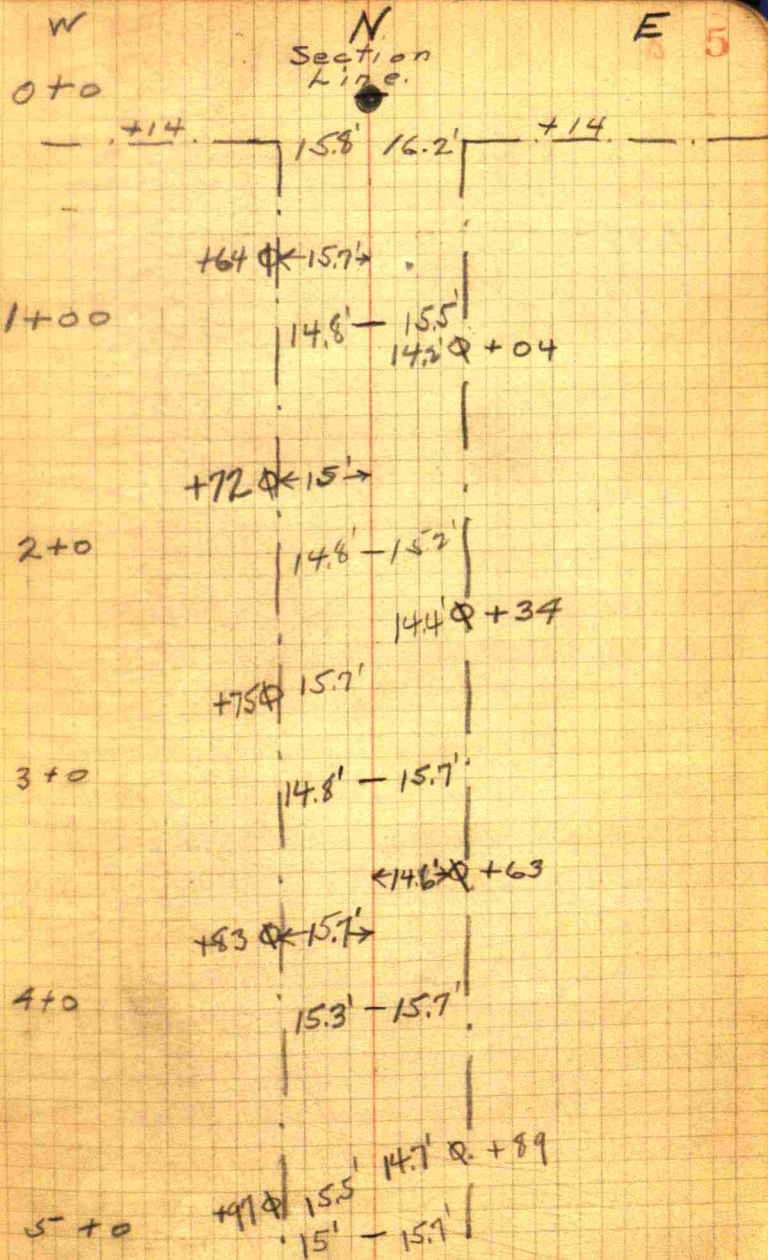
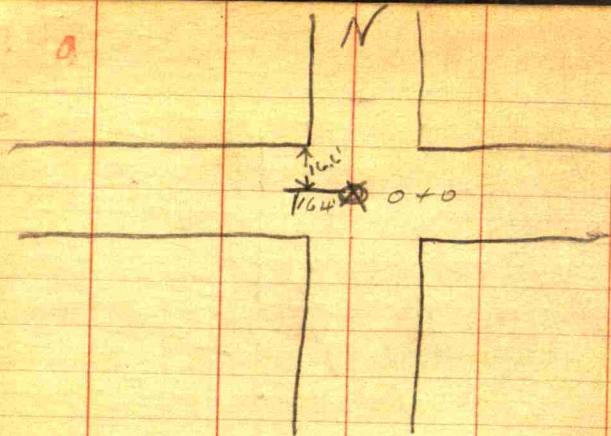
$$\begin{array}{r}
 .66 \\
 68 \\
 \hline
 528 \\
 396 \\
 \hline
 44.88
 \end{array}$$

$$\begin{array}{r}
 73.5 \\
 66 \\
 \hline
 4410 \\
 4410 \\
 \hline
 48.510
 \end{array}$$

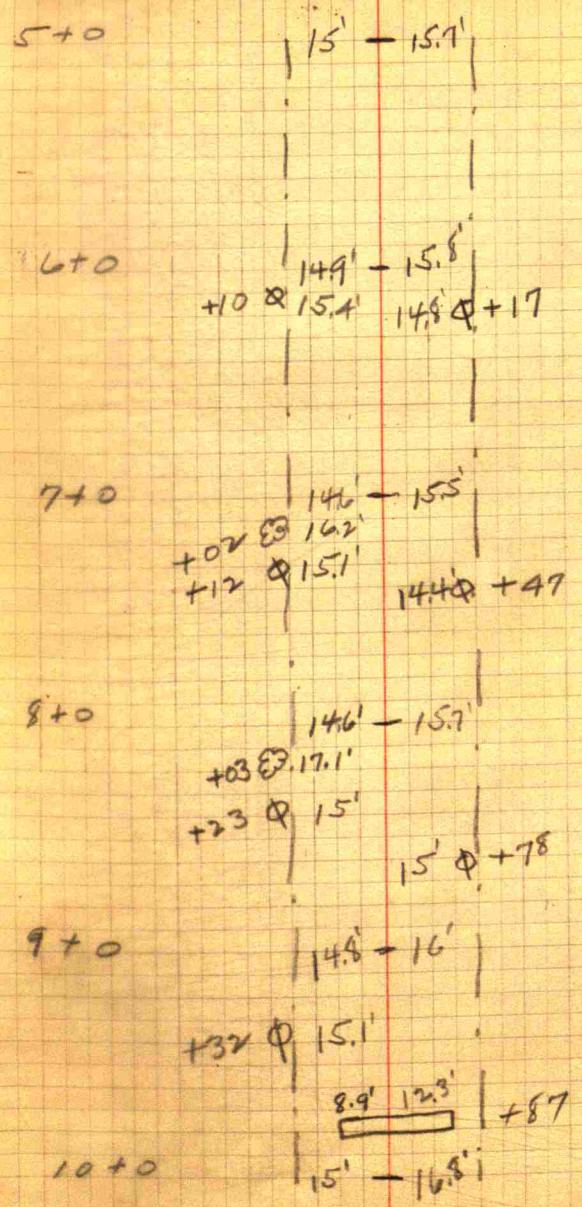
⊙ 106.59

⊙ 107.28

$$\begin{array}{r}
 65. \\
 37. \\
 \hline
 48. \\
 13
 \end{array}$$



9+87 - Culvert.
20" Vit. Tile



W

N

E

9

10+0

15' - 16.8'

14.8' + 06

+44' 15.1'

11+0

15.1' - 16.2'

15.1' + 35

+46' 15.4'

--- + 89 gate

12+0

14.7' - 16.6'

+46' 15.5'

15.2' + 65

13+0

14.9' - 15.6'

+48' 15.3'

+ 23

14+0

14.5' - 15.9'

15.1' + 94

+51' 14.8'

+ 88

125'

15+0

14.4' - 15.5'

10

Note!

Stakes from 0+00 to 16+00
inclusive are set 19' from ϕ
Begin with 17+00 - set 13'
from ϕ

15+0

14.4' - 15.5'

14.8' ϕ +24+55 ϕ 14.8'

16+0

14.2' - 15.4'

gods +41 =

+71 ϕ 14'15' ϕ +53

+41 gts

+47

17+0

13.5' - 16.4'

18+0

+74 ϕ 14.3'

13.5' - 16.3'

19+0

+57 ϕ 15'

13.6' - 17.2'

15.1' ϕ +01

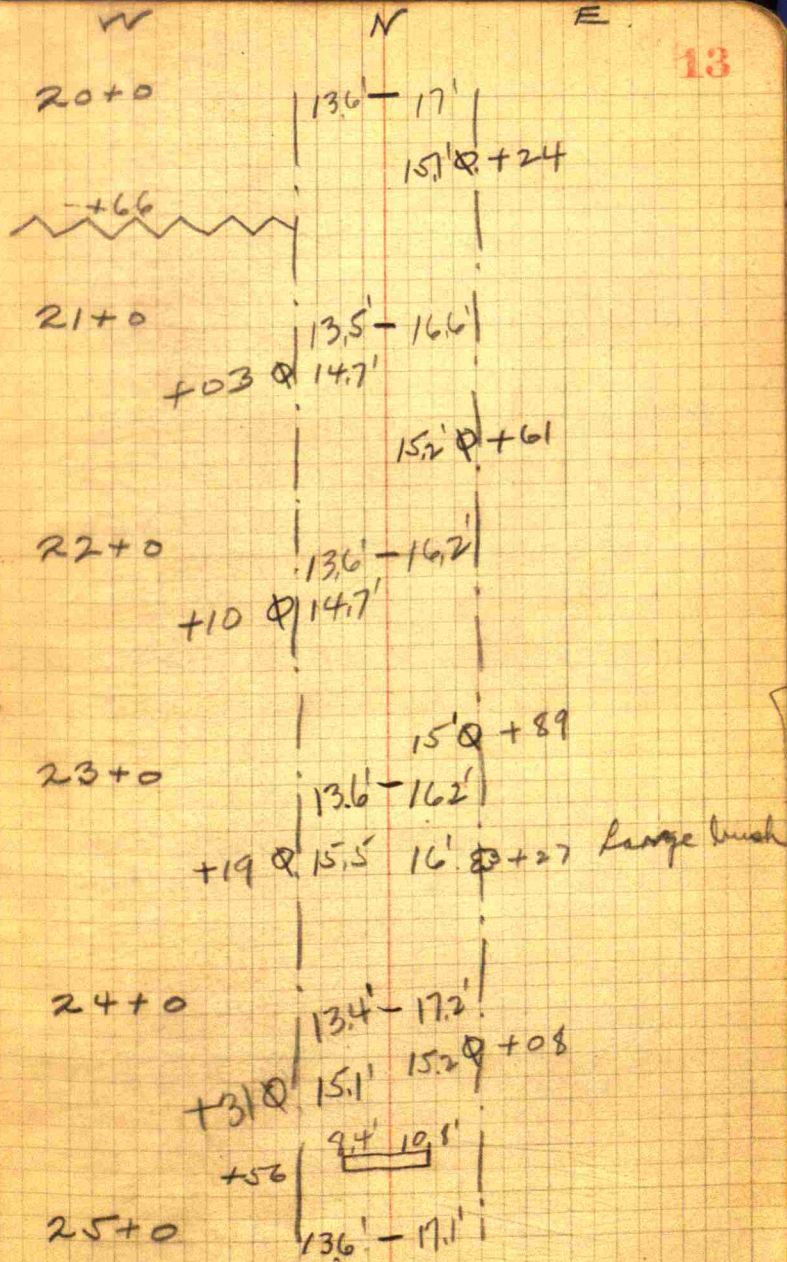
20+0

+97 ϕ 14.4'

13.6' - 17'

E.

11

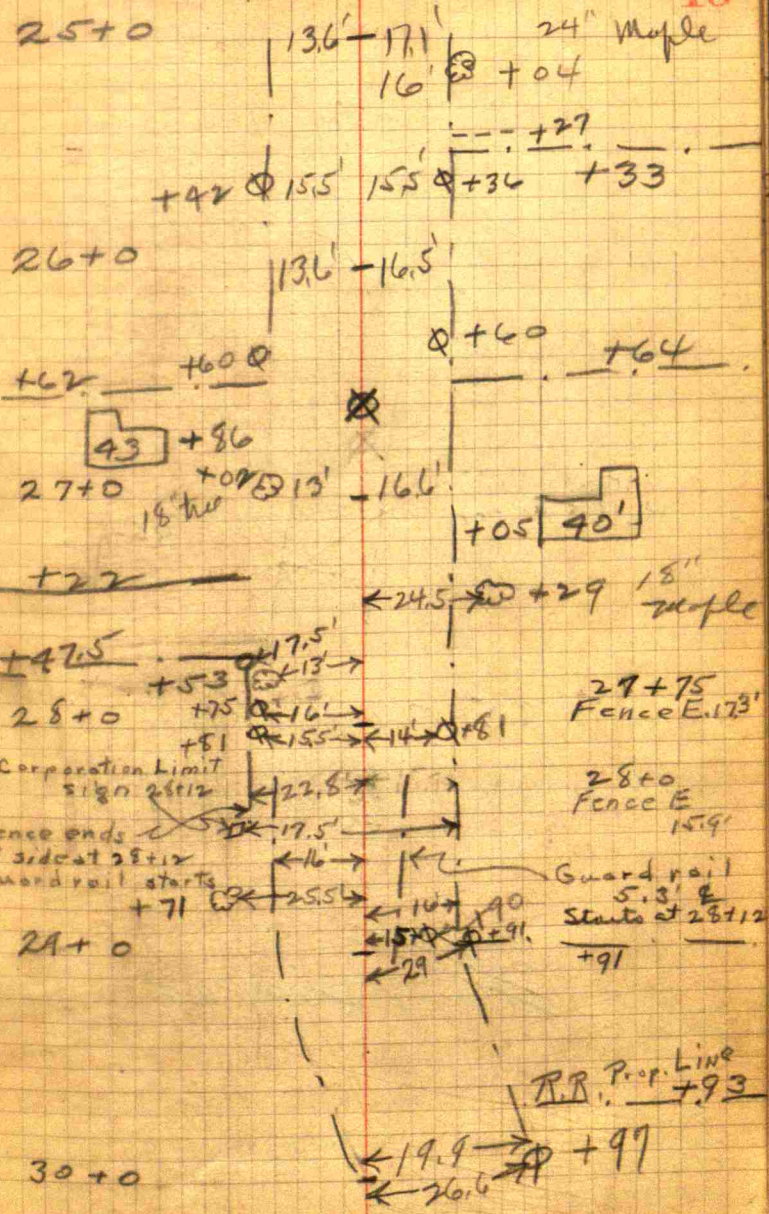


1/2 mi stone 26+66

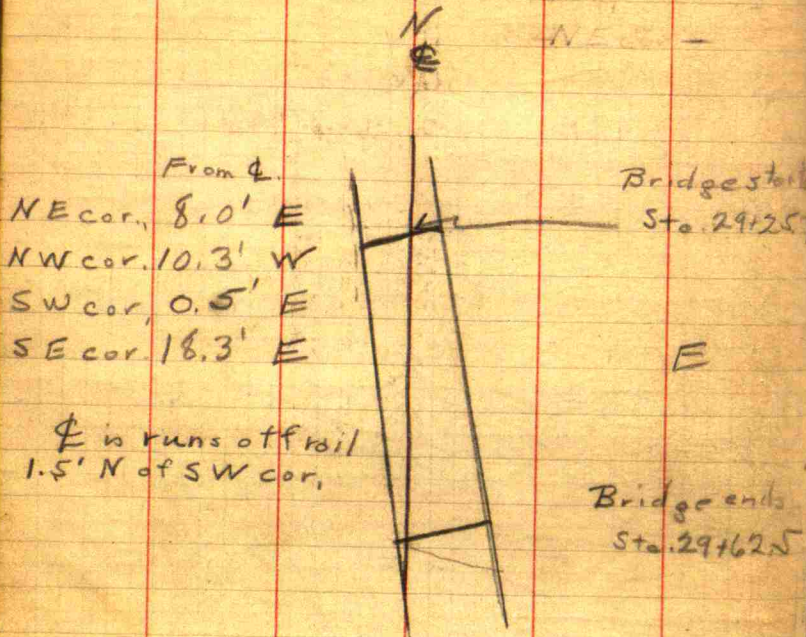
Guard rail E. side
 28+12 - 5.3' from E
 28+42 - 3.9' from E
 29+0 - 3.0' " E

Guard rail W side
 28+12 - 16' from E
 28+42 - 18' " " "
 29+0 - 16.4' " E

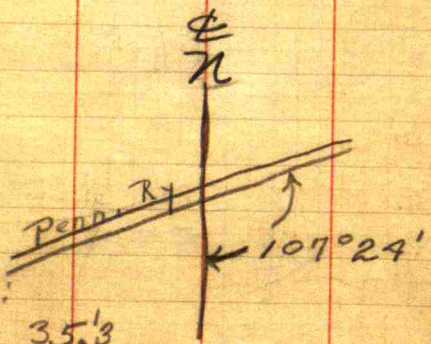
W Guard Rail is E of E
 29+75 2.6'
 29+85 3.0'
 30+0 2.8'
 E Guard Rail is E of E
 29+75 - 20.6'
 29+85 - 21.5'
 30+0 - 22.1'



