

← M → ← LETTER →

SPANGLER
DRAIN

157

MINING
TRANSIT BOOK
363 A

2

STR KitchBot

83	97.60	10004	
84	98.00	99.64	
85	97.30	98.94	9553
86	97.80	99.26	9550
87	97.85		9540
88	97.75	99.14	
89	98.10	99.30	
90	98.80	99.13	96.02
91	98.05	99.55	
92	97.55	99.30	9545
95	97.65	99.60	9521
96	97.85	99.43	
97	98.15	99.03	
97			
99		99399587	
98			
99			
100	9805	9930	9564
101	9900	10047	
102	10080	10224	
103	9990	10133	
104	9880	10019	9589
105	9865	10015	9524
106	9840	10033	
107	9830	9969	

← LETTER →

Lorn Ross

3

10004	9800
9760	9964
<u>2.44</u>	<u>9800</u>
	164

①100.09

①100.86 9884

9730

164

9924

9720

10325

10265

144

60

9930 9545

10015

9524

491

Sto-11	str	dist
108	9825 9998	9510
109	9830 99.21	
110	9855 99.96	9410
111	9870 100.15	
112	9840 99.80	9548
113	9900 100.88	
114	9910 100.36	
115	9860 100.03	9516
114	9830 99.67	9410
117	9845 99.84	
118	9855 99.94	
119	9760 98.98	9419
120	9785 99.00	
121	9820 99.93	
122	9900 100.40	
123	9850 99.80	
124	9840 99.63	9503
125	9790 99.14	
126	9775 98.97	9423
127	9740 98.67	9430
128	9785 99.05	
129	9805 99.29	
130	9850 99.81	
131	9725 99.13	9402
132	9815 99.40	
133	9735 98.68	
134		

010046
 010066
 09893

103.15
 B.M. check

B.M. 96.15 Ed of SEC Wing.

135-⁸ stk Dutch Int.
97909924

- 136
- 137
- 138
- 139
- 140

stk Dutch Int.

225	9390	9390	8845
227			
228			
229	9490	9463	8831
230	9440	9400	8770
231			8710
232	9465	9463	8760
233	9410	9415	8803
234	9345	9345	8794
235	9295	9298	
236	9285	9290	8791

8871
8780
91

8770

2936

10403

10224

	W		Q
9840	7388	7397	7400
98450	7410	7397	7380
9940 ✓	7394	7414	7395
99450 ✓	7411	7406	7386
10040 ✓	7407	7409	7404
100450 ✓	7421	7404	7398
10140 ✓	7376	7386	7358
101450 ✓	7360	7376	7370
10240 ✓	7379	7375	7386
102450 ✓	7375	7385	7378
10340 ✓	7400	7390	7397
103450 ✓	7455	7464	7476
10440 ✓	7518	7530	7532
104450 ✓	7611	7613	7622
10540 ✓	7690	7717	7706
105450 ✓	7805	7811	7824
10640 ✓	7889	7905	7900
106450 ✓	7995	8008	7990
10740 ✓	8086	8104	8074
107450 ✓	8172	8186	8184
10840 ✓	8287	8290	8297
108450 ✓	8428	8395	8401
10940 ✓	8544	8522	8570
109450 ✓	8651	8657	8640
11040			
110450			

086.50
07625

Brown Rd

59+0	4170	4221	4178
58+50	4211	4233	4214
58	L 4242	4266	4270
57+50	L 4288	4280	4322
57	L 4292	4326	4367
56+50	V 4386	4418	4394
56	L 4478	4482	4484
56+50	L 4578	4564	4528
56	V 4645	4667	4645
54+50	L 4711	4755	4745
54	L 4830	4870	4856
53+50	L 4956	4980	4967
53	L 5049	5092	5093
52+50	L 5195	5254	5218
52	L 5274	5385	5347
54+50	L 5494	5528	5533
54	L 5643	5678	5667
50+50	V 5801	5831	5800
50	5952	5977	5939
49+50	6082	6104	6071
49	6178	6210	6193
48+50	6344	6354	6335
48	6454	6493	6480
47+50	6690	6711	6715
47	6756	6823	6805
46+50	6857	6888	6896

4829

056.60

065.48

	W		Q
460	2-6874	6994	6954
45+50	-6869	6934	6914
450	-6880	6914	6868
44+50	-6849	6867	6848
44	-6851	6862	6790
43+50	-6778	6809	6750
43	-6745	6750	6741
42+50	-6539	6675	6626
42	-6565	6574	6526
41+50	6566	6570	6594
41	6627	6624	6643
40+50	6535	6562	6557
40+0	6622	6661	6662
39+50	6770	6836	6838
39+0	6958	6991	7028
38+50	7213	7187	7226
38	7356	7346	7341
37+50	7542	7558	7556
37+0	7720	7745	7763
36+50	7945	7965	7952
36	8095	8124	8176
35+50	8258	8323	8289
35	8415	8444	8415
34+50	8488	8519	8522
34+0	8515	8571	8477
33+50	8581	8600	8541

Brown Rd

6768 OK

076497

08514

W

E

3240

8611 8643 8601

32450

8637 8691 8643

3240

8722 8757 8676

31450

8782 8820 8725

11040

109450

10940

108450

10840

107

L 18

Richardson Road

Sta	Subgrade	Edge Cutler	Ed.	Top wall	Stake	
116+30	94.75	93.30	94.32	94.30	94.80	
+50	94.25	93.00	93.99	94.00	94.50	✓
+70	93.25	92.75	93.64	93.70	94.20	✓
+90	92.25	92.50	93.41	93.40	93.90	✓✓
117+10	91.25	91.50	93.17	93.10	93.60	✓✓
+30	90.25	90.50	93.35	92.80	93.30	✓✓
+50	89.25	89.50	93.15	92.50	93.00	✓✓
+70	88.25	87.50	92.30	92.70	92.70	✓✓
+90	87.25	87.50	90.28	90.50	90.50	
118+10	86.25	86.50	87.97	88.80	88.80	✓
118+30	85.25	85.50	85.30	87.00	87.10	✓✓

L 19

El 119+00 = 81.75
Subgrade

B.M. El - 81.68

on N edge end
E Hd wall of Culvert
Sta 119+26

92.00
 75.10
 87.10
 85.00
 87.10
 85.00
 92.00
 75.10
 87.10
 85.00
 87.10
 85.00

$\frac{1}{6}$ V 750
 $\frac{3}{8}$ V 770
 V 790
 $\sqrt{140}$ V 140
 $\sqrt{130}$ V 130
 $\sqrt{150}$ V 150
 $\sqrt{170}$ V 170
 $\sqrt{190}$ V 190
 $\sqrt{180}$ V 180
 $\sqrt{130}$ V 130

93109340 9310 92809150

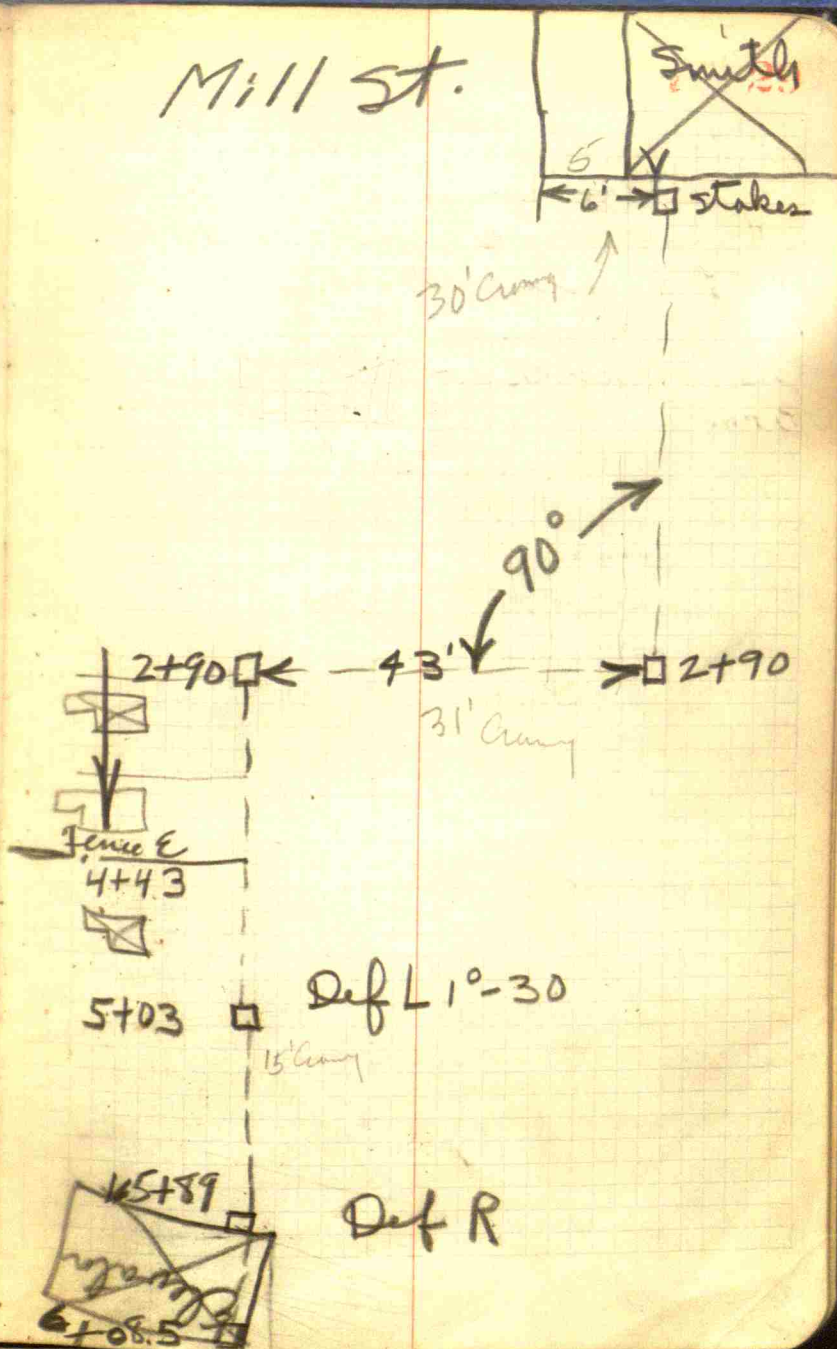
10/28

Stakes on W side are
1'-0" W of W edge walk and
stakes on E side are 1'-0"
E of E edge walk.

Sta	W side W of W edge	E side E of E edge	Cor. Pt
0+00	100.80	99.83	99.75
0+30	100.49	100.42	99.95
1+00	101.25	100.53	100.63
1+50	101.47	100.91	101.08
2+00	101.70	101.15	101.35
2+50	101.55	101.00	101.63
2+90 ^W	101.68	101.02	102.04
2+90 ^E	103.41	102.95	102.04
3+50	103.30	102.91	102.61
4+00	103.43	103.17	102.87
4+50	103.12	102.63	102.88
5+00	103.31	102.77	102.95
5+03	103.21	102.68	102.90
5+50	103.72	103.04	102.83
5+59	103.66	103.20	103.20

103.205 rail Smith
& center crossing

Mill St.



Wain

Wallo + Fence of Bridge 0+50
 Bridge C Side 0+56
 Bridge N side 0+74
 Cross E + Fence on N side 0+75
 Fence N+S Sta 4+43
 Cross N + Fence E+W Sta 22+55
 Cross S + Fence E+W Sta 22+91
 Fence E+W Sta 36+57
 Fence E+W Sta 39+22
~~Fence~~
 Arm running with 69+22
 Fence N+S 79+28
 Header at end of Ditch
 79+60

Arm. No 1.

