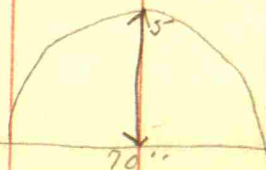
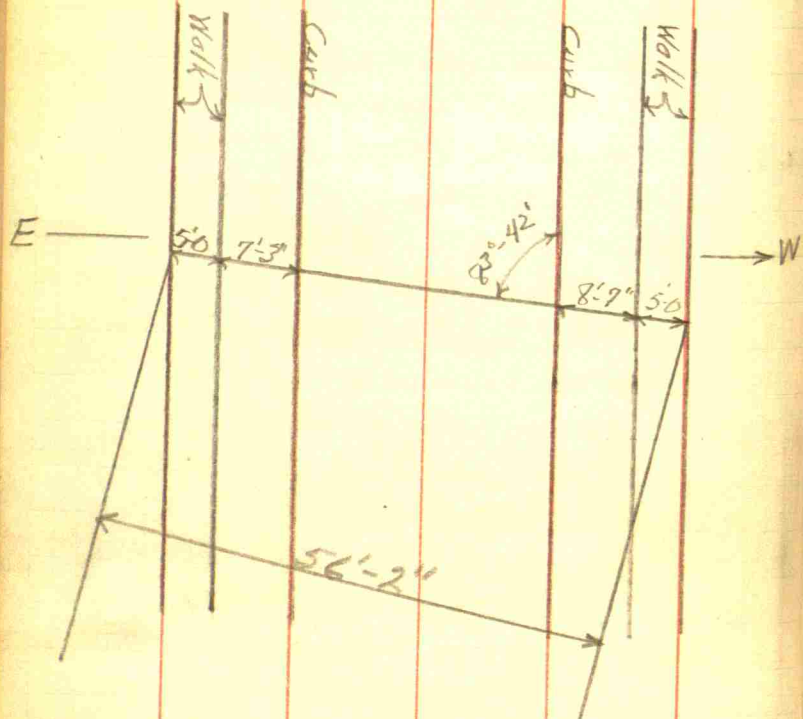
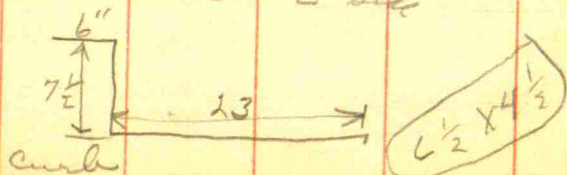


2

CALIFORNIA ST. BRIDGE



Side Walk - 15 - E side
 Curb - 15 - E side



3

Levels on Calif. St. Bridge

Sta.	B.S.	HI.	F.S.	Elev.
	3.76	-	103.76	100 Top Side Walk, W. Side South of tree.
T.W.S. W. side			4.06	99.70
Fl. W side			10.50	93.26
T. Curb W. side			4.95	99.01
Bot. Curb W. side			5.30	98.46
St. Street			4.58	99.19
Bot. Curb E. side			5 @ 4.63	99.13, 98.13
Top curb E. side			5.06	98.70
Top SW E side			4.81	98.93
Fl. E. side				93.88
			5 @ 11.9	91.86
			11.12	92.64
100' Downstream			12.36	91.40
100' Upstream			9.2	94.56

4

LEVELS ON Road Ditch draining to Boyless Ditch

Sta	BS	HI	FS	Elev
Bm	1.77	131.30		129.53

0+00

1+00

2+00

3+00

4+00

0

7

5+00

6+00

7+00

8+00

9+00

4.90 132.13

4.07 127.23

5

West End South Bridge Rail

IR	5	10	10	12	15	17.5	18	27	Level
3.78	3.6	3.71	3.15	2.55	2.8	2.8	2.2	5.0	
127.52	127.90	128.59	131.5	132.5	131.5	131.5	130.5	122.10	126.30

IR	6.5	9.5	11.5	16.5	21	22.5	27.5	29.5	Level
4.1	4.9	5.2	7.2	9.2	9.6	7.5	6.2		
126.37	126.40	126.10	124.10	122.10	121.0	123.50	123.10		

IR	6	10	14	17	20	23	25	Level
4.72	4.67	5.3	6.5	7.4	7.2	6.6	5.2	
126.58	126.63	126.00	124.80	121.90	122.10	124.70	126.10	

IR	6	10	12	14	17	18	22	26	28	30	Level
4.77	4.72	5.1	5.8	7.2	8.1	9.0	8.7	5.7	5.6	5.6	
126.53	126.58	126.20	125.50	124.10	123.20	122.30	122.60	125.60	125.70	125.70	

IR	7	12	15	18	21	25	31	Level
4.48	4.4	4.7	5.6	8.6	8.4	5.3	5	
126.82	126.90	126.60	125.00	122.90	122.90	126.00	126.30	

For 5+21
- 1004

IR	6	13	18	17	22	25	28	29	Level
4.95	4.90	5.7	7.2	9.2	9.4	6.4	5.8		
127.18	127.23	126.93	124.93	122.93	122.93	125.73	126.33		