30+80 - Canning Factory
200' E of Sec. Line

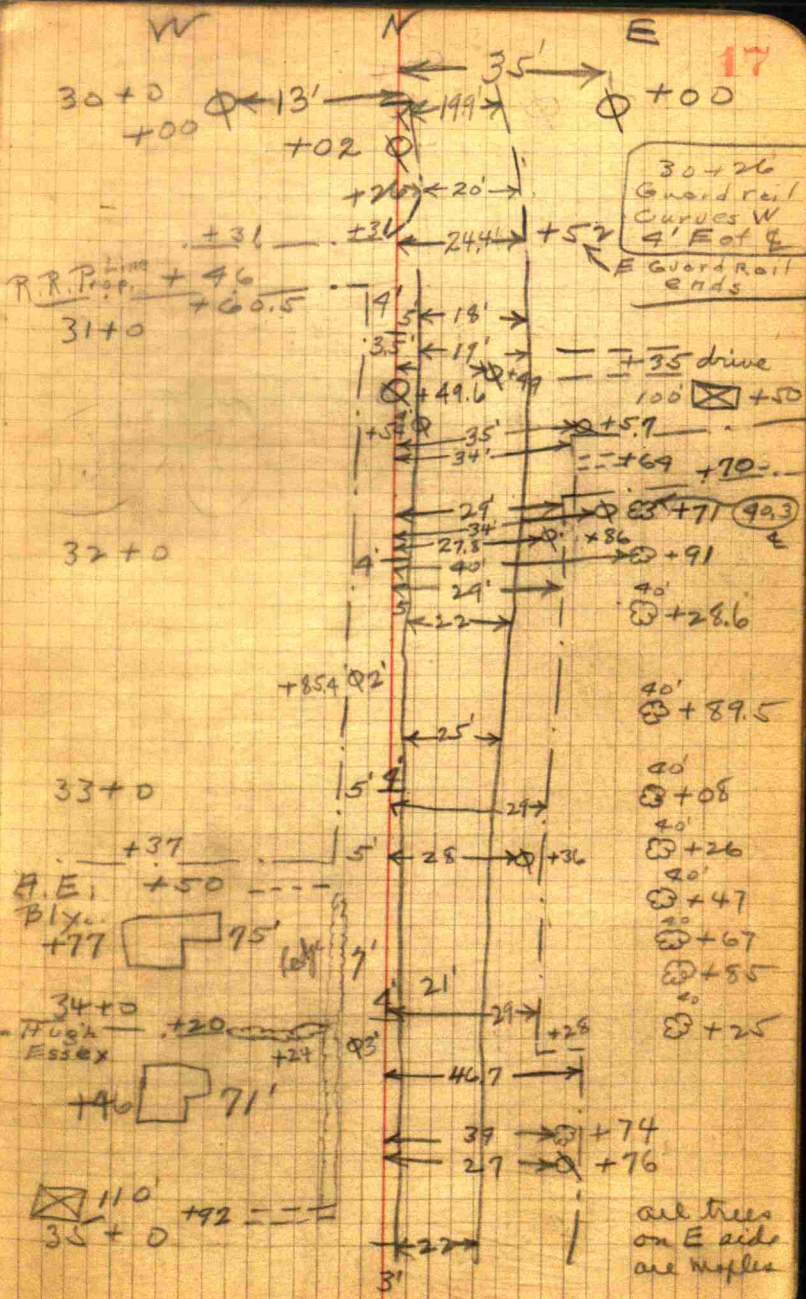


Sta. 29+42.5 N. rail of track



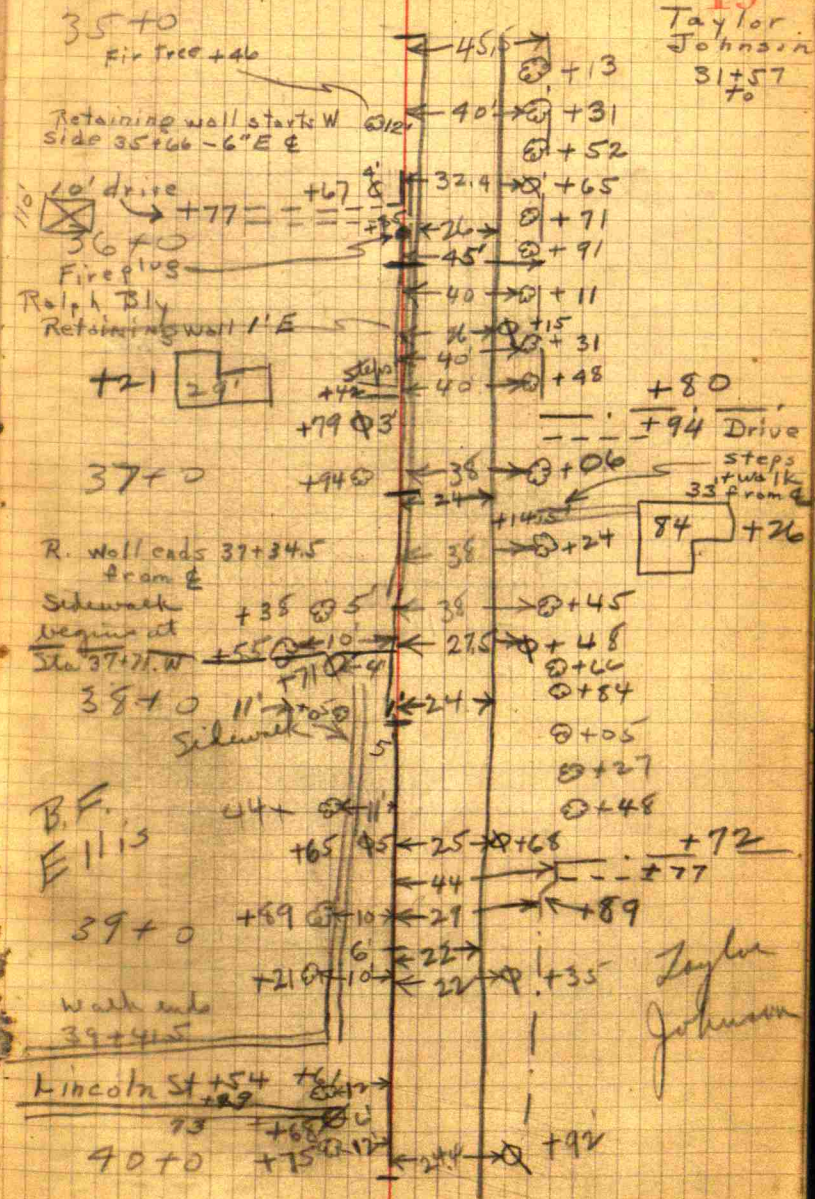
Bridge:

length 35.3
 width 18.3'
 Height from track to floor of bridge
 is 24.5'



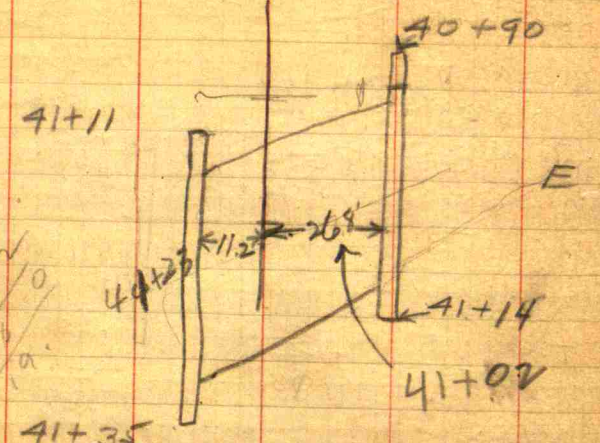
Ralph Bly - N property line
 is 35+0 - S prop. line
 Retaining Wall in front of
 Ralph Bly's house with gutter wide

B.F. Ellis - Vacant Lot
 S of Ralph Bly
 S.P.L. of Bly + N.P.L.
 of B.F. Ellis - 37+58



Taylor
 Johnson

N
Sec
line



Rails -

Length - 23.8' W - E - 24.2'

Width - 1'

Rd way between rails 38'

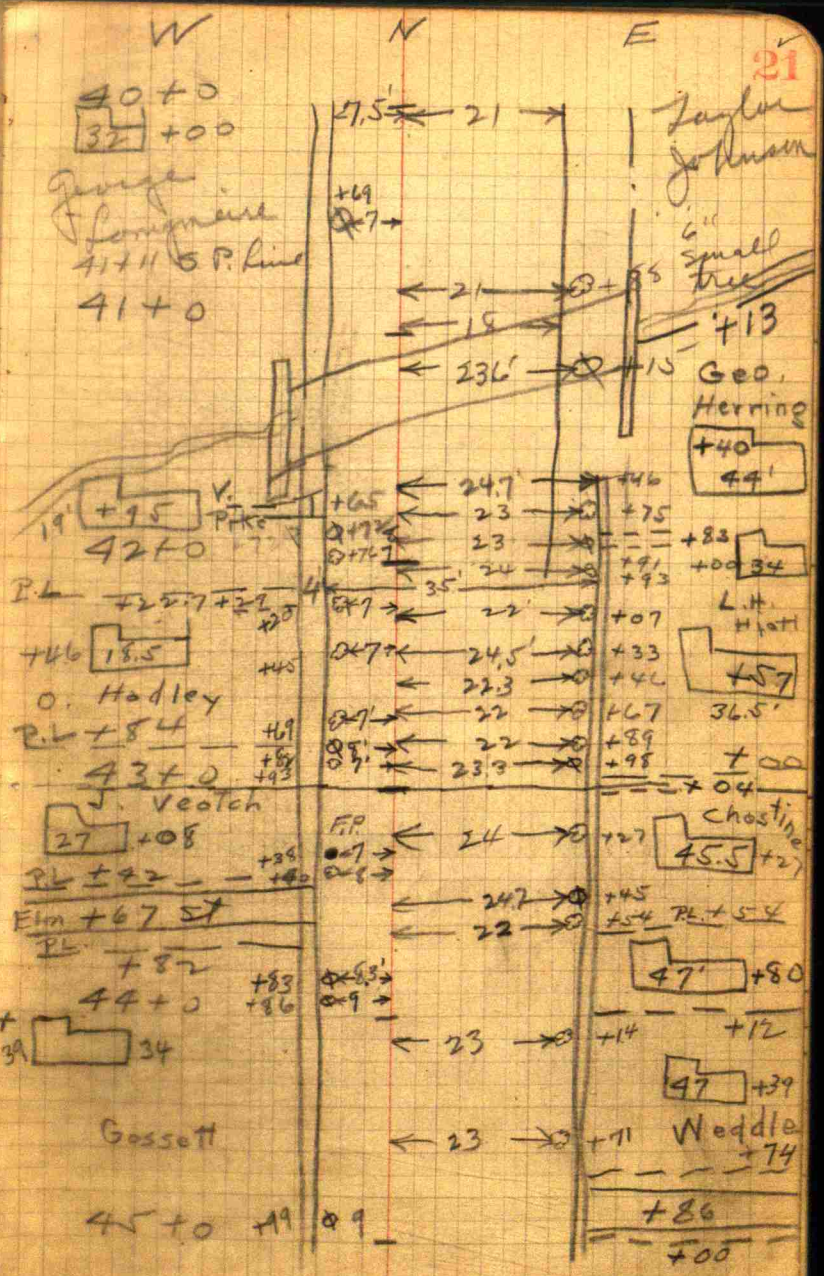
side walks 28.4'

Sidewalk begins on E side at 41+40

Between sidewalks Sta 42+0 - 35'

- Sta 43+0 - 26.3' E - W - 9.4'
- " 44+0 - 26.3' E - W - 10.3'
- " 45+0 - 26' E - W - 11.0'

26.8
11.2
39.0
10.0



40+0
32+00

Gauge
41+11.5 P. line
41+0

19' +15 V. Pike
42+0

P.L. +22.7 +22.5
+46 18.5
+45

O. Hadley
P.L. +84
43+0
+49
+89
+93

J. Vealch
27 +08
+38
+40

Elm +67 ST
P.L. +82
+83
44+0
+86

39 34
+89

Gossett
45+0 +11 89

27.5' 21'

+69
+7

21'

15'

236'

24.7'

23'

23'

35' 24'

22'

24.5'

22.3'

22'

22'

23.9'

24'

24.7'

22'

23'

23'

Taylor Johnson

6" small tree
41+13

Geo. Herring
+40
44'

+46
+75
+88
+91
+93

L.H. Hiett
+07
+33
+46
+67
+89
+98

+04
Chostine
45.5 +27

+45
+54 P.L. +54
47' +80

+14
+12
47' +39
+11 Woddlie
+74

+86
+00

Between Sidewalks
from sect. on line

Sta 46+0 - E 25.4 - W 11.7
 Sta 47+0 - E 24 - W 12.6
 Sta 48+0 - E 23 - W 13.3
 Sta 49+0 - E 22 - W 14
 Sta 50+0 - E 21 - W 14.5

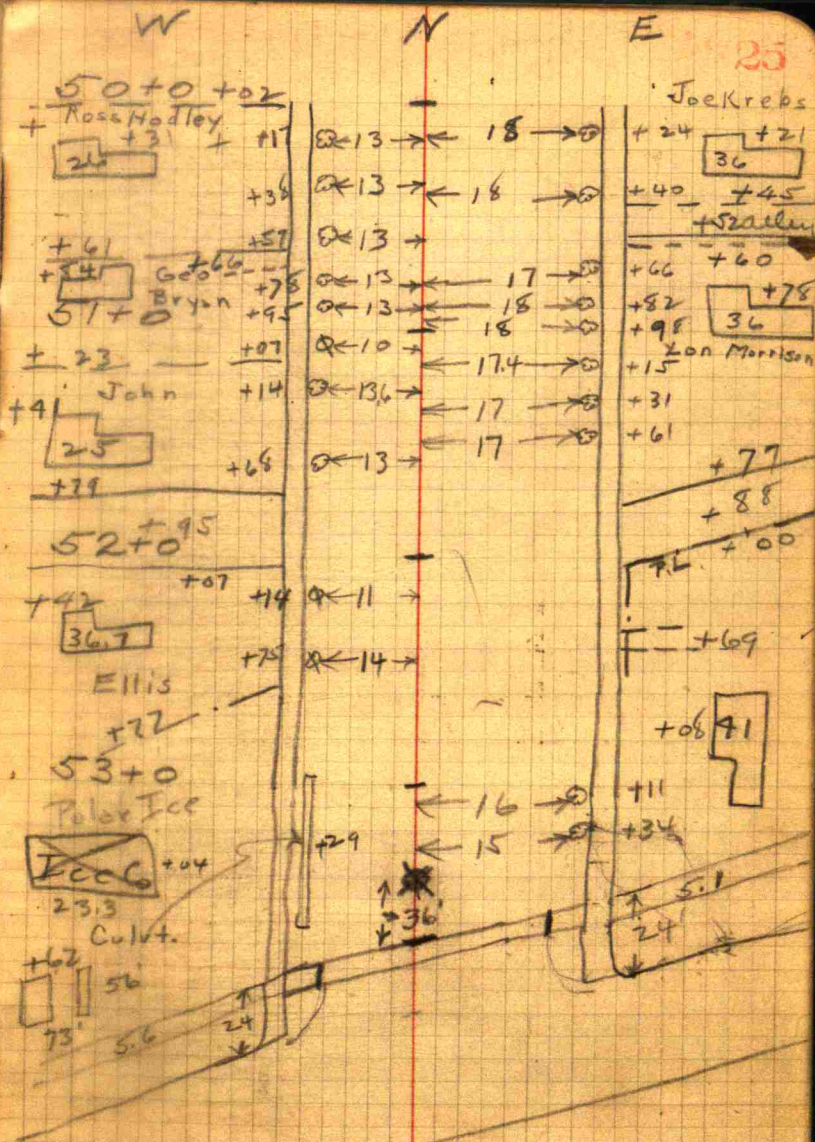
W	N	E
45+0		
+41		← 24 → +03 Neal Cooperider
+65	+53	← 23.5 → +24 49 +19
24	899.1	← 22.3 → +38
D. Ellis		← 22.2 → +58
46+0	+42 894.4	← 22.3 → +77
alley +07	+99 810.3	← 22.6 → +97
+14 Frank		← 22.6 → +52
31.6		
+66		
+72 alley		← 22 →
47+0	Φ 11	← 19 → +81 Sarah Campbell
Miles Hollowell		+00
+92		← 22.6 → +05 Sheppard
23.5	+75 8111	← 22.3 → +27
48+0	+80 8113	← 21.2 → +55 +60. Green
+49	+31 811	+66
Hadley	+51 811.5	← 22 → +88 +75
23	119 897.7	+97 45
49+0	+77 811.5	← 22 → +19. W Guyer
alley +25	+96 811.5	+35 +32
+29	+07 812.2	+67 33.4
25.5	+40 892.7	← 21.5 → +65 Jane Done
Hadley	+77 812.6	← 21 → +80 +99
50+0	+90 812.7	+10 St. Hill
	+79 812.6	+25 Dr. 1945
	+90 89	← 20 → +69 37
	+95 813	← 19.5 → +83
		← 19.3 → +92
		← 19 →

Between sidewalks from section line

Sta 51+0	E -20	W-15
" 52+0	E -19	W-16
" 53+0	E -17.8	W-16
" 53+68.5	E -10.8	W-10.9

Culvt. starts 52+98
 into Ice Co. & Filling Sta.
 End 53+49
 Intersection - 31' long

Stone
 Sta. 53+32.5
 N. edge of intersection
 Sta. 53+68.5



Sta.