End of Arm + Fence N+S
 19+55

69+62

64+22

5+40

79+30

69+62

9+68

E Russell Rd.

W 0
41.52BM 10.00
on SW. abut.

33

0 17.75

~~23.20~~

31.17

52.49

52.30

Sta.			£					
39+40 X		¹⁰ 10.22	10.32	¹⁰ 10.16				
37+00 X	²⁵ 14.25	¹⁰ 13.48	12.76	¹⁰ 11.34		¹⁶ 12.15		
38+60 X	²⁴ 2.75 ²⁰ 19.15	¹⁰ 17.81	17.53	¹⁰ 17.85		¹⁶ 18.33		
38+55 X	²³ 6.90 ¹⁷ 23.30	¹⁰ 20.24	19.12	² 19.15		⁴ 22.12	⁷ 22.43	⁸ 23.17
38+42 X	²¹ 5.70 ²⁷ 27.55	¹⁰ 24.40	23.71	¹⁵ 25.87				¹⁹ 24.86
38+0 X	²⁷ 32.10 ²⁵ 27.55	¹⁰ 25.51	24.90	¹⁴ 25.25		²⁰ 30.30		
37+50 X	²⁵ 31.15 ²⁷ 28.46	¹³ 26.00	26.70	¹² 26.80		¹⁶ 25.00	²¹ 32.00	
37+0 X	²⁴ 32.80	¹¹ 29.00	29.10	¹¹ 30.40		²⁰ 34.25		
36+50 X	²⁴ 38.93	¹¹ 34.45	33.84	¹³ 35.33		²³ 40.17		
36+0 X	¹⁶ 41.80	¹⁰ 40.38	39.00	³ 40.35		¹⁸ 42.00		
35+50 X	²³ 46.64	¹³ 43.67	42.31	¹⁴ 44.61		²² 48.14		
35+0 X	²⁴ 50.21	¹¹ 46.42	46.68	¹⁵ 47.96		²¹ 51.38		
34+50 X	²³ 56.20	¹⁹ 52.19	51.78	¹⁴ 53.21		²³ 56.81		
34+0 X	²² 60.05	¹⁸ 57.25	56.11	¹⁷ 57.50		²³ 61.04		
33+40 X	²⁰ 63.00	¹⁶ 59.25	58.41	¹³ 60.00		²⁴ 63.00		
33+0 X	²² 61.75	¹⁷ 59.02	57.85	¹⁷ 57.15		²⁰ 61.00	²¹ 62.00	
32+50 X	²³ 59.50	¹⁸ 56.71	55.82	¹⁶ 55.38		¹⁸ 56.68	²¹ 57.45	
32+0 X	²³ 59.00	¹⁷ 54.68	55.00	¹¹ 54.10		²⁰ 54.40		
31+50 X	²⁰ 52.85	¹⁰ 50.50	52.25	¹⁴ 52.18		¹⁴ 50.30	¹⁸ 52.00	²¹ 50.30
31+0 X	²³ 57.00	¹⁶ 47.60	49.70	⁹ 49.50		¹³ 48.05	¹⁸ 50.10	²² 48.20
30+50 X	³¹ 52.90	²⁰ 45.50	47.70	¹⁴ 47.87		²¹ 44.50		
30+0 X	³¹ 46.80	²⁵ 44.00	47.18	¹⁵ 47.05		¹⁹ 44.20		

29 35

E

E

W

55.73

35

29+50	²⁸ 42.00	¹⁶ 45.80	¹⁵ 46.58	¹⁹ 45.60	¹⁹ 42.50
29+0	²⁴ 41.80	¹⁴ 46.00	¹⁴ 47.38	¹⁴ 45.45	¹⁸ 44.00
28+50	²⁵ 54.60	¹⁷ 47.60	¹⁷ 47.89	¹⁵ 47.01	²¹ 44.50
28+0	¹⁸ 42.00	¹³ 48.70	¹³ 48.59	¹⁶ 47.70	²¹ 45.75
27+50	³² 55.20	¹⁹ 49.74	¹⁰ 51.00	¹⁶ 50.80	¹⁶ 50.98
27+0	²⁸ 46.38	²³ 48.05	¹³ 52.20	¹⁷ 53.16	¹⁷ 53.38
26+70	²⁶ 53.00	¹⁹ 54.00	¹⁴ 55.10	¹⁴ 55.25	²⁴ 48.15
26+45	³² 64.30	²⁸ 63.20	¹⁶ 55.03	² 56.10	
26+0	²⁹ 64.10	¹⁸ 56.85	¹⁵ 58.20	⁴ 58.40	

36

CUT SHEET
RUSSELL Rd.

Sta.	New Gd.	El. Gd. stk	CUT	FILL.
39+0	12.00	1560	3'-7½"	
38+50	15.91	2687	10'-11½"	
38+0	19.82	3050	10'-8½"	
37+50	23.73	3358	9'-10"	
37+0	27.64	3589	8'-3"	
36+50	31.55	3935	7'-10"	
36+0	35.46	4422	8'-9"	
35+50	39.37	4928	10'-6"	
35+0	43.28	5083	7'-7"	
34+50	47.19	5667	9'-6"	
34+0	51.10	6015	9'-0½"	
33+50	54.21	6118	6'-11½"	
33+0	55.73	6981	4'-1"	
32+50	55.83	5757	1'-9"	
32+0	54+0	5473	0'-4"	
31+50	53.15	5212		1'-0½"
31+0	51.90	5007		1'-10"
30+50	50.65	4827		2'-5"
30+0	49.40	4748		1'-11½"
29+50	48.52	4615		2'-4½"
29+0	48.40	4654		1'-10½"
28+50	49.02	4783		1'-2½"
28+0	50.40	4903		1'-4½"
27+50	52.15	5142		0'-9"
27+0	53.90	5443	0'-6½"	

37
01948

02903

03809

04880

06015

05213

Russell Rd

April 13-1928

	BM	East	10.00	W. edge	dent	
	Q	Ground	on S.	East	W	
39+0	12.75	10.9 ²²	1204 ²⁴	1523 ²⁷	12.2 ¹⁸	1535 ²⁰
38+50	17.82	19.06 ¹⁸	1963 ¹⁸	2660 ²¹	1853 ¹⁹	2353 ¹⁶
38+0	21.83	2320 ²⁰	2396 ²⁰	2976 ²⁵	2396 ¹⁶	2700 ¹⁶
37+50	26.77	2922 ²¹	3576 ²²	3478 ²³	2872 ¹³	3104 ¹⁷
37+0	29.00	3475 ²²	3826 ²²	3751 ²⁶	3443 ²⁶	3840 ²²
36+50	30.60	3923 ²³	4380 ²³	4308 ²³	3840 ¹⁷	4235 ²²
36+0	44.37	4490¹⁸	4875²⁵	4820²⁵	4427¹⁷	4708²²
36+0	72.03	4490 ¹⁸	4875 ²⁵	4820 ²⁵	4427 ¹⁷	4708 ²²
35+50	45.33	4815 ¹⁹	5195 ²⁵	5152 ²⁵	4871 ¹⁷	5238 ²⁴
35+0	49.22	5162 ¹⁸	5566 ²⁶	5505 ²⁵	5112 ¹⁴	5361 ²²
34+50	54.74	5602 ¹⁹	5970 ²⁶	5882 ²⁵	5553 ¹⁵	5760 ¹⁸
34+0	57.54	5901 ¹⁵	6352 ²²	6271 ²²	5970 ¹⁵	6322 ²²
33+50	59.72	6101 ¹⁵	6395 ²⁰	6330 ²⁰	6174 ¹⁵	6444 ²¹
33+0	59.67	6199 ¹⁵	6232 ²⁰	6150 ²¹	6022 ¹⁴	6265 ¹⁸
32+50	58.80	5865 ¹⁰	6178 ²²	6092 ²²	5923 ¹¹	6025 ²⁰
32+0	57.59	5720 ¹⁰	6125 ²¹	6045 ²¹	5822 ¹³	5746 ²¹
31+50	55.71	5640 ⁷	6085 ²⁰	5771 ²³	5532 ¹⁸	5480 ²²
31+0	54.13	5441 ¹⁹	5917 ²⁶	5835 ²⁰	5380 ²¹	5480 ²²
30+50	51.90	5090 ²⁰	5267 ²⁵	5344 ²⁶	5110 ¹⁸	4975 ²⁴
30+0	50.42	4980 ¹⁹	4691 ¹⁷	5050 ²⁴	5033 ¹⁷	4712 ²²
29+50	49.93	4847 ¹⁰	4537 ¹¹	5109 ³¹	5000 ¹⁷	4633 ²⁰
29+0	50.32	4911 ⁷	5057 ²⁴	4980 ²¹	5000 ¹⁹	4540 ²⁰
28+50	51.34	5210 ¹⁷		5510 ²³	5060 ¹⁷	4530 ²⁴
28+0	52.20	5178 ¹⁴		4680 ¹⁹	5206 ¹⁴	4521 ²⁰

4766²⁷
ad. at 200

- (032.35)
- (045.21)
- (5627)
- (5365)

1717
29.38

26
5086

E

E

E

E

W

W

27+50	5458	5277 ¹⁷	5658 ²⁷	5568 ²⁷	5458 ¹⁷
27+0	5703	6677 ⁶	5254 ¹⁴	5736 ¹⁴	5719 ¹⁵
26+50	5840			6125 ^{5E}	5943 ^{7W}
26+0	6250	6094 ^{50W}	6193 ^{7W}	6375 ^{2E}	6227 ^{7W}

5120 ¹⁷	
5318 ²⁹	
5744 ^{32W}	5980 ^{34W}
6173 ^{36W}	6036 ^{32W}
	6430 ^{36W}

5468

24

	B	E	E	Const	W	W
36+50	3382	3725 ²³	4000 ²⁵	4076	3642	4017 ¹⁹
36+0	3908	4279 ²⁴	4575 ²⁴	4574	4266 ¹⁵	3999 ²¹
35+50	4229	4601 ²²	4845 ²⁵	4893	4620 ¹⁴	4932 ²⁰
35+0	4626	4895 ²⁰	5186 ²⁵	5265	4937 ¹⁴	5088 ²²
34+50	5168	5286 ¹⁹	5570 ²³	6665 ²⁵	5285 ¹⁴	5458 ²¹
34+0	5455	5645 ¹⁷	5962 ²⁴	6084 ²⁴	5626 ¹⁴	6001 ²²
33+50	5696	5800	6045 ²⁰		5885 ¹⁴	5897 ²¹
33+0	5634	5700 ¹⁶	5857 ²⁰	5935 ²⁰	5740 ¹⁴	5921 ¹⁷
32+50	5575	5595 ¹⁸	5789 ²²	5872 ²²	5526 ¹⁴	5719 ²⁰
32+0	5454	5452 ¹⁶	5741 ²⁸	5821 ²⁰	5320 ¹⁷	5436 ²²
31+50	5269	5331 ¹⁴	5461 ²⁰	5549 ²⁰	5148 ²⁵	4648 ²⁸
31+0	5076	5746 ¹⁷	5570 ²⁷	6615 ²³	4950 ²³	4658 ²⁵
30+50	4810	4790 ²⁰	4953 ²⁴	5098 ²⁴	4805 ²⁰	4405 ²⁴
30+0	4742	4850 ¹⁶	4890 ¹⁴	4825 ²⁵	4711 ¹⁸	4321 ²⁰
29+50	4689	4568	4244 ²⁴	4808 ³¹	4375 ²⁵	4156 ²³
29+0	468	4045 ¹⁶	4673 ²⁴	4757 ²¹	4620 ²²	4120 ²⁵
28+50	4823	4916 ¹⁷	5245 ²⁷		4732 ²²	4331 ²⁵
28+0	4915	4872 ¹¹	4572 ²²	4569 ²⁷	4900 ¹⁵	4658 ¹⁴
27+50	5124	5070 ²³	5261 ²⁷	5344 ²⁷	5701 ¹⁶	4611 ²⁰
27+0	5400	4827 ¹⁴			5411 ²⁶	5011 ²⁹
26+50	5586	5837 ²⁵	5638 ²⁹	5533 ³¹	5714 ³¹	
26+0	5931	6275 ²⁶		5854 ³³	5814 ⁴⁰	6007 ⁴⁵