IR	6	12	14	16	19	22	25	Level
5.10	5.1	6.1	7.0	8.9	8.6	6.3	5.2	
126.79	126.83	126.03	125.13	122.23	123.53	124.33	126.73	

6+25 to 21
surface

IR	7	9	13	14	16	17	21	24	Level
5.02	4.98	5.3	7.3	8.7	8.7	7.6	6.7	5.1	
127.11	127.15	126.85	124.83	123.13	123.43	124.53	126.43	127.03	

IR	6	9	15	19	21	27	Level
4.5	4.9	6.8	7.8	8.4	6.2	4.7	
127.63	127.23	126.33	124.33	123.93	122.93	127.43	

8+26 to 21
Level8+25 to 21
surface

IR	7	11	16	19	21	28	Level
3.61	2.5	4.3	6.2	7.8	7.4	4.3	
127.82	127.62	127.83	125.73	124.33	124.53	127.63	

9+23 to 21
surface10+16 to 17
10+12 to 17

		132.13		
10+00				
0			3.15	128.98
π	5.75	134.73		
11+00				
11+32	Bridge Floor		9.70	125.03
12+00				
13+00				
0			4.71	130.02
π	4.58	134.60		
14+00				
16+00				
18+00			4.2	
0			4.25	130.36
π	5.14	135.49		
20+00				
22+00				
24+00				

#R	7	12	15	17	19	24	30	Final
5.32	5.2	3.4	4.6	6.6	7.4	7.4	3.9	
128.57	128.93	128.73	129.53	125.53	129.73	129.73	128.23	

#R	7	10	15	18	18	21	25	32	Final
5.85	5.2	5.6	8.2	8.6	9.7	9.7	7.6	6.8	
129.38	129.53	129.13	126.53	126.13	125.03	125.03	127.13	128.93	

#R	7	13	16	20	22	27	30	32	Final
5.05	5.1	5.8	7.2	9.3	9.1	8.4	7	6.4	
129.69	129.63	128.93	129.53	125.93	125.63	124.33	127.73	128.33	

#R	8	16	16	21	25	28	24	Final
4.85	5.1	4.85	8.9	8.7	8.3	7	6	
129.89	129.63	129.88	125.63	125.93	126.93	127.73	128.73	

MEMORIAL WALL
at Top of Lock

#R	8	15	20	22	27	29	33	35	Final
4.85	5.1	5.6	8.5	8.7	8.7	8	5.0	5.0	
129.95	129.50	128.00	126.10	125.90	125.90	126.60	129.30	129.60	

#R	8	17	17	22	25	28	30	32	35	Final
4.65	4.8	5.7	7.7	8.5	8.7	7.6	6.3	5.6	5.6	
129.95	129.90	128.80	126.80	126.10	124.30	124.00	128.30	129.00	129.00	

#R	8	12	21	24	31	35	Final
4.35	4.45	5	8.2	8.1	5.7	5.7	
130.25	130.15	129.60	126.90	126.20	128.90	128.90	

#R	8	13	21	25	32	34	Final
5.15	5.22	5.7	9.2	9.4	6.7	6.3	
130.34	130.17	130.32	126.29	126.09	129.99	129.19	

#R	8	13	17	19	22	26	32	30
4.75	5.0	5.6	7.3	8.5	8.9	8.8	5.7	6.1
130.74	130.49	129.89	128.19	126.99	126.59	126.69	129.99	129.39

#R	8	14	19	27	31	33	Final
4.4	4.7	5.1	8.2	7.9	5.5	5.5	
131.09	130.79	130.29	127.29	127.59	129.99	129.99	

8

135.79

0

4.33 131.16

K

6.21 137.47

26+00

28+00

30+00

30+62

2M

3.98 133.49

3.04
2.00

9

ER	8	12	14	17	19	25	21	33	From
5.19	6.05	6.3	7.2	9	9.9	9.7	7.3	7	
131.58	131.82	131.19	130.27	128.47	127.57	127.77	126.17	130.47	

ER	8	14	19	28	33	From
4.92	5.1	5.4	9.3	9.4	6.3	
132.55	132.57	132.87	129.17	128.87	131.17	

ER	8	14	23	28	33	From
4.12	4.3	5	9.2	9.1	7.1	
133.35	133.17	132.97	128.29	128.27	130.87	

ER	9	14	21	23	28	28	33	From
3.9	4.0	4.7	9.4	9.3	9.2	6.4	5.7	
133.57	133.47	132.77	129.07	128.17	128.87	121.07	131.87	

total E. ...