53+

53+0

52+50

52+0

51+50

51+0

50+50

50+0

49+50

49+0

48+50

48+0

47+50

47+0

46+50

46+0

45+50

45+0

44+50

44+0

43+50

43+0

42+50

42+0

41+50

Sta.	20' out	Ditch	Berm	Sec. Line	Berm	Ditch	20' out	B.M. on Top of Stake nailed to Telephone pole N of 0+00 - El. 100.00	
	50' N - 99.49	50' E - 98.30			50' W -		98.56		
0+00	98.80	98.79 ¹⁴	98.89 ¹⁴	99.17	99.11 ⁹	99.03 ¹⁵	98.96		
1+00	97.65	97.20 ¹¹	97.80 ^{7.5}	98.30	97.80 ^{8.5}	97.16 ¹²	97.50		
2+00	96.52	96.50 ¹²	96.93 ⁸	97.54	97.15 ¹⁰	96.47 ¹³	96.62		
3+00	95.60	95.63 ¹²	95.90 ⁸	96.39	96.12 ¹⁰	95.52 ¹⁴	96.20		
4+00	94.73	94.24 ⁹	94.89 ⁷	95.36	95.22 ¹⁰	94.50 ¹³	94.90	⊙ 91.59	
5+00	93.82	93.50 ¹¹	94.05 ⁶	94.48	94.19 ⁸	93.74 ¹⁴	93.85		
6+00	92.91	92.57 ⁹	92.81 ⁶	93.31	93.02 ⁸	92.25 ¹⁴	92.73		
7+00	91.30	90.89 ⁹	91.12 ⁶	91.55	91.28 ⁹	90.75 ¹⁵	91.35		
8+00	88.82	88.60 ¹¹	89.42 ⁶	89.79	89.50 ⁹	88.83 ¹³	88.97		
9+00	87.35	86.92 ¹²	88.45 ⁸	88.70	88.57 ¹⁰	87.13 ¹⁴	87.32		
9+87	Fl. 10 85.06	86.10	85.45 ¹²	87.65	88.20	87.74 ⁹	84.62 ¹³	85.05	Fl. 84.50
10+0	86.50	85.80 ¹¹	87.54 ⁶	88.05	87.60 ⁹	85.63 ¹⁴	85.00		
11+0	86.85	86.51 ¹²	87.62 ⁶	88.02	87.62 ⁹	86.30 ¹⁴	86.66		
11+89	Gate E -			87.57	87.05	87.00		⊙ 88.08	
12+0	87.36	86.86 ¹¹	87.19 ⁷	87.67	87.25 ⁹	87.06 ¹⁴	86.67		
13+0	86.25	85.96 ¹³	86.82 ⁷	87.25	87.05 ¹⁰	85.98 ¹⁴	85.96		
14+0	86.71	86.23 ⁹	86.90 ⁶	87.24	87.17 ¹⁰	86.81 ¹⁴	86.55		
15+0	87.30	86.90 ⁹	87.45 ⁷	88.16	88.00 ¹⁰	87.21 ¹⁴	87.00		
16+0	86.78	86.69 ¹¹	87.16 ⁸	87.62	87.47 ¹⁰	87.10 ¹⁵	86.62		
16+41	Gate E -								
16+41	Gate W -								
17+00	86.63	86.34 ¹¹	86.95 ⁷	87.53	87.31 ¹¹	86.69 ¹⁵	86.85		
18+00	86.35	86.11 ¹⁰	86.77 ⁶	87.15	87.09 ¹⁰	86.43 ¹¹	86.59		

West

East

	West				East				
	20' out	Ditch	Berm	Sec. Line	Berm	Ditch	20' out		
19+00	85.13	85.0 ⁹ ₈	85.8 ⁶ ₄	86.28	86.03 ¹²	85.45 ¹⁴	85.54		
20+00	84.22	84.2 ⁵ ₈	85.0 ⁵ ₂	85.39	85.28 ¹²	84.47 ¹⁴	84.48	⊙ 81.82	
21+00	83.98	84.0 ⁹ ₆	84.9 ⁶ ₆	85.25	85.02 ¹²	84.30 ¹⁵	84.17	B.M. on Top	
22+00	83.30	83.47 ⁹	84.3 ⁶ ₀	84.69	84.6 ¹⁰ ₆	84.45 ¹³	84.28	of Concrete post	
23+00	82.40	82.3 ¹⁵ ₀	83.0 ¹¹ ₈	83.15	82.78 ⁶	82.2 ⁸ ₆	81.85	18' W of Sta. 27+47.	
24+00	80.73	80.81 ¹¹	81.8 ⁵ ₅	82.29	82.1 ⁹ ₀	81.03 ¹³	80.78	↗ El. 85.97	
24+56	culv. g F.I. 79.97	80.32	80.0 ¹¹ ₁	81.5 ⁷ ₁	82.03	81.45 ⁹	79.6 ¹⁵ ₀	79.52	80.49" F.I.
25+00	80.47	80.3 ¹⁰ ₉	81.5 ⁷ ₀	81.90	81.7 ⁸ ₀	80.8 ¹³ ₀	79.50	B.M. on stone	
26+00	80.49	80.6 ¹⁰ ₇	81.6 ⁷ ₉	82.03	81.7 ¹⁰ ₅	81.17 ¹⁴	80.60	of Abut. N.W. - bridge	
								El. 91.24	
27+00	80.8 ²⁰ ₆	Ditch	Berm	Sec. Line	Old Rd	Berm	Ditch		
27+34	st. W. 81.1 ³⁸ ₃	81.1 ¹² ₂	81.5 ¹⁸ ₀	82.15	82.1 ⁴ ₄	82.1 ³ ₃	81.4 ²⁰ ₅	81.4 ²⁰ ₃	⊙ 85.46
27+50	80.9 ²⁵ ₂	81.3 ¹² ₁	81.6 ¹⁸ ₅	82.28	82.1 ³ ₄	82.1 ¹¹ ₃	81.6 ²⁵ ₀	80.7 ²⁵ ₇	⊙ 85.17
27+75	80.2 ²⁵ ₈	81.0 ¹³ ₇	82.5 ⁹ ₄	82.84	82.1 ⁴ ₂	82.6 ¹⁰ ₈	81.6 ³⁰ ₂	80.1 ³⁰ ₈	
28+00	80.4 ²⁰ ₅	83.0 ¹⁵ ₀	83.6 ⁹ ₉	83.87		83.8 ¹⁶ ₀	82.0 ¹⁶ ₃	80.5 ¹⁶ ₄	
28+25	79.8 ²⁴ ₉	83.7 ¹⁸ ₀	84.9 ¹³ ₃	84.87	4W 85.2 ⁴ ₄	85.0 ¹⁶ ₂	82.5 ¹⁶ ₅	80.2 ¹⁶ ₀	25' 79.20
28+50	79.5 ³⁰ ₀	82.9 ²⁰ ₀	84.7 ¹⁸ ₈	86.32	5W 86.7 ⁴ ₄	84.5 ⁸ ₄	84.5 ¹⁶ ₄	83.0 ¹⁶ ₀	25' 79.80
29+75	32' out to bottom	85.0 ²⁰ ₉	88.7 ¹² ₆	88.35	88.7 ^{5W} ₄	88.7 ⁴ ₉	84.1 ¹² ₇		20' out to bottom
29+0		88.4 ¹⁸ ₈	91.2 ¹³ ₀	90.60	6W 90.9 ⁰	90.8 ² ₁			
29+25	N end Bridge			93.02					Bridge Planks 3" thick.
	S. end Bridge			92.95					
29+75					12E 92.1 ³ ₃				
30+0					15E 89.0 ³				
30+25					16E 86.6 ¹				

West

W. Berm

Seachine

Gold Rd

East

078.83

33

074.39

BM. on
Top of Arrow
on fire plug
Sta. 35+85
El. 75.60

68.41

0

63.40

64.47

0

55.24

57.11

43

54.70

38

51.95

25

51.09

W. Berm

Old Road

W. Berm

E. Berm

W. Berm

Old Road

W. Berm

Old Road

W. Berm

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Old Road

W. Berm

Old Road

30+46 Drive W 35 79.50 82.22 84.10 85.23 82.83 82.99 83.26 77.47

30+75 78.69 80.02 82.83 82.99 83.26 77.47

31+00 78.44 79.09 81.58 81.63 81.42 78.80

31+35 Drive E 79.92 79.52 79.12 35

31+64 Drive E 79.37 78.70 78.42 35

32+0 78.94 78.30 78.49 77.78 77.76 77.56 30

33+0 76.67 76.20 77.55 76.20 76.67 76.40 33

33+50 Drive W 76.43 76.21 76.68 76.15 76.34

34+00 76.25 75.50 76.56 75.83 75.91 76.07 33

34+92 Drive W 75.74 75.20 75.07 74.90 74.30 74.10 74.65 40

35+0 75.68 74.33 74.90 74.30 74.10 74.65 40

35+77 Drive W 73.76 72.95 72.13 72.56 72.05 72.26 73.44 42

36+00 73.87 72.14 71.12 70.46 70.26 73.44 42

36+50 Level W 73.58 69.61 68.26 67.86 67.61 72.85 44

36+94 Drive E 65.13 64.59 64.21 67.21 68.41 45

37+00 69.51 65.63 63.85 64.59 64.21 67.21 40

37+50 58.47 59.57 59.27 59.91 59.34 59.43 60.49 30

38+00 Sidewalk Ditch Seachine 49.47 53.98 53.42 54.73 56.18 55.94 55.41 56.96 57.11 35

38+50 47.73 51.42 51.55 52.25 53.50 53.32 52.70 53.62 54.70 30

38+77 Drive E 52.30 51.94 51.94 51.04 50.82 51.09 38

39+00 46.97 49.75 49.78 50.54 51.29 51.04 50.82 51.09 25

West

	Sidewalk	Ditch	Sec. Line	Old E.
39+54 Lincoln St.	47.07 ³⁵	48.66 ⁸	49.13	49.85 ¹⁰
40+00	47.80 ⁷	47.61 ⁵	47.91	48.86 ⁵
41+00	47.27 ¹⁰	46.97 ⁶	47.66	48.21 ⁷
Bridge - Slab	47.68	Fl. 41.20		
♀	98.14			
41+65 Drive W	46.40 ²⁰	46.56 ⁷	46.85	47.41 ⁹
41+83 Drive E			46.56	47.39 ⁸
42+00	46.32 ¹⁰	46.24 ⁵	46.71	47.39 ²
42+29 Drive W	46.00 ¹⁸	46.20 ⁹	46.56	47.21 ³
43+0	45.86 ¹¹	45.71 ⁴	45.99	46.59 ¹⁵
43+04 Drive E			45.99	46.89 ⁵
43+67 Elm St W	45.75 ²⁴	45.65 ¹²	45.81	46.11 ¹
44+00	45.40 ¹²	44.99 ⁵	45.39	45.87 ¹³
44+86 Alley E				45.46 ¹⁶
45+00	44.52 ¹¹	44.22 ⁴	44.77	45.24 ⁶
46+00	43.40 ¹²	43.01 ⁵	43.49	44.02 ²
46+07 Alley W	43.03 ²⁵	43.40 ⁵	43.45	44.02 ²
46+29 Drive E				43.69 ⁵
46+72 Alley W	42.61 ²⁵	42.49 ¹¹	42.27 ⁵	42.71 ¹
47+00	42.38 ¹³	41.92 ⁶	42.47	42.87 ⁵
47+66 Int. E			42.26	42.55 ⁵
48+00	41.74 ¹⁴	41.50 ⁶	42.01	42.83 ¹⁷
49+00	41.05 ¹⁴	41.02 ⁵	41.52	41.84 ⁶
49+10 Int E				41.73 ⁷
49+25 Int W	40.70 ²⁵	40.93 ¹⁴	40.74	41.59 ⁶

East

0 48.05
33

Ditch	Sidewalk	
48.47 ²¹	47.80 ³¹	
47.73 ²²	B.M. on S. end E rail of bridge.	EI. 49.96
46.73 ³⁸	45.55	
45.78 ³⁸	41.75	
45.43 ³⁸	49.96	
43.26 ³⁵		
41.96 ³⁵		
41.14 ³⁵		

50+00

50+52 Int E.
50+66 Int W

51+00

51+88 Int E

51+95 Int W.

52+00

52+69 Int E.

53+0

53+49 Int W

53+68.5

Sidewalk

15
40.33

Ditch

6
40.25

Sec line

40.87

old E

5
41.16

Ditch

16
40.25

Sidewalk

23
40.48

39.16 37

39.81²⁵

40.02¹⁴

39.59⁷

40.56

40.80⁵

39.91

40.11²³

39.96³²

39.83¹⁵

40.02¹⁴

39.52⁸

40.62

40.29

40.38

39.54¹⁵

39.83²⁰

39.71

39.76³

39.34

39.40²⁰

39.49³⁵

39.64³⁵

39.63

39.61¹⁰

39.84

39.77²

39.34

39.40²⁰

39.63

39.61

39.84

39.92²

39.44

39.35²⁰

38.94¹⁷

38.57⁷

39.03

same

38.54¹³

38.94¹⁷

39.14²⁷

38.79¹⁴

38.60¹⁰

39.11

same

38.23¹³

38.94¹⁸

39.20³⁵

38.79¹⁴

38.60¹⁰

39.10

same

38.23¹³

38.94¹⁸

38.82

37.83

37.69

same

38.82¹⁰

38.64¹⁴

20' S. of Iron Pin 53+68.5

37.49

30' W. on Nat. N. side

gutter 37.16

28' E on Nat. in gutter 37.19

B.M. on arrow
on Top of
Fire plug W of
Sta 53+68.5
El. 41.46

Sta.	El. of Sub. Gd.	El. of Strk. on W. side	Cut To Sub Gd.
53+68.5	37.01		
53+0	37.44	39.44	2'-0"
52+50	37.76	38.76	1'-0"
52+0	38.08		
51+50	38.40	39.40	1'-0"
51+0	38.72	39.72	1'-0"
50+50	39.04	40.04	1'-0"
50+0	39.36	40.36	1'-0"
49+50	39.68	40.68	1'-0"
49+0	40.00	41.00	1'-0"
48+50	40.32	41.32	1'-0"
48+0	40.65	41.65	1'-0"
47+50	40.97	41.97	1'-0"
47+0	41.26	42.26	1'-0"
46+50	41.76	42.76	1'-0"
46+0	42.26	43.26	1'-0"
45+50	42.76	43.76	1'-0"
45+0	43.26	44.26	1'-0"
44+50	43.76	44.76	1'-0"
44+0	44.26	45.26	1'-0"
43+50	44.76	45.76	1'-0"
43+00	45.26	46.26	1'-0"
42+50	45.76	46.76	1'-0"
42+0	46.26	47.26	1'-0"
41+50	46.76	47.26	0'-6"

① 41.26

① 47.36

39

$$\begin{array}{r} 44.76 \\ 45.83 \\ \hline 45.59 \\ 25 \\ \hline 45.84 \\ 43.43 \\ \hline 2.41 \end{array}$$

$$\begin{array}{r} 38.08 \\ 43 \\ \hline 38.91 \\ 50 \\ \hline 39.41 \end{array}$$