3752

4935

5862

42

6004

5802

5134

S.M. Hendricks Drive.

edge Post	
0+00	12.89
0+10	13.37
0+20	13.70
0+30	14.56
0+40	15.70
0+50	17.15
0+60	18.28
0+70	19.42
0+80	20.44
0+90	21.58
1+0	22.70
1+10	23.85
1+20	25.15
1+30	26.70
1+40	28.47
1+50	29.85
1+60	31.32
1+70	32.82
1+80	34.10
1+90	35.71
2+0	37.01
2+10	38.41
2+20	39.72
2+30	40.73

B.M. on top of wood corner
Post 50' E of 0+20. EL. 10.00

○ 18.30
○ 27.87
○ 37.87

L 50

2+40		41.47
2+50		42.12
2+60		42.81
2+70		43.49
2+80		43.68
2+90		44.02
3+0		43.89
3+10		43.95
3+20		44.09
3+30		44.11
3+40	Conc. floor	44.02

L 51

B.M. on concrete wall
next to house - West side of
Garage door - EL. 45.91

ROSEBOOM DRAIN

BOTTOM WIDTH

0+0	-77+34	3'
77+34	-127+43	4'
127+43	-186+79	5'
186+79	-243+0	6'
243+0	267+30	8'
267+30	307+63	10'
307+63	360+53	12'
360+53	437+0	14'

STA.	TOP-W	CHECK TOP-W.	CHECK BOT-W	C.E. ELEV.
0+00	14 1/2	15		100.25
3+0	17 1/2	15		99.53
6+0	17	18 1/2		98.81
9+0	16 1/2	18		98.09
12+0	18 1/2	17 1/2		97.37
15+0	17 1/2	16		96.65
18+0	18 1/2	20		95.93
21+0	16	16		95.21
24+0	16	15		94.49
27+0	15	16		93.77
30+0	17	15		93.05
33+0	16	15 1/2		92.33
36+0	15	17 1/2		91.61
39+0	14	14		90.89
42+0	15?	14		90.17

Def. -

3+42 - R -	92+64 - L
5+29 - R -	95+0 - L
12+11 - R	96+22 - R
15+22 - L	99+0 - R
18+84 - R.	103+40 - L
25+48 - L -	106+48 - R
28+90 - L	108+68 - R
33+10 - L	116+34 - L
36+0 - R.	117+65 - L
42+77 - L	120+99 - R
44+20 - L	121+57 - R
46+14 - L	122+72 - L
47+53 - L	124+09 - R
50+12 - R	125+12 - L
52+32 - L	127+43 - R
53+67 - R	128+76 - R
59+35 - L	131+14 - R
66+29 - L	132+32 - L
69+45 - R	134+45 - R
77+34 - R	136+13 - R
82+22 - R	137+94 - L
83+34 - R	139+04 - R
86+01 - R	140+08 - L
88+20 - R.	141+56 - L
89+40 - R	142+80 - R

STA	TOP WIDTH	CHECK TOP WIDTH	CHECK BOT. WIDTH	ELEV.	CHECK ELEV.
45+0	15			89.53	
48+0	14			89.05	
51+0	14 1/2			88.57	
54+0	13 1/4			88.09	
57+0	14 1/4			87.61	
60+0	15'			87.73	
63+0	15			86.65	
66+0	15 1/2?			86.17	
69+0	15			85.69	
71+0	14 1/2			85.37	
3' 74+0	13			84.89	
> 77+34	18			84.35	
4' 80+0	19			84.11	
82+22	18			83.84	
83+34	21 1/2			83.78	
86+01	22?			83.51	
88+20	21			83.29	
89+40	23?			83.14	
92+64	23?			82.82	
95+0	24?			82.58	
96+22	22?			82.46	
99+0	14?			82.18	
101+0	18?			81.98	
103+40	18			81.74	
106+48	20			81.44	

- DEF. -
144+87 - R
147+25 - L
148+51 - R
152+26 - R
155+02 - L
158+18 - L
160+51 - R
163+03 - L
165+01 - R
166+51 - L
169+08 - L
170+86 - R
173+53 - L
178+40 - L
180+51 - L
182+55 - R
185+96 - R
186+79 - R
191+43 - R
194+18 - L
197+60 - R
199+11 - L
202+83 - R
204+15 - R
209+78 - R
210+83 - R

215+99 - L

224+63 - R

227+45 - L

Sta 120+41 Cool
in on both banks
Bad condition

119+25 cove in
on N. bank.
Washing on So. bank

115+34 - did not
leave lower end (W)
of cut-off open

113+0 - did not
leave lower end
of cut-off open (E)

109+75 Cool in
west bank -

573

Sta	Top width	Check Top width	check Bot width	ELEV.	check ELEV
108+68	25 1/2?	22		81.22	
110+0	21	18		81.09	
114+0	20 1/2	19		80.69	
116+34	20 1/2?	20		80.46	
✓ 117+65	22 1/2?	18 1/2		80.33	
✓ 120+99	23?	16		80.00	
✓ 121+57	20 1/2	16		79.97	
122+72	21	19		79.82	
124+09	20	15		79.69	
125+12	21	20		79.59	
127+43	22	20		79.36	
128+76	15			79.23	79.35
131+14	22	20		78.99	79.25
WALL TO CR. 132+32	21	21		78.84	79.00
134+45	21 1/2	23		78.63	79.20
136+13	24?	22		78.45	79.20
137+94	21 1/2	22		78.25	78.70
139+04	22	18		78.12	78.68
140+08	20	19		78.02	79.03
141+56	20 1/2	22		77.86	79.02
142+80	22	20		77.72	78.85
144+87	21?	21		77.49	79.00
147+25	23	25		77.23	78.50
148+57	21?	26		77.09	78.80
152+26	24	20		76.68	77.95

13613	13445	13904	12091
13445	3232	13794	12041
168	213	110	12041
1199			14280
127	13794	14008	14156
	13613	13904	14280
	161	409	134
		12272	14725
		3714487	
		238	

14156
14008
148
EI 91.03
Send E nail BR 131+65

5226
4851
375

90.86

Top SW wing. at end nail
EI 91.67

12099
11765
324

13232
13176
56

9050
135
1975

8035
133

12876
743
133

12272
137
115

14851
14725

126

⊙ 86.52

⊙ 86.46 ⊙ 86.56

Sta 143+80 Covel in on E. bank
about 6' into ditch - water 4' wide

Sta 149+50. to 151+00 Covel in
on both sides - Bad slope

Sta 152+26 Covel in on East
bank - Sta. 152+20 Covel in on
West bank

Sta 134+75 Covel in on West bank for 60'
Bad -

Sta	Top width	check Top	check Est.	E EL.	check EL
155+02	23	25		76.38	77.89
158+18	23 1/2	24		76.03	76.98
160+51	22	19		75.77	77.52
163+03	20	21 1/2		75.49	76.80
165+01	20	24		75.28	76.98
166+51	18	23		75.12	76.80
169+08	16	20		74.84	76.20
170+86	17	18		74.64	75.95
173+56	27 ?	22		74.43	75.60
174+50				74.33	75.30
177+0	22	21		74.05	74.85
178+40	24 ?	22		73.90	74.94
180+51	18 ?	24		73.67	74.75
182+55	18 ?	24		73.45	74.90
185+96	15 ?	21		73.08	74.35
186+79	18 ?	23		72.99	74.25
189+0	17 ?	25		72.75	73.52
191+43	24	25		72.47	73.30
194+18	21	28		72.17	73.10
197+60	22	28		71.79	72.80
199+11	25	25		71.62	72.75
202+83	20	29		71.22	72.50
204+15	20	32		71.02	72.40
207+0	22	24		70.76	72.05
209+78	15 ?	26 3/4		70.34	72.00

16908
16651
257

19760
19418
342

15818
5502
316

19418
19143
275

7475
50

160+51
15818
233
16803
16051
252

82.55

77.42

17450
17350
94

7430

18051
17640

170.86
169.28
178

84.05

17352
17082
270

77.75
78.15
81.90

Sta 175+50 bank on East side
covered in

00 61

20415
20283
132

18596
18255
341

283
89
372

19911
19760
151

19143

B.M. to quit on
June 3.
on Top stump
in center - on
West bank at
Sta 189+03
EL 85.91

B.M. on middle
on No. end of bridge
Sta 158+30.
EL. 86.68

Sta	Top Width	check Top	check Bot	E EL.	check EL.
210+83	23	25		70.23	72.00
213+07	17 ?	25		69.98	71.06
215+99	Bulge		70.55	69.64	70.55
219+0	21	23	70.50	69.31	70.50
222+0	21	22	70.15	68.98	70.15
224+63	18 1/2 ?	22	69.90	68.69	69.90
227+45	25			68.38	68.90
231+0					

BM El. 80.78 - Top SW
Wing at end - of rail

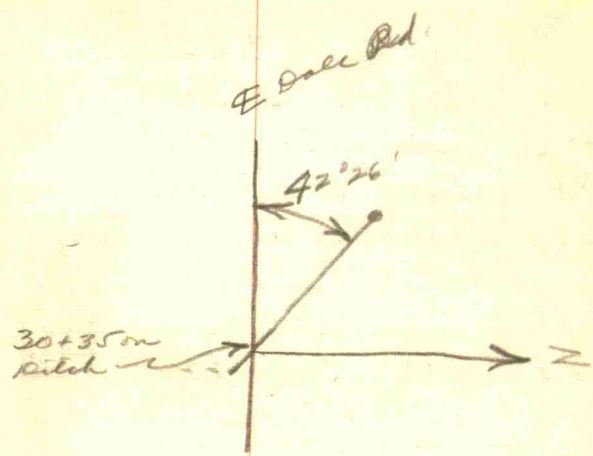
Cave-in at Sta 225+0 on West
bank.

① 70.80

63

Spangler Drain

- 0+0 Intention with French Well
- 2+86 Def L 3°31'
- 5+0 Cross Sec.
- 7+39 Def R. 45°00'
- 10+15 Def L 23°31'
- 13+15 Cross Sec.
- 14+60 Def R. 15°29'
- 16+60 Def L ~~16°52'~~ - 15°50'
- 19+0 Cross Sec.
- 22+0 " "
- 25+0 " "
- 27+85 Def L 48°28'
- 30+35 E E+W Road - Dale Rd
5th line intersects Dale
Rd at 72+62 on Dale Rd.
- 31+0 Cross Sec.
- 33+0 " "
- 33+80 Def R 45°53'
- 35+0 Cross Sec.
- 37+80 Def R 1°31'
- 40+0 Cross Sec.
- 42+0 " "
- 44+75 Spangler N. line Cross Sec.
- 46+0 Cross Sec.



