

ARMSTRONG DITCH  
WILLS + WATSON DITCH

153

MINING  
TRANSIT BOOK  
363 A

310 feet from Road <sup>T</sup>  
at start of ditch to the  
ditch

3+71 Bakers West line  
Englishes East line

17+16 Bakers East line  
Road + then J. Lones W.  
line

300 feet from stone

SE of 21 + SW of 22

17+45 Lones W line

tile 31 + 70

38+6.8 Lones South line

J. Hale North line 573 feet  
from West line of Hales

40 a.

58+40 Hale South line 135 feet from West line

76 + 36 South line  
of youngs + North line  
of Right of Way

77 + 57 South line of  
Right of Way + North of Parmous

86 + 30 Fence on South of Ditch  
turns W. along Parmous line  
Lit Swain N. line 600 feet to

91 + 30 Fence line + Ditch  
turns South.

104 + 88 End of ditch  
keeps along the fence  
which is on the East of  
the ditch after the last  
turn.

## STK DITCH

0+0	94.56	87.00
1+0	95.11	87.60
2+0	95.11	88.09
3+0	95.52	88.74
4+0	96.26	89.04
5+0	95.66	88.81
6+0	96.76	89.24
7+0	95.76	89.62
8+0	96.50	89.66
9+0	95.68	90.00
10+0	97.23	90.50
11+0	96.39	90.02
12+0	96.92	90.11
13+0	97.47	90.75
14+0	97.81	90.44
15+0	97.64	90.47
16+0	97.22	91.40
17+0	96.75	91.14
18+0	98.06	91.28
19+0	98.21	91.60
20+0	97.25	91.39
21+0	97.81	91.93
22+0	97.47	91.73
23+0	98.34	92.00
24+0	98.35	92.20

B.M. on  
concrete post at  
road. EL 100.00

⊙ 94.22

⊙ 98.34

4+40 - 4" tile  
from S. 91.67  
F.L. 92.21

7+20 - 6" tile  
from N.  
Top - 92.38  
F.L. 91.96

12+50

Tile from S.  
Top of Tile 91.45  
F.L. 90.68

B.M. EL. 99.98  
SW RAIL  
Bridge Sta  
17+40

Send Wraile

- 8" Tile from S  
92.65 Top T. 19+0  
92.00 FL

8" FROM N 22+98  
TT 9290  
FL 9230  
10" TILE from N  
FL - 91.65 2410  
TT 9250

	STK	FL DITCH
25+0	98.47	92.28
26+0	98.13	93.12
27+0	99.00	92.81
28+0	99.15	92.65
29+0	98.78	92.93
30+0	99.14	92.04
31+0	98.31	93.35
32+0	98.64	93.66
33+0	99.38	93.31
34+0	99.64	93.38
35+0	99.33	92.23
36+0	98.81	93.21
37+0	97.91	94.19
38+0	99.07	94.18
39+0	99.53	94.22
40+0	100.27	94.56
41+0	100.56	94.70
42+0	100.62	94.49
43+0	99.50	94.51
44+0	99.49	94.81
45+0	99.80	95.16
46+0	100.86	95.28
47+0	101.11	95.42
48+0	101.71	95.59
49+0	101.73	95.87
50+0	102.31	96.13

31+70-  
12" tile from E  
32. 93.40

36+90  
8" tile from W  
FL 95.96

43+10  
12" tile  
Joh 94.81  
32 93.92

7  
① Elev. 98.04  
② 96.68  
③ 102.64  
④ 99.50  
⑤ 101.76

S TK Ditch

51	102.55	96.12
52	101.11	95.94
53	103.82	96.09
54	102.81	96.08
55	103.61	96.38
56	103.81	96.01
57	102.07	96.61
58	104.36	96.90
59	104.29	97.26
60	105.35	97.01
61	105.93	96.91
62	106.05	97.25
63	106.88	97.65
64	105.84	97.74
65	105.85	98.23
66	106.30	98.36
67	104.79	98.52
68	104.51	99.06
69	104.78	99.00
70	105.28	98.91
71	105.06	99.15
72	104.81	99.08
73	104.61	99.23
74	104.66	99.34
75	104.72	99.38

tile

sta 6674  
10051 TOP  
10001 Flowline

010381

010381

0102.00

0105.85

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 tile at 672

Flowline 99.48

Top. 100.00

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~~Flowline 99.48~~


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~~Flowline 99.48~~

sta 68452

Flow. 99.65

From W. 6"

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 72497 Tile from  
E.

Flow. 98.94

10

	Stk	Ditch
76	104.75	99.52
77	104.64	99.17
78	104.53	99.45
79	103.54	100.05
80	103.90	99.98
81	104.31	99.74
82	104.02	100.02
83	103.21	99.88
84	104.16	99.93
85	104.53	99.78
86	104.45	100.08
87	104.30	99.47
88	104.25	99.97
89	104.38	99.79
90	103.90	99.85
91	104.10	100.33
92	104.39	100.05
93	104.75	100.39
94	104.57	100.28
95	104.16	100.17
96	103.61	100.59
97	103.75	100.60
98	103.74	100.43
99	103.00	100.87
100	104.23	101.15

10710 tile from  
E flow line 98.94

tile 81 + 50

From W.  
Flow line 99.41

tile 83 + 82  
from W.

100.93 flow line

93 + 27 tile  
From W.

Flow line  
101.00

96 + 90

tile from W.

Flow line 100.79

11  
B.M.  
on N.W. Cor  
of rail of  
Cul. under  
H I + E tracks  
El. 104.16

~~Flow line~~

101 10421/01.14  
 102 10420/01.18  
 103 10433/01.48  
 104 10410/01.97  
 104188 10421/01.81 ←

F.L.

2

	70%	Slk	Slk	5	10
0+0	9975	100.03	9995	10011	10024
0+10	10014		10035		10060
0+50	10279	10452	10437	10512	10615
1+0	10942	10926 <sup>013</sup>	11047	11097	11122
1+30	11122		11165		11190
<del>2+0</del>					
2+0	11023	11032 <sup>13</sup>	11065		11094
3+0	10920	10941			10953
4	10895	10880			10864
5	10883	10871			10853
6	10984	10961			10917
7	11581	11546			11482

10	2	15	10	5	5	Slk	103
10041	10052	10070	10075	10141	10160	10185	
	10090	10215	10470 <sup>12</sup>		10687	10866	
10697	10813	10841	10967	11025	11079	11150	
11135	11166	11212	11229	11235	11227	11227	
	11210		11206		11192	11200	
	11133		11139		11128	11129	
	10976		11017		11035	11068	
	10889		10925		10910	10935	
	10871		10897		10854	10857	
	10937		10915		10900	10896	
	11423		11360		11314	11256	

113580

16

B.M. No 1.

B.M., top of curb at 4. line  
Sta. Sta. 0+0. El. 100.08

B.M. No 2.

B.M. on N.W. Cor. Base of  
second brick post from  
N. El. 115.54  
Sta 7+05

17

9962 over Window  
 95.37

9962

450

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9512

9512

92.21

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2.91

- 1723 W. of CEN. N. OF CEN. SEC. 18 -  
 0+00 N  $88^{\circ}30' E$ .  
 3+42 DEF E.  $-43^{\circ}26'$   
 5+29 DEF E.  $-49^{\circ}10'$   
 12+11 DEF E.  $-12^{\circ}46'$   
 15+21 DEF. L  $-78^{\circ}28'$   
 18+84 DEF E  $-68^{\circ}15'$   
 19+33 E. & W. fence between W.C.  
 and R.L. Dillon.  
 19+33 -1039' E. to the Cen. of Sec. 18.  
 22+17 Def E.  $-28^{\circ}39'$   
 25+48 Def L  $-36^{\circ}52'$  ✓  
 28+90 Def. L  $-36^{\circ}03'$  ✓  
 33+10 DEF. L  $-17^{\circ}36'$  ✓  
 37+28 Def E  $-8^{\circ}14'$  ←  $8^{\circ}$   
 42+77 Def L  $-18^{\circ}04'$   
 44+20 Def L  $-17^{\circ}04'$   
 44+75 Fence along W side  
 of N + S Rd.  
 44+94 E of N + S Rd.  
 780' - South to S<sup>2</sup> mile  
 stone of Sec. 18. -  
 16' x 48" arched.  
 45+10 E. Fence line of N + S  
 Road and West line of Ohio  
 Suburban