Sta.			
41+0	46.98	47.48	0'-6"
40+50	47.24	47.74	0'-6"
40+0	47.50	48.00	0'-6"
39+50	48.09	49.59	1'-6"
39+0	50.75	50.36	0'-4 1/2"
38+50	53.75	52.46	1'-3 1/2"
38+0	56.75	55.22	1'-6 1/2"
37+50	59.75	59.61	0'-2"
37+0	62.75	67.49	4'-9"
36+50	65.75	70.47	4'-9"
36+0	68.75	72.62	3'-10 1/2"
35+50	71.75	73.21	1'-5 1/2"
35+0	73.75	74.74	1'-0"
34+50	74.75	75.56	0'-10"
34+0	75.75	75.86	0'-1 1/2"
33+50	76.75	76.39	0'-4 1/2"
33+0	77.75	76.53	1'-3"
32+50	78.75	76.87	1'-10 1/2"
32+0	79.75	77.65	2'-1 1/4"
31+70.5	80.36	77.97	2'-5"

0 51.49

0 62.71

0 73.21

75.56 41

$$\begin{array}{r} 49.50 \\ 28.00 \\ \hline 1.76 \end{array}$$

B.M. on top arrow
 of line plug Sta. 35+85
 El. 75.60

75.42

	El. of Sub. Cd	El. Sub. side	Cut To Sub. Cd	F. 1' To Sub. Cd
0+00	98.60	98.52		0'-1"
1+00	97.75	97.76	Xd.	
2+00	97.14	96.76		0'-4 1/2"
3+00	95.87	95.90	0'-1/2"	
4+00	94.84	94.85	Xd.	
5+00	93.81	94.15	0'-4"	
6+00	92.73	93.04	0'-4"	
7+00	90.89	91.29	0'-5"	
8+00	89.05	89.15	0'-1 1/2"	
9+00	88.00	87.62		0'-4 1/2"
10+00	87.09	86.89		0'-2 1/2"
11+00	87.25	87.15		0'-1 1/2"
12+00	87.49	87.69	0'-2 1/2"	
13+00	87.15	86.62		0'-6 1/2"
14+00	86.84	87.04	0'-2 1/2"	
15+00	87.00	87.56	0'-6 3/4"	
16+00	87.20	87.06		0'-1 3/4"
17+00	87.12	86.83		0'-3 1/2"
18+00	86.62	86.50		0'-1 1/2"
19+00	85.84	85.36		0'-5 1/2"
20+00	85.06	84.49		0'-7"
21+00	84.78	84.34	0'-1/2"	
22+00	83.50	83.80	0'-3 1/2"	
23+00	82.72	82.37		0'-4 1/4"
24+00	81.94	81.17		0'-9 1/4"

43
0 94.85

0 86.90

0 87.04

0 83.80

0 83.03

323

226.4

904.4

84.10

44	El. of Sub. Cd.	El. of Stk. W. side	Cut Below Stk.	Fill Below Stk.
25+0	81.69	80.68		1'-0"
26+0	81.97	80.87		1'-1 1/4"
27+0	82.25	81.21		1'-0 1/2"
27+25	82.32	81.21		1'-1 1/2"

82.01
86.01

82.675

37.51 Gutter
at 53+68 End

37.01

50

37.51

48 Tile - Extra Work

51+77 - 51+67 -

53+68 to 51+72 - 214' x 10"

1-10" x 8" Y

48' x 8" Tile

1-10" - Elbow

3-8" - Elbows

30' x 8" Tile

1-10" x 8" Y

2-8" Elbows

314' x 10"

222' x 10"

Fl. ~~47.96~~ at bridge

5368
5172

196
18

214

276
30

314

47

44.76

45.10

42.96

2.14

50

1.64

Fl. of tile 1.64
below gutter line

Sta	E. Edge Gutter	changed Grade
53+	37.51	37.59
53+60	37.56	37.62
53+50	37.62	37.66
53+40	37.68	37.70
53+30	37.75	37.77
53+20	37.81	
53+10	37.88	
53+0	37.94	
52+90	38.00	
52+80	38.07	
52+70	38.13	
52+60	38.20	
52+50	38.26	
52+40	38.32	
52+30	38.39	
52+20	38.45	
52+10	38.52	
52+0	38.58	
51+90	38.64	
51+80	38.71	
51+70	38.77	
51+60	38.84	
51+50	38.90	
51+40	38.96	
51+30	39.03	

Sta	E. Edge Gutter	changed Grade
38.10		
37.40		
37.73		
37.68		
37.94		
37.86		
37.69		
37.651		
37.612		
32.573		
37.534		
37.495		
37.456		
37.865		
37.846		
37.807		
37.768		
37.729		
37.690		
38.77		
37.0		
38.363		
37.55		
38.3		
37.94		
38.17		
38.17		
38.17		
39.17		
38.34		
39.17		
38.52		
37.86		
38.08		
38.041		
38.002		
37.963		
37.924		
37.885		
49		
37.59		
37.92		
37.75		
37.84		
37.09		
36.7		
37.75		
37.75		
38.34		
39.17		
38.52		
37.86		
38.08		
38.041		
38.002		
37.963		
37.924		
37.885		
1.70		
66.00		
51.0		
15.00		
15.30		

Sta	Top of Gutter outside edge	
51+20	39.09	✓
51+10	39.16	✓
51+0	39.22	✓
50+90	39.28	✓
50+80	39.35	✓
50+70	39.41	✓
50+60	39.48	✓
50+50	39.54	✓
50+40	39.60	✓ 39.65
50+30	39.67	✓
50+20	39.73	✓
50+10	39.80	✓
50+0	39.86	✓
49+90	39.92	✓
49+80	39.99	✓
49+70	40.05	✓
49+60	40.12	✓
49+50	40.18	✓
49+40	40.24	✓
49+30	40.31	✓
49+20	40.37	✓
49+10	40.44	✓
49+0	40.50	✓
48+90	40.56	✓
48+80	40.63	✓

39.36
 .064
 39.424
 .064
 39.488
 .064
 39.552
 .064
 39.616
 .064
 39.680
 .064
 39.744
 .064
 39.808
 .064
 39.872
 .064
 39.936
 .064
 40.000
 .064
 40.064
 .064
 40.128

① 40.29
 Walk of house

38.36
 C.B.

38.40
 .064
 38.336

38.40
 .064
 38.464
 .064
 38.528
 .064
 38.592
 .064 36
 38.656
 .064 50
 38.720
 .064 86

38.784
 .064
 38.848
 .064
 38.912
 .064
 38.976

① 39.69

38.77
 .41
 38.36

38.77
 .32
 38.45
 .30
 38.77
 .30
 38.47

38.14
 38.52

38.6 38.77
 .50
 38.976
 .064
 38.27

39.040
 .064
 39.104
 .064

39.168
 .064

39.232
 .064

39.296

39.27
 .75
 38.52

48+70	40.69	✓	
48+60	40.76	✓	
48+50	40.82	✓	
48+40	40.89	✓	
48+30	40.95	✓	
48+20	41.06	✓	
48+10	41.08	✓	
48+0	41.14	✓	
47+90	41.21	✓	X
47+80	41.27	✓	X
47+70	41.33	✓	X
47+60	41.40	✓	X
47+50	41.46	✓	X
47+40	41.53	✓	X
47+30	41.59	✓	X
47+20	41.65	✓	X
47+10	41.72	✓	X
47+0	41.76	✓	X
46+90	41.86	✓	X
46+80	41.96	✓	X
46+70	42.06	✓	X
46+60	42.16	✓	X
46+50	42.26	✓	X
46+40	42.36	✓	X
46+30	42.46	✓	X

40.128	064	41.77	39.19
40.192	064		38.72
40.258	064		47
40.322	064		39.60
40.386	064	40.60	39.19
40.450	064	50	47
40.514	064	41.14	
40.578	064		
40.642	064		38.40
40.706	064		064
40.770	064		064
40.834	064		38.528
40.898	064		83
40.962	064		39.358
41.026	064		33
41.090	064		39.028
41.154	064		41.262
41.218	064		10
41.282	064		41.36

38.77
39.08
39.58

42
614

B. M. ...
43.95

46+20	42.56	✓	X
46+10	42.66	✓	X
46+0	42.76	✓	X
45+90	42.86	✓	X
45+80	42.96	✓	X
45+70	43.06	✓	X
45+60	43.16	✓	X
45+50	43.26	✓	X
45+40	43.36	✓	X
45+30	43.46	✓	X
45+20	43.56	✓	X
45+10	43.66	✓	X
45+0	43.76	✓	X
44+90	43.86	X	
44+80	43.96	X	
44+70	44.06	X	
44+60	44.16	✓	X
44+50	44.26	✓	X
44+40	44.36	✓	X
44+30	44.46	✓	X
44+20	44.56	✓	X
44+10	44.66	✓	X
44+0	44.76	✓	X
43+90	44.86	✓	
43+80	44.96	✓	

○ 45.14

56

43+70	45.06	✓
43+60	45.16	✓
43+50	45.26	✓
43+40	45.36	✓ X
43+30	45.46	✓ X
43+20	45.56	✓ X
43+10	45.66	✓ X
43+0	45.76	✓ X
42+90	45.86	✓ X
42+80	45.96	✓ X
42+70	46.06	✓ X
42+60	46.16	✓ X
42+50	46.26	✓ X
42+40	46.36	✓ X
42+30	46.46	✓ X
42+20	46.56	✓ X
42+10	46.66	✓ X
42+0	46.76	✓ X
41+90	46.86	✓ X
41+80	46.96	✓ X
41+70	47.06	✓ X
41+60	47.16	✓ X
41+50	47.26	✓ X
41+40	47.36	✓ X
41+30	47.46	✓ X

$$\begin{array}{r} 45.36 \\ 48 \\ \hline 44.88 \end{array}$$

45.33

43.49

45.66

44.96

1.75

43.49

40.96

2.53

Vatch
 B.M. on SE,
 cor Bottom step
 El. 46.67

$$\begin{array}{r} 45.46 \\ 50 \\ \hline 44.96 \end{array}$$

$$\begin{array}{r} 45.66 \\ 04 \\ \hline 62 \end{array}$$

$$\begin{array}{r} 45.66 \\ 44.96 \\ \hline .70 \end{array}$$

44.92

57

1.47

W. side

1'-9" C.B.

Elbow -

Bottom P.M. 40.96

43.49

45.66

$$\begin{array}{r} 45.46 \\ 33 \\ \hline 45.79 \end{array}$$

45.79

75

45.04

58

Br. 41+12 1/2

41+20	47.56	✓
41+10	47.66	
41+0	47.70	None X
40+90	47.74	✓
40+80	47.78	✓ X
40+70	47.82	✓ X
40+60	47.86	✓ X
40+50	47.90	✓ X
40+40	47.94	✓ X
40+30	47.98	✓ X
40+20	48.02	✓ X
40+10	48.06	✓ X
40+0	48.10	✓ X
39+90	48.14	✓ X
39+80	48.18	✓ X
39+70	48.22	✓ X
39+60	48.54	✓ X
39+50	48.64	✓ X
39+40	48.85	✓ X
39+30	49.45	✓ X
39+20	50.05	✓ X
39+10	50.65	✓ X
39+0	51.25	✓ X
38+90	51.85	✓ X
38+80	52.45	✓ X

47.01
47.76
67
-09
25

47.75
47.09
66
4
150

48.66
47.74

48.09
47.62
47.62
50
48.12
049
48.071
049
48.022
049
47.973
049
47.924
049
47.875

52.45
60
51.85
60
51.25
60
50.65
60
50.05
60
49.45
60
48.85

484 50

48.35
50
47.68
47.98
47.75
49.33
48.64
50
1.71
47.48
48.59
50
48.08
049
024

47.796
049
47.747
049
47.698
049
47.649
049
47.60
049
47.551
049
47.502
049
47.453
049
47.404

60
50
14

51.85
47.01
41.26
5.75
54
35
36
47.75
47.0

48.08
47.75
049
48.09
049
47.701
049
48.041
049
47.652
47.992
049
47.943
049
47.894
049
47.845
049
47.796

10 | 10 | 10 | 10

42

38+70	53.05	✓	X
38+60	53.65	✓	X
38+50	54.25	✓	X
38+40	54.85	✓	X
38+30	55.45	✓	X
38+20	56.05	✓	X
38+10	56.65	✓	X
38+0	57.25	✓	X
37+90	57.85	✓	X
37+80	58.45	✓	X
37+70	59.05	✓	X
37+60	59.65	✓	X
37+50	60.25	✓	X
37+40	60.85	✓	X
37+30	61.45	✓	X
37+20	62.05	✓	X
37+10	62.65	✓	X
37+0	63.25	✓	X
36+90	63.85	✓	X
36+80	64.45	✓	X
36+70	65.05	✓	X
36+60	65.65	✓	X
36+50	66.25	✓	X
36+40	66.85	✓	X
36+30	67.45	✓	X

61.59

70.60
69.60

64.75
66.50
68.25

75
67
65
250

66.25
60
66.95
60
67.45

64.75
175
66.50
175
68.25

66.25
60
65.65
60
65.05
60

63.00

64.45
60
63.85
60
63.25
60
62.65
60

63.25

62.05
60
61.45
60
60.85
60

70.25

63.00

7.25

60.25
60
59.65
60
59.05
60
58.45
60

16.0

30) 6.00

57.85
60
57.25
60
56.65
60
56.05

48.44

56.05

66.52

60
55.45
60
54.85
60
54.25
60
53.65
60
53.05
60
52.45

63.98

64.85

66.30

67.35

67.75

6

36+20 68.05 ✓
 36+10 68.65 ✓
 36+0 69.25 ✓
 35+90 69.85 ✓
 35+80 ~~70.45~~ ✓
 35+70 71.05 ✓
 35+60 71.65 ✓
 35+50 72.25
 35+40 72.85
~~35+30 73.45~~
~~35+20 73.85~~
 35+10 74.05
 35+0 74.25
 34+90 74.45
 34+80 74.65
 34+70 74.85
 34+60 75.05
 34+50 75.25
 34+40 75.45
 34+30 75.65
 34+20 75.85
 34+10 76.05
 34+0 76.25
 33+90 76.45
 33+80 76.65

V.C. E.I.
^{67.45}
 67.73 67.95+
 68.33 68.56+
 Changed 68.93 69.06+
 69 69.53 69.58+
 70.13 70.13 V.C. + ✓
~~70.59~~ 70.64 x ✓
~~71.15~~ 71.05 x ✓
~~71.50~~ 71.46 + ✓
~~71.85~~ 71.87 ✓+
~~72.20~~ 72.20 ✓+
 72.55 ✓+
 72.90 ✓+
 73.25 ✓+
 73.60 ✓+
 73.95 ✓+
 74.30 74.30 ✓+
 74.60 74.65 ✓+
 74.93 74.93 V.C. + ✓
 75.14 75.18 ✓+
 75.35 75.35 ✓+
 75.63 ✓+
 75.84 ✓+
 76.04 ✓+
 76.25 ✓+
 76.46 ✓+

35+80 — 69.12
 35+50 — 70.92
 35+0 — 72.06
 34+50 — 74.05 69.28
 34+0 — 75.30
 33+50 — 76.48
 33+0 — 77.32
 32+50 — 78.45
 32+0 — 79.30
 31+70 — 80.25

076.58

$$\begin{array}{r} 73.60 \\ 35 \\ \hline 73.25 \\ 35 \\ \hline 72.90 \\ 35 \\ \hline 72.55 \end{array}$$

$$\begin{array}{r} 73.60 \\ 207 \\ \hline 74.609 \end{array}$$

$$\begin{array}{r} 73.95 \\ 73.60 \\ \hline 10.86 \end{array}$$
 209

33+70	76.85	76.67	✓ x
33+60	77.05	76.88	✓ x
33+50	77.25	77.09	✓ x
33+40	77.45	77.30	✓ x
33+30	77.65	77.51	✓ x
33+20	77.85	77.72	✓ x
33+10	78.05	77.93	✓ x
32+0	78.25	78.14	✓ x
32+90	78.45	78.34	✓ x
32+80	78.65	78.55	✓ x
32+70	78.85	78.76	✓ x
32+60	79.05	78.97	✓ x
32+50	79.25	79.18	✓ x
32+40	79.45	79.39	✓ x
32+30	79.65	79.60	✓ x
32+20	79.85	79.81	✓ x
32+10	80.05	80.02	✓ x
32+0	80.25	80.23	✓ x
31+90	80.45	80.43	✓ x
31+80	80.65	80.64	✓ x
31+70.5	80.86	80.86	✓ x

7896

Cone.
post brace80.36⁶⁵

Pavement

Base — .21 Bbl sq yd

Top — .14 Bbl sq yd

.35 Both " "

70 Bbls or 280 = per 100'

4923 Lin Ft 18' pavement

.7 bbl per lin ft

3446.1 Bbls

7 Bbls to 10'

68

North End.