37+75 - E+W Fence

- 48+43 Def L $49^{\circ}02'$
 49+79 Def R $25^{\circ}54'$
 52+25 Def R $18^{\circ}00'$
 54+0 Def R $9^{\circ}29'$
 56+0 Cross Sec.
 58+0 " "
 60+0 " "
 61+93 Def. R. $31^{\circ}22'$
 62+03 ∇ Old State Rd.
 63+32 is N. R. of W. line T.H. 1 & E
 63+35 Stk 15' W. of ~~24~~ N. end
 of 24" V. Tils under fraction.
 63+53 N. rail of T.H. 1 & E track
 63+80 So. End of 24" V. Tils under
 fraction.
 64+0 N. end of 22" Cast Iron
 Pipe under R.R.
 64+13 N. rail of R.R. track
 64+31 So. End 22" Pipe under R.R.
 64+52 N. End of 12" Or. Tils under
 State Rd.
 64+60 is N. end 24" R.C. under
 State Rd. - End of Improvement

52+90
 8" tile from
 Kibbey
 15' E to old ditch
 tile is 25' E of
 old ditch.

Top
Stn

Gal
at Stn

0+0 level
 2+86 "
 5+0 "
 7+39 "
 13+15 "
 14+60 "
 16+60 "
 19+0 "
 22+0 "
 25+0 "
 27+85 45' 20"
 29+0 level
 31+0 "
 33+0 "
 33+80 "
 35+0 61.66
 37+80 61.41
 40+0 60.43
 42+0 "
 44+75 "
 10+15 "

48.00 47.45 4735-15 42.02
 48.57 48.12 4758 44.70
 49.42 48.82 4882 45.50
 50.49 49.01-5 4751 46.35
 53.60 49.74 4751 49.51
 55.06 52.20-6 53.10 51.41
 55.06 53.10 51.41 49.51
 56.20 54.43 52.12 50.86
 56.20 55.35-5 51.85 51.69
 57.25 55.60 51.85 51.69
 57.25 56.82 57.16 54.20
 58.81 59.18 57.82 53.70
 60.32 58.62 58.62 54.95
 60.65 59.60 58.62 54.95
 60.65 60.00 60.22 54.95
 61.78
 62.52 61.87 61.25 57.90
 63.55 62.72 63.64 62.21
 64.69 63.93 62.93 63.96
 60.89 61.89 58.46 56.65
 62.46 62.00-3 59.50 57.50
 61.89 59.50 57.50
 61.56 61.02 59.24 57.67
 61.76 level 61.25 59.43
 61.32 60.43 60.08 58.25
 51.00 50.55 49.39 47.40

51.49
 51.69
 51.69
 51.69

42.00 41.40 46.80 47.68 level
 44.22 44.38 46.38 48.20 "
 45.32 45.55 48.82 level
 45.70 46.32 48.52
 49.48 49.50 50.56 53.14
 50.51 50.76 53.15 54.30 level
 53.10 53.80 56.76
 52.50 52.45 57.22 56.72
 53.40 57.92 58.53
 54.38 56.41 59.81 60.21
 56.22 55.85 56.28 57.62 61.52
 58.12 56.31 56.70 58.11 63.61
 58.92 56.79 56.72 58.36 64.56
 56.78 58.50 62.20 61.05
 57.60 59.25 61.40 60.85
 57.68 59.46 60.85 59.85
 58.05 57.89 59.71 61.58 60.80
 58.45 60.22 60.70
 46.62 47.32 47.82 48.60 50.85

B.M.
 Sta 30+
 on W.
 end of
 NW. Wing
 of Cons.
 Lined
 EL. 62.30

39
 62.70

Town Gd.

46+0	6223	6145	6039 ⁷	585 ¹¹
48+43	6353	6272	6312 ⁹	5932 ¹⁴
49+79	6467	6390	6335 ⁶	5955 ¹⁷
52+25	6500	6421	6430	6110 ¹⁷
54+0	6370	6280	6225 ¹⁰	6005 ¹³
56+0	6345	6283		
58+0	6344	6290	60'E to ditch	
60+0	6408	6355	80'E " "	
61+93	6618	6556	6399 ^E	
62+03			6594	
62+11		Good rd.	6072	
63+35	6475	6475	6380	
63+80	FL. So. end Culvert	T.H. 1.8 E	6070	FL. 2nd sewer
64+0	68.35		60.70	FL. N end of R.R. Culvert
64+31	FL. S. end R.R. Culvert		60.85	
64+60	A cut 68.83		61.40	
7. end Fl. R.C. Pipe	63.86			
64+52	6238	T.M. of 12" pipe		
		So. rail T.H. 1.8 E -	70.55	
		S. rail of R.R. track	72.06	
			61.38	
			62	
			69.38	

5885 ¹³	6035 ¹⁵	6180 ¹⁹	6190 ²⁵
5938 ¹⁷	6076 ¹⁹	6352 ²⁵	6310 ³¹
5952 ¹⁵	5952 ¹⁵	6312 ¹⁸	6415 ²³
5990 ¹³	6070 ¹⁶	6162 ¹⁷	6425 ²⁴
6040 ¹⁵	6150 ¹⁶	6276 ²¹	6256 ²⁶

level

B.M. 67.49
on W. end of
N. end of
State Rd. Culvert
64+60

L 178

Stone Cen. Sec. 29,
Twp 17. N R 1 E

Cor post S 45° W 22'
Cor post E — 16.5'

#4. cor. Stone

telephone pole N 30° W 58'

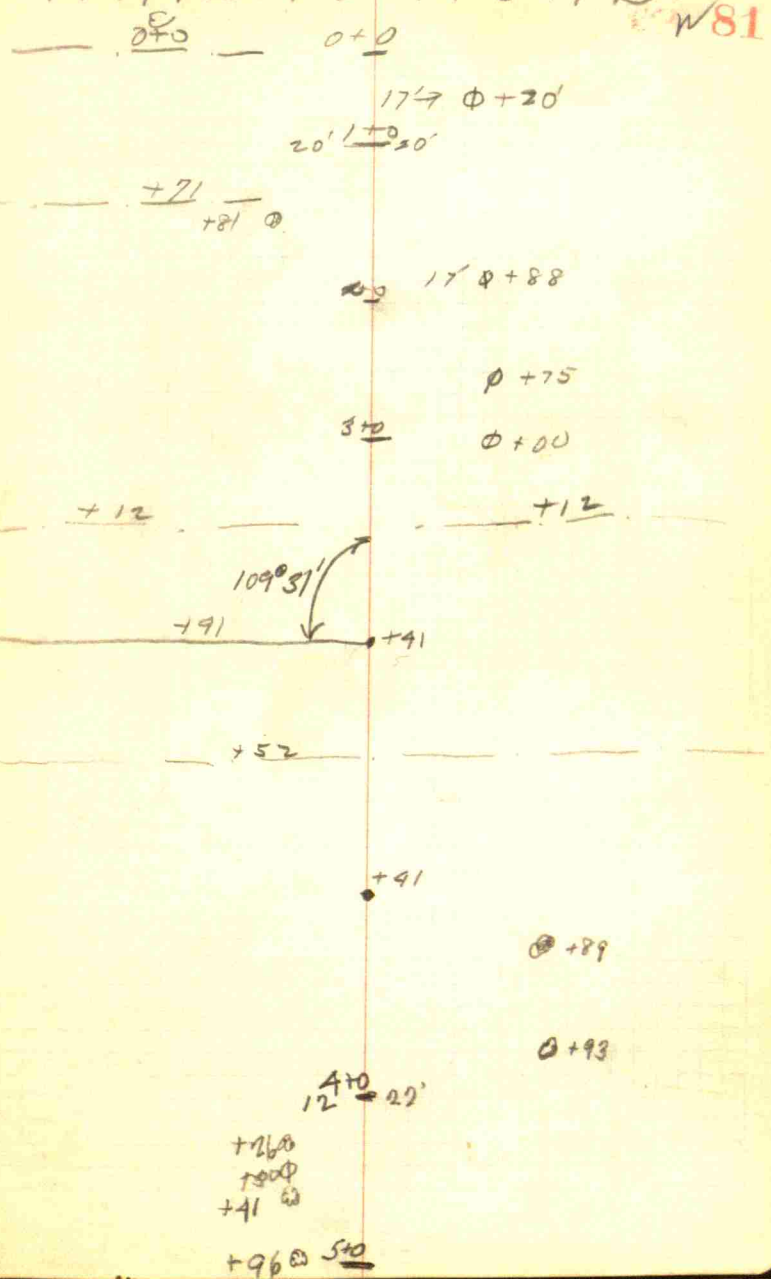
#5

cor Stone
Pine tree N 45° W 33.5'
SA Cor house N 60° W 76'

L 179

Beg. at Pittsboro; thence N & E
to the Cen. 29-17-1E

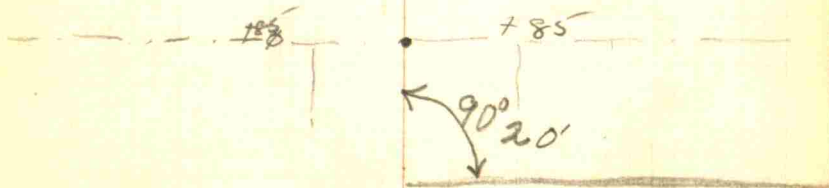
WATERS ROAD W81



+49 φ

5+0

+51



+85

6+0

+17 @ 13'

□ +52 100'

+71 @ 13'

+70

+02

7+0

13

108 @

+14 7'

+17

+29

+33

+40 @ 7'