10

LEVELS ON MALONEY ROAD

Sta	BS	HI	FS	Elev
BM	4.99	115.27		110.30
98+0				
97+0				
96+0				
95+0				
94+0				
93+19 P				
93+0				
92+50				
⊙			4.24	111.03
⊖	4.13	115.16		
BM			4.59	110.57 (110.53)
92+0				
91+68 PC				
91+0				
90+0				
89+0				
88+0				
87+0				
⊙			3.16	112.0
⊖	4.38	116.38		
86+0				
85+0				

11

West + South

East + North

West + South	East + North
	5.62 109.65
	4.47 110.80
	4.01 111.26
	3.10 112.17
	3.82 111.45
	4.32 110.95
4.82	
4.24	
5.12	110.04
	4.03 111.13
	3.22 111.94
	3.92 111.24
	3.93 111.23
	3.35 111.81
	3.16 112.00
	6.04 110.34
	6.20 110.18

	BS	HI	FS	
84+00		116.38		
83+0				
82+0				
81+0				
80+07 PT				
○			1.86	114.52
π	5.01	119.53		
80+0				
BM			5.02	114.51 (114.49)
79+50				
79+0				
78+80 PC				
78+0				
77+0				
76+0				
75+0				
○			5.59	113.94
π	7.63	121.57		
74+0				
73+0				
72+40 PT				
72+0				
71+50				
71+0				

West + South

East + North

	5.41	110.97
	4.73	111.65
	4.32	112.06
	2.72	113.66
	1.86	114.52
	5.02	119.51
	4.39	113.19
	4.56	114.97
	3.89	115.64
	4.0	115.53
	5.57	113.96
	5.72	113.81
	3.91	115.62
	5.56	116.01
	4.60	116.97
	3.92	117.65
	4.64	116.93
	5.05	116.52
	5.55	116.00

14

sta	BS	HI	FS	
		121.57		
BM				
⊗			5.02	116.55 (116.57)
70+89.5 RC.				
70+0				
69+0				
68+0				
⊙			4.44	117.13 ✓
⌞	6.82	123.95		
67+0				
66+0				
65+0				
64+0				
63+0				
62+0				
⊙			3.34	120.61 ✓
⌞	4.16	124.77		
61+0				
60+0				
59+0				
58+0				
⊙			4.98	119.79 ✓
⌞	4.80	124.59		
57+0				

15

West + South

East + North

5.72

115.85

5.90

115.67

5.29

116.28

4.44

117.13

6.01

117.94

5.59

118.36

5.18

118.77

4.0

119.95

2.77

121.18

3.34

120.61

4.88

119.89

5.57

119.20

5.41

119.36

5.18

119.59

4.29

120.20

16

Sta	BS	HI	FS	
56+00		124.59		
55+0				
①				
⌈	4.15	123.18	5.56	119.03 ✓
54+0				
53+0				
52+0				
①				
⌈	3.78	122.56	4.40	118.78 ✓
51+0				
50+0				
49+0				
48+0				
47+0				
46+0				
45+0				
①				
⌈	3.79	122.27	4.08	118.48 ✓
45+0				
44+0				
43+0				
42+0				
41+0				

17

West + South

East + North

4.84	119.75
4.27	120.32
3.74	119.94
3.98	119.20
3.48	119.70
3.06	119.50
4.26	118.30
3.96	118.60
2.25	120.31
3.28	119.28
4.05	118.57
4.63	117.64
5.04	117.23
4.98	117.29
5.24	116.93
4.77	117.50

18

Sta	BS	HI	FS	
		122.27		
40+0				
⊙			5.28	116.99
⌞	5.09	122.08		
39+0				
38+0				
37+0				
36+0				
35+0				
⊙			3.26	118.82
⌞	3.16	121.98		
34+0				
+ 33+0				
32+85.7c				
32+50				
32+0				
31+35pc				
31+0				
BM			5.74	116.24 117.29
⊙ ₃₅			3.16	118.82
⌞	3.46	122.28		
⊙ ₃₄			5.29	116.99
⌞	5.22	122.21		
⊙ ₃			3.76	118.45
			4.58	117.63 - Strauss

19

West + South

East + North

5.28 116.99

4.63 117.45

3.69 118.39

2.60 119.48

2.10 119.98

3.26 118.82

4.49 117.49

5.58 116.40

5.91 116.07

6.43 115.55

6.32 115.96

5.80 116.18

4.68 117.30

				118.45	
π	4.12	122.57			
o			3.82	118.75	
+	4.90	123.65			
			4.22	119.03	
·T	5.56	124.59			
			4.80	119.39	
T	4.82	124.61			
			3.98	120.63	
T	3.14	123.77			117.12
			6.58	117.19	
+	3.45	120.24			
			3.97	116.67	114.03
			6.64	114.02	113.94
					7-
3M				119.29	
T	6.92	124.21			
o			5.36	118.85	
T	3.78	122.63			
o			4.36	118.27	
T	2.99	121.26			
	3.69		1.24	1200.2	119.97
	10.96			117.29	
	2.13		10.96	2.73	

22

Sta BM	BS	HI	FS	
70+89.5 Fe	4.51	121.08		116.57
70+0				
69+0				
68+0				
67+0				
66+0				
0			2.74	118.34
⌊	7.92	126.26		
65+0				
64+0				
63+0				
62+0				
61+0				
60+0				
0			7.05	119.21
⌊	5.21	124.42		
59+0				
58+0				
57+0				
56+0				
55+0				
0			4.09	120.33
⌊	2.24	122.57		

