

← LETTER →

4  
4

EXHIBIT

368 L

164

# KEUFFEL & ESSER CO.

## DRAWING MATERIALS AND SURVEYING INSTRUMENTS. NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

### TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.  
FOR SINGLE TRACK EXCAVATION.

"Copyright, 1885, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

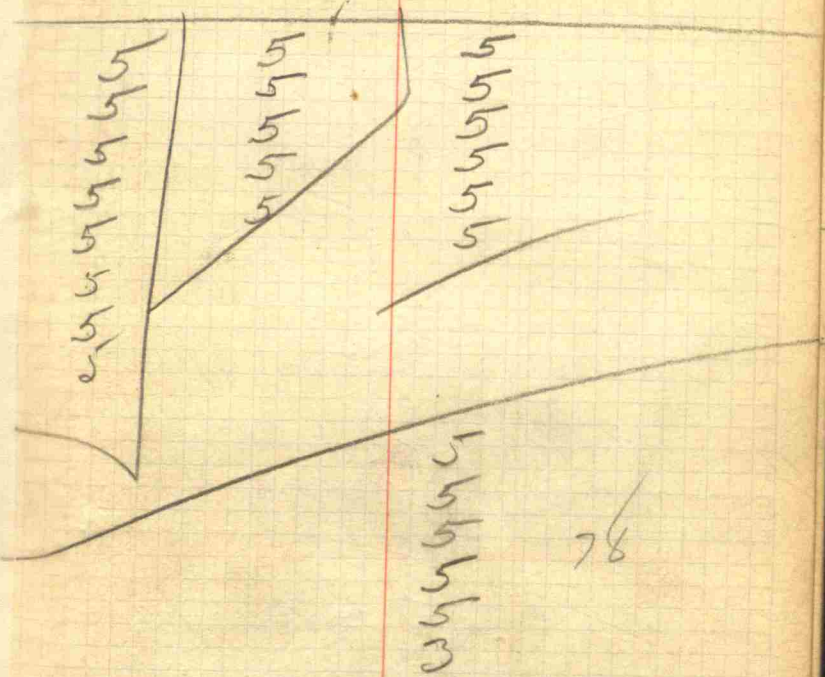
Calculated by Julien A. Hall, M. Am. Soc. C. E.

164

1

5-

1

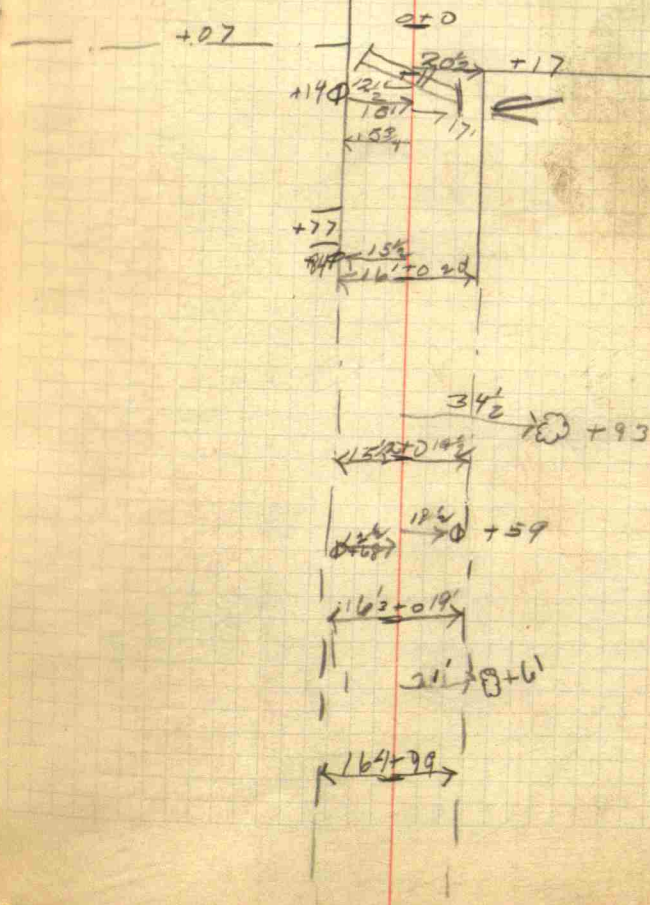


2

$$\begin{array}{r} 310 \\ 12.5 \\ \hline 125 \end{array}$$

O.N. TINDER RD. Beg. at  
 Cen. S. SE<sup>4</sup> 17-15-1W; thence  
 W. 1.55 miles to Center Twp.  
 line.

← N →  
 Tinder Rd. 3



4+9  
 26  
 12 70 = 60  
 12 70 = 57  
 +70 + 15  
 16'5" to 19'

12'0" to 19'

+61 11'  
 18'  
 17' 7" to 19 3/4" +42

+28  
 +28 18'  
 +36 18'

17' to +47

+71  
 17' 8" to 18 1/2"  
 +33 16'

20' to +56

17' 9" to 18'

16' to +29

11' 14'

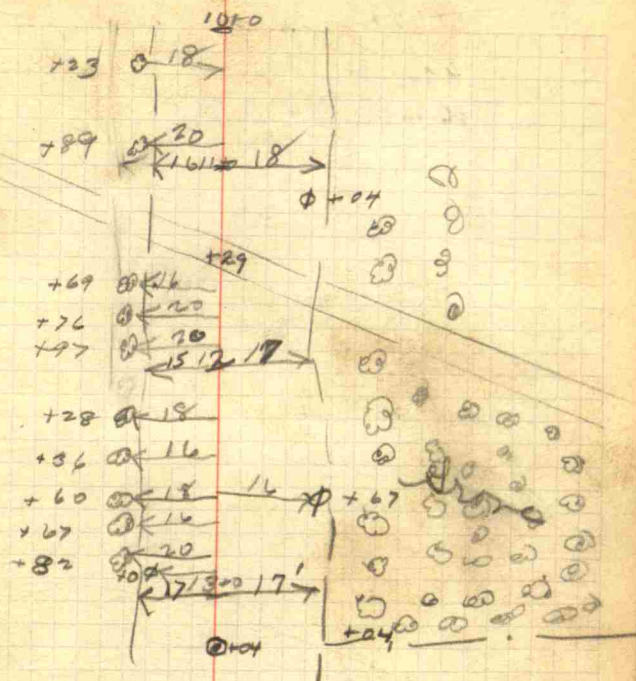
24' 1" to the curb  
 +55

+85  
 16' 1/2"  
 16' 1/2"

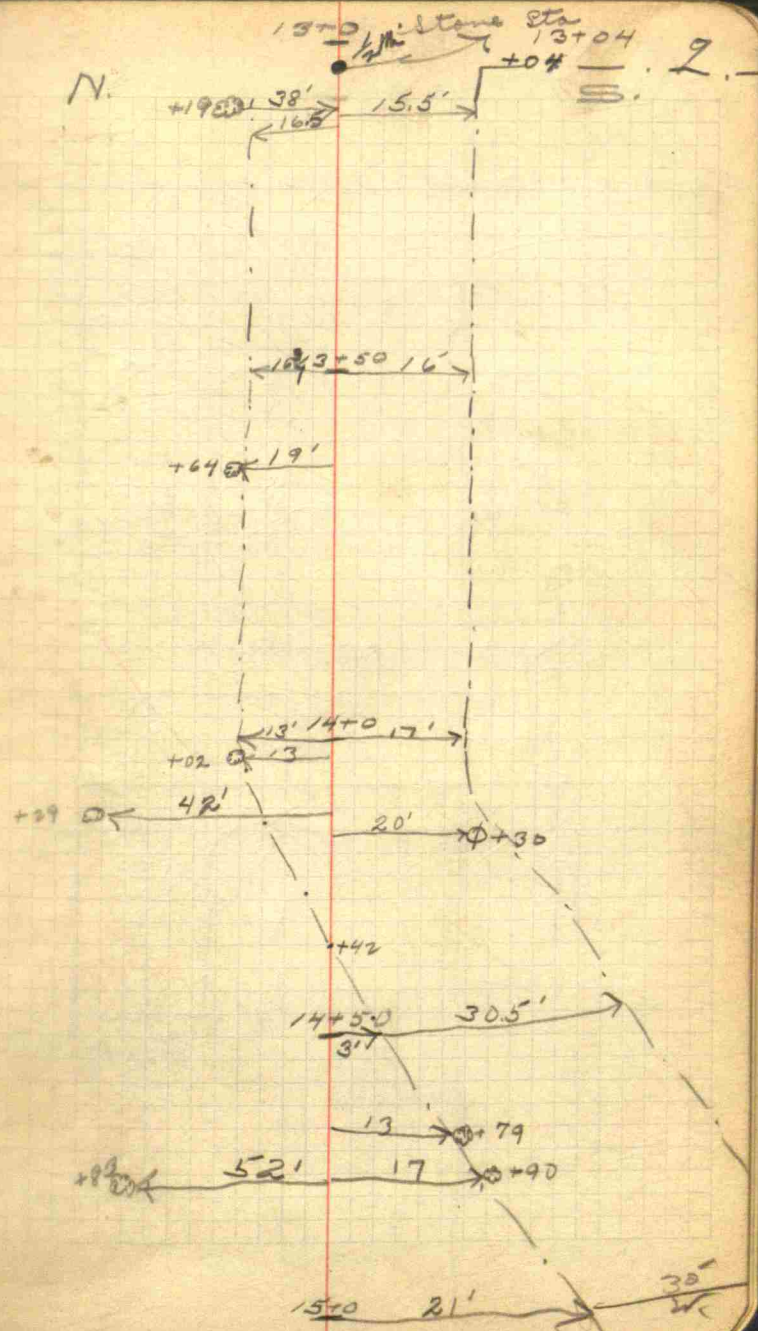
6

Witness for Cor Stone  
oak  
elm.

7



8 from Sta 13+04  
 Def  $\angle 0^{\circ} 18'$  to stone at  
 Sta. 26+07.