Sta	El. at Edge		
0+0	99.10		
0+50	98.67	✓	✓
1+00	98.25	✓	✓
1+50	97.82	✓	✓
2+0	97.17	W.C.	✓
2+50	96.88	✓	✓
3+0	96.37	✓	✓
3+50	95.85	✓	✓
4+0	95.34	✓	✓
4+50	94.82	✓	✓
5+0	94.31	✓	
5+50	93.79	✓	✓ C-2" H
6+0	93.23	V.C.	✓ C-3" H.
6+50	92.34	✓	✓ C-4" H.
7+0	91.39	✓	✓ C-1 1/2" H.
7+50	90.45	✓	C-1" H
8+0	89.55	V.C.	✓ C-2" H
8+50	89.00	✓	✓ C-3" L
9+0	88.50	✓	✓ C-1 1/2" H
9+50	88.00	✓	✓ C-1 1/2" L
10+0	87.59	V.C.	✓ C-4" H
10+50	87.63	✓	C-3" L
11+0	87.75	✓	C-4 1/2" L.
11+50	87.88	✓	C-1 1/2" L.
12+0	87.99	V.C.	✓ C-1 1/2" H.
12+50	87.82	✓	(C. OK)

⊙ 93.75

⊙ 97.39

97.82	99.10
23	.43
97.59	98.67
	42
	98.25
	43
97.40	97.82
23	
97.17	
	97.40
	52
94.31	96.88
52	51
93.79	96.37
51	52
93.28	95.85
94	51
1234	95.34
95	52
91.39	94.82
94	51
90.45	94.31
95	52
89.50	93.79
50	
	88.00
	18
	87.82

90 98.60 69

67 67
23 99.27
17+ 98.60 97.82
50
96.67 99.10
50 52
97.17 105

92.78

89.00

378

1.89

2√378

94

87.50

13

87.63

17

87.95

Sta	El. at Edge	
13+0	87.65	✓ (C.O.K)
13+50	87.47	✓
14+0	87.34	✓ V.C.
14+50	87.40	✓
15+0	87.50	✓
15+50	87.60	✓
16+0	87.70	✓
16+50	87.80	✓
17+0	87.78	✓ V.C.
17+50	87.51	✓
18+0	87.12	✓
18+50	86.73	✓
19+0	86.34	✓
19+50	85.95	✓
20+0	85.56	✓
20+50	85.17	✓
21+0	84.78	✓
21+50	84.39	✓
22+0	84.00	✓
22+50	83.61	✓
23+0	83.22	✓
23+50	82.83	✓
24+0	82.44	✓
24+50	82.12	✓
25+0	82.19	✓

$$72 \times 45 \times 19$$

$$72 \times 45 \times 9\frac{1}{2}$$

$$\odot 87.38$$

$$\odot 85.34$$

83	84.92	84.93
44	84.33	84.44
.05	84.10	39
.66	83.52	05
27	83.03	
88	82.80	
49	82.39	
17		
21		

85.56	87.82
- 31	17
85.17	87.65
39	15
84.78	87.47
37	17
84.39	87.30
39	
84.00	87.90
39	39
83.61	87.51
39	39
83.22	87.12
39	39
82.83	86.73
18	39
53	86.34
54	39
90	85.95
9.54	39
82.83	85.56
39	
82.44	93
39	78
81.75	15

$$86.80$$

$$50$$

$$8194$$

$$39$$

$$8155$$

$$50$$

$$8205$$

$$87.90$$

$$12$$

$$8778$$

$$3$$

$$63$$

$$72 \times 45 \times 18$$

$$1728$$

$$+44$$

$$72$$

$$+12$$

$$4$$

$$33.7$$

$$4 \overline{) 135.0}$$

$$93$$

$$78$$

$$15$$

$$337 \overline{) 180.00}$$

$$1685$$

$$1150$$

$$1011$$

$$139$$

25+50 82.33 ✓.33 30 ✓
 26+0 82.47 ✓.57 56
 26+50 82.61 ✓.71 91
 27+0 82.75 .85
 27+25 82.82

87.40
 81.55
585

750 | 585.00
 5250
6000
 6000

82.05
14
 82.19
14
 8233
14
 8247
14
 8261
14
 8275
7
 8282

82.45
 82.11 15
 82.73 30 34 19
30 135
 82.25 15 285
 1781
 16 | 285.00
 16 12 5 0 0 0
 16 12 5 0 0 0
 8 | 135
 8 55

B.M. on N. end ⁷³
 of W. headwall. Sta 24+56
 El. 83.10

82.05 82.61
 82.11 50 15
 72+45 x 19

1728 x 2
~~444~~
~~24~~
 8

72 x 45 x 9
~~1728~~
~~144~~
~~24~~
 8

9 1/2
 17.3
 32 | 555.0
 32
 295
 224
110
 96
 4

25+50 82.33 ✓.33 30 ✓
 26+0 82.47 ✓.57 56
 26+50 82.61 ✓.71 91
 27+0 82.75 .85
 27+25 82.82

87.40
 81.55
585

750 | 585.00
 5250
 6000
 6000

82.05
 14
 82.19
 14
 82.33
 14
 82.47
 14
 82.61
 14
 82.75
 7
 82.82

B.M. on N. end
 of W. headwall. Sta 24+56
 E.I. 83.10

82.05 $\frac{82.61}{50}$ 15
 82.11 $72 \times 45 \times 19$

82.45
 82.11 15
 82.92 34 19
 50 135
 82.25 15 285
 1781
 16 $\sqrt{285.00}$
 16
 1250 06 0
 11 20 0
 8 $\sqrt{135}$
 8 55

1728×2
~~444~~
~~24~~
 8
 72 \times 45 \times 9
~~1728~~
~~144~~
~~24~~
 8
 9 2
 17.3
 32 $\sqrt{555.0}$
 32
 235
 224
 110
 96

74 Town of Plainfield - East St.

Stones:

1/4 mi stone Sta. 12+36.3

N.W. cor. of foundation of
Mrs Pike's house S 45° E 50.5'
S.W. cor. of foundation of Mrs Gunns
house. N 75° W 29'

1/2 mi stone: Sta. 24+74.7

48" - Willow - 134' W -
6" - Catalpa - N 80° W 60.5'
- 20' So. of curbs

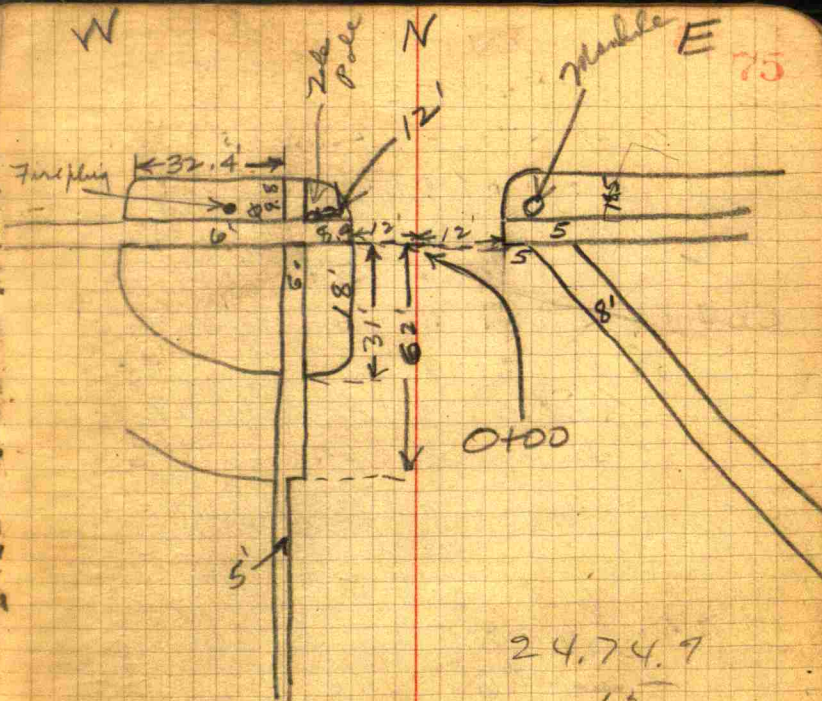
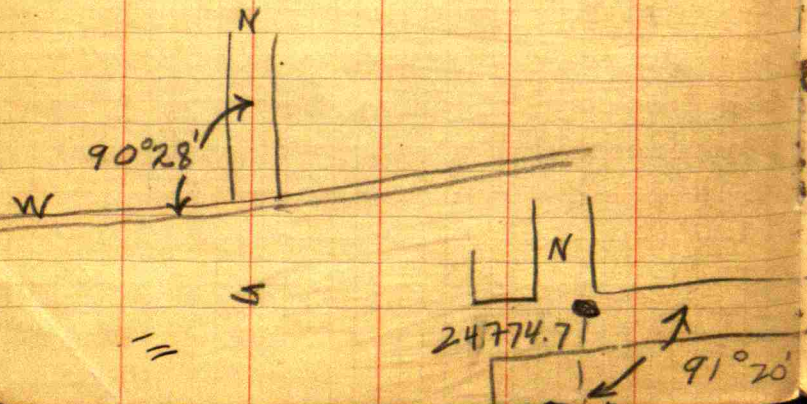
Sta. 10+65.9

Def. R. 22° 20'

T.H.I. & E. Trac. Co.

N. rail Sta. - 10+29.5

S. rail Sta. - 10+39.5



24.74.7
 15
 24+59.7

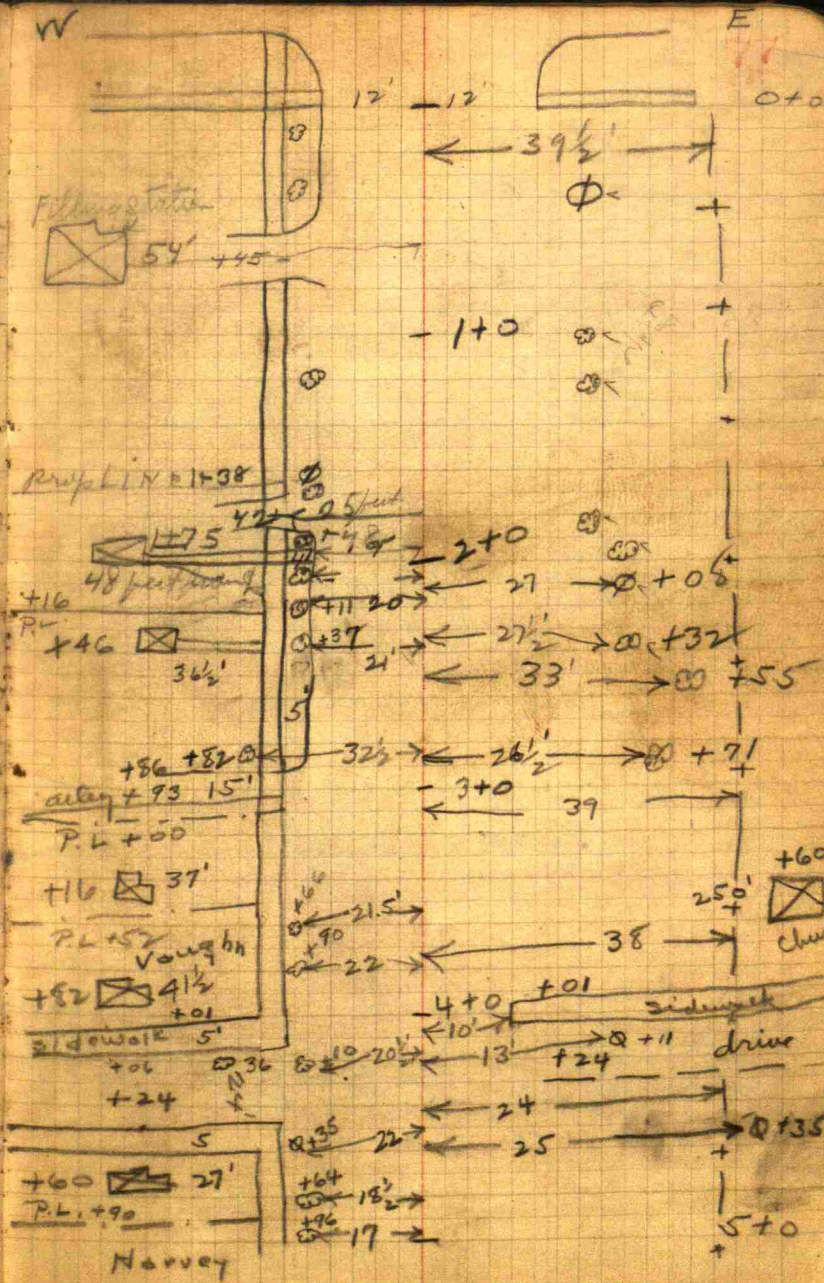
310 89

- 0+09 Maple 24" 20 feet from Q W
- 0+23 " " 20 5" " " Q W
- 0+23 telephone pole 25 " " Q E
- 0+45 filling station 54 feet from Q
- 0+95 Maple 6" 30 feet from Q E
- 1+03 Maple 12" 20 " " " Q W
- 1+09 Locust 12" 28 1/2 " " " Q E
- 1+21 telephone pole 20 " " " " Q W
- 1+24 Catalpa 24 " 21 feet from Q W
- 1+49
- 1+49 Locust 18" 28 feet from Q E
- 1+57 Maple 36" 18 feet from Q W
- 1+62 Elm 36" 34 feet from Q E
- 1+85 Locust 60" 24 feet from Q E
- 1+85 Elm 18" 21 " " " Q W

Sidewalk

- Sta 3+0 - W side 25'
- 4+0 - - 25'
- 5+0 - - 25'

Culvert. Sta. 3+52 starts on W side running parallel to Q. 20' from Q. 12' vit tile
 E. side - 3+92 12" tile under
 Quake church drive
 W 2+04 - Manhole W side 33'
 from Q. back of cut
 H W



78

Sedwalk

West side.

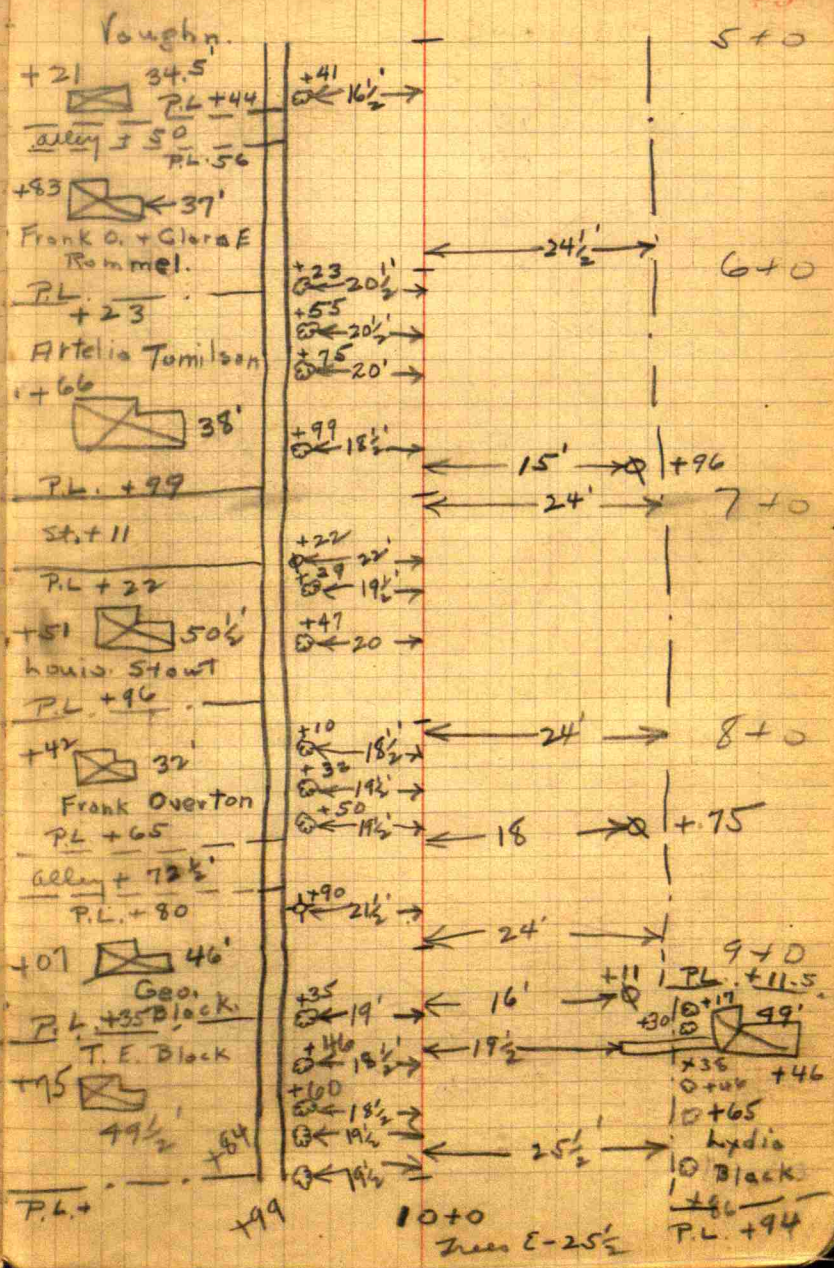
Sta.	6+0	25'
	7+0	25'
	8+0	25'
	9+0	25'
	10+0	25'