- 46+14 Def L.  $21^{\circ}22'$   
 47+53 Def L.  $30^{\circ}49'$   
 50+12 DEF R.  $38^{\circ}55'$   
 52+38 DEF L.  $25^{\circ}47'$   
 52+43 Surber E. line and  
 Thompson W. line.  
 53+67 Def R.  $-36^{\circ}57'$   
 59+31 Thompson E. line and  
 Dugan's W. line.  
 1048<sup>N</sup> S. to Cen S. of Cen  $58^{\circ}$   
 of Sec 18.  
 59+35 Def L.  $7^{\circ}02'$   
 66+29 Def L.  $46^{\circ}13'$   
 69+45 Def R.  $9^{\circ}20'$   
 75+01 N & S Fence. P. L. into  
 77+34 arm No 1, culptier  
 into main  
 77+34 Def R.  $-29^{\circ}41'$  Hill  
 82+22 DEF R.  $-5^{\circ}07'$   
 83+34.5 DEF L.  $-4^{\circ}15'$   
 86+01.5 DEF R.  $-28^{\circ}41'$  ✓  
 88+20 DEF R.  $-17^{\circ}20'$   
 89+40 DEF R.  $-52^{\circ}41'$   
 ARM # 2 ENTERS MAIN Ditch

- 92+64 DEF L - 9°36'
- 95+0 DEF L - 37°01'
- 96+22 DEF - R - 39°53'
- 99+0 DEF - R - 13°35'
- 103+40 DEF - L - 32°51'
- 106+48 DEF - R - 10°50'
- 108+41 STATE PROP Co. S. line  
and N. line of E. & W Road
- 108+57 E Road at Rosebaum  
Bridge
- 108+68 DEF R - 4°12'
- 108+74 S. Fence of E. & W Road  
and Rosebaum's N. Fence line
- 1010' - EAST TO 5<sup>th</sup> MILE STONE  
OF SEC. 17.
- 116+34 DEF L - 39°30'
- 117+65 DEF L - 47°00'
- 120+99 DEF R - 41°35'
- 121+57 DEF R 23°33'
- 122+72 DEF L 20°51'
- 124+09 DEF R 33°46'
- 125+12 DEF L 29°04'
- 127+0 Rosebaum E line and  
W. line of Kuro Rd.
- 127+30 E Kuro Rd.

ROSEBAUM BRIDGE  
CONCRETE FLAT TOP  
14' SPAN  
6' RISE

- 127+43 DEF R 28° 06'  
 127+56 E line of Kears Rd  
 and W line of Martin  
 Johnson  
 127+30 - 1248' N. to the N<sup>2</sup> mile  
 stone of Sec 20.  
 128+76 DEF R - 27° 13'  
 131+14 DEF R - 28° 09'  
 131+46 Martin Johnson's W line  
 and E line of Kears Rd.  
 131+76 E Rd.  
 132+05 W line of Rd. and E.  
 line of Rosebaum.  
 132+32 Def L 26° 44'  
 134+45 Def R 21° 45'  
 136+13 Def R 19° 26'  
 137+94 Def L 31° 07'  
 139+04 DEF R 70° 40' ✓  
 140+08 DEF L 28° 12'  
 141+56 DEF L 42° 37'  
 142+80 DEF R 32° 43'  
 144+13 Rosebaum S line and  
 Kears N. line  
 approx 46' N of Kears N. line.

BRIDGE on Kears Rd.  
 STA 127+30 - Concrete flat top.  
 5' Rise - 14' Span.

2nd Bridge on Kears Rd.  
 Sta 131+76 - Concrete flat top.  
 5' Rise - 14' Span.

144+87 DEF R 17°12'  
~~146+74 State Prop. S. line and~~  
~~Kuns N. line~~

147+25 Def L 49°30'  
 148+51 DEF R 32°26'  
 152+26 DEF R - 25°04'  
 155+02 DEF L - 27°09'  
 158+18 DEF L - 15°12'  
 160+51 DEF R - 15°52'  
 163+03 DEF L - 15°31'  
 165+01 DEF R - 50°33'  
 166+51 DEF L - 25°00'  
 169+08 DEF L - 28°46'  
 170+41 Dodd N. line and

Kuns S. line Ditch  
 goes into Dodd at Dodds  
 N. E. corner.

170+86 DEF R 43°50'  
 173+56 DEF L 50°28'  
 178+40 DEF L 43°26'  
 180+51 DEF L 40°30'  
 182+55 DEF R 22°49'  
 185+96 DEF R 15°16' ✓

186+91 Dodd S. line and  
 Dinsmore N. line but  
 ditch is about on Dodds E.  
 line and Dinsmore W. line

173.56

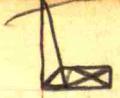
17.586

270

1213' from Dodd N. line  
 to acton N. line.

1312' W from acton  
 W line and Dodd E. line  
 to Rd.

- 186+79 DEF R 21° 28'
- 186+91 S.W. corner of Sec 20  
is 25' E. of ditch
- 191+43 DEF R 10° 24'
- 94+18 DEF L 27° 04'
- 196+94 Cross Denison W  
line and Odd E line
- 197+60 DEF R 10° 41'
- 199+11 DEF L 21° 09'
- 202+83 DEF R 21° 40'
- 04+15.5 DEF R 27° 47'
- 209+40 Chet Parker's E. line and  
Denison's W line
- 209+78 DEF R - 4° 36'
- 210+83 DEF R - 30° 42'
- 213+07 DEF L - 44° 19'
- 15+75 N. line of E+W. Road +  
Chet Parker's S. line.
- 215+91 E Rd.
- 15+99 DEF L 13° 18'
- 331' E. to the E<sup>2</sup> mile stone  
of Sec 30. Thence North  
490' to ditch at which point  
ditch crosses Parker's E. line



85' E to ditch from Chet  
Parker's N.E. corner approx  
Sta 200+50  
N.E. corner N. to ditch  
is 300'

350  
39307  
4537

216+06 S. line of E. + W. Rd  
and Waters N. line

224+63 DEF R  $40^{\circ}25'$

227+45 DEF L  $20^{\circ}42'$

231+26 Waters S. line + Wells  
N. line.

237+54 DEF R  $22^{\circ}00'$

238+76 DEF R  $55^{\circ}26'$

41+40 DEF L -  $13^{\circ}08'$

243+0 DEF R -  $94^{\circ}27'$

245+22 DEF R -  $54^{\circ}54'$  ✓

249+16 DEF L -  $14^{\circ}37'$

251+36 Wells S. line and

Waddle + Warrick N. line

872' W. to S<sup>r</sup> mile stone

Sec 30.

251+86 DEF L -  $34^{\circ}06'$

253+31 DEF L -  $1^{\circ}32'$

255+99 DEF L -  $9^{\circ}18'$

260+18 DEF R -  $32^{\circ}49'$

262+27 DEF R -  $36^{\circ}39'$

264+29 DEF R -  $19^{\circ}49'$

267+05 Thompson + Shultz entry

550' N. from Sta 267+05  
where Thompson + Shultz enters  
N. to 1<sup>st</sup> sec. line (E. + W.)

267+30 DEF L - 79°00'  
 272+25 DEF L - 15°31'  
 276+90 DEF L - 30°22'  
 280+31 DEF L - 45°06'  
 283+02 DEF R - 82°41'  
 285+61 END OF DITCH - NORTH

EDGE OF BRIDGE

1156' W - FROM DITCH TO THE  
 CEN. OF SEC. 31

30

## LEVELS

Flow LINE OF TILE  
FROM WEST, 102.83  
FL. TILE FROM NORTH.