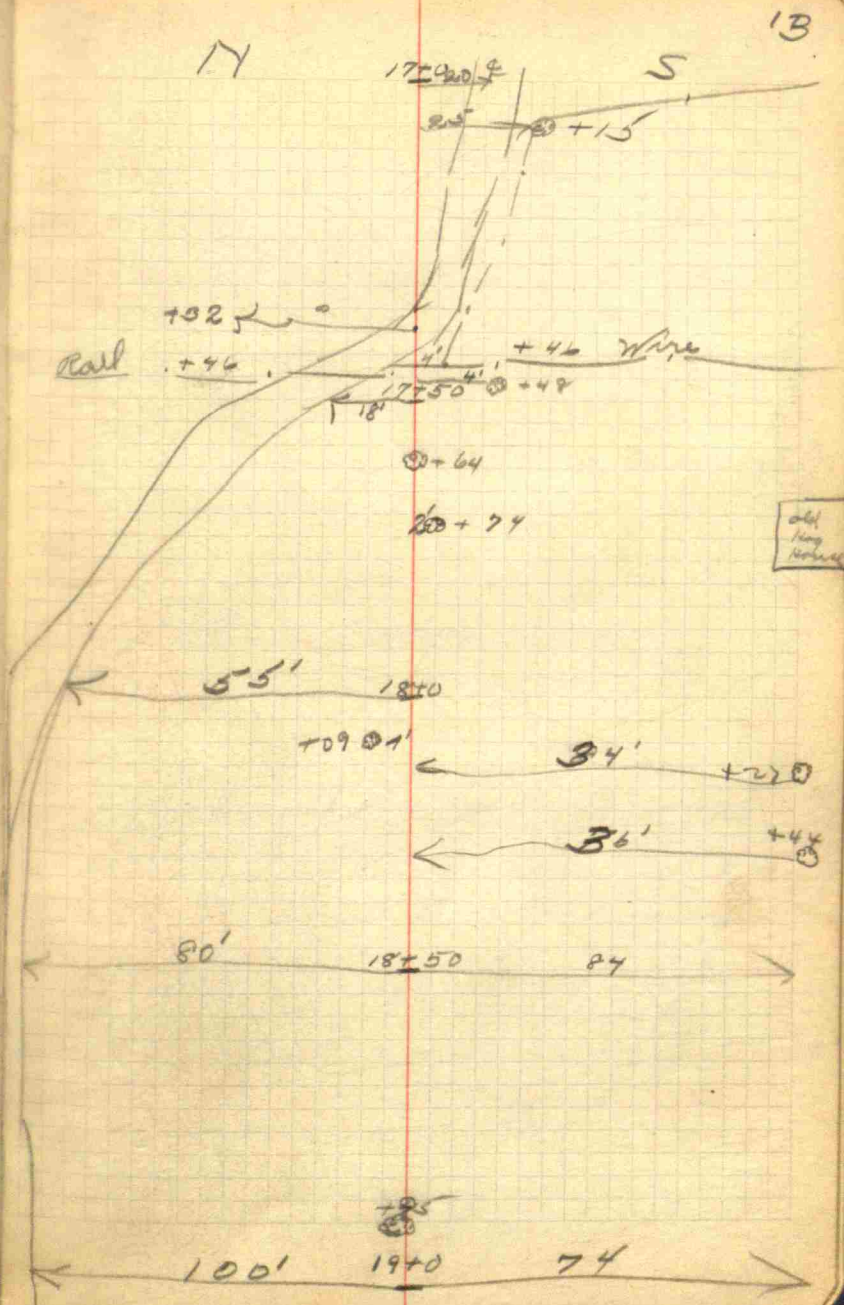


12

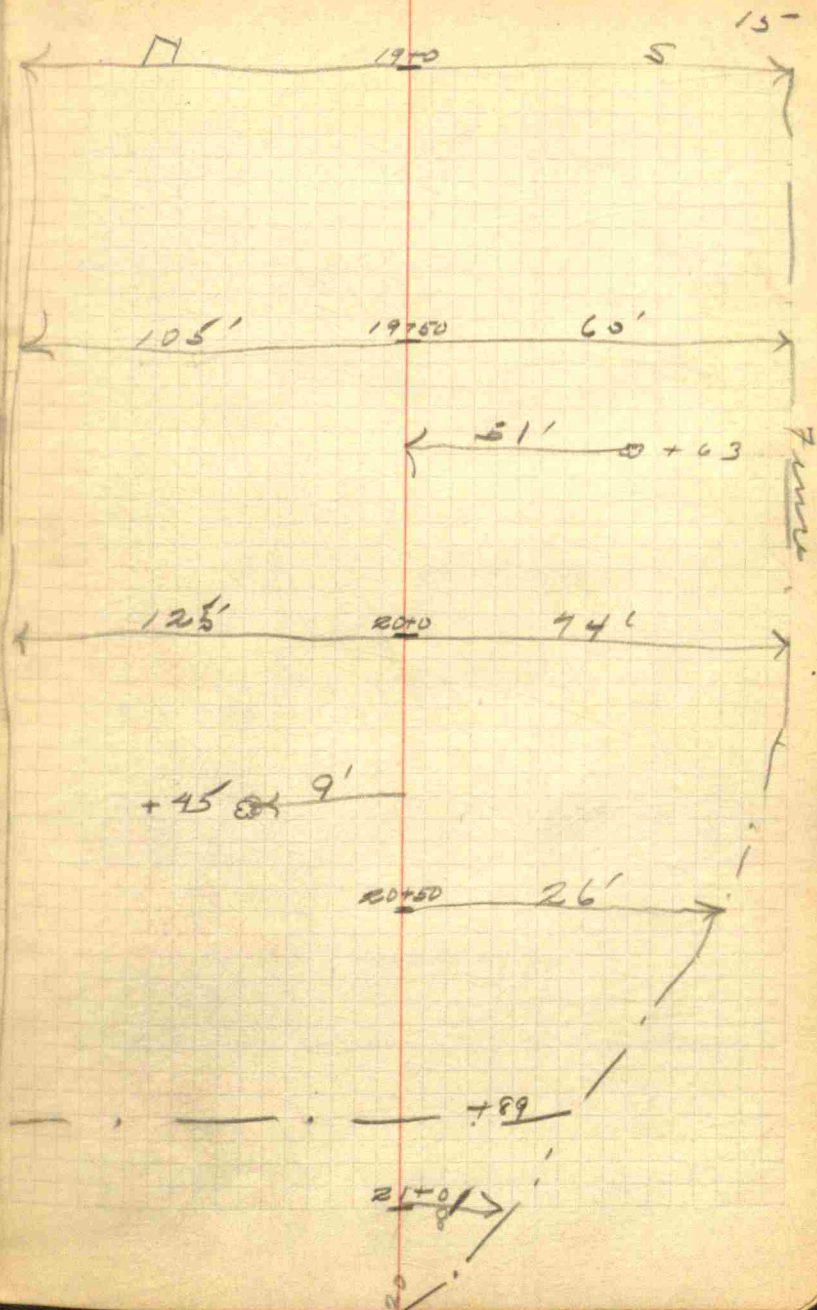
Sta 19+0	N. Road	Fence	South of	to is	83'
Sta 19+50	"	"	"	"	84'
Sta 19+0	"	"	"	"	74'

Fence goes South from rd 18+36  
 Tree on South side of old Road 19+25  
 Drive way on South side of old  
 Road Sta 19+60  
 center of House on South side  
 of Old Road 19+65

Fence runs South on South  
 side of Road Sta 20+0



14



16

N

21+08'

S

+20'

16' 21+50/3

8' 0' +85'

30.3' 22+0.75

+04' 29

+19' 32

+39' 32

Hand

70' 80.3' 22+50.7

+20' 32

+80

+87

20' 23+0.6' 18'

24'

+70' +81

17

18

N

23+0

S 119

+67  $\leftarrow$  20.5  
 +84  $\leftarrow$  20.5

TOT 100  $\leftarrow$  19.5 ~~24+0~~ 18.5

$\leftarrow$  7  $\Phi$  - 28

+54

$\leftarrow$  20.5 ~~25+0~~ 19.5

+36  $\leftarrow$  20.0

+56  $\leftarrow$  20.5

+68  $\leftarrow$  20.5

+11  $\leftarrow$  32  $\leftarrow$  20.5 ~~26+0~~ 19.5  
 $\leftarrow$  7  $\Phi$  + 28

26+07  $\leftarrow$  T07

20

2

← LETTER →

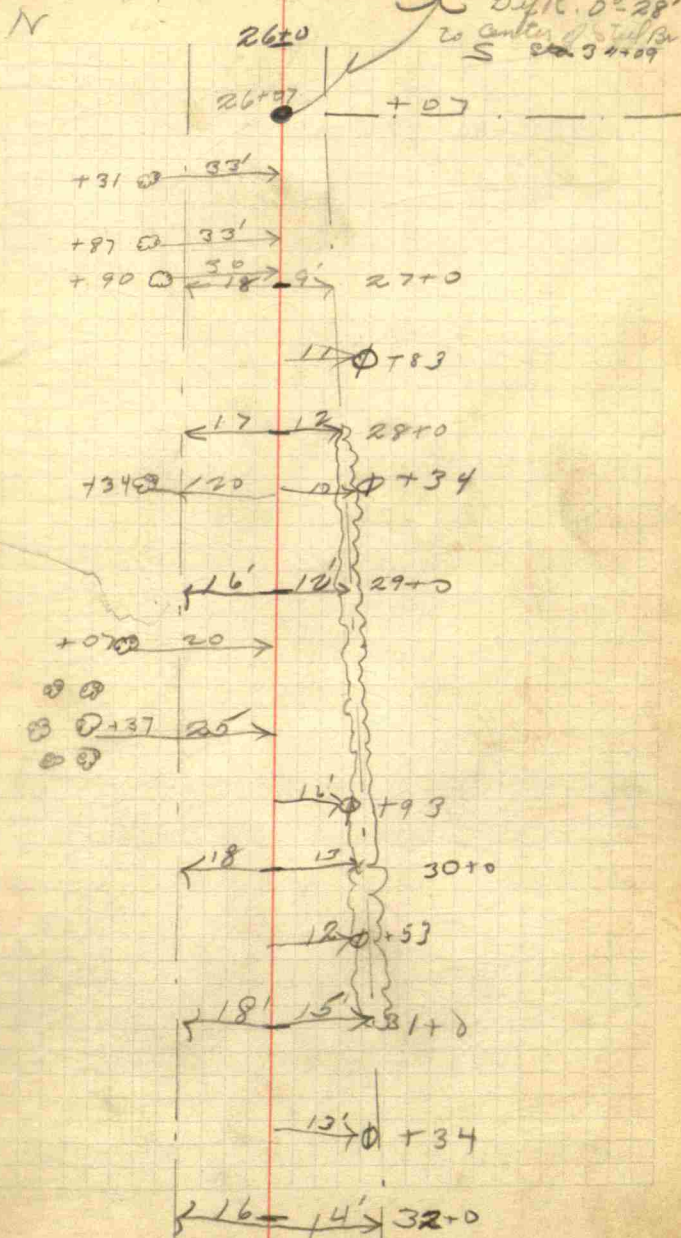
21

Stone at Sta 26107

Dy. R. 0° 28'

to center of tunnel

S 2° 34' 09"

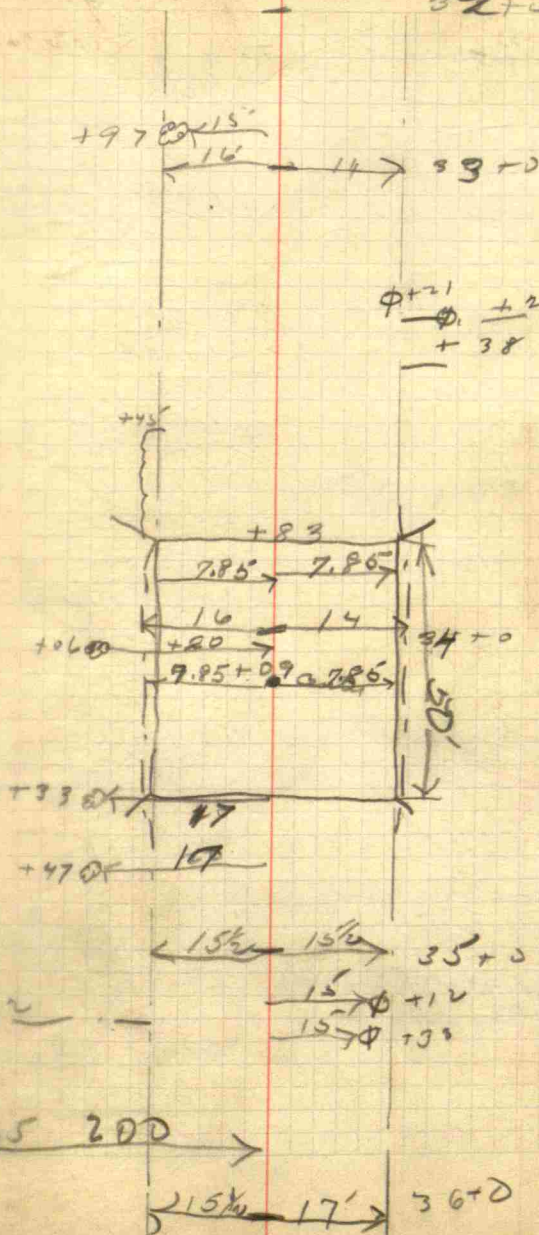


22 Def at Steel Bridge Sta 34+09  
 of 20'-53" to steel bridge  
 at Sta 41+08 1/2

11

5

23



Sta 33+09  
 River bridge  
 10'11"

24

N

36+0

5 25-

← 32 → 37'

+60

+80

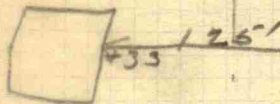
16 → 0 + 68

+91

← 27' → 16 → 37+0

+109 ⊗ 33'