23

West + South

East + North

5.48	115.60
5.45	115.63
4.87	116.21
3.98	117.10
3.19	117.89
2.74	118.34

7.51	118.75
6.32	119.94
5.14	121.13
5.67	120.59
6.35	119.91
7.05	119.21

5.09	119.33
4.88	119.54
4.16	120.26
4.69	119.73
4.09	120.33

24

Sta	BS	HI	FS	
		122.57		
54+0				
53+0				
52+0				
51+0				
50+0				
49+0				
0			3.98	118.59
⌵	4.44	123.03		
48+0				
47+0				
46+0				
45+0				
44+0				
0			5.74	119.29
⌵	4.35	121.64		
43+0				
42+0				
41+0				
40+0				
0			3.56	118.08
⌵	5.78	123.86		
39+0				
38+0				

25

West + South

East + North

2.30	119.27
3.38	119.19
2.37	119.90
3.09	119.48
4.28	118.29
3.98	118.59
2.74	120.29
3.91	119.12
4.54	118.99
5.28	119.65
5.74	119.29
4.21	119.33
4.68	116.96
4.15	117.49
4.62	117.02
6.22	117.64
5.32	118.54

26

37+0

BS

HI

FS

123.86

37+0

36+0

35+0

34+0

0

T

A.O

121.68

6.18

117.68

33+0

32+85

32+50

32+0

31+35A

31+0

BM

5.25

116.43

27

West + South

East + North

4.23

119.63

3.72

120.17

4.85

119.01

6.18

117.68

5.1

116.58

5.42

116.26

6.16

115.52

5.15

115.93

5.26

116.42

4.2

117.48

28

π	4.60	124.57		119.97
0			7.62	116.95
π	8.71	125.66		
0			4.72	120.94
π	2.20	123.44		
0			12.24	110.80
π	.77	111.57		
0			6.31	105.26
π	6.98	112.24		
0			7.62	104.62
π	3.19	107.81		
T.R. 5s			1.95	106.56
T.R. 6s			4.53	103.28
T.R. 7s			1.30	106.57
T.R. 8s			4.37	102.44

29

30

T	6.80	124.09			
0			5.35	118.74	
T	4.31	123.05			
0			5.53	117.52	
T	6.76	124.28			
0			5.09	119.19	
T	5.40	124.59			
			.11	124.48	
0			4.07	120.52	
T	4.98	125.50			
0			4.73	120.77	
T	4.12	124.89			
0			6.72	118.17	
T	3.34	121.51			
71+ BM			3.87	117.64	116.57

117.29

BM Sta 32 + 30

Post No. 5375

31

32

BM

T

4.32 124.29

O

1.61 122.68

T

6.02 128.70

16+66

17+0

16+60

16+0

15+0

14+81

14+27

14+0

13+73

O

4.55 124.15

T

.45 124.60

12+00

12+00

10+12

10+0

9+53

O

11.61 112.99

T

1#3 114.72

11+15

11+0

9+0

119.99

West + South

4.1 124.29

5.94 122.76

4.30 124.40

4.02 124.68

5.67 123.03

5.57 123.19

4.58 124.12

4.31 124.39

4.55 124.15

2.33 122.27

10.10 114.50

11.61 112.99

10.91 113.69

11.90 112.70

9.70 105.02

8.12 106.59

2.74 111.98

33

34

	114.72		
8+80			
8+03			
0		3.46	111.26
π	6.49	117.95	
8+0			
7+24			
7+23			
7+0			
6+40			
6+0			
5+0			
4+0			
3+0			
0		7.13	110.62
π	.96	111.58	
2+0			
1+0			
0+0			
SEnd Ero. Top		5.22	106.36

35

West + South

2.70	112.02
3.46	111.26
6.51	111.24
9.0	108.75
8.75-	109.00
7.84	109.91
6.51	111.24
5.29	112.46
4.50	113.25
5.70	112.05
7.12	110.62
4.21	107.37
9.09	102.49
10.91	100.67

36

BM	B.S	H.I	FS	
T	6.03	126.00		119.97
18+0				
FT. 18+14				
19+0				
20+0				
0			10.53	115.47
T	7.08	122.55		
21+0				
22+0				
23+0				
24+0				
0			5.05	117.50
T	5.22	122.72		
25+0				
26+0				
27+0				
28+0				
29+0				
0			2.63	119.09
T	5.26	124.35		
29+73.				
30+0				
30+50				
BM			7.12	117.23