Culvert, - Zils starts on
E. side from C

Black in Morning
Anderson Cabin
Mrs. Pike & Mrs. Beel

W

E



sidewalk - W. side

Sta. 11+0 13'
 12+0 15'
 13+0 15'
 13+62 16 1/2'

W. side Walk ends 10+12
 " starts 10+49

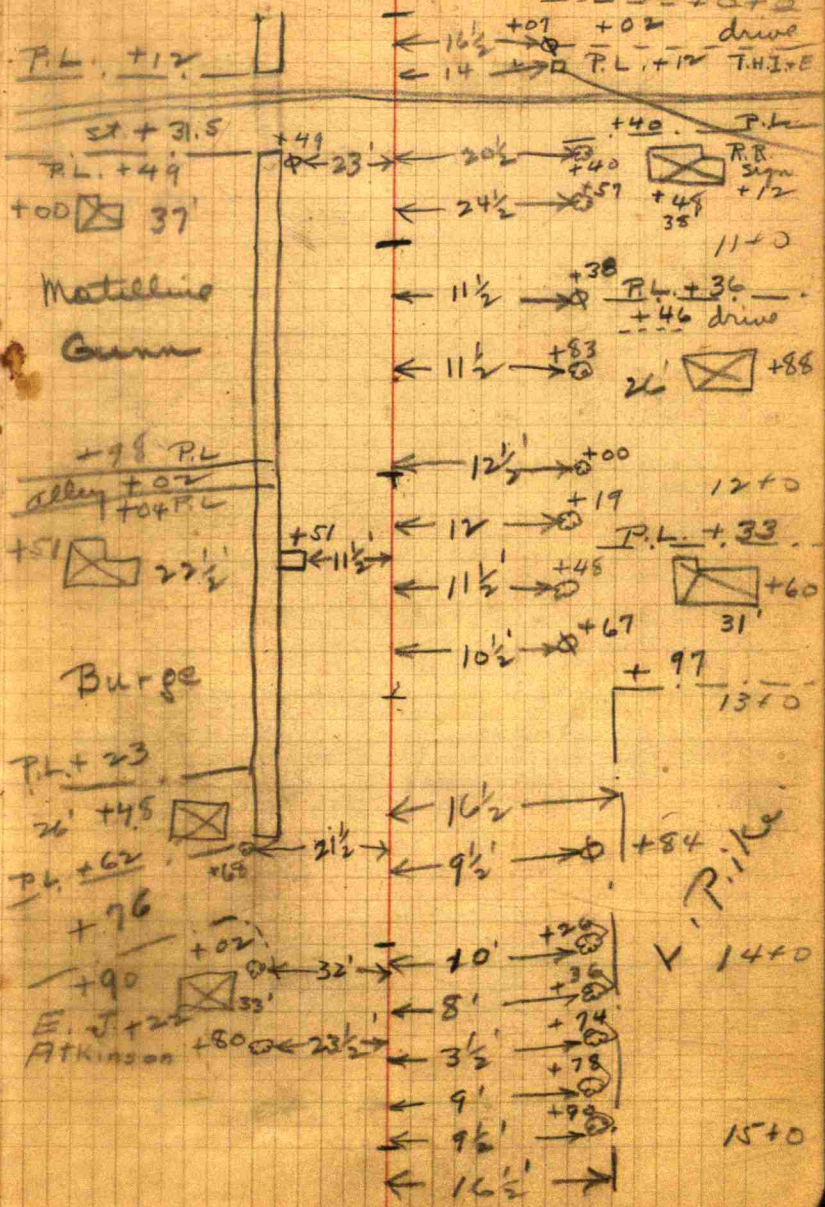
W. side - walk ends. - 13+62

90
 62
 28

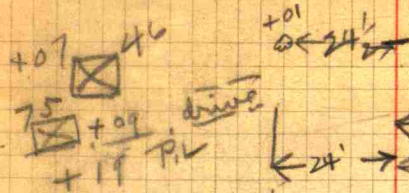
62
 44
 18

ellsworth
Linnelson

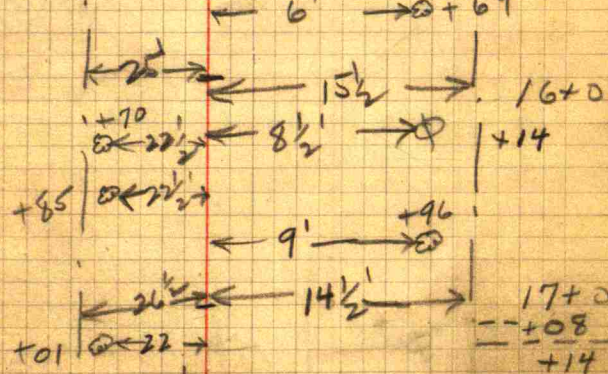
E. South St →



Harvey Herler - south of Nigges
 Mrs Albert. Harvey -



O.W.
 Nigges



Fence 28'E

+62 PL
 +86 Ark

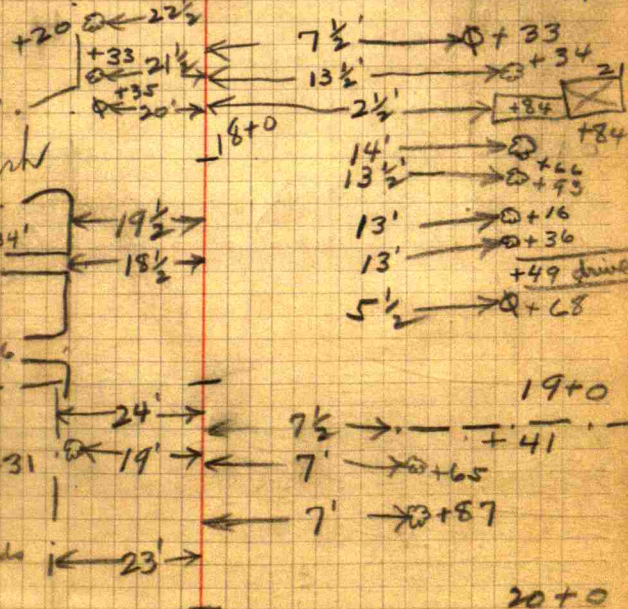
O.W.
 Nigges

PL 75

+31

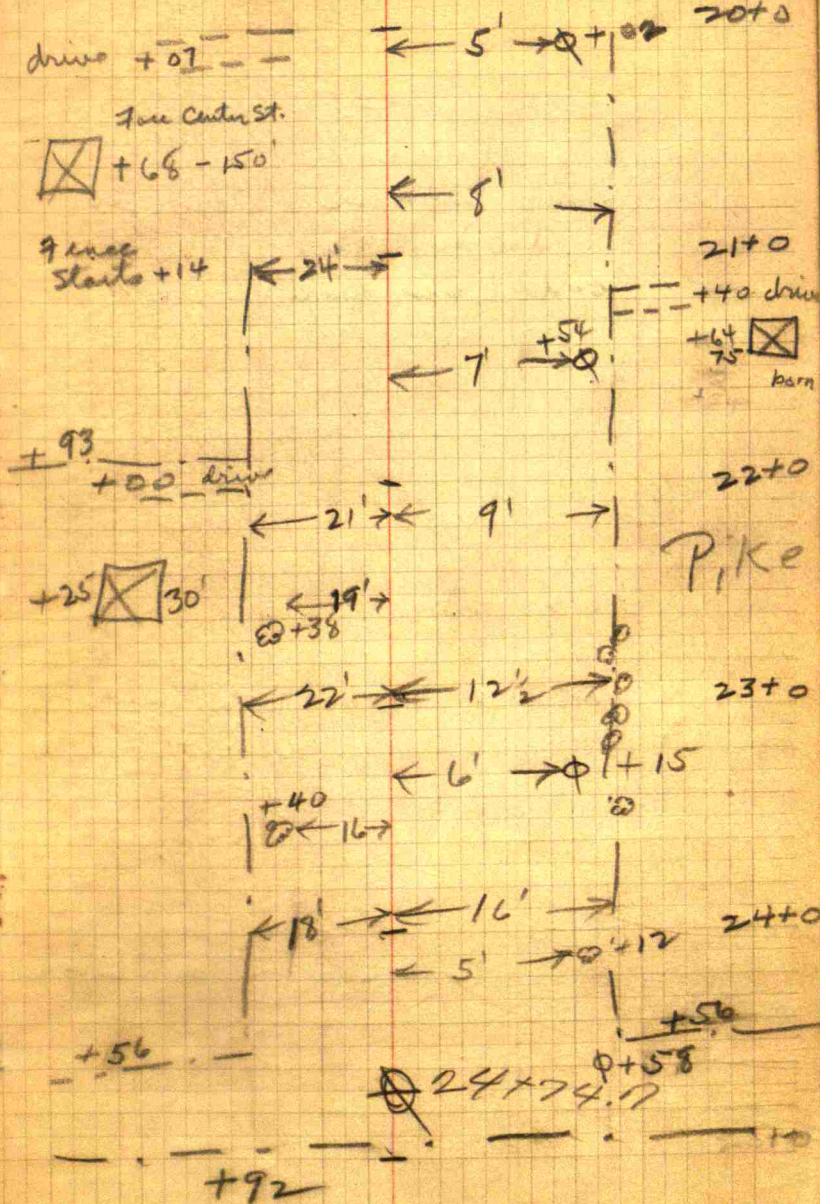
Fence ends

+96



Sta. 21+65 to 23+65
 Bushes grown up in
 fence line and some 4" to
 6" trees

From stone W. to E. side
 of Center St. 98'
 25' back curb to back
 curb.



86

W side

Std. Oil.

Artelia Tomilson

Dr. Thomas, C. B.

Mrs. Charlie Curlier

Malinda Jordan

Dellbert Vaughan

Harvey

M. E. Vaughan

W

E

87

Levels South East St. - Plainfield.

Nat. Road. 0-40 - 97.09 50' W. 97.36

W.

Sta.	Sidewalk	Curb	Gutter	℄.
X0+00	97.80	97.74	97.39	97.33
Int. W.	97.82		97.04	97.29
X1+00	97.46		96.59	97.08
Int. W.	97.46		96.99	97.16
X2+00	97.34	97.22	96.48	97.46
Int. W.	97.14		96.28	97.17
X3+00	97.03		96.06	97.22
X4+00	96.85		96.61	97.32
Int. W.	96.60		96.93	97.05
X5+00	95.93		95.34	96.23
Int. W.	95.51		95.09	95.55
X6+00	95.34		94.55	95.25
X7+00	94.81		94.21	95.03
Int. W.	94.83		94.35	95.02
X8+00	94.67		93.75	95.09
Int. W.	94.60		93.72	94.86
X9+00	94.37		93.40	94.68
X10+00	94.10		93.81	94.68
Int. W.	94.47		94.61	94.56
N. nail	94.51	S. nail	94.54	

50' E. - 97.30

B.M. Top of
arrow on fireplug
45' W. of Sta 0+00

E.L. 100.00.

Berm	Gutter	℄.
	97.45	
	96.31	96.03
	96.79	96.21
	96.30	95.51
	96.94	96.85
	97.26	97.99
	95.77	95.15
	94.94	94.06
	94.61	94.21
	94.43	94.07
	94.24	93.88
	95.12	95.09
	95.12	95.09

curb at 0+00 E. 97.70^{16'}

⊙ 97.48

Tile W. side Sta 3+
Fl. - 95.18
Tile E. side. Sta 3+90
Fl. - 94.53

Int. E.

⊙ 95.08

B.M. on arrow on

Top of Fire plug
Sta 8+91. W side of
street, E.L. 96.70Tile E side Sta. 9+80
Fl. - 92.22Tile W. side - 9+98
Fl. - 92.46

⊙ 94.41

Sta.	W	Sidewalk	Gutter	Old Rd	£	Berm	Gutter	E
10+65		25 94.49	17 94.10	7 94.45	94.16		7 93.85	20 94.55
11+00		13 94.43	10 93.75	1 94.40	94.24		9 93.70	16 94.96
Int. W.	30 94.63	15 94.36	9 93.63	same	94.23		9 93.76	22 94.52
12+00		15 94.36	9 93.63	same	94.15		6 93.60	12 94.55
13+00		13 94.32	10 93.70	same	93.93		9 93.36	15 93.91
Int. W.	35 93.49	21 93.36	14 93.12	4 93.40	93.11		6 91.57	17 92.23
14+00		21 93.36	14 93.12	4 93.40	92.92	2 92.88	6 91.57	17 92.23
15+00		22 92.90	19 93.50	6 94.04	93.81	same	12 92.60	17 92.50
Int. W.	32 93.04	24 93.62	13 94.27	6 94.27			15 91.40	15 99.02
16+00		24 98.90	13 97.51	6 97.70	97.17	3 97.80	7 99.40	15 99.40
17+00		25 99.74	14 101.44	8 101.77	101.42	same	10 100.65	12 100.15
Int. W.	44 107.11	18 106.93	8 107.20	8 101.56			10 100.92	22 100.90
18+00		33 107.48	16 107.16	9 107.50	107.24	9 111.68		17 100.90
Int. W.	30 106.53	14 106.95	7 107.55	8 107.39			same	15 109.22
19+00		21 103.99	13 105.15	7 105.50	105.92	same		11 105.44
20+00		24 103.12	14 103.25	5 103.85	103.93	3 103.64		19 102.91
Int. W.	40 103.22	21 103.12	14 103.25	5 103.85	103.93			
21+00		24 104.56	14 103.19	5 103.61	103.45	2 103.25		9 104.41
Int. W.	30 103.24	20 101.26	13 99.36	9 99.72	99.29	15 104.08		9 104.10
22+00		20 101.26	13 99.36	9 99.72	99.29	15 104.08		9 104.10
Int. W.	same as sta.							

77. walk 13'
 12 +95 7/8 edge
 12 +07 alley

Int. E.
 94.05
 Sta 14+20
 B.M. on bottom
 Conc. step of Atkinson house
 n. end step.
 El. 94.08

99.02
 107.53
 Int. E. 104.40

Int. E.
 Int. E.
 Int. E.

	Berm	old Rd	⊥
23+0	¹⁹ 89.25	¹³ 93.71	⁹ 92.62
24+0	¹⁸ 87.70	¹⁶ 87.44	⁷ 89.45
24+74		⁵⁰ 91.43	²³ 90.88
			³ 92.60
			92.52
			89.42
			90.19

Berm

Same

89.02

¹⁰91.44⁵87.36²⁵89.45⁵⁰89.32¹⁴87.28⁵⁰89.32

BM. on end
of curb E. side
of Center St.
100' W of Sta. 24+74
El. 91.35

⊙ 96.81

⊙ 90.95

9708

South-East St E16. of Gutter Line

09728

BM 46.70 - 8+9

①
95.64

Sta	E1.	Sta	E1.	Sta	E1.	Sta	E1.	Sta	E1.
0+0	97.12	2+60	96.18	5+10	95.28	7+60	94.38	10+10	94.15
0+10	97.08	2+70	96.15	5+20	95.25	7+70	94.35	10+20	94.23
0+20	97.05	2+80	96.11	5+30	95.21	7+80	94.31	10+29.5	94.30
0+30	97.01	2+90	96.08	5+40	95.18	7+90	94.28	10+34.5	—
0+40	96.98	3+0	96.04	5+50	95.14	8+0	94.24	10+40	
0+50	96.94	3+10	96.00	5+60	95.10	8+10	94.20	10+50	
0+60	96.90	3+20	95.97	5+70	95.07	8+20	94.17	10+60	
0+70	96.87	3+30	95.93	5+80	95.03	8+30	94.13	10+70	
0+80	96.83	3+40	95.90	5+90	95.00	8+40	94.10	10+80	
0+90	96.80	3+50	95.86	6+0	94.96	8+50	94.06	10+90	
1+0	96.76	3+60	95.82	6+10	94.92	8+60	94.02	11+0	
1+10	96.72	3+70	95.79	6+20	94.89	8+70	93.99		
1+20	96.69	3+80	95.75	6+30	94.85	8+80	93.95		
1+30	96.65	3+90	95.71	6+40	94.82	8+90	93.92		
1+40	96.62	4+0	95.68	6+50	94.78	9+0	93.88		
1+50	96.58	4+10	95.64	6+60	94.74	9+10	93.84		
1+60	96.54	4+20	95.61	6+70	94.71	9+20	93.81		
1+70	96.51	4+30	95.57	6+80	94.67	9+30	93.79		
1+80	96.47	4+40	95.54	6+90	94.64	9+40	93.75		
1+90	96.44	4+50	95.50	7+0	94.60	9+50	93.77		
2+0	96.40	4+60	95.46	7+10	94.56	9+60	93.78		
2+10	96.36	4+70	95.43	7+20	94.53	9+70	93.85		
2+20	96.33	4+80	95.39	7+30	94.49	9+80	93.93		
2+30	96.29	4+90	95.36	7+40	94.46	9+90	94.01		
2+40	96.26	5+0	95.32	7+50	94.42	10+0	94.08		
2+50	96.22								

93.8
67
99.51
24.69

50' V.C.