+41 @

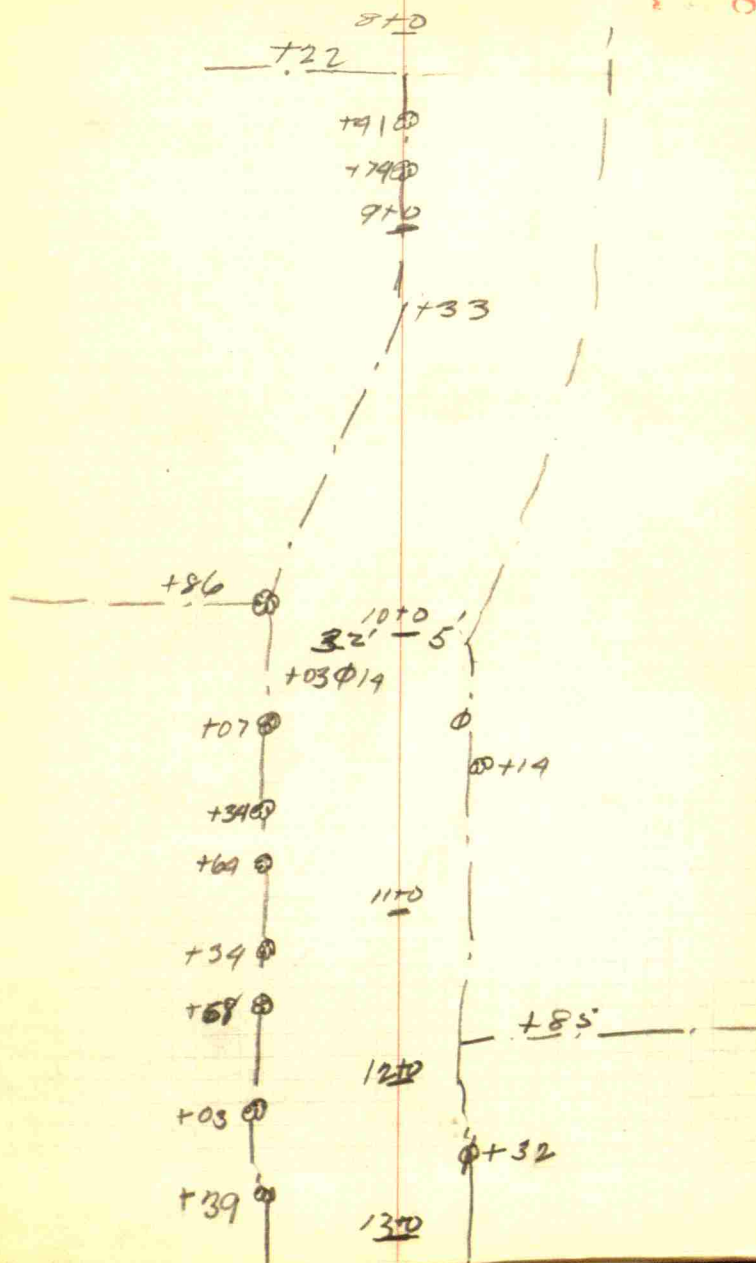
+49 @

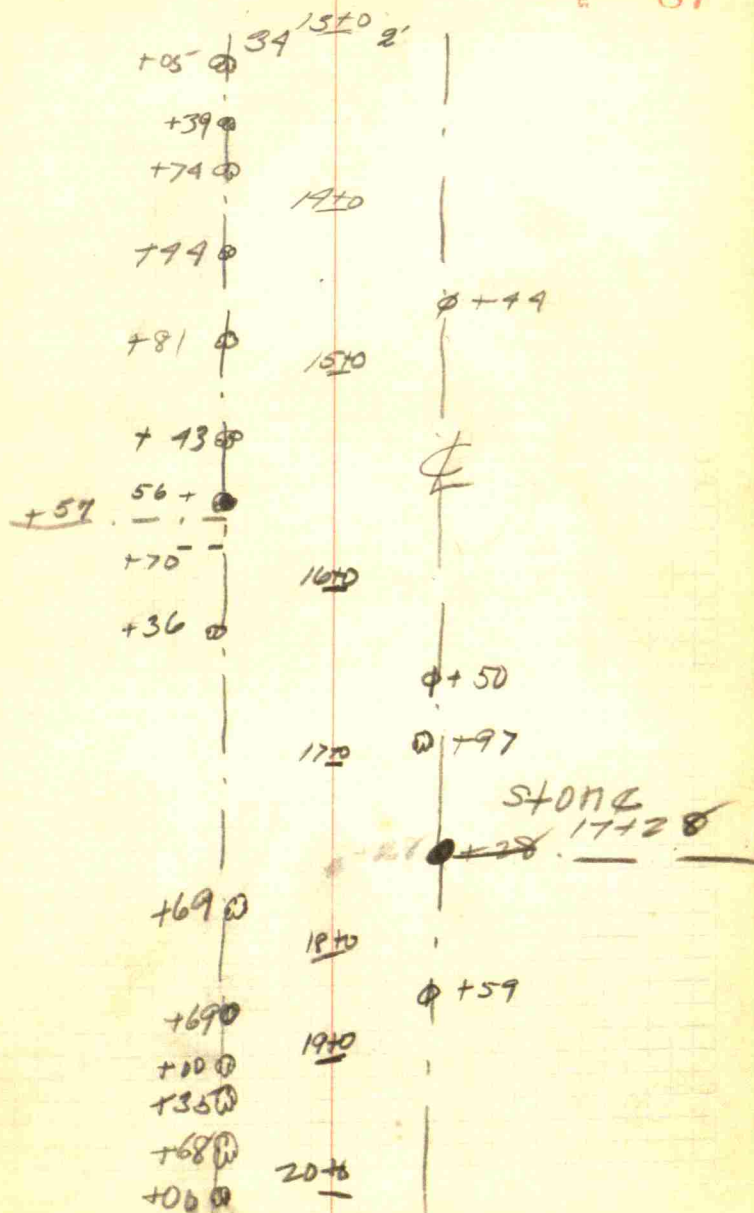
+71 φ

+80 @

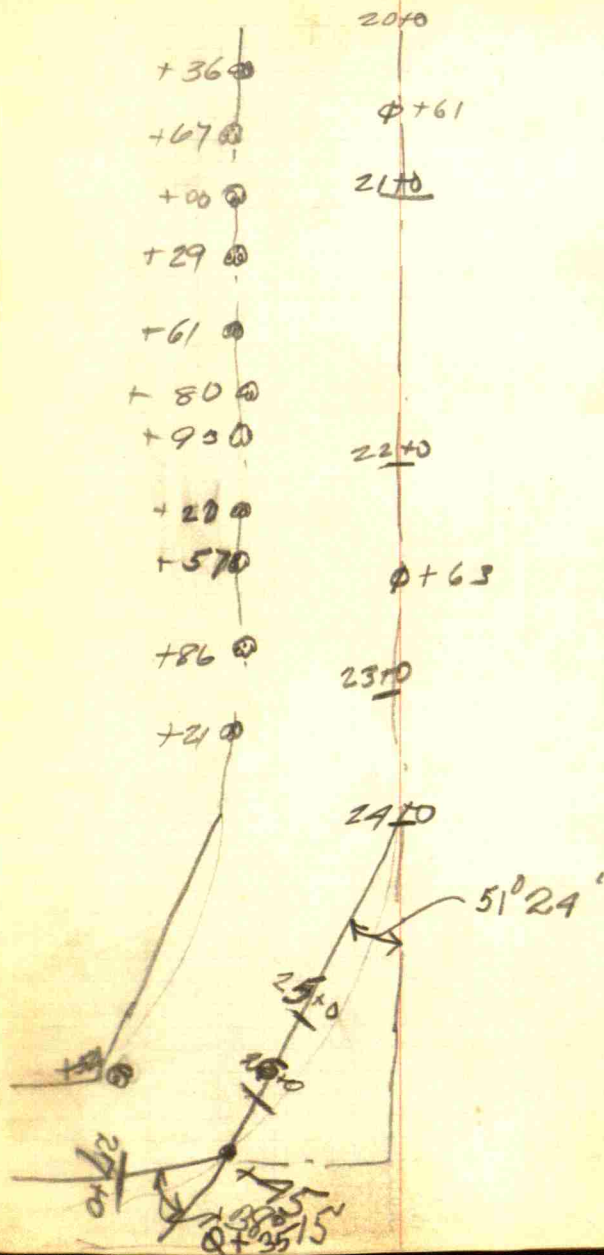
+84 @

8+0



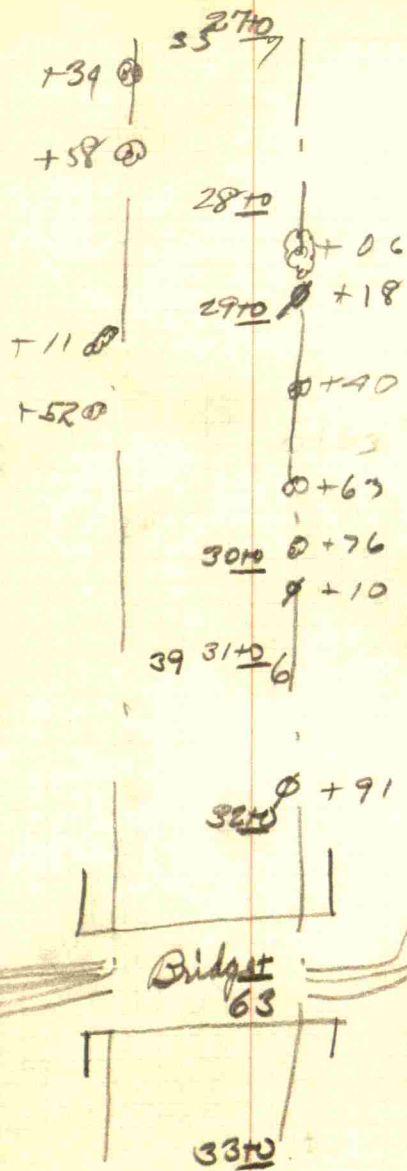


12836
5124
180.00



S

N 91



S
33^{to}

+35

+52

33^{to}

+61

+76

+89

34^{to}

+00

33^{to}

+61

35^{to}

+91

34^{to}36^{to}
39 - 21

+69

6 + 69

37^{to}

+52

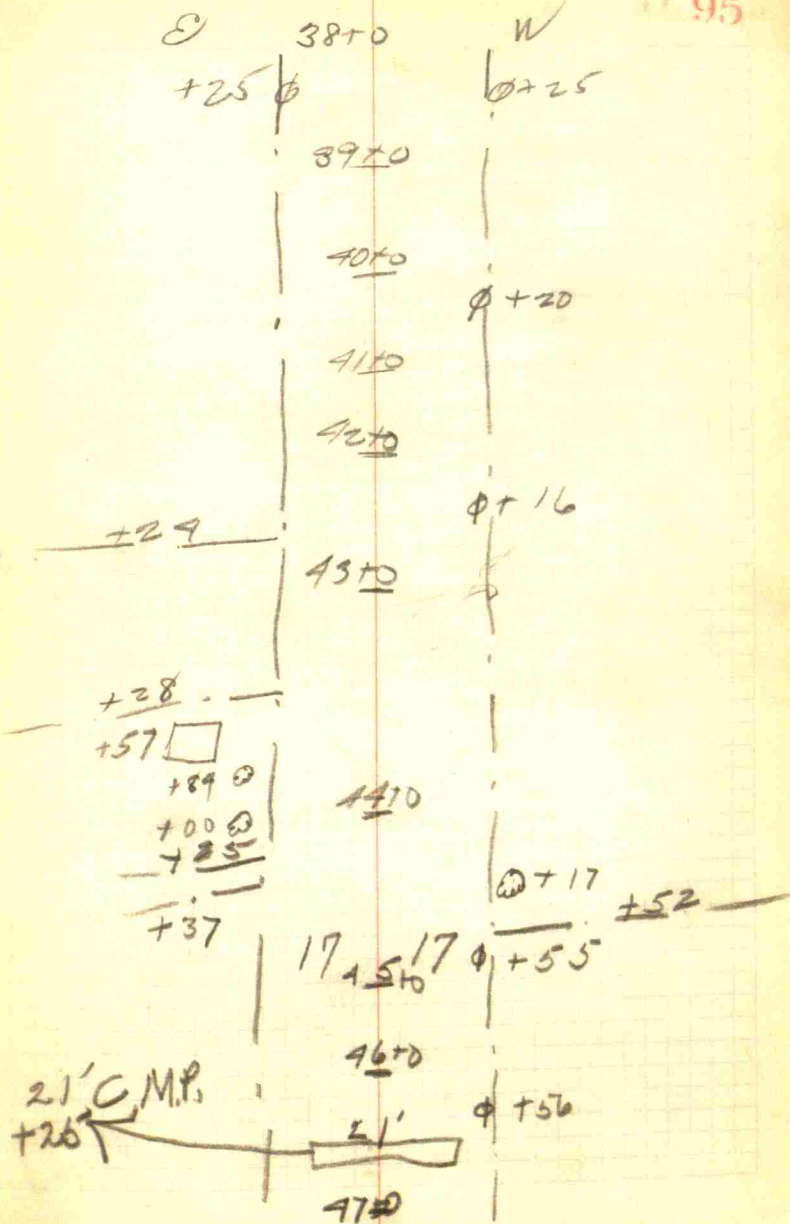
27

+59

21

38^{to}

+90



E | 17.5 ⁴²¹⁰ / 14' | W

| 17.5 ⁴⁸¹⁰ / 14' |


| 410 |

| 5010 |

| | $\phi + 32$

----- +59 ~~00~~ |

+74 \odot |

 +88 \odot |

+92 |

| 510 |

+75 \odot |

+28 \odot |

+44 | 35' |

+53 |

+60 |

+82 \odot |

+87 \odot | 16' |

| 520 |

| | $\phi + 38$

| 5310 |

E

5310

W

1099

+44

+53

+72

+88

+98

17 ⁵⁴¹⁰ 14

0148

+820

5570

5670

0117

5710

Stone

+59

+59

+59

68

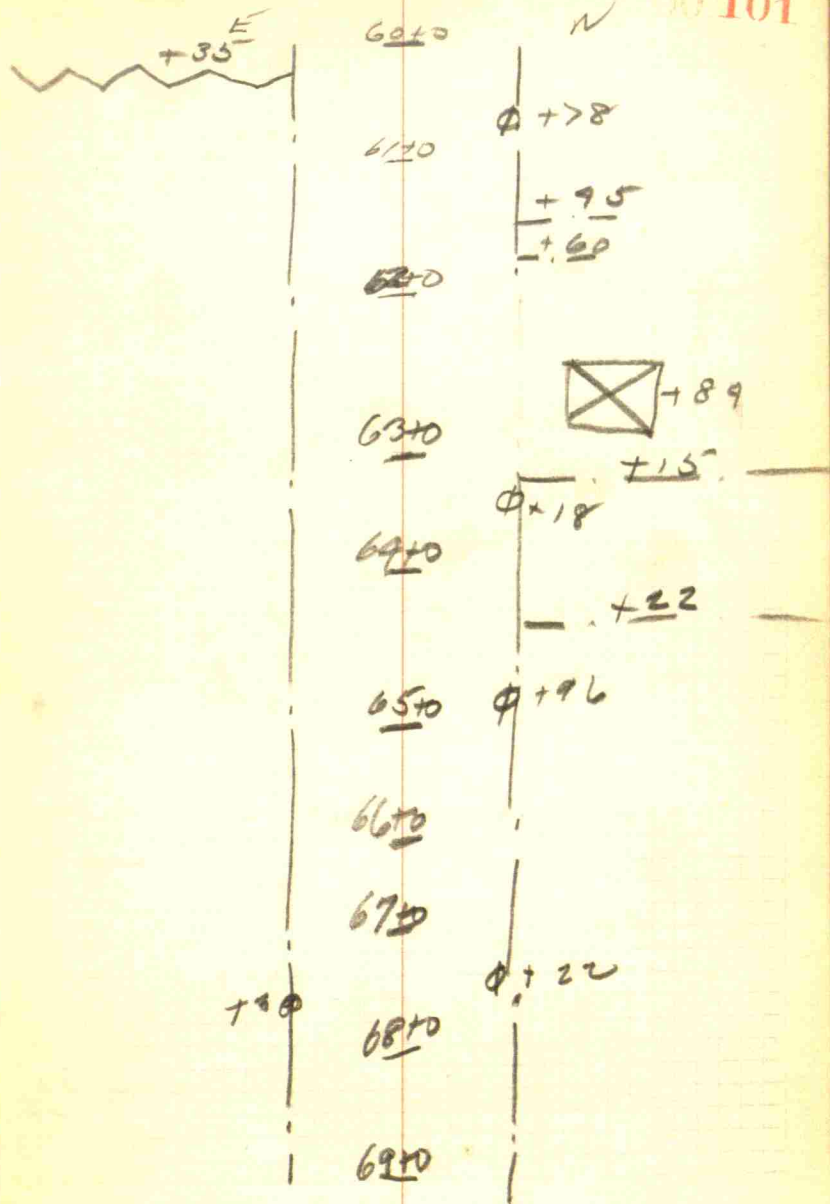
5810

0146

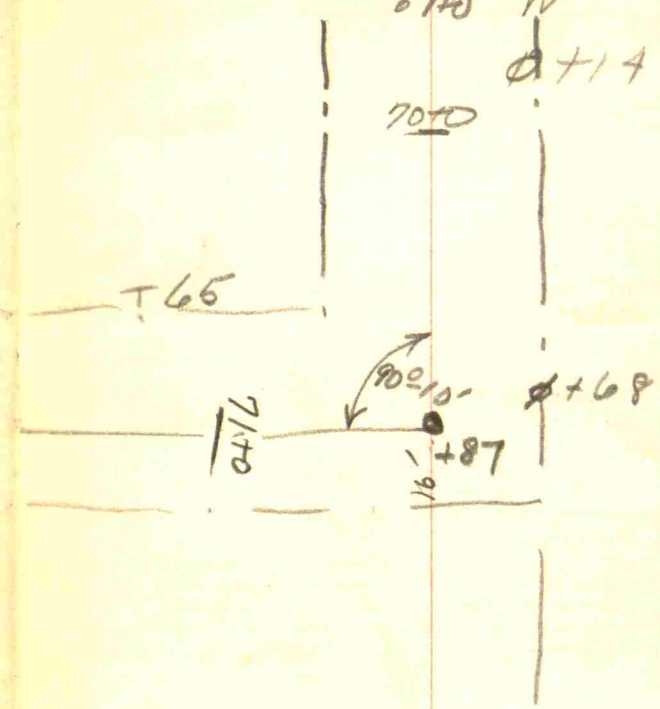
5910

+46

19 ⁶⁰¹⁰ 15



6940 W
 7070
 100
 87
 13



S

71+0

N

Ø +16

72+0

$$\begin{array}{r} +75 \\ +90 \\ \hline \end{array}$$

73+0

Ø +42

74+0

75+0

Ø +48

76+0

Ø +63

77+0

Ø +86

78+0

$$\begin{array}{r} +10 \\ \hline \end{array}$$
 Ø +53

+47

+51

+67

+80

79+0

Ø +75

80+0

5

80+0

81+0

φ+72

82+0

83+0

φ+79

stow

17 84+0/8

+0.0

19

+34

85+0

+16

86+0

φ+93

87+0

φ+15

88+0

89+0

φ+89

S

17 89+0

+66 @ 18

900

910

920

+53

+22

17 95+0

+00 @ 19 94 130 +00

+22

950

960

+75 @

970

980

+64

+77

+90

+57

+58

+53

+63

+72

+88

+06

+10

+20

+41

+59

		N
	9870	
	9910	
	10010	0-25
		+22
		+34
		+57
	10110	
18	15	0118
	102	
		0+95
	10310	0+99
	10410	+12
	10510	0+78
19	14	
	10610	0+32
	10710	0+52
	10810	0+52
		0+22
	10910	0+20
	11010	0+01
		+80
	11110	

91
+05
+35
+64

+70
+93

+14

+82

+22
+80

Continued on page
120.

112 Ditch for
Chas. O. Routh

0+0 is 60' 50" of N. Hdwell
and it is 6' more to end
of present tile

	Stn	Gd.	Tk. tile 10"
0+0 ✓	66.4 ³³	65.86	62.60
1+0 ✓	66.5 ⁶³	66.06	
2+0 ✓	65.7 ⁷⁴	65.20	
3+0 ✓	65.7 ¹²	64.55	
4+0 ✓	65.6 ⁸³	65.04	
5+0 ✓	65.5 ⁵¹	64.79	
6+0 ✓	65.6 ⁶⁰	65.18	
7+0 ✓	66.2 ¹⁵	65.64	
8+0 ✓	66.8 ⁸⁸	66.50	
9+0 ✓	66.6 ⁶⁸	66.09	
9+50 ✓	65.88	65.25	
10+0 ✓	65.86	65.30	
11+0 ✓	65.66	65.27	
12+0 ✓	65.46	65.00	