12 ⊗ + 23



48 → 0 + 62

+79

+84 ⊗ 24

← 26 → 10 → 38+0

12 ⊗ + 75

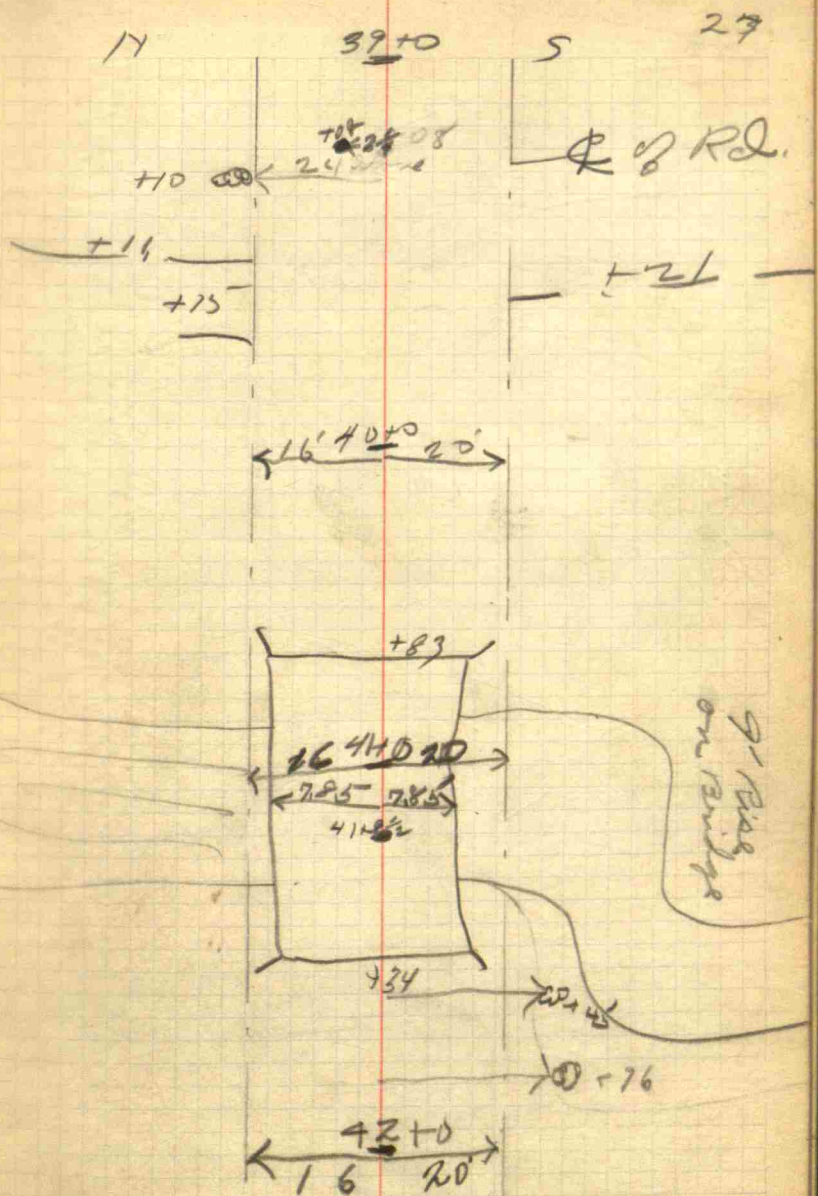
10 → + 90

39+0

← 24' →

26 Def. at Steel Bridge 41+08.4  
 Def. 10°-28' to Stone

Q of Project runs 2 1/4' South  
 of Stone at Sta 39+08.

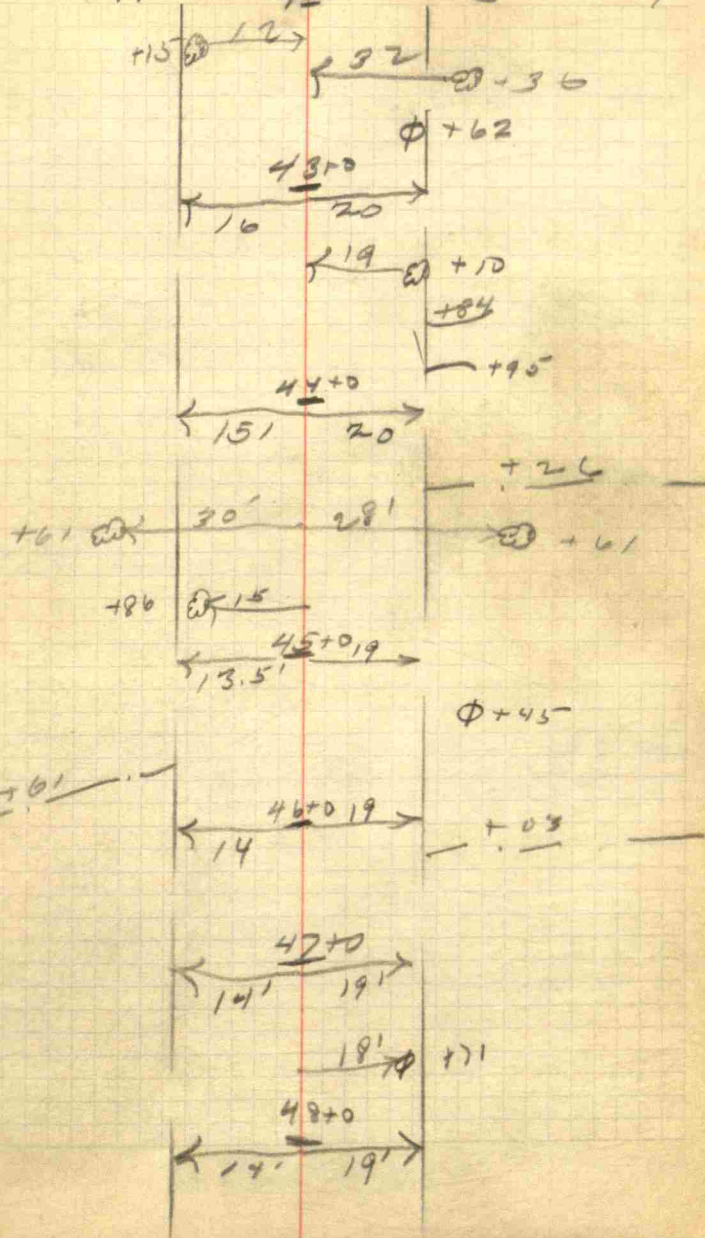


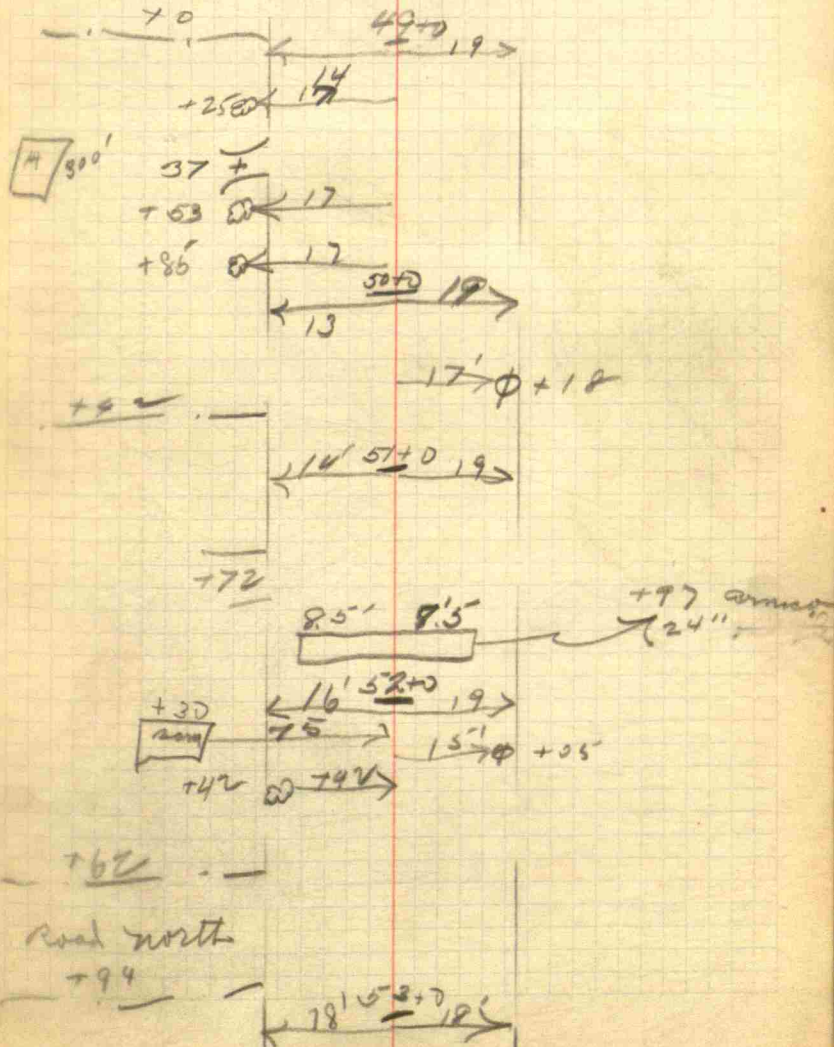


28

← LETTER →

N 42 S 29-





Road north

+94

82

14

53+0

5 38

 $\leftarrow 17 \begin{array}{c} 54+0 \\ \hline 18.5 \end{array} \rightarrow$ 
+10  $\leftarrow 15$ 
 $\leftarrow 17 \begin{array}{c} 55+0 \\ \hline 18.5 \end{array} \rightarrow$ 
 $\leftarrow 17 \begin{array}{c} 56+0 \\ \hline 18.5 \end{array} \rightarrow$ 
+29  $\leftarrow 15$ 
 $\leftarrow 20 \begin{array}{c} 57+0 \\ \hline 18 \end{array} \rightarrow$ 
+54  $\leftarrow 15$ 

+58

 $\leftarrow 16 \begin{array}{c} 59+0 \\ \hline 19 \end{array} \rightarrow$ 
+54  $\leftarrow 15$ 
 $\leftarrow 16 \begin{array}{c} 59+0 \\ \hline 19 \end{array} \rightarrow$ 

+51

 $\leftarrow 30 \begin{array}{c} 14 \end{array} \rightarrow$ 

+32

+66

 $\leftarrow 16 \begin{array}{c} 60+0 \\ \hline 14 \end{array} \rightarrow$

34

← LETTER →

IT 60+0 S 36-

+07  $\phi$  1.0+82  
+74

61+0 15'

+16  
60'

+51

+35

+57  $\phi$  1.8+41  $\phi$  3.0 100' Barn+36  $\phi$  1.9  
16 15  
60+0+36  $\phi$  1.9+49  $\phi$  3.0+00  $\phi$  3.0  
30 63+0  
17 15

+00

+78

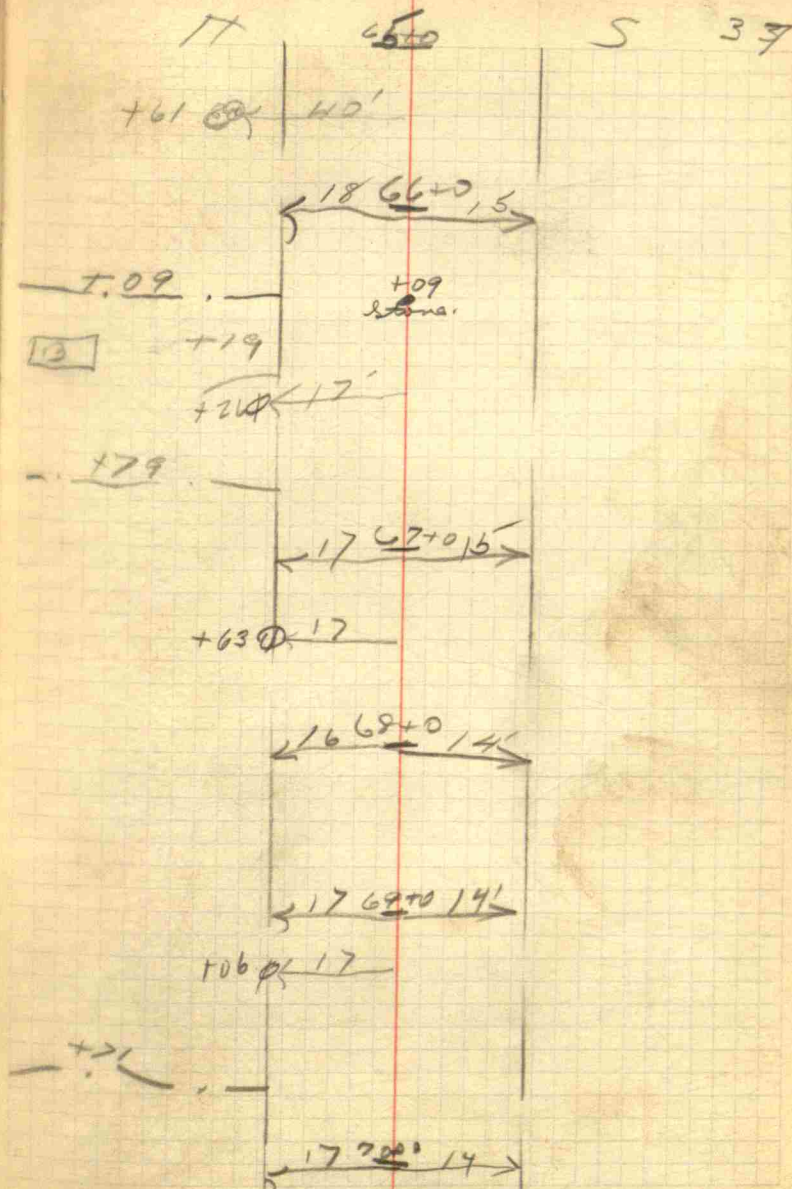
+85

+28  $\phi$  3.0  
17 64+0 16+00  $\phi$  3.0  
17 63+0 15

3 3/8 at Stone Sta 66+09  
 def to center of Stanley Rd.  
 def of R. 0<sup>e</sup> 12' cond to  
 end of Linden Rd. Proj.