STA	TOP OF STK.	℄	STA	TOP OF STAKE	℄
0+00	106.31	103.17	16+0	105.18	99.72
1+0	107.55	102.78	17+0	104.41	99.74
2+0	107.63	103.05	18+0	104.10	100.05
3+0	107.16	102.62	18+84	105.18	105.05
3+42	107.43	102.65	19+0	105.03	104.36
4+0	106.36	105.90	20+0	103.10	102.60
5+0	106.05	105.48	21+0	102.58	102.19
5+29	105.88	105.53	22+0	102.64	99.13
6+0	106.51	106.07	22+17	102.90	99.07
7+0	105.98	105.57	23+0	102.29	97.95
8+0	105.85	101.24	24+0	102.19	97.67
9+0	105.30	101.25	25+0	102.18	97.33
10+0	105.00	100.73	25+48	101.60	97.25
11+0	105.20	100.71	26+0	101.00	97.04
12+0	104.50	100.78	27+0	100.65	96.81
12+11	105.38	100.80	28+0	100.35	96.10
13+0	106.63	104.60	28+90	100.47	95.82
14+0	102.23	104.59	29+0	100.90	95.77
15+0	103.94	100.71	30+0	100.35	95.80
15+21	103.77	100.50	31+0	97.19	95.47

B.M. on E.  
corner post of gate  
300' W. of Sta 19+33  
EL. 112.06

610606  
ON APR 15 1937

~~104.52~~  
105.40

102.60

100.34

107.00

38		TOP OF STAKE		TOP STAKE	
STA	£	STA	£	STA	£
32+0	95.35	50+10	94.63	91.74	
33+0	99.66	95.30	51+0	95.64	91.47
33+10	99.92	94.68	52+0	95.10	91.58
34+0	99.40	95.04	52+38	94.87	91.08
35+0	98.85	94.00	53+0	94.76	91.67
36+0	97.86	93.60	53+67	94.52	91.35
37+0	98.14	93.70	54+0	94.30	91.32
37+28	97.86	93.60	55+0	94.80	91.00
38+0	97.49	93.86	56+0	94.77	90.83
39+0	96.82	93.55	57+0	93.92	90.64
40+0	96.45	93.30	58+0	94.40	90.61
41+0	96.32	92.97	59+0	94.41	90.34
42+0	95.53	92.81	59+35	93.42	90.22
42+77	95.50	92.14	60+0	93.42	89.76
43+0	95.66	92.22	61+0	92.88	89.71
44+0	95.45	92.50	62+0	92.70	89.82
44+20	95.58	92.60	63+0	91.85	90.20
45+0	95.93	91.44	64+0	91.69	89.71
46+0	95.22	92.25	65+0	91.73	89.59
46+14	95.15	92.43	66+29	91.27	88.94
47+0	94.36	92.14	67+0	91.63	88.90
47+53	95.27	92.35	68+0	91.33	89.20
48+0	94.83	92.23	69+0	91.80	91.57
49+0	94.45	91.60	69+45	91.84	91.47
50+0	94.69	91.55	70+0	91.95	91.40

39	
31+50 - 6" tile	EL 96.85
32+90 - 6" .. ..	96.38
35+50 6" .. ..	95.38
38+60 - " "	93.00
43+50 - " "	91.53 - Top
<hr/>	
92.70	95.93
<hr/>	
94.79	
<hr/>	
<del>4.40</del>	

B. 17. on SW corner of lower  
concrete step on So. side of this  
Surber's house EL. 101.75

47+20 - Tile 92.70 - Top  
53+95 - Tile 91.75 - Top  
54+80 - Tile 91.08 - Fl.

66+0 - <sup>sik</sup> 91.49 - <sup>£</sup> 88.80

91.96

Top STA	STK	E
71+0	91.03	90.95
72+0	91.87	88.93
73+0	91.74	88.20
74+0	91.16	88.60
75+0	9	88.29
76+0	91.21	88.80
77+0	91.18	88.12
77+34	92.42	87.81

Grade	STK	BANK	EDGE DITCH	EDGE DITCH	BANK
77+34	91.93	91.10 <sup>4</sup>	8818 <sup>8</sup>	8814 <sup>12</sup>	9080 <sup>13</sup>
80+0	91.09	9013 <sup>3</sup>	8813 <sup>8</sup>	8804 <sup>12</sup>	9210 <sup>13</sup>
82+22	9065 <sup>4</sup>	9070 <sup>4</sup>	8783 <sup>8</sup>	8791 <sup>14</sup>	9068 <sup>13</sup>
83+34	9254	9255 <sup>3</sup>	8810 <sup>8</sup>	8739 <sup>14</sup>	9318 <sup>13</sup>
86+0	9145	9145 <sup>8</sup>	8725 <sup>11</sup>	8776 <sup>12</sup>	9047 <sup>13</sup>
88+20	91.68	9200 <sup>4</sup>	8705 <sup>11</sup>	8730 <sup>16</sup>	9137 <sup>20</sup>
89+40					
92+4					
95+0					
96+22					
99+0					
01+0					
03+40					
06+48					
08+66					

50k-77+34-EL. 92.42

BTA on Concrete in general  
75' S. of sta 75+01  
on. Highest part EL. 92.37

OUTSIDE BANK	top of DITCH
91.20 <sup>24</sup>	9242
91.32 <sup>23</sup>	9145
9010 <sup>24</sup>	9100
9226 <sup>24</sup>	9275
9081 <sup>33</sup>	9182
91.11 <sup>25</sup>	9206
	9122

9140

9122

STA	TOP STK	GROUND STK.	BANK.	BOTTOM BANK	E	BOTTOM BANK	BANK.	GROUND.	Notes
39+40	9135	9099	9061	8836	8673	9748	7060 (24)	9047	tile from E. sta. 9568
42+64	9090	9045	9027	8726	8621	8733	9060	9040	Cl. 85.90 7L
45+00	9022	8984	8990	8700	8642	8765	9107	9042	rise 6"
46+22	9103	9063	9005	8713	8613	8759	8981	8990	tile from E. sta. 9895
49+0	9087	8995	8917	8669	8576	8703	8881	8905	Cl. 8591 top
51+0		9004	8976	8652	8537	8613	8952	8953	0 9038
53+40	8957	8900	8812	8625	8536	8647	9032	8998	8' tile from W. sta. 104600
56+48	8985	8948	8876	8607	8491	8620	8960	8961	Cl. 8597 top
58+68	9116	9080	9070	8511	8471	8573	9003	8997	08985
60+0		8904	8997	8685	8495	8605	8985	8966	tile from W. 14'
64+0		8885			8880			8990	108+70 sta
66+34	8893	8862	8923	8603	8475	8608	8936	8896	Cl. 10576 7L. some water
67+65	8900	8860	8760	8550	8480	8674	8904	8876	B.M. on top of wall at West end of hand rail
70+99	8920	8876	8864	8520	8411	8515	8795	8793	Cl. 91.67
71+57	8930	8886	8872	8482	8436	8536	8769	8792	Road barrier bridge 108+68
72+72	8917	8882	8863	8473	8384	8572	8822	8817	tile from E. sta. 110+25
74+09	8880	8840	8806	8463	8355	8486	8746	8787	Cl. 8689 7L
75+12	8855	8840	8857	8457	8364	8490	8806	8806	10" tile from W. 117+30
77+43	8824	8888	8830	8876	8317	8394	8674	8726	Cl. 85.02 top
78+76	8850	8809	8655	8402	8387	8445	8710	8701	
81+14	8812	8780	8731	8423	8300	8453	8706	8730	
82+32	8744	8709	8904	8408	8303	8448	8876	8717	
84+45	8704	8665	8642	8426	8215	8316	8697	8735	
86+13	8695	8660	8624	8406	8268	8300	8692		