Oct 12.

30

30

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19

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 570

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30

30 (15)

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 570

200

834

1043

1034

432

455

288²⁴

520

1128

840

1028³⁴

926

1202

1149

1082

 1140

13871 ✓

 13784 ✓

3446

4

 13784

13874

20

 13894

13784

 110

24	24	24
24	24	1238
24	24	
24	24	1202
24	24	
24	24	
24	24	
24	24	
12	24	29
28	880	
24	24	
28	24	
28	24	
28	24	
30	24	
24	24	
24	24	
24	24	
24	24	
24	24	
24	28	
24	1190	
24	24	
24	1214	

Limo
12
10
(27)

30	56	24
	14	12
		<u>48</u>
28	70	242
4		29288
		28
880	285	216
316	140	48
		<u>316</u>
1190		696
389		112
		425
243152		60
880		12
		280
1123		880
47		48
		(832)
		1120
		70
		<u>1190</u>
280		24
4		41
1120		24
		840
		96
(44)		984
		140
		72
		<u>6</u>
1214		
37		
<u>1177</u>		

Cement (Oct. 7)

Price

28

24

24

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280

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840

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28

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24

868

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868

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230

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504

360

800

640

300

300

300

300

300

300

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300

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300

300

300

300

24

16

144

24

384

28

356

280

76

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2107

24

112

56

672

38

642

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34

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Cement

Oct. 6

Line

144
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264
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24

1360 Feet
 Cement
 (Subsquares)

1028

17
8
24
15
120
24
300
280
3
740
160
900
28
168
24
43
72
96
1032
20112
52
84
96

240 672 20
280 24 28 144 31
940 2 2 3 17 5
24 84 2 2 3 17 5
924 3 2 41 2 280
4 624 96 280 560
4720 3 190 186
647 96 12 2 16 47
232 9 30 4 188
4/1028 12 28 28
280 3 28 28
8 40 4 84
103 6 2 8 28 28
6 2 8 4 4 84
237 94 80 720
4/1028 2 6 672
8 2 48
22 21 48
20 2 12
25 36

11.036

9640
46

9594

96.66
46

97.12

.036

97.064

.036

97.048

.036

97.012

.036

96.976

.036

96.940

.036

96.904

.036

96.868

.036

96.832

.036

96.796

.036

96.760

.036

96.724

96.76

46

96.30

96.724

.036

96.688

.036

96.652

.036

96.616

.036

96.580

.036

96.544

.036

96.508

.036

96.472

.036

96.436

.036

96400

18x4 = 22x7

18x = 810

2 1/2

x 8 1/2

5 1/2

96400

.036

96.364

.036

96.328

.036

96.292

.036

96.256

.036

96.220

.036

96.184

.036

96.148

.036

96.112

.036

96.076

.036

96.040

.036

96.004

.036

95.968

.036

95.932

.036

96.896

.036

96.860

8 1/3

40 1/2

4 1/2

2 80

8 40

196

1028

840

188

168

20

46

9604
46

9558

9528
46

9522

28

6

168

96.860

.036

96.824

.036

96.788

.036

95.752

.036

95.716

.036

95680

$$\begin{array}{r} 5 \\ 9 \overline{) 40.0} \\ \underline{4.4} \end{array}$$

48' walk

4

$$\begin{array}{r} 4132.55 \\ \underline{3.55} \\ 36 \end{array}$$

$$\begin{array}{r} 13 \\ 13 \\ \underline{39} \\ 13 \\ \underline{9169} \\ 19 \\ \underline{77} \\ 70 \end{array} \quad 18.7$$

47.80

39+50 117

40.86

40.82

47.78

47.74

47.70

47.80

47.16

16.64

.04

$$\begin{array}{r} 160 \\ \underline{.05} \\ 800 \end{array}$$

40+50

40+60

40+70

40+80

40+90

41+00

41+10

41+20

41+30

1.00

Assessment for Avon Ave

118

Town of Plainfield.

E. side - ~~38.8~~ 38.8' Cir curb. - Ave width 6.8'

E. side at Main St.

8' X 5.3' X 6"

2.9 X 9' X 6"

119

20.2

1.8.6

38.8

John McClain.

9' cir. curb.

75' str. curb

10' cir curb - s. side int.

10' cir curb n. side int.

14.7' wide X 5.4'

~~5.4'~~

47' str. curb

	Perk	Walks	ST
Curb	59yd	597T	Curb Hdws
Town	41'	26 ✓	80
John McClain	30'	8	125'
Town	21.5'	26	56

93.84
67

94.51

67
93.24
46

93.70
077

93.777
077

93.854
077

93.931
077

94.008

17
94.08
077

94.157
077

94.234
077

94.301
46

93.84
67

94.51

93.84
46

93.30

17
94.31

94.30
21

94.51

Tile	Front	ST
36'x8"	162'	- 37'

93.88
46

94.24

94.09
46

93.63

93.70
46

93.24

93.24
46

93.70

93.31
46

93.77

93.77
077

93.847

93.70
077

93.777
077

93.854
077

93.931
077

94.008
077

94.085

93.88
036

93.844
036

93.808
036

93.772
036

93.736
036

93.70

94.42
036

94.384
036

94.348
036

94.312
036

94.276
036

94.240
036

94.204
036

94.168
036

94.132
036

94.096
036

94.060
036

94.024
036

93.988
036

93.952
036

93.916
036

93.880

Off. No. Fifteen
Foot

- 24
- 24
- 24
- 24
- 24
- 24
- 24
- 24
- 24
- 24
- 24
- 24
- 24
- 24
- 24
- 24
- 24
- 24

(90
feet)

(370
Feet)

257 on last of
north side,

75	24	28	
24	24	28	
24	24	28	
24	24	28	
24	28	28	
24	32	28	
30	28	28	
24	28	30	
24	28	30	
24	28	30	
24	510		
24	29		
24	28		

(1078)

(936)

142

Line
10

3028 24 283 185

840 24 844

124
25

336 1101

840 1 1 2 322

929 5 1 0 652

282 28

(740)

936310

510 250

762

678 280

652

26

540

762

30

257

1049

19

1030

Account Oct 9.

Am
5
15

24	
24	
24	
24	
24	
24	144
36	36
50	
50	
50	50
50	
50	
50	350
50	
50	
50	
50	
50	
50	
50	
50	
50	
50	
50	850
50	1080
45	
24	

95.68
.036

95.644
.036

95.608
.036

95.572
.036

95.536
.036

95.500
.036

95.464
.036

95.428
.036

95.392
.036

95.356
.036

95.320
.036

95.284
.036

95.248
.036

95.212
.036

95.176

124	90.0	127
6	144	
144	36	
	45	

	25	60

90	144
	36
250	850
144	36
36	364

	1030
	75
	60
	30
	32

430	970
90	281101
	14
	42

340	280
280	3

	283
	840

	1125
	27

	1149

9666
46

97.12

||||| ||| ||| ||| ||| ||| ||

Bottom

Top. ||| ||| ||| ||

9460		195
036		5
94564	9496	<u>200</u>
036	036	
94528	94924	
036	036	
94492	94888	
036	036	
94456	94852	
036	036	
94420	94816	
	036	
	94780	
	036	
	94744	
	036	
	94708	
	036	
	94672	
	036	
	94636	
	036	
	9460	

hine -
||||

50
80
24
154
40
194

38
3

117

(115)

41193

546

95

46
188

212
72

284
115

169

42
4169

25

35

1044

36

39
4

156

48
4

192

Pavement

Date	Sacks	No. of Ft. Line	
Sept. 17	200	72.5	5
Sept. 18	834	323.0	16
Sept 20	1043	410.	22 -9%
Sept 21	1034	358	22 +3.2%
Sept 22	432	166	8
Sept 29	455	180	10
Sept 30	288	110	5
Oct 1	520	195	10
Oct. 2	Sept		
Oct. 3	Sum		
Oct. 4	1128	395	21
Oct. 5	840	295	19
Oct. 6	1028	360	21
Oct 7	926	315	20
Oct 8	1202	410	22
Oct 9	1149	380	20
Oct 11	1082	370	10
Oct 12	1140	385	2.5
Oct 13	570		

256
 152

 Total line 408
 50

 20400

1043
 $\frac{280}{3}$
 $\frac{800}{2}$
 $\frac{410}{2}$
 $\frac{323.0}{2}$
 $\frac{410}{2}$
 $\frac{358}{2}$
 $\frac{166}{2}$
 $\frac{180}{2}$
 $\frac{110}{2}$
 $\frac{195}{2}$
 $\frac{395}{2}$
 $\frac{295}{2}$
 $\frac{360}{2}$
 $\frac{315}{2}$
 $\frac{410}{2}$
 $\frac{380}{2}$
 $\frac{370}{2}$
 $\frac{385}{2}$
 $\frac{570}{2}$

$\frac{10877}{2}$
 $\frac{1149}{2}$
 $\frac{1064}{2}$
 $\frac{85}{2}$
 $\frac{28}{2}$
 $\frac{926}{2}$
 $\frac{882}{2}$
 $\frac{44}{2}$

Subgrade High could not take them
 two 15' foot Inters.
 one 12' by 20' Inters.
 556

$\frac{500}{2}$
 $\frac{280}{2}$
 $\frac{5}{2}$
 $\frac{1200}{2}$
 $\frac{350}{2}$
 $\frac{12161}{2}$
 $\frac{3040}{2}$

16 1/2
26

3.5
6.5
17.5
21.0
9) 22.75 (2.5
18
47
45
2.5
2.5
5.3

9) 250.75
27.86
7
25.5

8'-3"
7'6"
159
7'-7 1/2"

7 2/3
23
2 + 5/2 =

16

23
17
161
23
2391
17
52
8 1/2
85
9) 93.5
10.3

21.7
18) 391.0
36
31
15
130
126

32

1

Oct 18

30
30
30
30
30
30
30
30
30
30
30
30
30
30
30
30

13
30
290
160
550
36
514
sacks used

(790) 514
790 356
158

-36

292

27) 7900
54

125) 7900
63
650
1490
1375
25

250
243
70
54

292
63
356

Cement.

Line

Aug. 23	-68	Bags	1	curb bottom
" 25	-137	Bags	8	curb bottom
" 26	2 11	"	11	"
" 27	386	Bags	20	"
" 28	379	"	18	"
" 30	412	"	21	"
" 31	284	"	14	"
Sept 1	16	"	1	"
" 3	37	"	2	"
" 7	117	"	13	"
" 8	334	"	16	"
" 13	472	"	19	"
" 14	269	"	8	"
	<u>3022</u>		<u>152</u>	
Oct 13	20	"		

Cement

1 1/2 Bags.

Top Course

- 12 cu ft gravel
- 8 " " sand
- 4 " " cement

1-2-3-mix

Bottom

1-4 1/2 mix

138

$$\begin{array}{r}
 98.60 \\
 85 \\
 \hline
 97.75 \\
 85 \\
 \hline
 96.90 \\
 103 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 1103 \\
 51 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 96.90 \\
 51 \\
 \hline
 39
 \end{array}$$

$$\begin{array}{r}
 96.90 \\
 42 \\
 \hline
 48
 \end{array}$$

$$\begin{array}{r}
 96.46 \quad 96.90 \\
 \hline
 96.44 \quad 96.48 \\
 23 \quad 96.39 \\
 \hline
 67 \quad .09
 \end{array}$$

$$\begin{array}{r}
 97.75 \quad 96.90 \\
 \hline
 95.87
 \end{array}$$

87.30 139

$$\begin{array}{r}
 87.30 \quad 87.40 \quad 87.01 \\
 \hline
 87.16 \\
 12 \\
 \hline
 87.28
 \end{array}$$

$$\begin{array}{r}
 87.40 \\
 87.16 \\
 \hline
 24
 \end{array}$$

Base-

4

794

$$\begin{array}{r} 6.46 \\ 16 \end{array}$$

$$\begin{array}{r} 4 \\ 8 \\ 9 \overline{) 32.5} \\ \underline{27} \\ 55 \\ \underline{54} \\ 10 \\ 7.3 \end{array}$$

1-4

$$\begin{array}{r} 27 \overline{) 646} \\ \underline{54} \\ 106 \end{array}$$

$$\begin{array}{r} 75 \frac{1}{2} \\ 69 \frac{1}{2} \\ \hline 145 \\ 72.5 \\ \underline{.7} \\ 50.75 \\ \underline{4} \\ 203.00 \end{array}$$

4-2

Walk

Base

$$\begin{array}{r} 89.1 \\ 65.26 \\ 33.75 \\ \hline 188.11 \end{array}$$

$$\begin{array}{r} 6.8 \\ 6.1 \\ \hline 12.9 \end{array}$$

85.38

$$\begin{array}{r} 56.0 \\ 52.1 \\ \hline 108.1 \end{array}$$

$$\begin{array}{r} 25.7 \\ 1.2 \\ \hline 26.9 \end{array}$$

794 cu. ft.

141

$$\begin{array}{r} 8 \\ 12 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 596 \\ 4 \\ 3 \overline{) 2384} \end{array}$$

794.

24 yds. Gravel

$$\begin{array}{r} 159 \\ 5 \overline{) 795} \\ \underline{159} \\ 636.0 \end{array}$$

23.