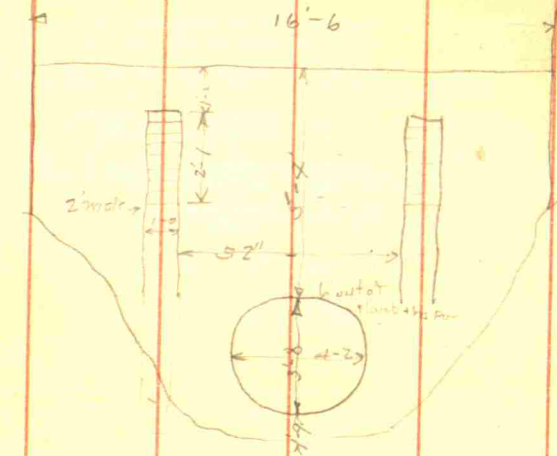
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Stake S. Side

3.97	122.03
3.54	122.46
4.14	121.86
8.20	117.80
8.81	113.14
3.91	118.64
4.56	117.99
3.53	119.02
4.57	118.15
4.60	118.12
4.22	118.50
2.82	119.90
3.50	119.22
5.46	118.89
5.41	118.94
5.89	118.46

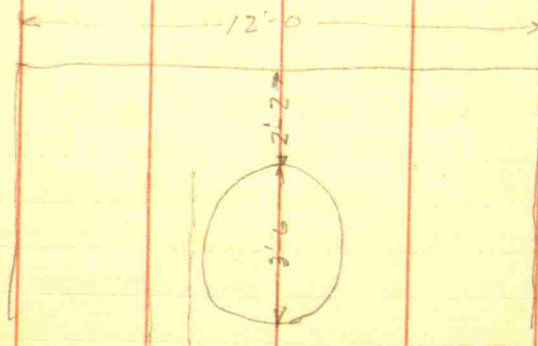
38

ARBUCKLE BRIDGE

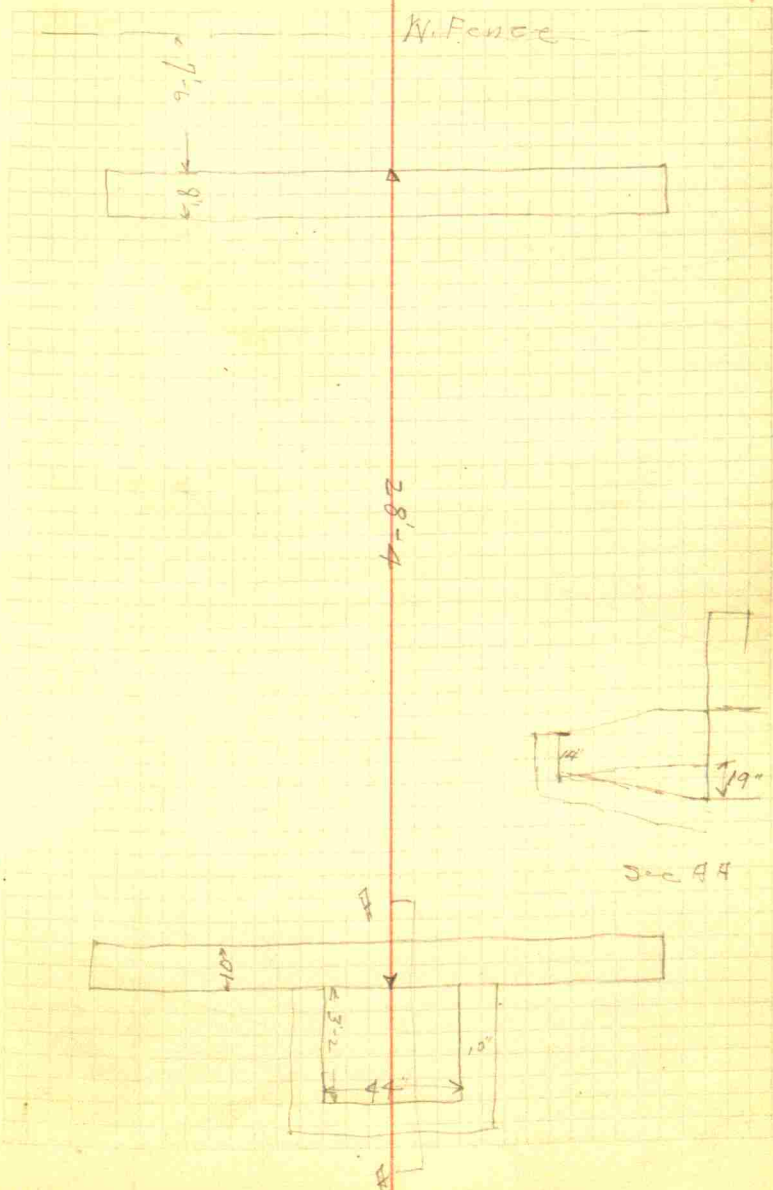


Length Barrier 15'-8"

West Elevation



39



40

BM

T

5.90

105.90

100

FL End	11.2	94.70
Esde Box	9.91	95.99
S. in Ditch	9.45	96.45
E. Wall Box	8.63	97.27
N. in Ditch	9.25	96.65
☞ Road	5.60	100.30
Top W. Hdwl	6.32	99.58
FL W. End Boiler	15.33	90.57
FL W. End Gravel	17.0	88.90