STA	TOP STK	GROUND AT STK	BANK	BOTTOM BANK	£	BOTTOM BANK	BANK	GROUND
137+94	8705	8660	8592 <sup>3</sup>	8528 <sup>7</sup>	8720 <sup>11</sup>	8365 <sup>15</sup>	8645 <sup>20</sup>	8680 <sup>27</sup>
139+04	8766	8735	8670 <sup>4</sup>	8605 <sup>8</sup>	8713 <sup>15</sup>	8248 <sup>19</sup>	8600 <sup>25</sup>	8685 <sup>30</sup>
140+08	8645	8598	8493 <sup>3</sup>	8280 <sup>8</sup>	8227 <sup>14</sup>	8330 <sup>18</sup>	8590 <sup>23</sup>	8642 <sup>30</sup>
141+56	8835	8796	8696 <sup>2</sup>	8350 <sup>10</sup>	8179 <sup>16</sup>	8330 <sup>20</sup>	8608 <sup>26</sup>	8640 <sup>31</sup>
142+80	8780	8698	8590 <sup>3</sup>	8257 <sup>7</sup>	8145 <sup>11</sup>	8257 <sup>18</sup>	8619 <sup>25</sup>	8625 <sup>29</sup>
144+87	8688	8636	8540 <sup>3</sup>	8302 <sup>8</sup>	8185 <sup>15</sup>	8309 <sup>22</sup>	8607 <sup>27</sup>	8566 <sup>33</sup>
147+25	8650	8611	8614 <sup>4</sup>	8206 <sup>4</sup>	8095 <sup>14</sup>	8206 <sup>10</sup>	8690 <sup>25</sup>	8677 <sup>32</sup>
148+51	8719	8685	8604 <sup>5</sup>	8209 <sup>4</sup>	8124 <sup>14</sup>	8244 <sup>15</sup>	8726 <sup>25</sup>	8586 <sup>34</sup>
152+26	8620	85.71	85.74	81.95	80.65	8170 <sup>18</sup>	8571 <sup>25</sup>	8690 <sup>30</sup>
155+02	85.82	85.30		80.82	79.90	81.08 <sup>14</sup>	86.00 <sup>24</sup>	86.03 <sup>31</sup>
158+18	85.58	85.05	84.78	80.91	79.35	81.16 <sup>18</sup>	85.60 <sup>24</sup>	85.90 <sup>30</sup>
160+51	84.43	83.97	82.75	79.98	79.46	79.80 <sup>18</sup>	85.31 <sup>25</sup>	85.63 <sup>33</sup>
163+03	85.36	84.93	81.94	79.22	78.35	79.90 <sup>21</sup>	82.33 <sup>25</sup>	84.65 <sup>33</sup>
165+01	85.12	84.76	84.33	79.32	78.37	79.45 <sup>48</sup>	83.06 <sup>48</sup>	84.67 <sup>54</sup>
166+51	84.63	82.21	81.37	79.36	78.32	79.81 <sup>15</sup>	81.94 <sup>24</sup>	84.24 <sup>31</sup>
169+08	84.4	84.06	83.84	79.52	78.95	79.50 <sup>31</sup>	81.07 <sup>38</sup>	83.11 <sup>43</sup>
170+86	84.76	84.30	83.52	80.0	79.06	79.43 <sup>24</sup>	84.03 <sup>31</sup>	83.42 <sup>35</sup>
173+56	84.81	84.44	84.60	79.42	78.35	79.38 <sup>22</sup>	81.13 <sup>27</sup>	84.26 <sup>32</sup>
174+50		84.13	84.38	84.60	82.93	80.05 <sup>23</sup>	78.30 <sup>28</sup>	
177+0	84.07	83.66		83.14			81.28 <sup>30</sup>	82.50 <sup>45</sup>
178+10	83.75	83.42	83.64	78.31	77.64	79.94 <sup>20</sup>	80.74 <sup>28</sup>	83.43 <sup>33</sup>
180+51	85.02	84.60	83.91	78.90	77.65	80.79 <sup>28</sup>	80.35 <sup>35</sup>	83.21 <sup>32</sup>
182+55	83.79	83.08	82.10	78.88	77.77	79.76 <sup>20</sup>	82.40 <sup>35</sup>	82.19 <sup>40</sup>
185+96	83.77	83.35	83.13	78.35	76.95	77.62 <sup>25</sup>	81.42 <sup>33</sup>	81.47 <sup>36</sup>
186+79	82.50	82.19	82.21	77.47	76.92	78.06 <sup>26</sup>	81.80 <sup>35</sup>	82.36 <sup>38</sup>

6" fill  
from West  
Sta 137+94  
El. 844074

---

13A on  
top of 8 E wing  
next to hand  
rail  
El. 8875

---

tile from E  
128+10  
El. 847574

---

B.M. on Bend  
east Rail of  
Bridge Sta  
131+65  
El. 91.03

---

tile from  
6" fill  
El. 841674  
Sta 130+15

---

6" fill from  
West Sta 137+10  
El. 84.10

---

tile from E 138+35  
83.46 34.

---

tile from W 6"  
140+95  
El. 84.77

---

tile from  
Sta 145+35  
El. 82.15

STA 46	TOP OF STK	GROUND AT STK	BANK	BOTTOM OF BANK	4	BOTTOM OF BANK	BANK	GROUND	472
189+0		8220	8233	7757	7653	7734	7815	829040	tile from W 67
191+43	8171	8135	8201	7730	7629	7761	8096	8136	Sta 16890
194+18	8072	8036	8040	7675	7556	7656	8094		Fl. 8125
197+60	8177	8140	8052	7661	7479	7590	7764	8236	12' tile from W
199+11	8140	8103	8068	7497	7470	7581	7702	8147	Sta 18185
202+83	8075	8070	7965	7560	7410	7494	7695	8087	tile from E
204+15.5	8104	8072	7964	7490	7420	7452	7680	8024	Sta 188180
207+0		7985	7973	7585	7362	7463	7995	7910	Fl. 7716
209+78	7968	7929	7840	7476	7442	7470	7911		tile from E
210+83	8011	7977	8001	7536	7485	7455	7913		Sta 206+75
213+07	7980	7887	7829	7531	7365	7485	7880	7983	Fl. 7027
215+99	8053	8023	7976	7359	7374	7370	8000	8001	tile from W 87
219+0	7805	7786	7892		7281	7392	7751	7760	Sta 21450
222+0		7783	7708	7371	7245	7367	7805	7779	Fl. 7464
224+63	7810	7760	7645	7371	7231	7400	7733	7704	tile from W 4
227+45	7830	7788	7635	9920	7181	7330	7683	7690	Sta 215+60
231+0		7600	7586	7200	7108	7234	7570	7521	Fl. 7472
234+0		7636	7624	7210	7091	7217	7582	7581	B.M. on
237+54	7611	7566	7520	7128	7097	7087	7441	7831	Top of SW
238+76	7581	7552	7671	7170	7072	7060	7690		at Bottom
241+40	7606	7553	7587	7101	7006	7203	7507	7497	of Handrail
243+0	7465	7414	7430	7097	6968	7063	7488	7462	Sta 218+25
245+22	7404	7363	7238	6971	6943	7031	4556	8000	Fl. 7420
247+0		7426		6923	6885	6981	7305	7372	076.54
249+16	7386	7347	7172	6916	6882	6928	7211	7280	076.10

B.M. on  
 Top of SW  
 at Bottom  
 of Handrail  
 Sta 215+99  
 Fl. 80.78  
 tile from E 6"  
 Sta 218+25  
 Fl. 74.20  
 076.54  
 076.10  
 074.65

STA	TOP STK	GROUND AT STK	BANK	BOTTOM OF BANK	±	BOTTOM OF BANK	BANK	GROUND	
251+86	7358 <sup>0</sup>	7331	7210 <sup>9</sup>	6945 <sup>8</sup>	6263 <sup>21</sup>	6917 <sup>23</sup>	7206 <sup>32</sup>	7227 <sup>32</sup>	7346 <sup>0</sup> 6907 <sup>0</sup>
253+31	7305	7252	7161 <sup>9</sup>	6785 <sup>7</sup>	6756 <sup>2</sup>	6821 <sup>20</sup>	7222 <sup>22</sup>	7340 <sup>30</sup>	6692 <sup>0</sup>
255+99	7257	7209	7119 <sup>5</sup>	6871 <sup>13</sup>	6747 <sup>11</sup>	6860 <sup>22</sup>	710 <sup>27</sup>	7263 <sup>38</sup>	
258+0		7279	7282 <sup>0</sup>	7240 <sup>10</sup>	7222 <sup>21</sup>	7209 <sup>30</sup>	7306 <sup>40</sup>		7293 50
260+18	7130	7094	7068 <sup>4</sup>	6850 <sup>8</sup>	6726 <sup>3</sup>	6808 <sup>25</sup>	7068 <sup>28</sup>	7130 <sup>32</sup>	7343
262+27	7164	7127	7095 <sup>3</sup>	6808 <sup>6</sup>	6710 <sup>14</sup>	6784 <sup>20</sup>	6930 <sup>26</sup> 7253 <sup>29</sup>	7355 <sup>40</sup>	6831 <sup>0</sup>
264+29	7120	7080	7067 <sup>5</sup>	6740 <sup>8</sup>	6661 <sup>16</sup>	6735 <sup>21</sup>	7070 <sup>27</sup>	7150 <sup>35</sup>	7200 <sup>0</sup>
267+30	7053	707	7000 <sup>12</sup>	6685 <sup>21</sup>	6575 <sup>1</sup>	6720 <sup>34</sup>	7065 <sup>45</sup>	7023 <sup>50</sup>	
270+0		7110	7021 <sup>5</sup>	6697 <sup>7</sup>	6570 <sup>2</sup>	6728 <sup>34</sup>	6917 <sup>36</sup>	6996 <sup>40</sup>	
272+25	7284	7246	7036 <sup>1</sup>	6592 <sup>17</sup>	6542 <sup>2</sup>	6692 <sup>31</sup>	7131 <sup>35</sup>	7187 <sup>45</sup>	
275+0	7152 <sup>0</sup>	6878	6817 <sup>2</sup>	6618 <sup>8</sup>	6548 <sup>2</sup>	6565 <sup>20</sup>	6860 <sup>35</sup>	6857 <sup>45</sup>	
276+90	7743 <sup>3</sup>	7373	7293 <sup>5</sup>	6604 <sup>17</sup>	6753 <sup>11</sup>	6629 <sup>3</sup>	6735 <sup>36</sup>	6806 <sup>40</sup>	
280+31	6937	6901	6815 <sup>7</sup>	6426 <sup>20</sup>	6320 <sup>10</sup>	6442 <sup>30</sup>	6645 <sup>33</sup>	6770 <sup>40</sup>	
283+02	6747	6707	6618 <sup>5</sup>	6362 <sup>11</sup>	6275 <sup>4</sup>	6419 <sup>25</sup>	6550 <sup>28</sup>	6770 <sup>36</sup>	6680 <sup>41</sup>
285+61			6875 <sup>1</sup>	6403 <sup>2</sup>	6243 <sup>10</sup>	6413 <sup>36</sup>		661340	

cross section north of Thompson Valley Drain  
±

6630

Sta 285+61  
B.M. on N. end of W. about  
NE corner at bottom of  
mud wall.  
EL. 73.16