B.T. 1. on West end of
North Hdwell of Culvert
Sta. 64+60 - EL. 67.49

Fl. line of tile N. side
of state rd.
EL. 61.20
New Grade Tile 59.58

65.08

26.90

24.0

114

Arm # 1

0+0 = 6+0

0+0 same as 6+0

stk Gd

1+0 6585 6525

2+0 6608 6550

3+0 6670 6603

4+0 6685 6622

5+0 6660 6585

6+0

Pond. 65.00

115

116

Ann # 2

$$0+0 = 9+50$$

0+0
 1+0 ✓ 66.00 65.24
 2+0 ✓ 65.36 64.74
 3+0 ✓ 66.38 65.52
 4+0 ✓ 66.38 65.73
 5+0 ✓ 65.91 65.22
 6+0 ✓ 65.98 65.47
 7+0 63.50
 8+0

64.80 7h. present tide
at Sta about 5+50

Pond at 6+0 to 8+0

65.40 Top water
64.70 Bottom (shallow)

Charles O. Routh

Lebanon Ind.

117

6540

6470

$$\begin{array}{r} 6572 \\ 6260 \\ \hline \end{array}$$

65.40

59.52

1.60

$$\begin{array}{r} 59.52 \\ 1.60 \\ \hline 61.12 \end{array}$$

Sub Area to Area #2

$$0+0 = 2+0$$

1+0 6568 6501

2+0 6710 6661

3+0 6500

4+0 6690 6622

5+0 6682 6621

6+0 6630 6562

7+0 6645 6572

Pond at 3+0 - 65.00

S

+38

+62

+39

+99

N

+83

+61

+42

+17

+93

+72

+36

+90

+99

+18

15 11+0 19

112+0

113+0

119+0

113+0

116+0

112+0

118+0

17 119+0 16

120+0

121+0

122+0

123+0

122+0

23+0	8552	8465	8533	8535	8549
24+0	8162	8412	8509	8489	8361
25+0		8122	8273	8396	8439
26+0		8253	8262	8563	8397
27+0	8388	8251	8313	8420	8431
28+0	8519	8340	8359	8449	8473
29+0	8979	8479	8450	8472	8481
30+0	8471	8306	8361	8403	8420
31+0	8229	8400	8292	8325	8216
32+0	8127	8188	8179	8288	8500
33+0	8043	8100	8218	8277	8292
34+0	8177	8125	8178	8276	8316
35+0	8269	8177	8312	8359	8374
36+0	8188	8235	8363	8429	8429
37+0	8143	8159	8440	8503	8476
38+0	8492	8405	8458	8657	8659
39+0	8910	8818	8649	8780	8795
40+0	8846	8773	8744	8870	8886
41+0	9023	8962	8904	9036	9048
42+0	9275	9100	9073	9161	9175
43+0	9201	9140	9065	9150	9213
44+0	9092	9010	8970	9012	9062
45+0	8928	8990	8768	8825	8842
46+0	8636	8662	8622	8755	8752
47+0	8582	8605	8600	8795	8748

about 15' to 20' high

8425	8545	8494
8140	8114	
8457	8203	8129
8137	8080	
8328	8206	8250
8480	8387	8679
8465	8389	8365
8372	8265	
8269	8025	
8245	8089	8088
8140	8025	7972
8319	8320	8720
8385	8335	8400
8419	8263	8300
8236	8203	8417
8586	8372	8382
8745	8543	8609
8849	8687	8807
9027	8900	9018
9106	9094	9399
9003	9104	9313
9019	8946	9039
8848	8725	8830
8753	8570	8605
8745	8600	8665