41

Center E. Hdwl Top

42

STOUT-RICHARDSON DITCH

Sts BM	BS	HI	FS	Elev
	2.11	102.11 ✓		100
0+00 ○				
π	2.34	102.22 ✓	2.22	99.88 ✓
1+00				
2+00 ○				
π	5.39	98.68 ✓	8.92	93.29 ✓
3+00				
4+00				
5+00				
6+00 ○				
π	4.07	98.44 ✓	4.31	94.37 ✓
7+00 ○				
π			4.45	93.99 ✓
8+00 π	4.19	98.18 ✓		
9+00				
10+00 ○				
π	4.85	98.89 ✓	4.14	94.04 ✓

8-22-32

12.02
12.01

FRANKLIN-LIBERTY TUNNS

43

On Concrete at NE shoe of Bridge over Mud Creek
about 100' south of mouth of Ditch
stake

stream			
3.27	98.84	16.60	85.51
5.39	96.83	15.74	86.37
9.01	93.21	15.17	87.03
4.42	94.26	10.99	87.69
4.52	94.16	10.60	88.08
4.83	93.85	10.04	88.64
4.31	94.37	10.15	88.53
4.14	94.30	10.05	88.39
4.45	93.99	10.05	88.39
4.20	93.88	9.54	88.64
4.14	94.04	9.20	88.98

Sta	BS	HI	FS	Elev
		98.89		
11+00				
12+00				
13+00				
14+00				
0			4.38	94.51 ✓
⌊	4.78	99.29 ✓		
15+00				
16+00				
17+00				
BM			.74	98.55 ✓
⌊	1.58	100.13 ✓		
18+00				
19+00				
20+00				
21+00				
22+00				
23+00				
0			3.78	96.35 ✓
⌊	4.20	100.55 ✓		
24+00				
25+00				
26+00				
27+00				

Stake	stream
4.47 94.42	9.10 89.79
	9.93 88.86
4.54 94.35	9.15 89.74
4.38 94.51	9.12 89.77
4.23 95.06	9.60 89.69
4.89 94.40	9.14 90.15
4.30 94.99	8.66 90.63
Center West Rail 1st Road Crossing Ditch N+S	
5.01 95.12	9.91 90.22
	10.58 89.55
4.57 95.56	9.43 90.70
4.36 95.77	9.48 90.65
4.13 96.00	9.00 91.13
3.78 96.35	9.14 90.99
4.32 96.22	9.21 91.34
4.29 96.26	9.25 91.30
5.21 95.34	8.94 91.61
4.33 96.22	8.68 91.87

Sto	BS	HS	FS	EL
		100.55		
28+00				
29+00				
30+00				
⊙			3.38	97.17 V
π	5.45	102.62 V		
31+00				
32+00				
33+00				
34+00				
35+00				
36+00				
37+00				
⊙			4.38	98.24 V
π	4.44	102.68 V		
38+00				
39+00				
40+00				
41+00				
42+00				
43+00				
⊙			7.58	95.10 V
π	7.36	102.46 V		
44+00				

stake	stream
3.74 96.81	8.66 91.89
3.84 96.71	8.65 91.90
3.38 97.17	8.56 91.99
5.13 97.49	10.48 92.14
5.39 97.23	10.32 92.30
4.06 98.56	10.11 92.51
4.36 98.26	9.95 92.67
3.82 98.80	9.98 92.64
4.57 98.05	9.76 92.86
4.38 98.24	9.84 92.78
3.95 98.73	9.35 93.33
4.42 98.26	9.61 93.07
4.64 98.04	9.32 93.36
4.57 98.11	8.87 93.81
4.13 98.55	9.12 93.56
4.09 98.59	9.00 93.68
3.80 98.66	8.53 93.93

48

sta	Bs	HI	Fs
45+00		102.46	
46+00			
47+00			
48+00			
49+00			
50+00			
51+00			
○			
⌊	3.37	104.05 ✓	1.78 100.68 ✓
52+00			
53+00			
54+00			
55+00			
56+00			
57+00			
58+00			
○			
⌊	4.74	105.92 ✓	2.87 101.18 ✓
59+00			
60+00			
61+00			
○			
⌊	4.76	106.19 ✓	4.49 101.43 ✓

← LETTER →

49

stake		stream	
3.96	98.50	8.61	93.85
3.66	98.80	8.56	93.90
2.98	99.48	8.56	93.90
3.02	99.43	8.35	94.11
3.12	99.33	8.75	93.71
2.50	99.96	8.75	93.71
1.78	100.68	8.70	93.76
3.16	100.89	9.60	94.45
2.62	101.43	9.70	94.35
3.22	100.83	9.86	94.19
3.57	100.48	9.53	94.52
3.66	100.39	9.26	94.79
3.27	100.78	9.17	94.88
2.87	101.18	8.95	95.10
4.24	101.68	10.76	95.16
5.45	100.47	10.22	95.70
4.50	101.42	10.21	95.71