Last page of this book:

66+09  
 Beech N43°E? 62'  
 Pear N60°W 71'



38

17

70+0

S 39

+47

10' 16



24" Vit. Tile  
Sta. 70+98

← 17 71+0 14 →

+47

+47

← 19 72+0 14 →

← 19 73+0 14 →

738

+80 0 ← 19

← 19 74+0 13 →

16 0 +14

17 0 +90

← 19.5 75+0 13 →

40

← LETTER →  
N 7510 S 81

+2053 16 19 26

← 21 76+0 126 →

+450 ← 20

← 20 77+0 12 →

+700 19

← 21 78+0 11 →

+986

← 21 79+0 11 →

+10

+67 20

← 21 82+0 10 →

+87 End of Proj.

42 BENCH MARKS

- #1 ON SW CORNER OF W. END OF Hdwall. - STA. 0+07  
EL. 100.00
- #2 ON W END OF NORTH Hdwall. OF OLD Rd. STA 17+0  
EL. 88.12. check ✓
- #3 ON SE CORNER OF SIDE WALK AT FENCE AT OSCAR TINDER'S HOUSE - STA. 22+40  
EL. 81.43 check ✓
- #A ON E. MUDWALL 2' FROM S. END. STA. 33+80  
EL. 50.68 check 50.71
- #5 ON SE corner of SW Wing of Bridge Sta 41+70  
EL. 48.59 check 48.61
- #6 ON N. end of West headwall on road going N. at Sta. 52+75  
EL. 66.10 check 66.13

TURNING POINTS

- 0 95.96
- 0 88.63
- 0 82.55
- 0 77.66
- 0 66.05
- 0 55.07
- 0 51.07
- 0 53.55
- 0 64.17
- 0 70.67
- 0 81.55



44

#7 On SW. corner of  
Concrete porch of house  
on N. side of Rd. Sta 61+20  
E.L. 92.05 check 92.03

○ 83.39

○ 75.00

○ 83.32

○ 94.69

#15-

#8 on base of concrete  
post on N. side of Stanley  
Rd 150' W of Sta 80+87  
E.L. 98.64  
check 98.60

46	5			20'	40'			72	48
Str.	5' out	Stk		E			Stk	5' out	⊙ 94.75
	99.55	50'	E						⊙ 90.43
	98.90	50'	S						
0+17	<sup>5</sup> 97.39	<sup>FL. 2</sup> 97.50	<sup>5</sup> 98.97	99.27	<sup>30</sup> 98.96	<sup>34</sup> 97.74	<sup>FL. 34</sup> 97.35		
1+0	<sup>5</sup> 97.67	<sup>6</sup> 97.74	<sup>6</sup> 97.65	<sup>5</sup> 99.21	<sup>25</sup> 98.25	<sup>29</sup> 98.15	<sup>40</sup> 98.91	<sup>45</sup> 98.71	
2+0	99.28	99.44	98.81	99.87	100.09	<sup>26</sup> 99.61	<sup>31</sup> 98.59	<sup>40</sup> 100.30	<sup>45</sup> 99.91
3+0	97.65	97.83	97.45	98.82	99.38	<sup>25</sup> 98.85	<sup>31</sup> 97.87	<sup>40</sup> 99.83	99.50
4+0	96.54	96.85	96.05	97.46	97.82	<sup>25</sup> 97.45	<sup>34</sup> 96.04	98.00	97.61
5+0	94.67	94.72	94.27	95.73	96.19	<sup>25</sup> 95.65	<sup>29</sup> 94.56	96.56	96.17
6+0	93.72	93.96	92.94	94.27	94.66	<sup>25</sup> 94.40	<sup>29</sup> 93.07	94.71	94.33
7+0	91.91	92.22	91.24	92.52	92.95	<sup>25</sup> 92.55	<sup>29</sup> 91.83	93.00	93.10
8+0	90.51	90.50	89.98	91.05	91.25	<sup>24</sup> 91.00	<sup>28</sup> 90.41	91.20	91.23
9+0	87.52	87.37	88.31	90.20	90.54	<sup>23</sup> 90.37	<sup>29</sup> 89.00	89.11	89.20
9+55	<sup>FL. 6</sup> 86.30	<sup>7</sup> 86.26	<sup>7</sup> 88.09	<sup>12</sup> 89.84	90.00	<sup>24</sup> 89.44	<sup>31</sup> 87.71	<sup>FL. 31</sup> 86.54	<sup>35</sup> 85.95
10+0	90.15	90.04	89.14	90.38	90.37	<sup>24</sup> 90.16	<sup>30</sup> 89.06	89.08	88.84
11+0	92.50	92.47	91.03	91.86	92.00	<sup>24</sup> 91.69	<sup>28</sup> 90.77	<sup>34</sup> 92.34	<sup>55</sup> 92.30
12+0	91.39	91.35	89.55	90.45	90.52	<sup>25</sup> 90.33	<sup>29</sup> 89.24	88.87	88.73
13+0	89.50	89.45	88.25	89.33	89.60	<sup>25</sup> 89.36	<sup>31</sup> 87.66	87.47	87.18
13+50	88.94	88.73	88.03	88.76	89.14	<sup>25</sup> 88.93	<sup>30</sup> 87.57	87.03	85.07

84.89<sup>60</sup>

48

S

071.56

17 49

83.42

14+0	5.5 89.14	sth 88.92	77.1 88.05	8 88.42	20 88.80	27 87.59	40 86.30	53 84.30	65 81.15	73.73	
14+50	7-5 87.81	sth 88.41	97.1 88.24	12 87.11	20 86.86	45 86.03	61 81.04	75 76.00		72.16	
15+0	E-15.5 88.62	sth 86.89	n 20' 85.60	40 84.10	54 82.12	68 79.35	82 70.65			82.44	
15+50	37-5 89.39	sth 88.77	n 20' 82.83	20'n 80.00	28 73.78	40 71.05	77 71.07	87 74.45	102 74.25	110 67.51 - dunnell	
15+75	E 25.5 88.75	sth 86.80	n 20' 85.60	40' 77.65	60' 74.22	97 74.43	110 67.93				
16+0	89.53 65 88.82-50.5	35.5 80.89	sth 75.18	15 n 71.20	ch. 20 n 66.30	ch. 29 65.70	45 71.14	62 71.77	ch. -64 65.95	ch. 94 66.00	98 71.86
16+50	80.17-60.5 80.93-50.5	14-5 75.25	sth 70.40	5 n 66.30	ch. 20 n 66.26	21 n 68.72	40 70.55	100 71.57			
	15.5 69.44	ch. 10.5 65.06	sth 66.23	18 n 69.15	20 n 71.16	n. 40' 71.93	50 71.85	60 71.95	70 72.00		
	E-75.5 89.18	68.5 88.76	40.5 74.66	32.5 72.00							
✓17+0	E-80.5 88.30	70.5 87.95	60.5 84.85	45.5 80.55	15.5 70.69	ch. sth 64.95	15 n. 66.58	20 n. 67.65	40 n. 70.55	60' 69.63	80 n. 70.00
✓17+50	E-80.5 88.36	21.5 85.00	5.5 80.86	sth 78.95	20 n. 70.95	28 n 68.27	ch. 33 n 63.65	ch. 46 n 64.60	51 n 68.95	80 n 68.67	
✓17+75			E 75.5 88.85	42.5 87.30	sth 84.20	20 n 82.74	35 n 63.70	42 n 64.15	45 n 68.31	80' 68.60	
✓18+0	E 85.5 88.52	24.5 85.60	sth 82.62	48 n 79.85	20 n 77.85	40 n. 76.63	52 n. 73.25	70 n. 65.50	90 n 63.47	93 n. 68.05	100 n 68.77
✓18+50	E-85.5 87.61	74.5 86.55	55.5 80.90	sth 74.00	20 n. 73.40	53 n 72.25	64 n. 67.75	84 n 67.07	94 n 63.70	104 n 63.85	109 n. 67.65 Level
✓19+0	E 72.5 87.21	58.5 85.72	45.5 79.63	sth 73.85	20 n 70.61	40 n 68.85	75 n 65.35	108 66.94	145 62.80	135 n 64.00	140 n 67.48 Level

50

S

✓ 19+50	E-56'S 85.38	53'S 82.95	26'S 75.10	sch 72.94	20'N 68.97
20+0	E 37' 84.60	21' S 82.14	19-S 82.40	41-S 74.60	20.N. 69.78
20+50	E 22'S 83.95	7'S 82.74	sch 80.25	20.N 72.15	
21+0	15'S 83.50	E 3'S 83.20	sch 83.45	20'N 77.00	
21+38	5'S 83.50	5' 83.00	sch 82.85	E-20'10' 83.18	20'N 82.55
21+50	5'S 83.50	sch 83.37	10'N 82.25	20'N 83.06	26 81.82
22+0	5'S 82.77	sch 82.68	16'N 81.70	20'N 82.25	25'N 82.61
22+50	5'S 82.22	sch 82.20	16'N 81.35	20'N 82.00	28'N 82.28
23+0	5'S 81.63	sch 81.55	14'N 80.93	20'N 81.53	28 81.68

51

40'N 67.63	77'N 67.63	88'N 64.65	105 65.75	115 63.20
40'N 69.30	86'N 67.70	94'N 65.67	115'N 65.45	
40'N 66.33	60'N 65.38	115'N 65.00	118'N 61.97	
40'N 69.89	60'N 67.50	80'N 66.80		
34'N 81.05	52'N 76.00			
28 83.00	40 82.08	50 79.90		
36' 82.05	43' 82.33			
38 81.47	50' 81.43			
37 81.23	45'N 81.05			

~~81.48.40~~

67.13

74.54

82.84

Sta	5'S	stk	16'n	20'n	26'n
24+0	80.72	80.62	79.74 <sup>16'n</sup>	79.90 <sup>20'n</sup>	80.28 <sup>26'n</sup>
25+0	78.56	78.64	78.03 <sup>16'n</sup>	78.46 <sup>20'n</sup>	78.83 <sup>26'n</sup>
26+0	76.15	76.00	76.26 <sup>16'n</sup>	77.00 <sup>20'n</sup>	77.08 <sup>26'n</sup>
27+0	74.10	74.23	73.60 <sup>15'n</sup>	74.26 <sup>20'n</sup>	74.58 <sup>25'n</sup>
28+0	71.02	71.41	70.12 <sup>14'n</sup>	71.02 <sup>18'n</sup>	71.23 <sup>20'n</sup>
29+0	67.87	68.10	62.87 <sup>15'n</sup>	63.97 <sup>19'n</sup>	64.00 <sup>20'n</sup>
30+0	64.04 <sup>5'S</sup>	63.03 <sup>stk</sup>	56.62 <sup>9'n</sup>	57.12 <sup>10'</sup>	56.95 <sup>10'n</sup>
31+0	51.44	51.78	52.47 <sup>10'n</sup>	53.67 <sup>12'</sup>	53.61 <sup>20'n</sup>
32+0	50.60	50.80	51.12 <sup>9'n</sup>	51.82 <sup>12'</sup>	52.20 <sup>20'</sup>
33+0	50.05	50.31	49.90 <sup>9'n</sup>	50.45 <sup>12'</sup>	51.02 <sup>20'</sup>
33+	Bridge Flow		50.68		