Check Bench Marks

B.M. - Sta 285461 - EL. 73.16

- 0 83.50
- 0 88.88
- 0 93.45
- 0 91.38
- 0 90.96
- 0 87.00
- 0 80.09
- 0 79.02
- 0 80.08
- 0 83.28
- 0 84.47
- 0 8071
- 0 8406
- 0 8343
- 0 8080
- 0 8535
- 0 87.65
- 0 8210
- 0 80.24
- 0 85.07
- 0 90.56
- 0 89.77
- 0 89.25
- 0 89.20

SW. cor. Patton St

SE cor. C. and S. rail

check of B.M. at Chet Parkers B.M. 21549

Noon.

9103  
9105

9103 B.M.  
9110 check

check

0 91.10  
 0 88.82  
 0 94.27  
 0 91.71  
 0 91.13  
 0 96.49  
 0 92.59  
 0 92.10  
 0 94.64  
 0 95.75  
 0 90.74  
 0 92.35  
 0 91.57  
 0 91.83  
 0 92.61  
 0 94.34  
 0 100.42  
 0 105.57  
 0 108.67  
 0 105.12  
 0 104.38  
 0 102.07  
 0 101.72

BM }  
 91.03 }  
 88.75 }  
 88.75 }

along  
 road  
 1200 ft

BM  
 91.67 }  
 Roadway  
 Bridge

BM  
 96.43 }  
 at outlet  
 of arm #1

BM  
 95.75 }  
 head of  
 arm #2

BM on con. slope  
 92.37 }  
 at outlet of  
 arm #1

BM  
 108.65 }  
 at head of  
 arm #1

BM  
 112.06 }  
 101.75 }  
 at head of  
 Main  
 arm  
 #1

56

Sta	Sh. of Stk	Bank	Bank	Bank	Bank
0+0	10600	10530	10591	10496	10617
3+0	10667	10617	10319	10312	10611
6+0	106.01		10572		10527
9+0	104.72	10495	10180	10130	10460
12+0	104.21	105.00	10090	10095	1056
15+0	103.70	104.66	10070	10080	10477
18+0	10371	10330	10022	9995	10379
21+0	10185		10120		10195
24+0	10178	10123	9845	9812	10129
27+0	9997	10081	9772	9733	9982
30+0	10046	9992	9617	9585	9992
33+0	9920	9867	9536	9537	9813
36+0	9750	9711	9423	9467	9755
39+0	9640	9590	9385	9396	9657
42+0	9543	9486	9315	9319	9490
45+0	9580	9534	9335	9342	9510
48+0	9445	9394	9266	9267	9476
51+0	9538	9455	9234	9225	9415
54+0	9388	9368	9197	9190	9850
57+0	9371	9338	9163	9095	9367
60+0	9320	9280	9050	9085	9351
63+0	9170	9225	9073	9001	9260
66+0	9126	9115	8967	8974	9129
69+0	9150	9144	9170	9192	9207
72+0	9091	9100	9116	9137	
75+0	9075	9001	8875	8863	9004

Bank	Bank
10666 <sup>6</sup>	
10668 <sup>16</sup>	
10473 <sup>23</sup>	
10470 <sup>17</sup>	
10470 <sup>20</sup>	
10408 <sup>20</sup>	
10330 <sup>19</sup>	
10208 <sup>26</sup>	
9964 <sup>18</sup>	
9998 <sup>20</sup>	
9853 <sup>20</sup>	
9705 <sup>22</sup>	
9645 <sup>15</sup>	
9468 <sup>21</sup>	
7547 <sup>18</sup>	
7515 <sup>18</sup>	
7425 <sup>22</sup>	
9376 <sup>22</sup>	
9340 <sup>22</sup>	
9290 <sup>24</sup>	
9184 <sup>25</sup>	
9127 <sup>24</sup>	
9197 <sup>25</sup>	
9220 <sup>26</sup>	
9040 <sup>21</sup>	

105.13

~~102.84~~~~104.91~~~~99.70~~~~97.71~~~~96.6~~~~94.5~~~~91.63~~

92.36 check

Bm Cl. Sta 75+0

Bm Cl 92.37

2 Q of lower end

2 of W+W From Near Bridge on,

13	6237
26	6230
39	6100
12	5931
15	6025
18	5968
21	5686
24	5619
27	5510
30	5550
33	5540
36	5564
39	5440
42	5501
45	5377
48	5426
51	5345
<del>54</del>	
57	5233
60	5145
63	5138
66	50.31
69	
72	
75	

From ditch  
6065

6243  
50.31  

---

12.12

~~69290~~  
~~6500~~  
B.M. EL. 67.16  
on Warwick Bridge  
on S. Wabut. on Secor  
where wing turns  
S.W.

{  
on Parks. } ~~56265~~  
~~53997~~

5345  
~~6243~~  
~~5345~~  

---

71.03  
8.

~~5525~~  
~~557.18~~  

---

056.42

55.75  
50.07

B.M. EL. 59.14  
on W Wabut wall.  
where wing breaks from  
abutment

check arm #2

0+0  
0+50  
1+0  
1+50  
2+0  
2+50  
3+0  
3+50  
4+0  
4+50  
5+0



Arm of Arm #1  
♀

<del>0</del>		
1	8981	
2	9031	
3	9018	
4	9069	
5	9091	
6	9116	
7	9148	
8	9173	
9	9271	
10	9298	
11	9295	9145 Flight 8" tile
11491	9299	tile

D 9151

285+61 DEF L -  $32^{\circ}36'$  - sk 30' 78

286+50 Leave old channel

289+0

289+80 Intersects old channel 289+80

292+0

294+79 Def L  $29^{\circ}03'$   
Crosses old channel

296+0

297+0 crosses old channel.

298+0 Pittsboro Ditch crosses in

298+57 Def L  $65^{\circ}33'$

300+0

301+0 Def L  $30^{\circ}45'$

302+0 Def. L  $18^{\circ}-18'$

304+0 Def. L  $8^{\circ}-48'$  crosses into old channel

305+0 leaves old channel.

306+0

307+63 Def R  $11^{\circ}-50'$  re-enters old channel

1103 Feet from Weaver Bridge to  
Warwick Bridge

(309+75) Def. R. 15°-57'

310+50 Crosses old channel, 4th

(312+0) Def. R.

312+50 Crosses old channel.

(313+0) Def. R. 42°-42'

(314+85)

(318+0)

319+42 Def. R. 8°-51'

319+72 Crosses old channel.

(322+0)

324+78 Crosses old channel (B)

(326+0)

328+83 Crosses old channel.

(330+28) Def. L. 30°-10'

(332+10) Crosses old channel.

(335+0)

338+0

339+0 Def R.  $56^{\circ}26'$

341+0

into old channel.

343+66

345+0

347+30 center of bridge

348+06 Def L  $61^{\circ}00'$

351+70

354+75 Def R  $17^{\circ}20'$

356+54 Def R.  $32^{\circ}18'$

360+53 Def R.  $50^{\circ}41'$  ✓

362+58

364+76 Def R.  $28^{\circ}04'$

368+22 Def R.  $26^{\circ}58'$

371+0

372+0 ditch near old channel

823 feet from S end of  
main Road to Bridge at  
N. + N.

81

82  
373+0

374+75 Ditch 1/2 old channel

375+34 Def. R.  $5^{\circ} 23'$

377+63 Def. L  $17^{\circ} 06'$

379+51 Def. L  $28^{\circ} 18'$

382+85 Def. L  $37^{\circ} 21'$

386+0

390+0

392+35 Def. L  $2^{\circ} 55'$

394+09 Ditch leaves old channel

395+40 Def. R  $13^{\circ} 30'$

397+39 Def. R  $69^{\circ} 07'$

400+75

403+13 Def. L  $23^{\circ} 00'$

407+0

83  
480 feet from Ditch to  
on stone at Sparks cemetery

789

51

540

410+0

412+43 Def. L  $25^{\circ}-45'$

413+0 Ditch leaves old channel

416+21 Def. R  $26^{\circ}-47'$

418+13 Def. R.  $39^{\circ}-25'$

421+47 Def. R  $23^{\circ}-24'$

422+20 Hits old channel  
422+47 leaves old "

423+20 Hits old channel.  
~~423+37 leaves "~~

425+34 Def. R  $32^{\circ}-40'$

428+57 Def. R  $4^{\circ}-54'$

429+95 Ditch, leaves old channel.