Non
8770
8754

Bm on N.W. corner of bridge Sta 32+63
E.L. 8568

Sta	S'out	Stk	Ditch	Berm	℄
48+0	8670	8663	8631 ⁷	8762 ¹¹	8768
49+0	8820	8835	8690 ⁷	8893 ¹¹	8809
50+0	8997	8989	8875 ⁷	9021 ¹¹	9011
51+0	8908	9016	8880 ⁷	8776	8915
52+0	8763	8771	8771 ⁷	8800 ¹¹	8803
53+0	8685	8685	8622 ⁶	8738 ¹¹	8743
54+0	8678	8670	8545 ⁶	8653 ¹¹	8665
55+0	8532	8536	8456 ⁹	8618 ¹²	8630
56+0	8473	8474	8407 ⁷	8556 ¹²	8571
57+0	8382	8385	8386 ⁷	8476 ¹²	8478
58+0	8368	8362	8305 ⁷	8430 ¹³	8435
59+0	8220	8225	8259 ⁷	8469 ¹³	8490
60+0	8306	8315	8294 ⁴	8460 ¹³	8450
61+0	8927	8962	8362 ⁵	8468 ¹⁰	8480
62+0	8595	8599	8965 ⁶	8529 ¹⁰	8570
63+0	8982	9021	8652 ⁶	8863 ¹⁰	8887
64+0	8845	8875	8720 ⁶	8979 ¹⁰	8970
65+0	8883	8915	8800 ⁵	8962 ¹¹	8969
66+0	9174	9159	8954 ⁶	9092 ¹¹	9093
67+0	8988	9011	8860 ⁶	9014 ¹¹	9012
68+0	8850	8832	8845 ⁶	9016 ¹²	9005
69+0	8996	9001	8914 ⁷	9056 ¹³	9028
70+0	9171	9185	9015 ⁶	9154 ¹⁰	9151
71+0	9135		9275 ⁸	9335 ¹⁹	9357
72+0	9373	9371	9270 ⁷	9385 ¹⁹	9430

Berm	Ditch	Stk	S'out
8760 ²⁵	8626 ²⁰	8716	8705
8825 ²⁶	8711 ³⁰	8828	8823
8990 ²⁷	8820 ³⁰	8994	9013
8882 ²⁵	8746 ³⁰	8843	8857
8782 ²⁵	8647 ³⁰	8745	8756
8713 ²⁵	8596 ³⁰	8662	8667
8657 ²⁶	8530 ²⁹	8613	8621
8593 ²⁶	8470 ³⁰	8540	8531
8548 ²⁵	8437 ³⁰	8522	8520
8483 ²⁶	8390 ³⁰	8504	8505
8406 ²⁷	8362 ⁴⁰	8352	
8464 ²⁶	8336 ³²	8318	8289
8456 ²⁶	8262 ¹⁰	8301 ¹⁵	
8381 ³⁰	8415 ³⁰	8398 ²⁵	
8569 ²⁶	8511 ³⁰	8620	8622
8880 ²⁵	8695 ³⁰	8901	8972
8975 ²⁹	8782 ³¹	8870	8906
8970 ²⁵	8800 ³¹	8865	8902
9072 ²⁵	8950 ³⁰	9062	9087
9055 ²⁵	8876 ³⁰	8959	8980
9006 ²⁵	8856 ³¹	8856	8878
9038 ²⁷	8920 ³⁰	8944	8969
9140 ²⁸	9010 ³⁰	9096	9098
9310 ²⁸	9322 ³³	9390	
9410 ²⁹	9327 ³⁷	9439	9437

08699
08887

0 9307

B.M. on W. side of E. rail of bridge
Sta 59+46 — E.L. 89947

Sta	5' out	Stk	Ditch	Burn	To
73+0	9355	9354	9249	9338 ¹³	9392
74+0	9171	9203	9165 ⁷	9267	9305
75+0	9156	9194	9067	9185 ¹²	9228
76+0	9035	9070	8910 ⁷	9020 ¹²	9056
77+0	8809	8217	8790 ⁷	8900 ¹²	8930
78+0	8752	8758	8720 ⁶	8860 ¹³	8976
79+0	8646	8691	8620 ⁶	8771 ¹¹	8794
80+0	8646	8682	8610 ⁶	8703 ¹²	8735
81+0	8605	8637	8545 ⁶	8706 ¹³	8720
82+0	8552	8585	8545 ⁶	8682 ¹³	8710
83+0	8602	8620	8576 ⁶	8682 ¹²	8722
84+0	8693	8702	8652 ⁶	8779 ¹³	8794
85+0	8905	8959	8797 ⁵	8891 ¹¹	8991 ¹⁸
86+0	9091	9082	9027 ⁹	9017 ¹⁰	9056
87+0	8955	8936	8841 ⁹	9002 ¹¹	9045
88+0	8955	8941	8839 ⁹	8982 ¹¹	9035
89+0	9020	9018	8864 ⁹	9024 ¹²	9050
90+0	8965	8990	8875 ³	9039 ¹⁰	9063
91+0	9110	9020	8802 ³	8941 ¹⁰	8988
92+0	8665	8636	8500 ⁴	8643 ¹⁰	8660
93+0	8450	8430	8365 ³	8520 ¹⁰	8538
94+0	8438	8432		8582 ⁹	8629
95+0	8426	8457	8403 ³	8602 ⁹	8643
96+0	8737	8710	8516 ³	8661 ⁸	8675
97+0	8790	8750	8617 ⁴	8765 ⁴	8792

Burny	Ditch	Stk	5' out
9344 ²⁶	9197	9326	9373
9281 ²⁶	9137 ³³	9237	9262
9188 ²⁶	9056 ³³	9274	9302
9030 ²⁵	8899 ³³	9195	9137 ¹⁸
8890 ²⁵	8779 ³³	8878	8874
8857 ²⁵	8706 ³⁴	8760	8768
8745 ²⁵	8502 ³³	8690	8715
8712 ²⁶	8532 ³³	8663	8694
8699 ²⁶	8526 ³⁴	8590	8543
8687 ²⁶	8515 ³⁵	8579	8578
8710 ²⁰	8570 ³⁵	8615	8617
8662 ³⁵	8729 ⁴⁰	8715	
8894 ²³	8797 ³¹	8955 ³⁵	8924
9020 ²⁵	8885 ³¹	9015	8974
9020 ²⁵	8859 ³¹	8969	8940
8991 ²³	8817 ³²	8914	8905
8997 ²³	8833 ³⁰	8944 ³⁹	8924
8926 ²⁹	8828 ²⁹	8951 ³³	8956
8958 ²²	8783 ²⁹	9079 ⁴⁰	9072
8629 ²²	8499 ³⁰	8690 ³²	8610
8496 ²⁵	8440 ²⁹	8425 ³⁴	8420 ³⁶
8575 ²³	8287 ²⁹	8387 ³¹	8385
8616 ²²	8441 ²⁹	8532 ³³	8490
8642 ²³	8565 ²⁹	8695 ³³	8726
8781 ²¹	8639 ²⁹	8780 ³³	8780

127
\$ Bridge Sta 784

EL. 88.36

87.74

90.45

86.58

\$ Bridge Sta 944

96.59

for site
S.E. Cor of G Parkers
front strip
EL. 88.17

Sta	Sout	Stk	Ditch	Berm	\$
98+0	8696	8720	8691	8817 ¹⁰	8943
99+0	8732	8748	8693	8807	8980
100+0	8902	8900	8796 ³	8895 ⁴	8931
101+0	9083	9084	8872 ³	9007	9090
102+0	9180				9198
103+0	9201	9200	9031 ²	9170 ⁸	9229
104+0	9123	9102	9015 ⁵	9181 ⁹	9229
105+0	9115	9097	9031	9200 ¹⁰	9225
106+0	9186	9185	9047 ²	9210 ¹⁰	9260
107+0	9206	9198	9072 ²	9225 ⁹	9259
108+0	9284	9255	9152 ²	9306 ¹⁰	9321
109+0	9495	9470	9315 ²	9452 ¹⁰	9495
110+0	9972	9860	9653 ³	9741 ¹⁰	9760
111+0	9860	9882	9705 ³	9807 ¹⁰	9830
112+0	9571	9557	9430 ³	9587 ¹⁰	9617
113+0	9419	9432	9297 ³	9427 ¹⁰	9493
114+0	9380	9400	9220 ³	9368 ¹⁰	9390
115+0	9225	9252	9109 ³	9290 ¹⁰	9305
116+0	9197	9190	9048 ³	9216 ¹⁰	9242
117+0	9171	9160	9022 ⁹	9142 ⁹	9175
118+0	9055	9001	8865 ²	9003 ¹¹	9024
119+0	8945	8936	8720 ⁹	8862 ¹⁰	8882
120+0	8675	8690	8601 ⁹	8742 ¹¹	8757
121+0	8547	8689	8492 ⁹	8703 ¹³	8709
122+0	8532	8561	8421 ⁵	8641 ¹¹	8680

Berm	Ditch	Stk	Sout
8870 ²¹	8664 ²⁹	8758 ³³	8731
8859 ²²	8721 ²⁹	8782 ³³	8748 ⁴⁰
8876 ²⁵	8787 ²⁹	8705 ³²	8889 ⁷⁰
9014 ²¹	8880 ²⁴	9080 ³¹	9074
9162 ²⁵	8995 ³⁰	9157 ³¹	9141
9176 ²³	9040 ³⁰	9180 ³²	9187
9179 ²³	9031 ³⁰	9125 ³²	9111
9170 ²⁴	9015 ²⁹	9150 ³¹	9112
9210 ²²	9082 ²⁹	9172 ³¹	9149
9416 ²²	9103 ³⁰	9223 ³²	9160
9286 ²³	9150 ²⁹	9264 ³¹	9226
9431 ²³	9311 ²⁹	9439 ³²	1390
9712 ²³	9624 ²⁹	9862 ³²	9770
9787 ²³	9734 ³⁰	9956 ³²	9887
9575 ²³	9447 ²⁹	9570 ³³	9548
9463 ²⁴	9337 ³⁰	9435 ³²	9400
9352 ²³	9235 ³⁰	9345 ³²	9344
9265 ²³	9551 ³¹	9236 ³²	9200 ⁷⁰
9205 ²³	9053 ³⁰	9151 ³²	9098
9156 ²⁹	9009 ³⁰	9076 ³³	9060
9005 ²⁹	8885 ³¹	9036 ³³	9020
8853 ²⁴	8741 ³⁰	8852 ³⁶	8845
8730 ²³	8589 ³⁰	8665 ³⁶	8692
8680 ²⁵	8574 ³¹	8575 ⁷⁰	
8627 ²⁴	8439 ³⁰	8496 ³⁵	8481