Sta	FL 9'	8'	E
34+0	40.68	50.68	50.68
35+0	46.00	48.42 <sup>6'</sup>	51.77 <sup>14'</sup>
36+0	59.90	59.92 <sup>6</sup>	60.00 <sup>14</sup>
36+50	65.44	65.60 <sup>5</sup>	65.74 <sup>14</sup>
37+0	63.75	63.60 <sup>7</sup>	63.28 <sup>16</sup>
38+0	57.17	57.05 <sup>11</sup>	56.65 <sup>15</sup>
39+0	49.40	49.70 <sup>11</sup>	50.50 <sup>15</sup>
39+	E of Rd South		50' - 47.95

40+0	47.71	48.00 <sup>3</sup>	47.66 <sup>6</sup>	48.00 <sup>13</sup>	49.49
41+0	Bridge	FL 9'	8'	2	49.51
		40.00	49.51	49.49	

33	36	40'	45'n
80.04 <sup>32</sup>	79.37 <sup>38</sup>	79.78 <sup>40</sup>	79.72 <sup>45'n</sup>
78.44 <sup>32'n</sup>	77.55 <sup>36</sup>	78.33 <sup>40</sup>	77.97 <sup>45</sup>
76.89 <sup>32'n</sup>	76.11 <sup>36</sup>	77.20 <sup>40</sup>	77.25 <sup>45</sup>
74.44 <sup>32'n</sup>	73.74 <sup>35</sup>	74.74 <sup>40</sup>	74.75 <sup>45</sup>
70.90 <sup>20'n</sup>	70.19 <sup>33</sup>	71.28 <sup>40</sup>	71.62 <sup>45'n</sup>
63.94 <sup>28'n</sup>	62.36 <sup>32'n</sup>	65.84 <sup>40'n</sup>	67.85 <sup>48'</sup>
56.82 <sup>29</sup>	56.26 <sup>33</sup>	56.65 <sup>37</sup>	55.42 <sup>40'n</sup>
53.86 <sup>31'n</sup>	53.20 <sup>33</sup>	52.03 <sup>40</sup>	51.95 <sup>45</sup>
51.91 <sup>31</sup>	51.84 <sup>33</sup>	51.42 <sup>40</sup>	51.30 <sup>45</sup>
50.35 <sup>29'n</sup>	50.95 <sup>35</sup>	49.60 <sup>40</sup>	49.05 <sup>45'n</sup>

FL 9'	40	45'n
50.68 <sup>8</sup>	40.68 <sup>35</sup>	50.31 <sup>45'n</sup>
51.83 <sup>29</sup>	49.58 <sup>40</sup>	49.84 <sup>33</sup>
55.00 <sup>20</sup>	55.09 <sup>30</sup>	54.80 <sup>33</sup>
56.40 <sup>33</sup>	57.72 <sup>35</sup>	60.10 <sup>40</sup>
57.01 <sup>20</sup>	57.41 <sup>36</sup>	59.41 <sup>40</sup>
54.42 <sup>32</sup>	53.95 <sup>34</sup>	57.51 <sup>40</sup>
50.08 <sup>33</sup>	49.45 <sup>37</sup>	49.81 <sup>40</sup>
		49.62 <sup>45</sup>

50.04 <sup>20</sup>	49.60 <sup>30</sup>	48.02 <sup>36</sup>	48.01-47.80 <sup>40 45</sup>
49.51 <sup>31</sup>	40.00 <sup>FL 9'</sup>		

076.80

066.71

057.93

051.75

45  
55.35

051.27

061.16

068.37

076.92

053.35

058.01

Sta	S out	sth	S	54	20	25	30	37	40	Level
41+0	45.70 <sup>3' out</sup>	45.40 <sup>1' n.</sup>	46.51 <sup>9'</sup>	49.41 <sup>14</sup>	49.56 <sup>20</sup>	49.35 <sup>25</sup>	47.50 <sup>30</sup>	41.60 <sup>37</sup>	40.50 <sup>40</sup>	Level
42+0	46.78	46.85	46.55 <sup>6</sup>	47.96 <sup>11</sup>	48.18 <sup>20</sup>	48.18 <sup>27</sup>	44.43 <sup>34</sup>	44.40 <sup>40</sup>	43.90 <sup>45</sup>	⊙ 50.92
43+0	46.22	46.44	46.93 <sup>7</sup>	47.59 <sup>12</sup>	48.25 <sup>20</sup>	48.16 <sup>27</sup>	47.30 <sup>31</sup>	48.00 <sup>40</sup>	47.40 <sup>45</sup>	⊙ 58.78
44+0	48.75	49.00	49.05 <sup>2</sup>	49.80 <sup>8</sup>	50.05 <sup>20</sup>	49.50 <sup>27</sup>	48.80 <sup>30</sup>	49.71 <sup>40</sup>	48.82 <sup>40</sup>	
45+0	63.00 <sup>12' out</sup>	62.75 <sup>7' out</sup>	59.08 <sup>sth</sup>	57.00 <sup>5</sup>	54.10 <sup>9</sup>	54.32 <sup>11</sup>	54.90 <sup>20</sup>	54.53 <sup>25</sup>	53.50 <sup>34</sup> / 59.30 <sup>40</sup> / 61.15 <sup>49</sup> / 63.89-level	
46+0	60.90	61.10	61.37 <sup>5</sup>	60.18 <sup>6</sup>	60.49 <sup>7</sup>	60.61 <sup>20</sup>	60.07 <sup>24</sup>	59.25 <sup>20</sup>	62.15 <sup>40</sup> - 62.19 <sup>45</sup>	
47+0	62.52	62.74	63.00 <sup>6</sup>	63.40 <sup>10</sup>	63.79 <sup>20</sup>	63.32 <sup>34</sup>	62.64 <sup>29</sup>	64.29 <sup>40</sup>	64.34 <sup>45</sup>	⊙ 65.84
48+0	64.55	64.69	64.46 <sup>6</sup>	64.60 <sup>11</sup>	65.00 <sup>20</sup>	64.56 <sup>27</sup>	64.18 <sup>30</sup>	65.07 <sup>40</sup>	65.14 <sup>45</sup>	
49+0	64.65	64.78	64.61 <sup>6</sup>	65.15 <sup>9</sup>	65.74 <sup>20</sup>	65.40 <sup>28</sup>	64.81 <sup>30</sup>	65.25 <sup>40</sup>	65.33 <sup>45</sup>	⊙ 70.70
50+0	65.65	65.96	65.39 <sup>7</sup>	65.71 <sup>10</sup>	65.80 <sup>20</sup>	65.60 <sup>27</sup>	65.18 <sup>29</sup>	66.00 <sup>40</sup>	65.85 <sup>45</sup>	
51+0	64.50	64.70	64.45 <sup>7</sup>	64.97 <sup>10</sup>	65.50 <sup>20</sup>	65.00 <sup>27</sup>	64.78 <sup>30</sup>	64.97 <sup>40</sup>	64.83 <sup>45</sup>	⊙ 79.23
51+97	62.80 <sup>20</sup>	62.19 <sup>15</sup>	63.17 <sup>8' FL.</sup>	64.96 <sup>7.5' FL.</sup>	65.39 <sup>20</sup>	64.85 <sup>8.5' FL.</sup>	63.12 <sup>9' FL.</sup>	63.55 <sup>16</sup>		
52+0	64.05	63.95	63.70 <sup>7</sup>	65.35 <sup>12</sup>	65.47 <sup>20</sup>	65.38 <sup>28</sup>	64.54 <sup>33</sup>	64.70 <sup>40</sup>	63.95 <sup>45</sup>	
52+75	50' n. on Rd			66.23						
53+0	66.33	66.64	65.82 <sup>10</sup>	66.46 <sup>12</sup>	67.00 <sup>20</sup>	66.36 <sup>28</sup>	66.03 <sup>32</sup>	66.20 <sup>40</sup>	66.01 <sup>45</sup>	
54+0	68.11	68.52	67.87 <sup>11</sup>	68.22 <sup>13</sup>	68.61 <sup>20</sup>	68.32 <sup>28</sup>	67.60 <sup>32</sup>	67.95 <sup>40</sup>	67.60 <sup>45</sup>	
55+0	70.73	70.90	69.80 <sup>11</sup>	70.53 <sup>15</sup>	70.53 <sup>20</sup>	70.42 <sup>28</sup>	69.56 <sup>32</sup>	69.40 <sup>40</sup>	69.25 <sup>45</sup>	
56+0	72.95	73.26	72.31 <sup>10</sup>	73.12 <sup>14</sup>	73.37 <sup>20</sup>	73.19 <sup>27</sup>	72.20 <sup>32</sup>	72.50 <sup>40</sup>	72.44 <sup>45</sup>	
57+0	76.03	76.01	74.84 <sup>10</sup>	75.54 <sup>13</sup>	76.05 <sup>20</sup>	75.74 <sup>28</sup>	74.58 <sup>32</sup>	76.01 <sup>40</sup>	76.12 <sup>45</sup>	
58+0	78.67	78.75	77.77 <sup>11</sup>	78.47 <sup>14</sup>	79.15 <sup>20</sup>	78.76 <sup>28</sup>	78.26 <sup>31</sup>	79.00 <sup>40</sup>	79.15 <sup>45</sup>	
59+0	81.91	81.83	81.20 <sup>11</sup>	81.48 <sup>12</sup>	82.16 <sup>20</sup>	82.00 <sup>27</sup>	81.23 <sup>30</sup>	81.95 <sup>40</sup>	82.00 <sup>45</sup>	
60+0	84.94	85.09	84.18 <sup>9</sup>	84.55 <sup>11</sup>	85.36 <sup>20</sup>	84.91 <sup>28</sup>	84.28 <sup>32</sup>	85.55 <sup>40</sup>	85.51 <sup>45</sup>	

Sta	5' ant	stk	5	14	20
61+0	89.17	89.52	8837 <sup>11</sup>	8880 <sup>14</sup>	8900 <sup>20</sup>
62+0	89.06	89.20	8853 <sup>10</sup>	8933 <sup>14</sup>	8993 <sup>20</sup>
63+0	86.87	87.04	8617 <sup>9</sup>	8681 <sup>14</sup>	8718 <sup>20</sup>
64+0	83.25	83.40	8290 <sup>11</sup>	8350 <sup>13</sup>	8387 <sup>20</sup>
65+0	80.56	80.82	8038 <sup>10</sup>	8138 <sup>13</sup>	8174 <sup>20</sup>
66+0	79.70	79.15	7888 <sup>9</sup>	8014 <sup>14</sup>	8022 <sup>20</sup>
67+0	77.11	77.30	7681 <sup>9</sup>	7795 <sup>12</sup>	7823 <sup>20</sup>
68+0	75.57	75.79	7545 <sup>11</sup>	7634 <sup>14</sup>	7660 <sup>20</sup>
69+0	74.74	74.85	7440 <sup>11</sup>	7550 <sup>14</sup>	7574 <sup>20</sup>
70+0	72.74	72.91	7366 <sup>10</sup>	7500 <sup>15</sup>	7550 <sup>20</sup>
70+38	70.13	70.75 <sup>FL 11</sup>	7290 <sup>FL 11</sup>	7433 <sup>81</sup>	7475 <sup>20</sup>
71+0	72.57	72.78	7295 <sup>10</sup>	7462 <sup>16</sup>	7510 <sup>20</sup>
72+0	73.50	73.65	7418 <sup>12</sup>	7534 <sup>15</sup>	7540 <sup>20</sup>
73+0	74.05	74.15	7447 <sup>12</sup>	7575 <sup>16</sup>	7594 <sup>20</sup>
74+0	75.10	75.11	7574 <sup>11</sup>	7682 <sup>16</sup>	7700 <sup>20</sup>
75+0	76.82	76.53	7738 <sup>11</sup>	7824 <sup>17</sup>	7836 <sup>20</sup>
76+0	79.27	79.31	7951 <sup>13</sup>	8047 <sup>17</sup>	8041 <sup>20</sup>
77+0	82.00	81.98	8205 <sup>14</sup>	8254 <sup>16</sup>	8263 <sup>20</sup>
78+0	85.00	84.92	8454 <sup>11</sup>	8521 <sup>14</sup>	8543 <sup>20</sup>
79+0	88.41	88.40	8767 <sup>13</sup>	8828 <sup>17</sup>	8844 <sup>20</sup>
80+0	91.71	91.61	9112 <sup>15</sup>	9161 <sup>16</sup>	9178 <sup>20</sup>
80+87	96.06	96.16	9406 <sup>8</sup>	9428 <sup>15</sup>	9440 <sup>20</sup>
50' W - E			95.86		
140' W - E			96.84		
200' W - E			95.66		