431+0

432+97 Def. L  $54^{\circ}-28'$

437+0 End of drain

429+34

'85

2273 feet from Cor. Stone  
at Sparks Cem. S to Surber  
Arch.

88

TJK  
skkGround  
at  
skk

Bank

Bottom  
Bank

E

Bottom  
Bank

Bank

Ground.

64.74

89

286+50	64.74	64.10	Bank 25'E 67.30	Bottom Bank	62.80
x 287+0					67.25
288+0	68.35	67.49	Bank 25'E 66.43		
x 289+0					66.10
289+80					65.95
+90					62.05
+96					62.40
290+10					68.95
291+0					67.75
291+75					66.65
291+80					64.50
292+0	65.58	65.00	Bank 25'E 64.40	Level	
293+0					66.00
294+0					67.25
294+10					65.45
294+19	64.00	63.71		Bot. stream 60.40	
294+85					60.40
294+95					60.60
295+0					64.30
295+25					66.90
296+0	65.20	64.55		Level	65.30
296+60					62.45
+70					61.20
+80					63.65
+90					63.80

65.25

Bottom  
Bank  
15W  
66.75

B.M.  
285+61  
17 end of W.  
about. NE  
Cor. of bottom  
of mud wall  
73.16

Top  
shGround  
sh

E

297+0					6045
297+20					5972
297+25					6310
297+95					6260
298+0					5985
298+57	65.12	64.61	60.10		60.50 <sup>20</sup>
299+0	73.75 <sup>15</sup>				60.69
300+0	63.78		63.45 <sup>8</sup>	60.40 <sup>15</sup>	60.30 <sup>20</sup>
301+0					6012
302+0	62.80 <sup>0</sup>				5945
303+0					5930
304+0	74.08 <sup>E</sup> 64.10	63.38	59.90 <sup>14</sup>		5910
305+0	red silt 59.20 <sup>0</sup>				5860
306+0	60.25	59.72	61.71 <sup>20</sup>	62.00 <sup>40</sup>	
307+60	61	61.25	58.23 <sup>10</sup>		5657
308+0					5627
309+0					5645
309+75	61.45	60.87	59.00 <sup>26</sup>	56.58 <sup>30</sup>	5844 <sup>40</sup>
310+0					5815
310+30					5706
311+0					5677
312+0	5911	5820	red silt 64.56 <sup>10</sup> 56.95 <sup>20</sup>	60.62 <sup>40</sup>	
312+25					5789
312+30					5687
312+95					5794
312+90					6157

	30	40'
61.15		63.70
60.50 <sup>30</sup>		63.05 <sup>40</sup>
59.25 <sup>25</sup>		61.70 <sup>35</sup>
58.58 <sup>0</sup>		59.58 <sup>40</sup>
58.44 <sup>40</sup>		61.55 <sup>50</sup>

60 63<sup>40</sup>

		Dred:		R					
		at sth	20'	25'		30	40		
92	313+0	2th 6252	62.00	5987	5645	0531	5891	6043	5817
	314+0					6017			
	314+0	5820	5750	5769	5624 <sup>20</sup>		5590 <sup>30</sup>	5788 <sup>40</sup>	
	315+0					5670			
	315+5					5600			
	315+85					6090			
	316+0					6074			
	317+0					5917			
	318+0	6180	6090	5687 <sup>10</sup>		5550	5696 <sup>30</sup>	5879 <sup>40</sup>	
	319+0	✓				5941			
	319+72					5874			
	319+77					5563			
	319+95					5596			
	320+0					5805			
	321+0					5983			
	322+0	6030	5960			5894			
	323+0					5996			
	323+30					5941			
	323+65					5703			
	324+0					5887			
	324+78					5748			
	324+88					5560			
	324+98					5539			
	325+0					5780			
	326+0	5827	5757	5550 <sup>10</sup>		5359 <sup>20</sup>	5565 <sup>30</sup>	5856 <sup>40</sup>	5900 <sup>40</sup>
	327+0					5377			
	328+0					5470			

	Lat	Long	at note
329+83			
329+0			
330+28	5931	5836	
331+0			
332+0			
332+50			
333+0	5715	5649	5640 <sup>25</sup>
333+03			
333+10			
333+20			
333+25			
335+0	5846	5802	
336+0			
337+0			
337+10			
337+15			
338+0	5406	5330	5250 <sup>5</sup>
339+0			
340+0			
341+0	5365	5310	5225 <sup>5</sup> 5090 <sup>8</sup>
342+0			
343+0			
343+66	5463	5420	5221 <sup>15</sup>
344+0			
344+10			
344+20			
345+0	5597	5530	

2

5387

5887

5788

5752

5345

5443

5263

5395

5772

5750

5753

5526

5318

5770

5661

5610

5280<sup>5</sup>

5125

5130

5090

5041

5447

5025

5327<sup>25</sup>

5475<sup>35</sup>

5385<sup>40</sup>

5317<sup>30</sup>

5785<sup>45</sup>

5846 (1)

5460 0

95

Site ad site  
Fund

346+0					5090
347+0					5091 <sup>15</sup>
348+06	6174	6138	5432 <sup>15</sup>	5145 <sup>17</sup>	5025
349+0					5060
350+0					5019
351+0					4992
351+70	5292	5224	4995 <sup>3</sup>		4955 <sup>10</sup>
353+0					4980
354+0					4990
354+75	5357	5293	5703 <sup>10</sup>		4955 <sup>10</sup>
356+0					486
356+54	5321	5215	5047 <sup>6</sup>		4835 <sup>10</sup>
358+0					4840
359+0					4779
360+53	5338	5213	4815 <sup>10</sup>		4727
362+0					4680
363+0					4647
364+0					4650
364+76	5154	5056 <sup>6</sup>	478 <sup>10</sup>		4715 <sup>10</sup>
366+0					4682
368+22	5140	5092	4810 <sup>10</sup>		4695
369+0					4694
<del>370+0</del>					
371+0	4885 <sup>0</sup>	4840	4641 <sup>10</sup>		4573 <sup>10</sup>
372+0					4523
372+05					4895

5-7-20

B.M. 21 5914

					5165 <sup>38</sup>	5344 <sup>42</sup>	
					5250 <sup>30</sup>	5224 <sup>70</sup>	
					4970 <sup>38</sup>	5024 <sup>33</sup>	5450 <sup>40</sup>
					4895 <sup>30</sup>	5049 <sup>40</sup>	5345 <sup>47</sup>
						4776 <sup>37</sup>	4976 <sup>40</sup>
						4772 <sup>40</sup>	5205 <sup>50</sup>
					4746 <sup>30</sup>	5543 <sup>40</sup>	
					4658 <sup>35</sup>	5042 <sup>30</sup>	

5142

5300

stk  
Bound  
at  
stk

373+0	5065				5006
374+0					4799
374+75					4380
375+34	5046	4920 <sup>4</sup>	4390 <sup>8</sup>		4375
377+63	4923	4866	4453 <sup>8</sup>		4365
379+51		5964	4864	4332 <sup>14</sup>	4321
381+0					4231
382+85	4670	4620		4319 <sup>10</sup>	4331 <sup>4</sup>
384+0					4195
386+0	4595	4542	4342 <sup>6</sup>		4126
388+0					4231
390+0	4630	4509	4240 <sup>4</sup>		4192 <sup>20</sup>
392+55	4770	4704	4230 <sup>12</sup>		4175 <sup>24</sup>
394+09					4063
394+15					4467
394+90					4445
395+0					4158
395+20					4193
395+40	4947	4845	4571 <sup>14</sup>	4415 <sup>20</sup>	
399+34	4576	4515			4365 <sup>30</sup>
399+0					4265
400+75	4197	4114	4014 <sup>3</sup>		4000
402+0					3780
403+13	4255		4201		
405+0					4116
407+0	4625	4164	3812 <sup>10</sup>		3723