09228

09792

9301

0
8759

11050 Sout Stk
 10039 10009 9234 9941 9966 9914 9846 10257

Sta	5'cut	5'46	Ditch	Berm	\$
98+0	8696	8720	8691	8817 ⁹	8943
99+0	8732	8748	8693 ³	8807	8980
100+0	8902	8900	8796 ³	8895 ⁴	8931
101+0	9083	9084	8872 ⁹	9007	9090
102+0	9180				9198
103+0	9201	9200	9031 ²	9170 ⁸	9229
104+0	9123	9102	9015 ⁵	9181 ⁹	9229
105+0	9115	9097	9031 ¹⁰	9202	9225
106+0	9196	9185	9047 ²	9210 ¹⁰	9260
107+0	9206	9198	9072 ²	9222 ⁷	9259
108+0	9284	9255	9152 ²	9306 ¹⁰	9321
109+0	9495	9470	9315 ²	9452 ¹⁰	9495
110+0	9972	9860	9653 ³	9741 ¹⁰	9760
111+0	9860	9882	9705 ³	9807 ¹⁰	9830
112+0	9571	9557	9430 ³	9587 ¹⁰	9617
113+0	9419	9432	9297 ³	9427 ¹⁰	9493
114+0	9380	9400	9220 ³	9368 ¹⁰	9390
115+0	9225	9252	9109 ³	9290 ¹⁰	9305
116+0	9197	9190	9048 ³	9216 ¹⁰	9240
117+0	9171	9160	9022 ⁹	9142 ⁹	9175
118+0	9055	9001	8865 ⁷	9003 ¹¹	9024
119+0	8945	8936	8720 ⁹	8862 ¹⁰	8842
120+0	8675	8690	8601 ⁹	8742 ¹¹	8757
121+0	8547	8689	8492 ⁴	8703 ¹³	8709
122+0	8532	8561	8421 ⁵	8641 ¹¹	8680

Berm	Atch	Stk	5'cut
8870 ²¹	8664 ²⁹	8758 ³³	8731
8859 ²²	8721 ²⁹	8782 ³³	8748 ⁴⁰
8896 ²⁵	8787 ²⁹	8705 ³²	8889 ⁷⁰
9014 ²¹	8880 ²⁴	9080 ³¹	9074
9162 ²⁵	8995 ³⁰	9157 ³⁴	9141
9176 ²³	9040 ³⁰	9180 ³²	9187
9179 ²³	9031 ³⁰	9125 ³²	9111
9170 ²³	9015 ²⁹	9150 ³¹	9112
9210 ²²	9082 ²⁹	9192 ³¹	9199
9216 ²²	9103 ³⁰	9223 ³²	9160
9286 ²³	9150 ²⁹	9264 ³¹	9226
9431 ²³	9311 ²⁹	9439 ³²	9390
9712 ²³	9624 ²⁹	9862 ³²	9770
9787 ²³	9734 ³⁰	9956 ³²	9887
9575 ²³	9447 ²⁹	9570 ³³	9548
9463 ²⁴	9337 ³⁰	9435 ³²	9400
9352 ²³	9235 ³⁰	9345 ³²	9344
9265 ²⁵	9551 ³¹	9236 ³²	9200 ⁷⁰
9205 ²³	9053 ³⁰	9151 ³²	9098
9156 ²⁰	9009 ³⁰	9076 ³³	9060
9005 ²⁹	8885 ³¹	9036 ³³	9020
8853 ²⁴	8741 ³⁰	8852 ³⁶	8845
8730 ²³	8589 ³⁰	8665 ³⁶	8692
8680 ²⁵	8574 ³¹	8575 ⁷⁰	
8627 ²⁴	8439 ³⁰	8496 ³⁵	8481

092.28

097.92

93.01

0
87.59

11050 5'cut
 10039 100.09 9234
 9941 9866 9914 9846 10057

130

Sta	S'out	Stk	Ditch	Berm	£
123+0	8543	8600	837 ¹ / ₂	8530 ¹¹	8559
124+0	8327	8321	8275	8440 ⁶	9522
124+18			50' N	8500	8509

B M on S end of concrete
had wall Sta. 124+25

EL. 85.86

131

Berm	Ditch	Stk	S'out
8501 ²⁴	835 ³⁰ 2	8466 ³⁵	8470
8455 ²⁹	8221 ³²	8270 ⁴⁰	
50'S	8487		

Survey For Bob
Parker

Sta.	Top 5+k	ground	Top tile	© 98.74
0+0	93.88	93.24	90.00	
1+0	93.70	93.25		
2+0	94.56	93.88		
3+0	94.23	93.70		
4+0	94.90	94.34		
5+0	96.90	95.92		
6+0	97.44	97.03		
7+0	97.95	97.69		
8+0	98.70	97.96		
9+0	98.74	98.22		
10+0	99.31	98.57		
11+0	99.66	98.94		
12+0	98.81	98.23		
13+0	98.48	97.91		
14+0	97.74	97.20		

Mudex Dam

64+60	67.71	6052	7.19	
62+11	66.13	6029	5.89	
61+93	65.79	5993	6.86	
60+0	64.13	5951	4.62	
58+0	63.55	5907	4.98	
56+0	63.09	-0-	63.08	5863
54+0	62.80	5819	4.61	
52+26'	64.63	-0-	5779	6.84
49+79	64.49	57.17	7.32	
48+43	63.08	5683	6.25	
46+0	61.86	5627	5.64	
44+50	60.88	5585	5.03	

Station	EI Stake	Grade	
56+0	63.08	58.38	4.70
58+0	63.55	58.66	4.89
60+0	64.13	58.94	5.19
61+93	65.79	59.21	6.58
64+60	67.71	59.58	8.13

W. 158 E.

3.64
 3.65 3.95
 3.11 - 4.51
 3.77 4.08
 X 4.51 4.55
 4.31 4.15
 3.10 SK-701
 SK-639 3.65
 3.50

1.51
 3.61
 90
 3.61
 1.00
 6.39
 4.51
 6.39
 4.61
 1.78
 7.01
 4.60
 2.41

2.540
 1.3
 3.60
 77.10

Natural Trigonometrical Ratios.

Angle.	Sine.	Tan.	Sec.	Cosec.	Colg.	Cosin.	Angle.	Sine.	Tan.	Sec.	Cosec.	Colg.	Cosin.
0	0	0	1.	∞	∞	1.	90	0	0	1.	∞	∞	1.
10	.0029	.0029		343.8	343.8	1.	50	10	.1421	.1435	1.0102	7.040	6.968
20	.0058	.0058		171.9	171.9	.99998	40	20	.1449	.1465	1.0107	6.900	6.827
30	.0087	.0087		114.6	114.6	.99996	30	30	.1478	.1495	1.0111	6.766	6.691
40	.0116	.0116	1.0001	85.94	85.94	.99993	20	40	.1507	.1524	1.0115	6.636	6.561
50	.0145	.0145	1.0001	68.76	68.75	.99989	10	50	.1536	.1554	1.0120	6.512	6.435
60	.0175	.0175	1.0002	57.30	57.29	.99985	89	9	.1564	.1584	1.0125	6.394	6.314
70	.0204	.0204	1.0002	49.11	49.10	.99979	50	10	.1593	.1614	1.0129	6.277	6.197
80	.0233	.0233	1.0003	42.92	42.96	.99973	40	20	.1622	.1644	1.0134	6.166	6.084
90	.0262	.0262	1.0003	38.20	38.19	.99966	30	30	.1650	.1673	1.0139	6.059	5.976
	.0291	.0291	1.0004	34.38	34.37	.99958	20	40	.1679	.1703	1.0144	5.955	5.871
	.0320	.0320	1.0005	31.26	31.24	.99949	10	50	.1708	.1733	1.0149	5.855	5.769
	.0349	.0349	1.0006	28.65	28.64	.99939	88	10	.1736	.1763	1.0154	5.759	5.671
	.0378	.0378	1.0007	26.45	26.43	.99929	50	10	.1765	.1793	1.0160	5.665	5.576
	.0407	.0407	1.0008	24.56	24.54	.99917	40	20	.1794	.1823	1.0165	5.575	5.485
	.0436	.0437	1.0010	22.93	22.90	.99905	30	30	.1822	.1853	1.0170	5.488	5.396
	.0465	.0466	1.0011	21.49	21.47	.99892	20	40	.1851	.1883	1.0176	5.403	5.309
	.0494	.0495	1.0012	20.23	20.21	.99878	10	50	.1880	.1914	1.0181	5.320	5.226
	.0523	.0524	1.0014	19.11	19.08	.99863	87	11	.1908	.1944	1.0187	5.241	5.145
	.0552	.0553	1.0015	18.10	18.07	.99847	50	10	.1937	.1974	1.0193	5.164	5.066
	.0581	.0582	1.0017	17.20	17.17	.99831	40	20	.1965	.2004	1.0199	5.089	4.989
	.0610	.0612	1.0019	16.38	16.35	.99813	30	30	.1994	.2035	1.0205	5.016	4.915
	.0640	.0641	1.0020	15.64	15.60	.99795	20	40	.2022	.2065	1.0211	4.945	4.843
	.0669	.0670	1.0022	14.96	14.92	.99776	10	50	.2051	.2095	1.0217	4.877	4.773
	.0698	.0699	1.0024	14.34	14.30	.99756	86	12	.2079	.2126	1.0223	4.810	4.705
	.0727	.0729	1.0027	13.76	13.73	.99736	50	10	.2108	.2156	1.0230	4.745	4.638
	.0756	.0758	1.0029	13.23	13.20	.99714	40	20	.2136	.2186	1.0236	4.682	4.574
	.0785	.0787	1.0031	12.75	12.71	.99692	30	30	.2164	.2217	1.0243	4.620	4.511
	.0814	.0816	1.0033	12.29	12.25	.99668	20	40	.2193	.2247	1.0249	4.560	4.449
	.0843	.0846	1.0036	11.87	11.83	.99644	10	50	.2221	.2278	1.0256	4.502	4.390
	.0872	.0875	1.0038	11.47	11.43	.99619	85	13	.2250	.2309	1.0263	4.445	4.331
	.0901	.0904	1.0041	11.10	11.06	.99594	50	10	.2278	.2339	1.0270	4.390	4.275
	.0929	.0934	1.0043	10.76	10.71	.99567	40	20	.2306	.2370	1.0277	4.336	4.219
	.0958	.0963	1.0046	10.43	10.39	.99540	30	30	.2334	.2401	1.0284	4.284	4.165
	.0987	.0992	1.0049	10.13	10.08	.99511	20	40	.2363	.2432	1.0291	4.232	4.113
	.1016	.1022	1.0052	9.839	9.788	.99482	10	50	.2391	.2462	1.0299	4.182	4.061
	.1045	.1051	1.0055	9.567	9.514	.99452	84	14	.2419	.2493	1.0306	4.133	4.011
	.1074	.1080	1.0058	9.309	9.255	.99421	50	10	.2447	.2524	1.0314	4.086	3.982
	.1103	.1110	1.0061	9.065	9.010	.99390	40	20	.2476	.2555	1.0321	4.039	3.914
	.1132	.1139	1.0065	8.834	8.777	.99357	30	30	.2504	.2586	1.0329	3.994	3.867
	.1161	.1169	1.0068	8.614	8.556	.99324	20	40	.2532	.2617	1.0337	3.949	3.821
	.1190	.1198	1.0072	8.405	8.345	.99290	10	50	.2560	.2648	1.0345	3.906	3.776
	.1219	.1228	1.0075	8.206	8.144	.99255	83	15	.2588	.2679	1.0353	3.864	3.732
	.1248	.1257	1.0079	8.016	7.953	.99219	50	10	.2616	.2711	1.0361	3.822	3.688
	.1276	.1287	1.0082	7.834	7.770	.99182	40	20	.2644	.2742	1.0369	3.782	3.647
	.1305	.1317	1.0086	7.661	7.596	.99144	30	30	.2672	.2773	1.0377	3.742	3.606
	.1334	.1346	1.0090	7.496	7.429	.99106	20	40	.2700	.2805	1.0386	3.703	3.566
	.1363	.1376	1.0094	7.337	7.269	.99067	10	50	.2728	.2836	1.0394	3.665	3.526
							82						74

Cosin. Colg. Cosec. Sec. Tan. Sine. Angle.

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