~~596 x 4 x~~

$$\sqrt{2384}$$

$$\begin{array}{r} 596 \\ 1192 \\ 2384 \times 3.25 \\ \hline 1937.00 \end{array}$$

$$\begin{array}{r} 646 \\ 3 \overline{) 1937} \end{array}$$

Q	N.S.	E.S.
4490	43.52	44.18
	44.06	
	44.65	

$$\begin{array}{r} 44.06 \\ 1.00 \\ \hline 43.06 \end{array}$$

44.68

$$\begin{array}{r} 44.69 \\ 25 \\ \hline 44.44 \end{array}$$

$$\begin{array}{r} 44.44 \\ 44.18 \\ \hline \end{array}$$

$$\begin{array}{r} 43.52 \\ 69 \\ \hline 44.99 \end{array}$$

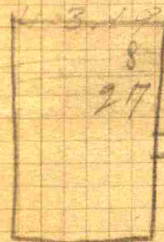
Rain Water 8"
" E side

$$\begin{array}{r} 44.06 \\ 1.17 \\ \hline 42.89 \\ 69 \\ \hline 43.52 \\ 25 \\ \hline 42.69 \end{array}$$

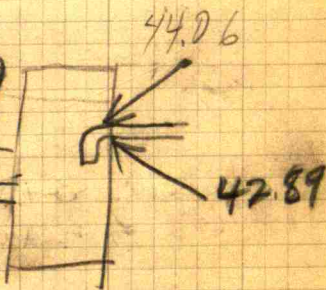
$$\begin{array}{r} 44.69 \\ 44.30 \end{array}$$

44.06	44.18
1.17	25
<u>42.89</u>	44.43
	83
	<u>43.60</u>

$$\begin{array}{r} 43.52 \\ 83 \\ \hline \end{array}$$

$$\begin{array}{r} 42.69 \\ 50 \\ \hline \end{array}$$


43.29



$$\begin{array}{r} 44.26 \\ .60 \\ \hline \end{array}$$

44.86 El. of sub-gd.

$$\begin{array}{r} 17 \\ \hline 44.69 \end{array}$$

El. of gutter line ^{sub-gd.}

$$\begin{array}{r} 174 \\ 848 \end{array}$$

$$\begin{array}{r} 9350 \\ 2586 \end{array}$$

$$\begin{array}{r} 93.896 \\ 174 \\ \hline 94.07 \end{array}$$

$$\begin{array}{r} 19 \\ 932 \end{array}$$

$$\begin{array}{r} 9340 \\ 20 \\ \hline 93.29 \end{array}$$

Sidewalk - N. side of Elm St. - Plainfield

old walk starts 2+65
and ends at 3+84
no alley int. now removed

Walk to remain starts
at 3+97 runs to
4+57

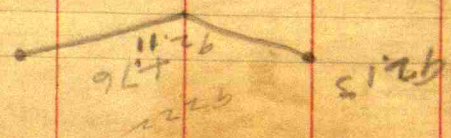
Moore & Regan's Add

LS
61

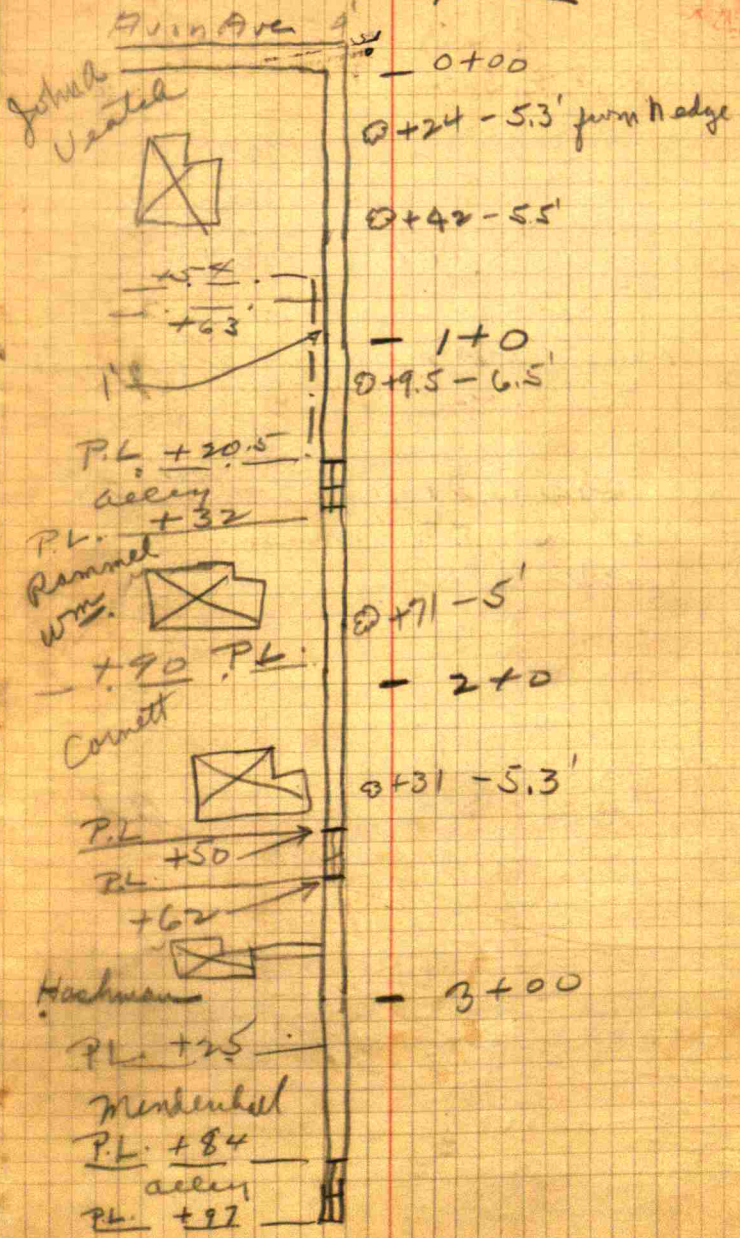
LS
26
25

0026

LS
26
6526



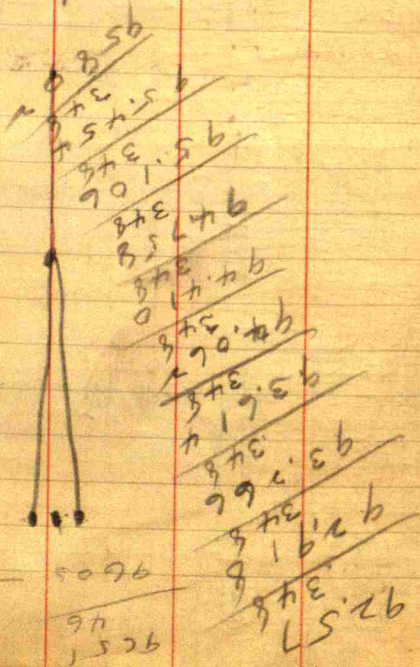
N ←



old wack to be removed start at Sta 5+31 to 5+96

15.96
9h
90.96
94E
LS26

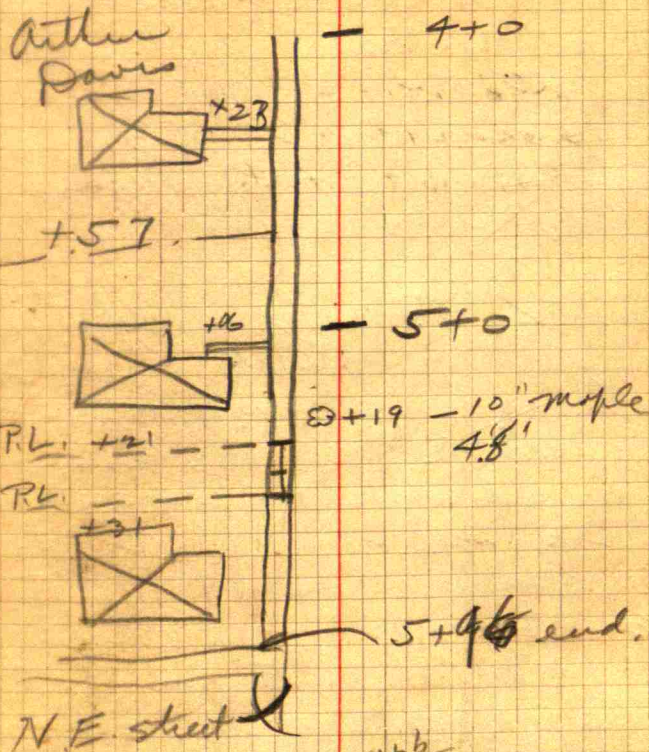
Simple Mendenhall



864.96
84E
851.96
84E
88.5b

LS26
94E
93.5

96.05
94
95.5



080.86 ox
 84E
 85.5b ox
 84E
 83.78
 84E
 84.8 ox
 84E
 84.7 ox
 84E
 84.0 ox
 84E
 84.2 ox
 84E
 84.2 ox

ox + 22.4b
 84E
 ox + 0.6b
 84E
 ox + 8.1b
 84E
 ox + 9.5b
 84E
 ox + 9.9b
 84E
 ox + 18.5b
 84E
 ox + 18.9b
 84E
 ox + 19.9b
 84E
 ox + 15.9b

Levels - Sidewalk

Sta. Gd. Stk 5'S.

0+0 7.52 7.41

1+00 6.65 6.19

Alley North 25' 6.45

2+00 6.13 5.85

Alley North 25' 5.63

3+00 5.58 5.42

Alley North 25' 5.24

E. end walk to remain 5.10-N

4+00 5.00 5.07

N. 4.60

W. end walk to remain - 5 4.67

5+00 4.13 4.02

Alley North - 25' 3.89

5+96 3.92 3.82

sidewalk on E. side of N.E. st

E 3.81

56.701

46.8

10.501

84E

55.66

84E

9.05

84E

65.26

62.36

19.56

37E

37E

37E

37E

37E

37E

37E

37E

37E

37E

20.56

37E

37E

37E

37E

37E

37E

37E

37E

37E

37E

37E

El. sidewalk W. side of Avon Ave. - at 0+00

E 7.61

D.M. on Arrow + tire plug 10' NE of Sta 0+00 El. 10.00

392

10.00

3.81

6.19

100.00

6.19

93.81

05.156

37E

37E

37E

37E

37E

37E

37E

37E

37E

37E

37E

11.00

09.56

37E

37E

37E

37E

37E

37E

37E

37E

43.02
43.38
43.11
43.59
42.92

43.02
41
43.43

Info at Bridge
Send - 43.43
100'N - 43.26
100'N - 43.09

13.5
7.0
6.5
10.5

32.5
65.0

9 68.25

7.58
3.4

11.

EB ab
20
LS ab

0.86
63
LS ab



8.26

24
257
626
0.86

901
3826
7026

8.33
100.0
96
40
3/40

8.33

8.33

8.33

91.63

LB

LS ab

8.26

LS ab

43.43
17

43.26
17

43.09

46.26
3 17
5

46.37
3 19

5

4 1/2

4.5
3 2/3

19.0

30

13.5

16.5

4

64.86
11.16
58

4'-11"

4.92
3 2/3

319.84

328

1476

18.04

LS ab
20
EB

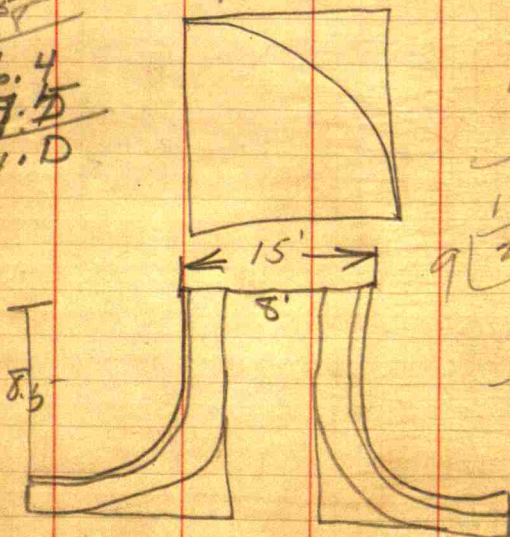
4.1
EB ab
5.26

$$\begin{array}{r} 17 \\ 9 \overline{) 155} \\ \underline{24} \\ 7 \end{array}$$

$$\begin{array}{r} 9.5 \\ 6 \\ \hline 57.0 \\ 6.33 \\ \hline 116.7 \end{array}$$

$$\begin{array}{r} 17 \\ 14 \\ \hline 68 \\ 17 \\ \hline 9 \overline{) 235} \\ \underline{264} \\ 7.5 \\ \hline 34.0 \end{array}$$

$$\begin{array}{r} 9.5 \\ 3.5 \\ \hline 13.0 \end{array}$$



$$\begin{array}{r} 208.26 \\ 260 \\ \hline 946.26 \\ 90 \\ \hline 5526 \\ 90 \\ \hline 6145 \end{array}$$

14
7

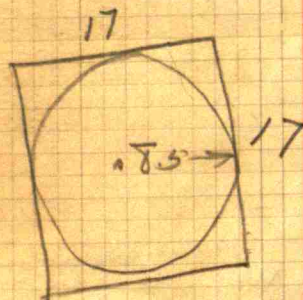
9.8

$$\begin{array}{r} 9 \overline{) 77} \\ \underline{8} \\ 3.5 \end{array}$$

$$\begin{array}{r} 16 \\ 16 \\ \hline 96 \\ 1676 \\ \hline 9 \overline{) 2576} \\ \underline{285} \\ 28.7 \\ \hline 95.5 \end{array}$$

$$\begin{array}{r} 162 \\ 26 \\ \hline 136 \\ 19 \\ \hline 155 \end{array}$$

$$\begin{array}{r} 44 \\ 506 \\ \hline 22 \\ 2200 \\ \hline 2222 \\ 12 \\ \hline 4444 \\ 2222 \\ \hline 26664 \end{array}$$



$$\begin{array}{r} 8.5 \\ 85 \\ \hline 425 \\ 680 \\ \hline 7225 \\ 84 \\ \hline 1032 \\ 21675 \\ \hline 22707 \end{array}$$

$$\begin{array}{r} 1728 \overline{) 26664.0} \\ \underline{1728} \\ 9384 \\ \hline 8640 \\ \hline 7440 \\ 6912 \\ \hline 5280 \end{array}$$

$$\begin{array}{r} 17 \\ 17 \\ \hline 119 \\ 17 \\ \hline 289 \\ 227 \\ \hline 4 \overline{) 62} \\ \underline{4} \\ 19 \\ \hline 1.75 \end{array}$$

May 15

21.1926 - Boss Prother Tile
Grade Top Cut. 30

80/100
Fall
per
100r

0+00	92.80	95.32	2'-6"
1+00	93.60	98.32	4'-8 1/2"
1+50	94.00	98.71	4'-8 1/2"
2+0	94.40	98.07	3'-8"
2+50	94.80	99.69	4'-11"
3+0	95.20	101.29	6'-1"
3+50	95.60	99.19	3'-7"
4+0	96.00	99.21	3'-2 1/2"
4+50	96.40	100.42	4'-0"
5+0	96.80	99.84	3'-0 1/2"
5+50	97.20	102.66	5'-5 1/2"
5+75	97.40	99.89	3'-6"
0+50	93.20	97.70	4'-6"

Zoning Culverts

	W-Fi.	E.	W:	E
6+03	86.50	94.00	C. 7'-0"	C. 2'-0"
7+97	82.50	90.50		95.50 C. 5'-0"
9+27.5	91.00	95.00	95.00 4'-0"	100.00 C. 5'-0"
11+12	92.50	93.00	94.50 2'-0"	

B.M. E1. -100.00 Stone N edge of farm.

155

100.24	99.69
98.07	94.80
94.40	489
3.67	92.83
95.32	99.01
92.80	1.50
2.52	97.51
99.19	99.01
98.32	100.42
93.60	96.40
3.59	4.72
97.70	97.51
99.84	99.01
93.20	92.83
4.68	97.40
4.50	4.68
3.04	1.61

101.29	81
95.20	575
6.09	4.68.00
	4600
	800
99.58	93.50
99.45	86.50
97.44	7.20
95.01	
12.10	
350	

$$\begin{array}{r} 38.40 \\ .064 \\ \hline \end{array}$$

$$\begin{array}{r} 38.336 \\ .064 \\ \hline \end{array}$$

$$\begin{array}{r} 38.272 \\ .064 \\ \hline \end{array}$$

$$\begin{array}{r} 38.208 \\ .064 \\ \hline \end{array}$$

$$\begin{array}{r} 38.144 \\ .064 \\ \hline \end{array}$$

$$\begin{array}{r} 38.080 \\ .064 \\ \hline \end{array}$$

$$\begin{array}{r} 38.016 \\ \hline \end{array}$$

$$\begin{array}{r} 37.44 \\ .064 \\ \hline \end{array}$$

$$\begin{array}{r} 37.376 \\ .064 \\ \hline \end{array}$$

$$\begin{array}{r} 37.312 \\ .064 \\ \hline \end{array}$$

$$\begin{array}{r} 37.248 \\ .064 \\ \hline \end{array}$$

$$\begin{array}{r} 37.184 \\ .064 \\ \hline \end{array}$$

$$\begin{array}{r} 37.120 \\ .064 \\ \hline \end{array}$$

$$\begin{array}{r} 37.056 \\ .064 \\ \hline \end{array}$$

$$\begin{array}{r} 36.992 \\ \hline \end{array}$$

.064

3834

50

3884

38,016

.064

37,952

.064

37,888

.064

37,824

.064

37,760

.064

37,696

.064

37,632

.064

37,568

.064

37,504

.064

37,440

50

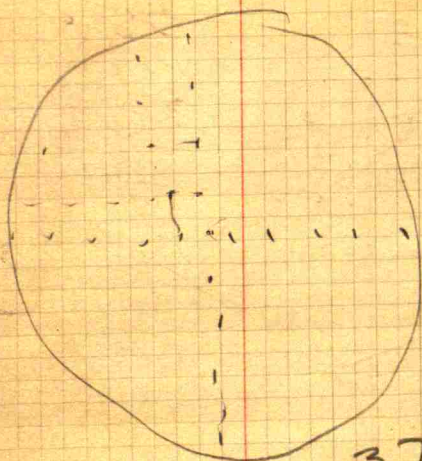
38.72

32

38.40

50

37.01



37.44

32

76

3808

32

38.26

41.26

37.01

4.25

60

$$\begin{array}{r} 668 \overline{) 425.00} \\ \underline{400} \\ 2500 \\ \underline{2420} \\ 800 \\ \underline{770} \\ 300 \end{array}$$