~~46150~~  
46450

	36	40
4423	4935	
4482 <sup>35</sup>	4684 <sup>40</sup>	
4463 <sup>25</sup>	4725 <sup>40</sup>	
	35	40
4417	4657	
	28	40
4389	4630	
4244 <sup>23</sup>	4600 <sup>40</sup>	
	35	39
4182	4395	

BM on  
S.E. Cor. of  
Concrete Box  
at S.E. Cor. of  
Sparks Cem. Co.  
Q. 4855

4151

4338<sup>40</sup>

3950<sup>25</sup>

3881<sup>25</sup> 3940<sup>33</sup> 4030<sup>40</sup>

F 100

2012

Hand  
at site

Q  
37.50

40850							
410+0	4090	4025	3841	10			
411+0							
412+43	4067	4015	3844	4	3765	16	
413+0							
713+20							
414+0				10	3925		
415+0							
416+21	3912	3838	3695	8	3840	16	
418+13	3757	3701	3670				
419+50							
421+47	3590	3523	3377	7	3351	12	
422+20							
422+25							
422+47							
422+52							
423+22							
423+32							
425+35	3467	3410	2980	12			
426+50							
428+51	3434	3376	3312	10	2995	28	
429+95							
430+10							
431+10	3435	3380					
432+00							
432+70							
432+97							
	31.80	28.12	27.20	10			

3750							
3750	30	3820	4195	40			
3690							
3690							
3641	40	3730	3865	45			
3605							
3950							
3956							
3980							
3620							
3440							
3480							
3410							
3353							
3247							
3037							
3563							
3443							
2960							
2910							
2916							
2840							
3525							
3144							
2710							
2700							
2765	34						
2870		40					

T 101

BNA  
on top SE  
Wing of Surber  
Arch.  
El. 3742

032.95

Tot  
stk

Drawn  
at  
stk

£

43570

43710

30.71

30.14

<sup>5</sup>  
28.24

<sup>18</sup>  
27.50

26.67

26.27

<sup>35</sup>  
26.90

<sup>40</sup>  
31.52

Sub-arm No 1.

Sta	6d.5th	New Rd	Cut	6d.5th	Cut.
0+00	91.25	86.01	5.24	91.31	5.30
1+0	90.95	86.36	4.59	91.00	4.64
2+00	91.65	86.71	4.94	91.80	5.09
3+0	91.41	87.06	4.35	92.75	5.69
4+0	92.26	87.41	4.85	93.00	5.59
5+00	93.04	87.76	5.28	93.45	5.69
6+0	93.90	88.11	5.79	94.00	5.89
7+0	93.75	88.46	5.29	94.60	6.14
8+0	93.85	88.81	5.04	94.06	5.25
9+0	94.28	89.16	5.12	94.29	5.13
10+0	94.41	89.51	4.90	94.55	5.04
11+0	94.51	89.86	4.87	94.72	4.86

Tile check

0+0	87.41	6+0	89.24
0+50	87.55	6+50	89.39
1+0	87.58	7+0	89.74
1+50	87.69	7+50	89.78
2+0	87.82	8+0	89.91
2+50	87.95	8+50	89.93
3+0	88.15	9+0	90.12
3+50	88.34	9+50	90.36
4+0	88.44	10+0	90.46
4+50	88.52	10+50	90.64
5+0	88.67	11+0	
5+50	88.91		

91.31  
86.01  
530  
90.95  
86.36  
4.59

9226 9141  
8741 8706  
485 4.35

9390  
8811  
579

9385  
8881  
504

9471  
8986  
4.85

9131  
86.01  
5.30

9345  
8776  
5.69

9406 8846  
8881 6.14

91.75

9304  
8776  
528

9375  
8846  
5.29

9429  
13

9441  
8951  
490

8916  
132

9048 9100  
8636  
4.64

9180  
8671  
5.09

9400  
8811  
589

107

9339  
B.M.

1.

9275  
8706

5.69

9455  
8951

504

WILLS &amp; WATSON

6" Tile from West  
 10" Vit. Tile under N.S.  
 Road - Tile badly broken.  
 10" tile from N. of Sta.  
 0+8 and East side ditch  
 672' North to the N.  
 mile stone Sec 18 from 0+00

0+00 N 89 $\frac{1}{2}$ ° E.0+12 Collins W. line and  
E line of Road.

1+56 Def. R. 140° 36'

4+67 Def. R. 27° 59'

7+15 Def. R. 26° 48'

8+35 Def. R. 52° 33'

9+99 Def. L. 22° 0'

11+61 Collins S line and  
Ditzgenburger N. line  
E + W. Fence.

11+81 Def. R. - 13° 47'

12+48 Def. L. - 39° 13'

13+65 DEF. L. - 27° 00'

15+23 DEF. R. - 42° 14'

17+93 Def. L. - 91° 02'

21+24 Def. R. - 9° 37'

- 22+35 DEF L -  $14^{\circ}54'$   
 24+48 Def L -  $14^{\circ}02'$   
 28+65 DEF R -  $19^{\circ}46'$   
 31+42 Def R -  $61^{\circ}20'$   
 34+30 DEF L -  $58^{\circ}38'$   
 37+01 DEF R -  $8^{\circ}26'$   
 39+35 Ditzgenburg's E. line and  
 Mullins W. line. - N + S. Fence  
 39+47 Def R -  $1014'$   
 Approx. 20' N. of Ditzgenburg's  
 S. line and Braups N. line  
 43+43 DEF R -  $69^{\circ}53'$   
 45+64 DEF R -  $22^{\circ}48'$   
 48+43 E + W Fence  
 57+90 DEF L -  $13^{\circ}04'$   
 58+30 END OF ARM #1  
 Def Left onto main ditch  
 Angle  $96^{\circ}28'$

ARM #2

Starts 20' West of Roadman  
and Schenk corner and  
10' South of Tom Conroy  
Ditch in Dillon.

6" tile from East and  
10" tile from North and some  
tile from South -

0+00 N 90° W

9+90 DEF L 86° 49'

18+93 DEF R 86° 42'

21+64 DEF L 90°

29+85 Dillon's S line and  
State Prop Co. N. line

33+88 End of Arm #2

534' from Ditch East to  
West line of Dillon line

AREA # 1 - LEVELS

118

FL TILE FROM NW. 100.39-6"  
 FL TILE FROM W- 100.44-4"  
 FL TILE FROM N- 100.21-8"

STA.	STK	E	STA.	STK	E
10+0	104.47	101.54	14+0	100.25	97.17
1+0	102.86	100.35	15+0	100.28	96.30
1+56	104.83	100.22	15+23	99.75	96.35
2+0	104.85 <sup>out</sup>	100.10	16+0	100.00	96.30
3+0	101.90 <sup>out</sup>	100.27	17+0	99.80	95.95
4+0	101.42 <sup>out</sup>	100.30	17+93	100.40	97.53
4+67	101.68	100.20	18+0	99.80	98.48
5+0	102.50	100.11	19+0	99.05	94.65
6+0	101.70	100.00	20+0	98.58	94.50
7+0	102.45	99.80	21+0	98.20	94.73
7+15	103.22	99.40	21+24	98.27	94.35
8+0	102.65	99.08	22+0	98.02	94.07
8+35	101.68 <sup>out</sup>	99.36	22+35	97.76	94.25
9+0	100.06	99.04	23+0	97.58	93.95
9+99	101.79	98.73	24+0	96.95	93.61
11+0	102.20	97.64	24+48	96.99	93.34
11+81	102.50	97.68	25+0	96.65	92.81
12+0	102.50	97.90	26+0	96.45	92.95
12+48	101.89	98.80	27+0	96.44	92.60
13+0	101.11	97.70	28+0	95.92	92.34
13+65	100.10	97.06	28+65	95.10 <sup>out</sup>	92.35

46.470

119

B.M. on  
 Corner Post 25'  
 N. of 0+15.  
 EL. 108.65  
 near Hugh McCurdy

096.44  
 098.27  
 0102.50  
 0104.95

27+50-5" tile 92.50 FL. from road  
 11+25-6" " 98.09 " " W.  
 8+40- " 99.65 top " E

97.560 0103.33  
~~100.65~~  
 0100.08  
~~0102.7~~  
~~0103.27~~

120

STA	TOP STK ✓	℄	STA	STR ✓	℄
29+0	96.01	92.45	49+0	92.02	89.25
30+0	95.05	92.06	50+0	91.48	88.02
31+0	94.49	91.95	51+0	91.11	88.50
31+42	94.35	91.55	52+0	91.18	88.79
32+0	94.72	90.96	53+0	91.95	88.92
33+0	94.18	90.85	54+0	91.80	88.82
34+0	93.22	93.45	55+0	91.43	88.64
34+30	94.33	90.61	56+0	91.38	88.43
35+0	94.21	90.53	57+0	91.74	88.07
36+0	93.78	90.49	57+90	91.85	88.44
37+01	93.35	90.35			91.85
38+0	93.79	89.70	58+30		88.55
39+0	93.23	90.30			Tiled
39+47	92.62	90.72	58+0	92.38	84.60
40+0	93.54	92.65			
41+0	92.70	92.05			
42+0	92.73	90.00			
43+0	91.35	89.88			
43+93	91.25	89.84			
44+0	9	-			
45+0	91.47	90.51			
45+64	91.85	89.10			
46+0	91.94	89.22			
47+0	92.91	89.22			
48+0	92.53	89.24			

094.35

121

BM. Set Set Sept  
25<sup>th</sup>  
on brace post lower  
end 150. No of sta  
31+42 EL. 95.97

~~091.38~~  
~~092.03~~  
~~091.86~~  
~~091.55~~  
093.78

Tide 36+50 - EL - 90.68, top.