50

sta	BS	HI	Fs
		106.19	
62+00			
63+00			
64+00			
⊙			4.60 101.59 ✓
⊥	4.80	106.39 ✓	
65+00			
66+00			
⊙			3.38 103.01 ✓
⊥	2.34	105.35 ✓	
67+00			
68+00			
69+00			
70+00			
71+00			
⊙			3.98 101.37 ✓
⊥	4.54	105.91 ✓	
72+00			
73+00			
74+00			
75+00			
76+00			
⊙			3.80 102.11 ✓
⊥	4.97	107.08 ✓	

← LETTER →

51

stake		stream	
4.57	101.62	10.35	95.84
4.78	101.41	10.44	95.75
4.60	101.59	9.83	96.36
4.48	101.91	10.00	96.39
4.47	101.92	9.90	96.49
		9.01	96.34
4.18	101.17	9.47	95.88
3.72	101.63	9.10	96.25
3.74	101.61	9.20	96.15
3.98	101.37	8.66	96.69
4.51	101.40	9.00	96.91
4.10	101.81	9.06	96.86
4.59	101.32	8.95	96.96
4.90	101.01	8.60	97.31
3.80	102.11	8.64	97.27

52

Sta	BS	HI	I-S	
		107.08		
77+00				
78+00				
79+00				
80+00				
○			4.34	102.74 ✓
↑	3.26	106.20 ✓		
81+00				
82+00				
○			3.23	102.97 ✓
↑	5.20	108.17 ✓		
82+00				
83+00				
84+00				
○			3.09	105.08 <i>Platypus</i>
↑	3.44	108.52 ✓		
85+00				
86+00				
87+00				
88+00				
89+00			3.65	
○			3.63	104.89 ✓
↑	3.86	108.75 ✓		
90+00				

53

Stake		Stream	
4.56	102.52	9.45	97.63
4.91	102.17	9.46	97.62
4.55	102.53	9.40	97.68
4.24	102.74	9.05	98.03
3.45	102.75	8.42	97.77
3.28	102.97		
		10.15	98.02
5.17	103.00	9.68	98.49
5.92	102.25	12.04	98.13
4.89	103.64	10.10	98.42
3.44	105.08	9.60	98.92
3.96	104.56	10.25	99.27
3.22	105.30	9.35	99.17
3.63	104.89	9.42	99.10
3.90	104.85	9.40	99.35

54

Sta	BS	HI	FS
		108.75	
91+00			
92+00			
93+00			
94+00			
95+00			
①			3.52 108.23 ✓
II	4.41	109.64 ✓	
96+00			
97+00			
98+00			
99+00			
100+00			
101+00			
102+00			
103+00			
104+00			
②			5.37 102.25 ✓
III	7.45	111.70 ✓	
105+00			
106+00			
107+00			
108+00			
109+00			

← LETTER →

55

Stake	Stream
4.00 104.75	9.15 99.60
3.37 105.36	8.92 99.83
	8.52 100.23
5.28 103.37	8.06 100.69
3.52 105.23	7.90 100.85
4.53 105.11	8.52 101.12
5.09 104.55	7.80 101.84
4.63 105.01	8.50 101.14
4.08 105.56	8.16 101.48
3.90 105.74	7.88 101.76
4.57 105.05	7.68 101.96
3.83 105.76	7.00 102.14
2.78 106.86	7.60 102.04
4.50 105.14	6.55 103.09
4.79 106.91	9.40 102.30
4.36 107.34	9.15 102.55
4.32 107.58	9.24 102.46
3.74 107.96	9.16 102.54
3.52 108.18	9.15 102.55

56

sta	B ₆	HI	FS	
		111.70		
110+00				
111+00				
112+00				
113+00				
B ₁₇				
⊥	4.56	113.87	2.39	109.21 ✓
114+00				
115+00				
116+00				
117+00				
118+00				
0				
⊥	4.29	114.00	4.16	109.71 ✓
119+00				
120+00				
0				
⊥	5.61	114.82	4.79	109.21 ✓
121+00				
122+00				
0				
⊥	4.92	115.29	4.45	110.37 ✓
123+00				
124+00				

57

stake		stac w	
3.55	108.15	8.90	102.80
3.55	108.15	8.55	103.15
2.78	108.72	8.31	103.39
2.25	109.45	8.10	103.60
Top Curb South End East Rail sta 113+25			
4.78	109.09	9.65	104.22
4.53	109.34	7.55	104.32
5.27	108.60	9.26	104.61
4.93	108.94	9.21	104.66
4.16	109.71	8.61	105.26
3.49	110.51	8.08	105.92
4.79	109.21	8.19	105.81
5.31	109.51	8.94	105.88
4.45	110.37	8.50	106.32
4.57	110.72	8.32	106.47
3.98	111.31	8.64	106.65