Sta	31	40	45	57.1
8882 <sup>28</sup>	8864 <sup>31</sup>	8977 <sup>40</sup>	8984 <sup>45</sup>	88.15
8943 <sup>28</sup>	8873 <sup>33</sup>	8921 <sup>40</sup>	8910 <sup>45</sup>	83.54
8680 <sup>27</sup>	8635 <sup>33</sup>	8700 <sup>40</sup>	8726 <sup>45</sup>	80.01
8347 <sup>26</sup>	8277 <sup>31</sup>	8335 <sup>40</sup>	8327 <sup>45</sup>	75.75
8153 <sup>26</sup>	8034 <sup>31</sup>	8152 <sup>40</sup>	8165 <sup>45</sup>	75.45
8007 <sup>26</sup>	7920 <sup>33</sup>	8028 <sup>40</sup>	8031 <sup>45</sup>	80.09
7794 <sup>25</sup>	7693 <sup>31</sup>	7831 <sup>40</sup>	7851 <sup>45</sup>	84.84
7671 <sup>25</sup>	7577 <sup>31</sup>	7610 <sup>40</sup>	7622 <sup>45</sup>	91.36
7587 <sup>25</sup>	7471 <sup>32</sup>	7543 <sup>40</sup>	Level	
7498 <sup>26</sup>	7210 <sup>33</sup>	7330 <sup>40</sup>	7340 <sup>45</sup>	
7460 <sup>26</sup>	7330 <sup>34</sup>	7165 <sup>40</sup>	7090 <sup>45</sup>	
7495 <sup>26</sup>	7330 <sup>35</sup>	7400 <sup>40</sup>	7400 <sup>45</sup>	
7537 <sup>26</sup>	7398 <sup>34</sup>	7435 <sup>40</sup>	7427 <sup>45</sup>	
7591 <sup>27</sup>	7506 <sup>34</sup>	7484 <sup>40</sup>	7478 <sup>45</sup>	
7713 <sup>26</sup>	7599 <sup>35</sup>	7627 <sup>40</sup>	7635 <sup>45</sup>	
7846 <sup>26</sup>	7747 <sup>32</sup>	7795 <sup>40</sup>	7827 <sup>45</sup>	
8045 <sup>27</sup>	7930 <sup>32</sup>	8050 <sup>40</sup>	8052 <sup>45</sup>	
8270 <sup>27</sup>	8186 <sup>32</sup>	8354 <sup>40</sup>	8371 <sup>45</sup>	
8525 <sup>27</sup>	8421 <sup>32</sup>	8617 <sup>40</sup>	8603 <sup>45</sup>	
8837 <sup>26</sup>	8728 <sup>33</sup>	8992 <sup>40</sup>	8877 <sup>45</sup>	
9153 <sup>27</sup>	9100 <sup>34</sup>	9252 <sup>40</sup>	9220 <sup>45</sup>	
9435 <sup>27</sup>	9402 <sup>34</sup>	9600 <sup>40</sup>	9516 <sup>45</sup>	

60

S

15+70	66.50	6777	7019	6983
15+80	6971	6658	7774	7216
16+0	6659	6671	7185	7210
16+50		7124		7160
17+0		7029		6773
16+75		7355		7203
17+50		6765		6841
18+0		6347	6801?	6757
18+20		6397		6347

617

0 77.88

7211	
7250	
7196	
7103	
7076	
7095	
7031	
6915	
6347	6801
	6850



62

## ESTIMATE - TIMBER ROAD,

11,896 Cu. Yds. Exc.	@ 40c
72' X 24" R.C. PIPE	@ 3.50
30' X 18" R.C. PIPE	@ 2.50
160' X 12" C.M. PIPE	@ 1.50
26' X 15" PIPE-RELAID	@ .30
600 Cu. Yds. SPECIAL EXC.	@ 40c
163 Cu. Yds. COITC.	@ 14.00
6767 LBS. STEEL	@ .05
2750 TONS (4 1/2" X 2 3/4") STONE	@ 2.50
728 TONS (3/4" TO DUST) "	@ 2.50
1698 TONS (4" X 2 1/2") "	@ 2.50
222 TONS (1" X 1/2") "	@ 2.50
222 TONS (3/4" X 1/2") "	@ 2.50
35,942 GALS. TAR.	@ .14

63

4,758.40 ✓
252.00 ✓
75.00 ✓
240.00 ✓
7.80 ✓
240.00 ✓
2282.00 ✓
338.35
6875.00 ✓
1820.00 ✓
4245.00 ✓
555.00
555.00
<u>5031.88</u>

Total - \$27,275.43

Bonds 28600<sup>00</sup>

Sta	No. side	Cut	street	Fill
	2th	New Gd.	Cut	
Sta	EL	SUBGDEL		
0+0	99.71	98.50	1'-3 $\frac{1}{2}$ "	
1+0	99.52	98.66	0'-10"	
2+0	100.72	98.82	1'-11"	
3+0	100.36	98.77	1'-7"	
4+0	98.37	97.98	0'-10 $\frac{3}{4}$ "	
5+0	96.95	95.98	1'-0"	
6+0	95.24	94.48	0'-9"	
7+0	94.05	92.98	1'-1"	
8+0	91.96	91.48	0'-6"	
9+0	89.85	90.09		0'-2"
10+0	89.56	89.58	GRADE	
11+0	93.24	89.18	4'-1"	
12+0	89.81	88.78	1'-0 $\frac{1}{2}$ "	
13+0	88.20	87.62	0'-7"	
13+50	87.53	86.48	1'-0 $\frac{1}{2}$ "	
14+0	86.92	84.95	2'-0"	
14+50	86.45	83.24	3'-2 $\frac{1}{2}$ "	
⊙ 15+0	84.44	81.52	2'-11"	
⊙ 15+25	76.79	80.66		3'-10 $\frac{1}{2}$ "
15+50	69.41	79.81		10'-5"
15+75	72.32	78.95		6'-8"
16+0	71.76	78.09		6'-4"
16+50	72.49	76.37		3'-10 $\frac{1}{2}$ "
17+0	70.54	74.66		4'-1 $\frac{1}{2}$ "
17+50	70.10	73.32		3'-3"

99.50

⊙ 9245 27

Sta	Top side Elev	NEW Gd. Sub Gd. Elev @ E	CUT.	FILL
17+75	73.11	72.76	0'-4"	
18+0	74.12	72.73	1'-4½"	
18+50	73.55	72.89	0'-8"	
19+0	72.13	73.81		1'-8½"
<del>19+50</del>				
20+0	68.75	76.39		7'-8"
20+50	66.00	77.68		11'-8½"
21+0	70.75	78.97		8'-3"
21+50	81.60	80.01	1'-7"	
22+0	83.00	80.53	2'-6"	
22+50	81.90	80.55	1'-4"	
23+0	81.69	80.05	1'-8"	
24+0	80.33	78.55	1'-9"	
25+0	78.60	77.05	1'-7"	
26+0	77.44	75.41	2'-0½"	
27+0	75.38	72.74	2'-8"	
28+0	72.20	69.09	3'-1½"	
29+0	66.89	65.30	1'-7"	
⊙ 30+00	55.33	61.51		6'-2"
31+0	52.62	57.72		5'-1¼"
32+0	51.92	54.10		2'-2"
33+0	49.48	51.67		2'-2½"
35+0	50.45	52.04		1'-7"
36+0	59.40	55.01	4'-5"	
36+50	59.94	56.10	3'-10"	

⊙ 75.76  
 ⊙ 76.40  
 ⊙ 66.30

50.75

56.70

69

Sta	No side Stk EL	MEW Gd Sub Gd, EL @E	CUT.	FILL
37+0	64.36	56.36	8'-0"	
38+0	58.56	54.48	4'-1"	
39+0	50.24	51.56		1'-4"
40+0	48.61	49.82		1'-2 1/2"
43+0	48.12	52.06		3'-11"
44+0	49.83	53.81		4'-0"
45+0	64.07	55.56	8'-6"	
46+0	62.70	57.68	5'-0"	
47+0	64.88	60.18	4'-8 1/2"	
48+0	65.57	62.68	2'-11"	
49+00	65.77	64.54	1'-3"	
50+0	66.58	65.12	1'-5 1/2"	
51+0	65.48	65.06	0'-5"	
52+0	cut	—	—	—
53+0	66.82	66.89		0'-1"
54+0	68.48	68.77		0'-3 1/2"
55+0	70.72	70.65	0'-1"	
56+0	73.01	72.90	0'-1 1/2"	
57+0	76.66	75.71	0'-11 1/2"	
58+0	79.48	78.89	0'-7"	
59+0	82.48	82.07	0'-5"	
60+0	86.21	85.25	0'-11 1/2"	
61+0	90.30	88.10	2'-2 1/2"	
62+0	89.55	88.62	0'-11"	
63+0	87.43	86.80	0'-8"	

049.61

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BM. Sta 41+20 on  
wing at E end of SW  
Aerial - EL - 49.95

~~058.89~~

~~066.74~~

~~074.56~~

083.84

Sta	No. side Set E.L.	NEW Gd. Sub-Gd. E.L. @ E	CUT.	FILL
64+0	83.68	84.65		1'-0"
65+0	82.12	82.50		0'-4 $\frac{1}{2}$ "
66+0	80.81	80.35	0'-5 $\frac{1}{2}$ "	
67+0	78.71	78.20	0'-6"	
68+0	76.97	76.40	0'-7"	
69+0	75.96	75.30	0'-8"	
70+0	73.62	74.55		0'-11"
71+0	74.50	74.48	GRADE	
72+0	74.75	75.08		0'-4"
73+0	75.76	75.68		0'-5"
74+0	76.80	76.08	0'-8 $\frac{3}{4}$ "	
75+0	78.53	77.52	1'-0"	
76+0	80.90	79.70	1'-2 $\frac{1}{2}$ "	
77+0	84.23	82.07	2'-2"	
78+0	86.71	85.02	1'-8 $\frac{1}{2}$ "	
79+0	90.32	88.06	2'-3"	
80+0	93.12	91.10	2'-0"	
80+87	96.38	93.74	2'-8"	