Tide 31+38 - EL - 92.15

B.M. set  
Aug 14 - 1928  
60' W. of sta.  
45+0 -  
High point on  
stump  
E.L. 93.39

091.35

90.57

91.55 4400

91.95 4600

90.92 3200

91.75

9238  
8460  
7.78

F 122

 AREA #2  
 LEVELS

STA	STK	℄	STA	STK	℄
0+0	93.82	92.31	21+64	92.83	89.25
1+0	95.94	92.09	22+0	92.13	88.83
2+0	96.24	91.66	23+0	93.73	88.22
3+0	95.06	91.61	24+0	93.70	88.85
4+0	94.90	91.40	25+0	92.00	88.62
5+0	94.17	91.35	26+0	91.70	88.90
① 6+0	94.48	91.58	27+0	91.78	88.30
7+0	93.44	91.45	28+0	92.53	88.34
8+0 <sup>out</sup>	93.17	91.30	29+0	92.29	88.42
9+0 <sup>out</sup>	93.25	90.61	30+0	91.50	88.60
9+90 <sup>out</sup>	94.35	91.15	31+0	91.37	88.30
10+0 <sup>out</sup>	93.76	91.15	32+0	91.71	88.10
11+0 <sup>out</sup>	93.05	90.85	33+0	91.26	87.70
12+0	92.29	90.80	33+88	90.82	86.98
① 13+0	92.84	90.32			
14+0	93.10	90.30			
15+0	92.78	90.10			
16+0	93.00	89.62			
17+0	92.89	89.65			
18+0	92.36	89.65			
18+93	92.10	89.90			
19+0	92.20	89.90			
20+0	92.03	89.62			
21+0	91.74	88.80			

$$\begin{array}{r} 216 \\ 1893 \\ \hline 771 \end{array}$$

0 91.22

123

 B.M. on Top of wood  
 corner post 40' West of  
 ditch at Sta 29+85 - EL. 96.43

① 92.85

0 95.05

~~0 91.00~~
 8" Tile from E. at Sta 29+65  
 FL. - 87.63

 18+27 - 6" tile FL. 90.43 from E. ~~0 91.10~~

16+50 - 4" tile F.L. 90.75 from E

12+0 - 2" tile 91.10 from E

 B.M. on heart of 36" stump  
 75' S. of Sta. 10-10  
 EL. 95.75

TILE AT. BEGIN OF ARM #2

APPROX

6"	TILE FROM E,	TOP. 91.77
10"	" " N.E.	TOP. 92.75
" "	" S.	TOP.

E Sta

Run 7121

Check	Stk	Date	Stk	
		45+50	87.60	
57+90	86.89	9237	45+0	87.67
57+0	86.92	91.85	044+50	87.89
56+50	86.83		44+0	88.00
56+0	86.50		43+50	87.65
55+50	86.68		43+0	87.70
55+0	86.81		42+50	88.04
54+50	86.80		42+0	88.12
54+0	87.03	91.93	41+50	88.27
53+50	87.16		41+0	88.32
53+0	87.15		40+50	88.55
52+50	87.05		40+0	88.77
52+0	87.20	91.25	039+50	88.75
51+50	87.08		39+0	88.94
51+0	87.20		38+50	89.06
50+50	87.17		38+0	89.50
50+0	87.32		37+50	89.52
49+50	87.41		37+0	89.56
49+0	87.46		36+50	89.69
48+50	87.40		36+0	89.91
48+0	87.33		35+50	89.91
47+50	87.39		35+0	90.07
47+0	87.45		34+50	90.33
46+50	87.44		34+0	90.47
46+0	87.69		33+50	90.69

92.50

87.890

93.42  
BM

92.37

93.640

131

33+0	90.82		20+50	93.80
32+50	91.02		20+0	93.81
32+0	91.22	94.88	19+50	93.90
31+50	91.36	94.550	19+0	94.17
31+0	91.60		18+50	94.20
30+50	91.57		18+0	94.31
30+0	91.48	95.19	17+50	94.95
29+50	91.51		17+0	95.28
29+0	91.50		16+50	95.18
28+50	91.53		16+0	95.12
28+0	91.91		15+50	95.27
27+50	92.21		15+0	95.35
27+0	92.13		14+50	95.31
26+50	92.20		14+0	95.64
26+0	92.27		13+50	95.92
25+50	92.73		13+0	96.11
25+0	92.55		12+50	96.31
24+50	92.67		12+0	
24+0	92.77		11+50	96.36
23+50	92.81		11+0	96.48
23+0	92.92		10+50	96.65
22+50	92.91		10+0	96.89
22+0	93.12		9+50	97.04
21+50	93.28		9+0	97.14
21+0	93.40		8+50	97.40

9273

8+0	-	97.68
7+50	-	97.79
7+0	-	97.84
6+50	-	97.88
6+0	-	98.12
5+50	-	98.04
5+0	-	98.17
4+50	-	98.35
4+0	-	98.60
3+50	-	98.94
3+0	-	98.94
2+50	-	99.16
2+0	-	99.13
1+50	-	99.25
1+0	-	99.36
0+50	-	99.80
0+0	-	100.17

100.60

102.84

104.78

Check

0+0	91.30		12+50	89.10
0+50	91.10		13+0	88.90
1+0	91.08	96.00	13+50	88.76
1+50	90.95		14+0	88.69
2+0	90.60		14+50	88.63
2+50	90.45		15+0	88.85
3+0	90.33		14+50	88.53
3+50	90.45		15+0	88.45
4+0	90.42		15+50	88.36
4+50	90.39		16+0	88.40
5+0	90.22		16+50	88.15
5+50	90.09		17+0	88.06
6+0	90.03		17+50	87.97
6+50	90.02		18+93	87.88
7+0	89.90	93.50	19+50	87.70
7+50	89.79		20+0	87.70
8+0	89.90		20+50	87.52
8+50	89.88		21+0	87.35
9+0	89.80		21+50	87.30
9+50	89.85		22+0	87.18
10+0	89.80		22+50	87.32
10+50	89.61		23+0	87.30
11+0	89.53		23+50	87.20
11+50	89.39		24+0	87.08
12+0	89.29		24+50	87.10

Ann # 2  
check

93.50

⊙ 92.16

25+0	86.89
25+50	86.88
26+0	86.88
26+50	86.72
27+0	86.61
27+50	86.49
28+0	86.45
28+50	86.34
29+0	86.09
29+50	86.08
30+0	86.05
30+50	86.00
31+0	85.60
31+50	85.64
32+0	85.65
32+50	85.62
33+0	85.58
33+50	85.20
33+88	

91.72

138

ARM #2

0+0

↑ average  
of 24"

↓

9+0 24"

9+75 18"

10+50 30"

12+0 30"

15+0 30"

20+0 36"

23+0 32"

139

Arm #1

from lower end to Mullin  
line not complete 48+43

to 48+43 to 43+93

average 33"

39+0 - 35"

152

## Mausoleum

SW. 7.00 8.37

SE 2.64

NE 3.62

NW 5.27

5.80 4.25

7

2

3

5

10

17

25

BLDG. —

Foundation Muds. — 5.90

NW. 5.90 6.76

SW 5.90 8.48

S.E. 5.90 4.01

N.E. 5.90 5.20

Tot.

Cut

2.58-

7.11

1.89

.70

153

6.76  
5.90  
— .868.48  
5.90  
— 2.585.90  
4.01  
— 1.892.19  
10

1-9

E 154

80.28

88.69

92.50

90.90 <sup>SW on</sup> in Sligoat Crossroads just

7.0 P. H. H. H. H.

89.01

85.65

77.62

80.10

157