○ 83.82

B.M. on W. end of N. rail  
of Bridge at Sta. 70+42  
E.L. 75.85

○ ~~75.62~~

○ ~~80.57~~

○ 90.32

73

74 STA	Sub at 4	STA	Sub at 2		
0+0	98.50	98.80	16+50	8820	88.50X 88.33 ✓
0+50	98.58	98.85	13+0	8762	87.92X 87.75 ✓
1+0	98.66	98.96	9+50	8648	86.78X 86.61 ✓
1+50	98.74	99.04	14+0	8495	85.25X 85.08 ✓
2+0	98.82	99.12	14+50	8324	83.54X 83.37 ✓
2+50	98.90	99.20	15+0	8152	81.82X 81.65 ✓
3+0	98.77	99.03	15+50	7981	80.11X 79.94 ✓
3+50	98.83	98.53	16+0	7809	78.39X 78.22 ✓
4+0	97.48	97.78	16+50	7697	76.67X 76.50 ✓
4+50	96.73	97.03	17+0	7466	74.96X 74.79 ✓
5+0	95.98	96.28	17+50	7332	73.62X 73.45 ✓
5+50	95.23	95.53	18+0	7273	73.03X 72.86 ✓
6+0	94.48	94.78	18+50	7289	73.19X 73.02 ✓
6+50	93.73	94.03	19+0	7381	74.11X 73.94 ✓
7+0	92.98	93.28	19+50	7510	75.40X 75.23 ✓
7+50	92.23	92.53	20+0	7639	76.69X 76.52 ✓
8+0	91.48	91.78	20+50	7768	77.98X 77.82 ✓
8+50	90.73	91.03	21+0	7897	79.27X 79.11 ✓
9+0	90.09	90.39	21+50	8001	80.31X 80.14 ✓
9+50	89.78	90.08	22+0	8053	80.83X 80.66 ✓
10+0	89.58	89.88	22+50	8055	80.85X 80.78 ✓
10+50	89.38	89.68	23+0	8005	80.35X 80.35 ✓
11+0	89.18	89.48	23+50	7930	79.60X
11+50	88.98	89.28	24+0	7855	78.85X
12+0	88.78	89.08	24+50	7780	78.10 X

BW. 58 cu  
Swamp Timber  
22+40 - 81.43

12+0	—	88.91 ✓
12+50	—	89.11 ✓
11+0	—	89.31 ✓
10+50	—	89.51 ✓
10+0	—	89.71 ✓
9+50	—	89.91 ✓
9+0	—	90.22 ✓
8+50	—	90.86 ✓
8+0	—	91.61 ✓
7+50	—	92.36 ✓
7+0	—	93.11 ✓
6+50	—	93.86 ✓
6+0	—	94.61 ✓
5+50	—	95.36 ✓
5+0	—	96.11 ✓
4+50	—	96.86 ✓
4+0	—	97.61 ✓
3+50	—	98.45 ✓

476

+30

STA	Subst at Sta	Form hind STA	Subst at Sta
25+0	7705	77.35X	37+50 5583
25+50	7630	76.60X	38+0 5448
26+0	7541	75.71X	38+50 5302
26+50	7422	74.52X	39+0 5156
27+0	7274	73.04X	39+50 5062
27+50	7098	71.28X	40+0 4998
28+0	6909	69.39X	40+50 4948
28+50	6720	67.50X	41+0 4934
29+0	6530	65.60X	41+50 49.47
29+50	6341	63.71X	42+0 50.34
30+0	6151	61.81X	42+50 51.21
30+50	5962	59.92X	43+0 52.08
31+0	5772	57.02X	43+50 52.95
31+50	5583	55.13X	44+0 53.82
32+0	5410	54.40X	44+50 54.69
32+50	5271	53.01X	45+0 55.56
33+0	5167	51.97X	45+50 56.50
33+50	5054	50.84X	46+0 57.68
34+0	Bridge		46+50 58.93
34+50	5056	50.86X	47+0 60.18
35+0	5204	52.34X	47+50 61.43
35+50	5352	53.82X	48+0 62.68
36+0	5501	55.31X	48+50 63.61
36+50	5610	56.40X	49+0 64.54
37+0	5636	56.66X	49+50 64.83

0 51.34

0.75

- 26+50 - 74.52 X
- 27+0 - 72.94 X
- 27+50 - 71.08 X
- 28+0 - 69.09 X
- 28+50 - 67.10 X
- 29+0 - 65.10 X
- 29+50 - 63.21 X
- 30+0 - 61.31 X
- 30+50 - 59.42 X
- 31+0 - 57.52 X
- 31+50 - 55.73 X
- 32+0 - 54.20 X
- 32+50 - 53.01
- 33+0

47

OUT. E. MIDWALL 2  
 FROM So. end  
 Sta 33+80  
 EL. 50.68

Sw wing  
 of bridge Sta 41+20  
 EL. 48.59  
 Done

Sta 41+20  
 East Sw wing  
 on wing at E end  
 of Sw tondrail  
 EL. 49.95

STA	out at		STA	Sub of	
50+0	6572	6542X	62+50	8788	88.15X
50+50	6509	6539X	63+0	8680	87.10X
51+0	6506	6536X	63+50	8573	86.03X
51+50	6527	6557X	64+0	8465	84.95X
52+0	6549	6579X	64+50	8368	83.88X
52+50	6619	6649X	65+0	8250	82.80X
53+0	6689	6719V	65+50	8143	81.73X
53+50	6783	6813V	66+0	8035	80.65X
54+0	6877	6907X	66+50	7928	79.58X
54+50	6971	7001V	67+0	7820	78.50X
55+0	7065	7095V	67+50	7730	77.60X
55+50	7173	7205V	68+0	7645	76.75X
56+0	7290	7320V	68+50	7598	76.28X
56+50	7428	7458V	69+0	7550	75.80X
57+0	7571	7601V	69+50	7523	75.58X
57+50	7730	7760V	70+0	7495	75.25X
58+0	7889	7919V	70+50	7485	75.15X
58+50	8048	8078V	71+0	7498	75.28X
59+0	8207	8237V	71+50	7528	75.58X
59+50	8366	8396V	72+0	7558	75.88X
60+0	8525	8555V	72+50	7588	76.18X
60+50	8684	8714V	73+0	7617	76.48X
61+0	8810	8840X	73+50	7648	76.78X
61+50	8868	8898X	74+0	7697	77.27X
62+0	8962	8992X	74+50	7747	77.97X

8250  
107

79  
sw. con. Pouch  
E.L. 9205  
Sta. 61+40

560

76.05  
27  
75.78

75.25 ✓  
75.05 -10  
75.08 -20  
75.38 -25  
75.58 -30  
75.88  
76.18 ✓  
76.48 ✓  
76.78 ✓  
76.97 ✓  
77.3



80	sub	ad	Farmer	line
st	e			
(75+0)	7835	78.65	X <del>78.47</del>	77.35 ✓
75+50	79.24	79.54	X <del>79.24</del>	79.24 ✓
76+0	80.32	80.62	X	80.32 ✓
76+50	81.40	81.70	X	81.45 ✓
(77+0)	82.59	82.89	X 82.67	✓
77+50	83.98	84.28	X 84.10	✓
78+0	85.48	85.78	X 85.53	✓
78+50	86.98	87.28	X 86.96	✓
79+0	88.48	88.78	X 88.39	✓
79+50	89.98	90.28	X 89.99	✓
80+0	91.48	91.78	X 91.60	✓
80+50	92.98	93.28	X 93.20	
80+87	94.09	94.39	X 94.39	

2 | 3.20  
1.60

187 | 6.00 | .320 81  
5.61  
390  
374  
160

8267 94.14  
82.48

20 387 | 11.66  
3 11.66

20 82.48

82.48  
339  
82.69

4 | 5.72 | 8267  
1.43 72  
50 83.39

1.43  
50

7150

88.39  
1.60

89.99  
1.61

91.60  
1.60

93.20  
1.18

78.

78.3'

143  
50

7250 2784  
1184

32  
87

224  
96

143  
8267

84.10  
1.43

85.53  
1.43

86.96  
1.43

88.39

82

5267

78.35

4 4.32

1.08

78.35

1.08

79.43

5267

77.42

5 5.25

1.05

77.42

1.05

78.47

84

Ratliff  
Tinden

181.4  
2048.5

2848.00

← LETTER →

85

86

Edg  
6's

0-100	✓ 99.65	11+50	104.97	104.86
0-50	✓ 99.45	12+00	104.80	104.66
0+00	✓ 99.35	12+50	105.18	
0+50	99.55	13+00	104.95	
1+00	99.65	13+50	105.19	
1+50	99.78	14+00	105.66	
2+0	99.96	14+50	106.35	
2+50	100.30	15+00	107.35	
3+0	100.63	15+50	108.58	
3+50	101.09	16+00	109.42	
4+00	101.64	16+50	110.37	
4+50	102.10	17+00	111.04	
5+00	102.35	17+50	111.66	
5+50	102.75	18+00	112.20	
6+00	103.35	18+50	112.89	
6+50	104.35	19+00	113.66	
7+00	105.20	19+50	114.82	
7+50	106.25	20+00	115.52	
8+0	106.95	20+50	116.69	
8+50	107.12	21+00	118.15	
9+0	106.90	21+50	119.75	
9+50	106.65	22+00	121.55	
10+0	106.41	22+50	123.60	123.52
10+50	105.89	23+00	125.25	
11+0	105.27	23+50	126.60	126.60

24+00	127.42
24+50	127.96
25+00	128.15
25+50	128.00
26+00	127.85

98

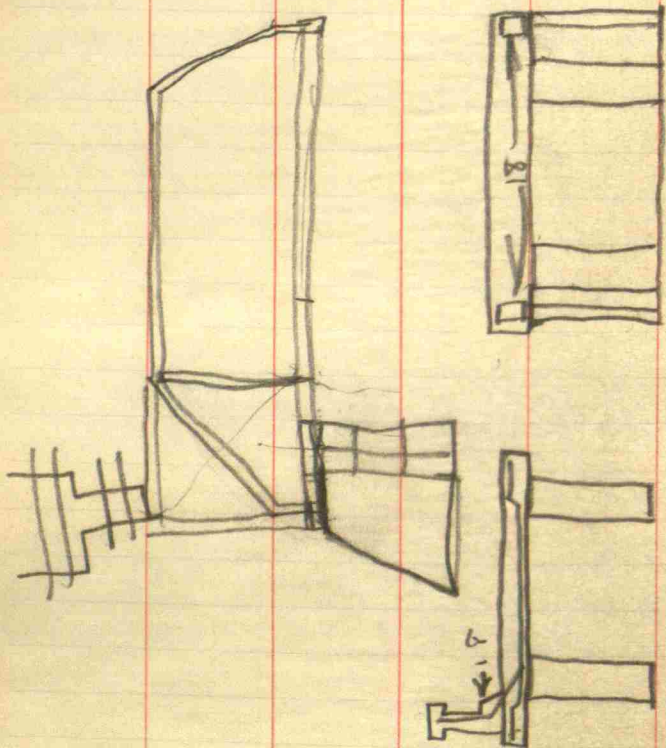
0+50	99.55	✓X	14	105.78	X -
1	99.75	✓X	+50	106.51	X -
+50	99.95	✓X	15	107.42	X -
2	100.15	✓X	+50	108.39	X -
+50	100.42	✓X	16	109.39	X -
3	100.78	✓X	+50	110.31	X -
+50	101.21	✓X	17	111.05	X -
4	101.64	✓X	+50	111.71	X -
+50	102.07	✓X	18	112.37	X -
5	102.50	✓X -	+50	113.03	X -
+50	102.93	✓X -	19	113.78	X - 0
6	103.48	✓X -	+50	114.69	X -
+50	104.30	✓X -	20	115.69	X -
7	105.24	✓X -	+50	116.84	-
+50	106.18	✓X -	21	118.31	-
8	106.88	✓X -	+50	119.93	-
+50	107.06	✓X -	22	121.63	
9	106.88	✓X -	+50	123.45	
+50	106.60	✓X -	23	125.20	
10	106.23	✓X -	+50	126.50	
+50	105.82	0 X -	24	127.42	
11	105.41	X -	+50	127.90	
+50	105.11	0 -	25	128.05	
12	105.05	0 -	+50	128.00	
+50	105.10	X -	26	127.85	
13	105.15	X -			
+50	105.20	X -			

← LETTER →

917

Mackey Road  
Ext - E from  
Tinden Road

84



95

← LETTER →

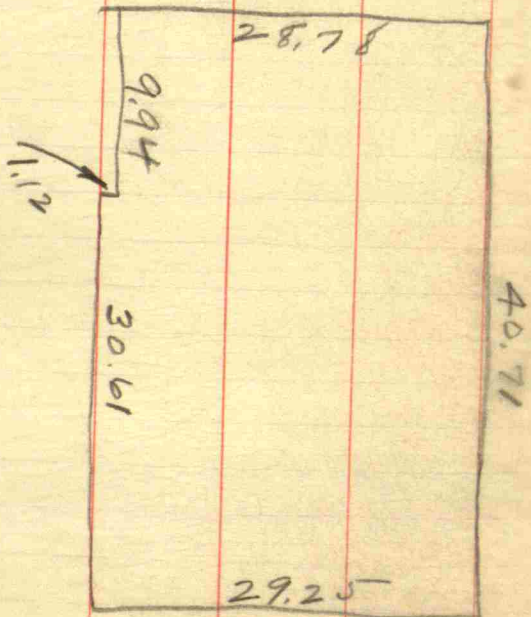
98

99

$$\begin{array}{r} 5643 \\ 48.85 \\ \hline 47 \overline{) 758} \\ \underline{417} \\ 3410 \\ \underline{3336} \\ 740 \end{array} \quad \left. \begin{array}{l} \\ \\ \\ \end{array} \right\} 1.52$$

$$\begin{array}{r} 1.52 \\ 17 \\ \hline 1294 \\ \underline{1824} \\ 3094 \end{array} \quad 31$$

NASH PARTITION.



2925  
4  
-----  
117.00



3 1/2

7

$$\begin{array}{r}
 100 \\
 300 \quad 2 \\
 \hline
 8100 \times 16 \times 7 \\
 27 \quad 24 \\
 \quad \quad 3
 \end{array}$$

1400  
3

$$\begin{array}{r}
 300 \quad 2 \\
 \hline
 8100 \times 16 \times 3 \\
 27 \quad 24 \\
 300 \quad 4 \quad 3 \\
 \hline
 8100 \times 16 \times 3 \\
 27 \quad 24 \\
 \quad \quad 3
 \end{array}$$

1200  
300

STA. 13+04      ON RAMPDOWN  
N      80'  
S

18+00      80'

22+00      80'

26+00      80'  
→ Stone 7.75' R and 1/2" dia

0°-20'

3°-21'

.58 of a foot to the 100'

10000  
9  

---

900.00

1278.00  
900  

---

9 | 378.00  
4200

14200

50.98  
49.48

50

4550  
4133

417

5643  
49.34

4 | 7.09 | 174

30

28  
29

53

56.43  
.87

5556  
87

5469  
87

53.82  
87

52.95  
87

52.08  
87

51.21  
87

503.41

950  
9100  
5400  
3600  
14400

47

87 8087 X 16  
A

799  
16  
4794  
799  
12784

← LETTER →

39 —

50.98  
49.64

1.22

50.98  
49.34

183 | 1.640 | .90  
1647

50.98  
45

50.53

33  
90

2970

49.34  
30

49.64  
45

50.09

50.01  
.67

49.34

$$\begin{array}{r} 53.70 \\ 91 \\ \hline 79 \end{array}$$

$$\begin{array}{r} 4550 \\ 4133 \\ \hline \end{array}$$

417

$$\begin{array}{r} 52.79 \\ 91 \\ \hline \end{array}$$

$$\begin{array}{r} 51.88 \\ 91 \\ \hline \end{array}$$

97

$$\begin{array}{r} 56.43 \\ 48.85 \\ \hline 56.43 \end{array}$$

242

$$\begin{array}{r} 7.58 \\ 4.17 \\ \hline \end{array}$$

417

4.17

1.82

$$\begin{array}{r} 3410 \\ 3336 \\ \hline \end{array}$$

740

$$\begin{array}{r} 56.43 \\ 55.90 \\ \hline \end{array}$$

$$\begin{array}{r} 55.59 \\ 91 \\ \hline \end{array}$$

$$\begin{array}{r} 54.61 \\ 90 \\ \hline \end{array}$$

$$\begin{array}{r} 53.70 \\ 91 \\ \hline \end{array}$$

$$\begin{array}{r} 52.81 \\ 90 \\ \hline \end{array}$$

$$\begin{array}{r} 51.91 \\ 91 \\ \hline \end{array}$$

### Natural Trigonometrical Ratios.

Angle.	Sine.	Tan.	Sec.	Cosec.	Cotg.	Cosin.	Angle.	Sine.	Tan.	Sec.	Cosec.	Cotg.	Cosin.
0	0	0	1.	$\infty$	$\infty$	1.	90	1.	$\infty$	$\infty$	0	0	0
10	.0029	.0029		343.8	343.8	1.	50	.1421	.1435	1.0102	7.040	6.868	.98986
20	.0058	.0058		171.9	171.9	.99998	40	.2449	.1465	1.0107	6.900	6.827	.98944
30	.0087	.0087		114.6	114.6	.99996	30	.3478	.1495	1.0111	6.768	6.681	.98902
40	.0116	.0116	1.0001	85.94	85.94	.99993	20	.4507	.1524	1.0115	6.636	6.561	.98858
50	.0145	.0145	1.0001	68.76	68.75	.99989	10	.5536	.1554	1.0120	6.512	6.435	.98814
1	.0175	.0175	1.0002	57.30	57.29	.99985	9	.6565	.1584	1.0125	6.394	6.314	.98769
10	.0204	.0204	1.0002	49.11	49.10	.99979	50	.7594	.1614	1.0129	6.277	6.197	.98723
20	.0233	.0233	1.0003	42.99	42.96	.99973	40	.8623	.1644	1.0134	6.166	6.084	.98676
30	.0262	.0262	1.0003	38.20	38.19	.99966	30	.9652	.1673	1.0139	6.059	5.978	.98629
40	.0291	.0291	1.0004	34.38	34.37	.99958	20	1.0681	.1703	1.0144	5.955	5.871	.98580
50	.0320	.0320	1.0005	31.26	31.24	.99949	10	1.1710	.1733	1.0149	5.855	5.769	.98531
2	.0349	.0349	1.0008	28.65	28.64	.99939	88	1.2739	.1763	1.0154	5.759	5.671	.98481
10	.0378	.0378	1.0007	26.45	26.43	.99929	50	1.3768	.1793	1.0160	5.665	5.576	.98430
20	.0407	.0407	1.0008	24.56	24.54	.99917	40	1.4797	.1823	1.0165	5.575	5.485	.98378
30	.0436	.0437	1.0010	22.93	22.90	.99905	30	1.5826	.1853	1.0170	5.488	5.398	.98325
40	.0465	.0466	1.0011	21.49	21.47	.99892	20	1.6855	.1883	1.0178	5.403	5.309	.98272
50	.0494	.0495	1.0012	20.23	20.21	.99878	10	1.7884	.1914	1.0181	5.320	5.226	.98218
3	.0523	.0524	1.0014	19.11	19.08	.99863	87	1.8913	.1944	1.0187	5.241	5.145	.98163
10	.0552	.0553	1.0015	18.10	18.07	.99847	50	1.9942	.1974	1.0193	5.164	5.066	.98107
20	.0581	.0582	1.0017	17.20	17.17	.99831	40	2.0971	.2004	1.0199	5.089	4.989	.98050
30	.0610	.0612	1.0019	16.38	16.35	.99813	30	2.2000	.2035	1.0205	5.016	4.915	.97992
40	.0640	.0641	1.0020	15.64	15.60	.99795	20	2.3029	.2065	1.0211	4.945	4.843	.97934
50	.0669	.0670	1.0022	14.96	14.92	.99776	10	2.4058	.2095	1.0217	4.877	4.773	.97875
4	.0698	.0699	1.0024	14.34	14.30	.99756	86	2.5087	.2126	1.0223	4.810	4.705	.97815
10	.0727	.0729	1.0027	13.76	13.73	.99736	50	2.6116	.2156	1.0230	4.745	4.638	.97754
20	.0756	.0758	1.0029	13.23	13.20	.99714	40	2.7145	.2186	1.0236	4.682	4.574	.97692
30	.0785	.0787	1.0031	12.75	12.71	.99692	30	2.8174	.2217	1.0243	4.620	4.511	.97630
40	.0814	.0816	1.0033	12.29	12.25	.99668	20	2.9203	.2247	1.0249	4.560	4.449	.97566
50	.0843	.0846	1.0036	11.87	11.83	.99644	10	3.0232	.2278	1.0256	4.502	4.390	.97502
5	.0872	.0875	1.0038	11.47	11.43	.99619	85	3.1261	.2309	1.0263	4.445	4.331	.97437
10	.0901	.0904	1.0041	11.10	11.06	.99594	50	3.2290	.2339	1.0270	4.390	4.275	.97371
20	.0929	.0934	1.0043	10.76	10.71	.99567	40	3.3319	.2370	1.0277	4.336	4.219	.97304
30	.0958	.0963	1.0046	10.43	10.39	.99540	30	3.4348	.2401	1.0284	4.284	4.165	.97237
40	.0987	.0992	1.0049	10.13	10.08	.99511	20	3.5377	.2432	1.0291	4.232	4.113	.97169
50	.1016	.1022	1.0052	9.839	9.788	.99482	10	3.6406	.2462	1.0299	4.182	4.061	.97100
6	.1045	.1051	1.0055	9.567	9.514	.99452	84	3.7435	.2493	1.0306	4.133	4.011	.97030
10	.1074	.1080	1.0058	9.309	9.255	.99421	50	3.8464	.2524	1.0314	4.086	3.962	.96959
20	.1103	.1110	1.0061	9.065	9.010	.99390	40	3.9493	.2555	1.0321	4.039	3.914	.96887
30	.1132	.1139	1.0065	8.834	8.777	.99357	30	4.0522	.2586	1.0329	3.994	3.867	.96815
40	.1161	.1169	1.0068	8.614	8.556	.99324	20	4.1551	.2617	1.0337	3.949	3.821	.96742
50	.1190	.1198	1.0072	8.405	8.345	.99290	10	4.2580	.2648	1.0345	3.906	3.776	.96667
7	.1219	.1228	1.0075	8.206	8.144	.99255	83	4.3609	.2679	1.0353	3.864	3.732	.96593
10	.1248	.1257	1.0079	8.016	7.953	.99219	50	4.4638	.2711	1.0361	3.822	3.689	.96517
20	.1276	.1287	1.0082	7.834	7.770	.99182	40	4.5667	.2742	1.0369	3.782	3.647	.96440
30	.1305	.1317	1.0086	7.661	7.596	.99144	30	4.6696	.2773	1.0377	3.742	3.606	.96363
40	.1334	.1346	1.0090	7.496	7.429	.99106	20	4.7725	.2805	1.0386	3.703	3.566	.96285
50	.1363	.1376	1.0094	7.337	7.269	.99067	10	4.8754	.2836	1.0394	3.665	3.526	.96206
							82						74

Cosin. Cotg. Cosec. Sec. Tan. Sine. Angle.

Cosin. Cotg. Cosec. Sec. Tan. Sine. Angle.



66409

Bench N 43° 00' - 62'

Peak N 60° W - 71'

$$\begin{array}{r} 50.98 \\ 48.85 \\ \hline 2.13 \end{array}$$

$$\begin{array}{r} 1.75 \\ 17 \\ \hline 12.25 \\ 17.5 \\ \hline 29.75 \end{array}$$

$$\begin{array}{r} 1.81 \\ 11 \\ \hline 126.7 \\ 151 \\ \hline 307.7 \\ 48.85 \end{array}$$
  

$$\begin{array}{r} 50.31 \\ 48.85 \\ \hline 1.46 \end{array}$$

$$\begin{array}{r} 1.75 \\ 17.5 \\ \hline 19.25 \\ 22.0 \\ \hline 41.25 \end{array}$$

$$\begin{array}{r} 1.17 \\ 5 \\ \hline 40.83 \\ 39 \\ \hline 1.83 \end{array}$$
  

$$\begin{array}{r} 183 \overline{) 213} \\ 183 \\ \hline 300 \\ 183 \\ \hline 1170 \end{array}$$

FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
 ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.  
 FOR SINGLE TRACK EMBANKMENT.

1	2	3	4	5	6	7	8	9	
7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0	
8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1	
10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2	
11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3	
13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4	
14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5	
16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6	
17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7	
19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8	
20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9	
22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10	
23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11	
25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12	
26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13	
28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14	
29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15	
31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16	
32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17	
34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18	
35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19	
37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20	
38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21	
40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22	
41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23	
43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24	
44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25	
46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26	
47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27	
49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28	
50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29	
52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30	
53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31	
55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32	
56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33	
58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34	
59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35	
61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36	

Compiled by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.