58

59

Sta	BS	HI	FS	
125+00		115.29		
126+00				
⊙			3.50	111.79 ✓
⊥	4.18	115.97 ✓		
127+00				
128+00				
129+00				
130+00				
⊙			3.48	112.49 ✓
⊥	3.79	116.28 ✓		
131+00				
132+00				
133+00				
134+00				
⊙			2.38	113.90 ✓
⊥	5.32	119.22 ✓		
135+00				
136+00				
137+00				
138+00				
⊙			3.13	116.09 ✓
⊥	4.36	120.45 ✓		
139+00				

Stake		Stream	
3.69	111.60	8.53	106.76
3.50	111.79	8.38	106.91
4.76	111.21	8.53	107.44
4.38	111.59	8.04	107.93
3.18	112.79	8.20	107.77
3.48	112.49	7.61	108.36
2.74	113.54	8.05	108.23
2.45	113.83	7.82	108.46
2.56	113.72	7.61	108.67
2.38	113.90	7.15	109.13
		9.96	109.26
4.23	114.99	9.45	109.74
4.11	115.11	9.60	109.62
3.13	116.09	9.60	109.62
4.71	115.74	10.18	110.27

60

Sta	Bs	HI	FS
		120.45	
140+00			
○			
π	4.75	121.59 ✓	3.61 116.84 ✓
141+00			
142+00			
143+00			
144+00			
○			
π	4.14	122.50 ✓	3.23 118.36 ✓
145+00			
146+00			
147+00			
148+00			
○			
π	5.73	124.18 ✓	4.05 118.45 ✓
149+00			
150+00			
151+00			
152+00			
+50			
BMP 1	1.50	101.50	16.46 85.04

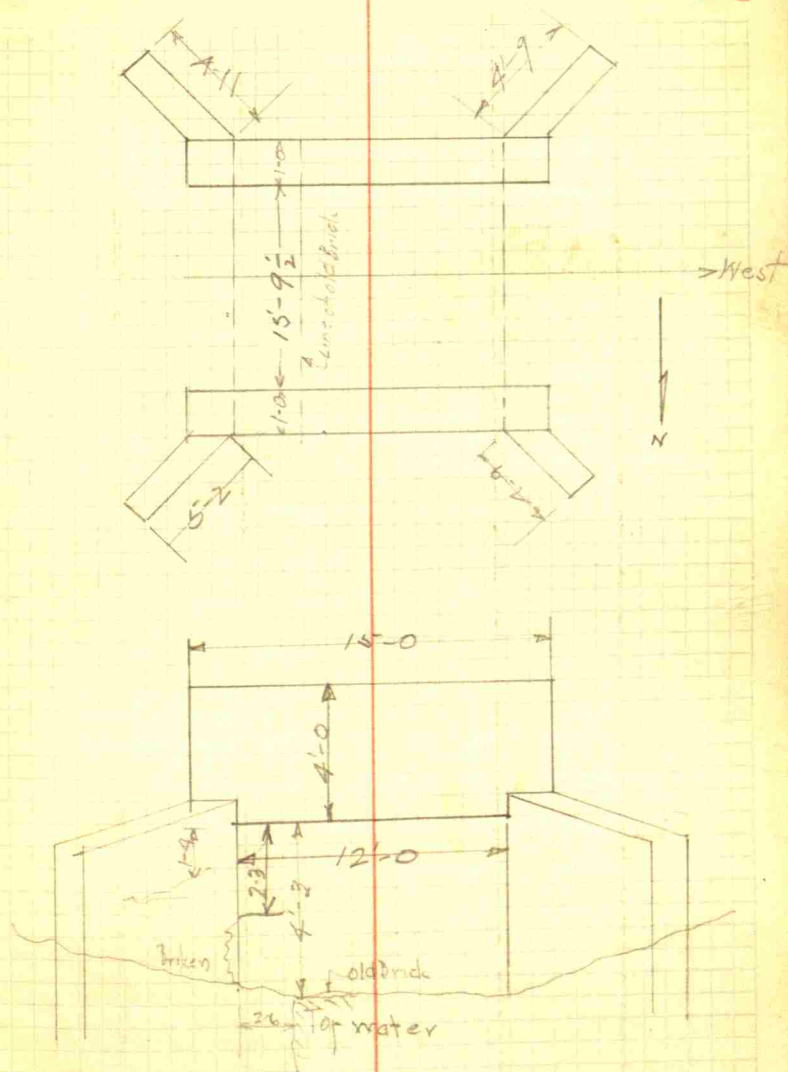
61

stake	stream
3.61 116.84	10.18 110.29
5.16 116.43	10.45 110.64
4.55 117.04	10.69 110.90
3.83 117.76	10.35 111.24
3.23 118.36	10.22 111.37
3.98 118.52	10.72 111.78
4.21 118.29	10.13 112.37
3.78 118.72	9.78 112.72
4.05 118.45	9.30 113.20
4.72 119.46	10.55 113.63
4.47 119.71	10.02 114.14
3.78 120.40	9.42 114.76
4.81 119.37	8.55 115.63
2.70 121.48	7.80 116.38

62

First Bridge West of New Winchester Road
on New Marysville Road

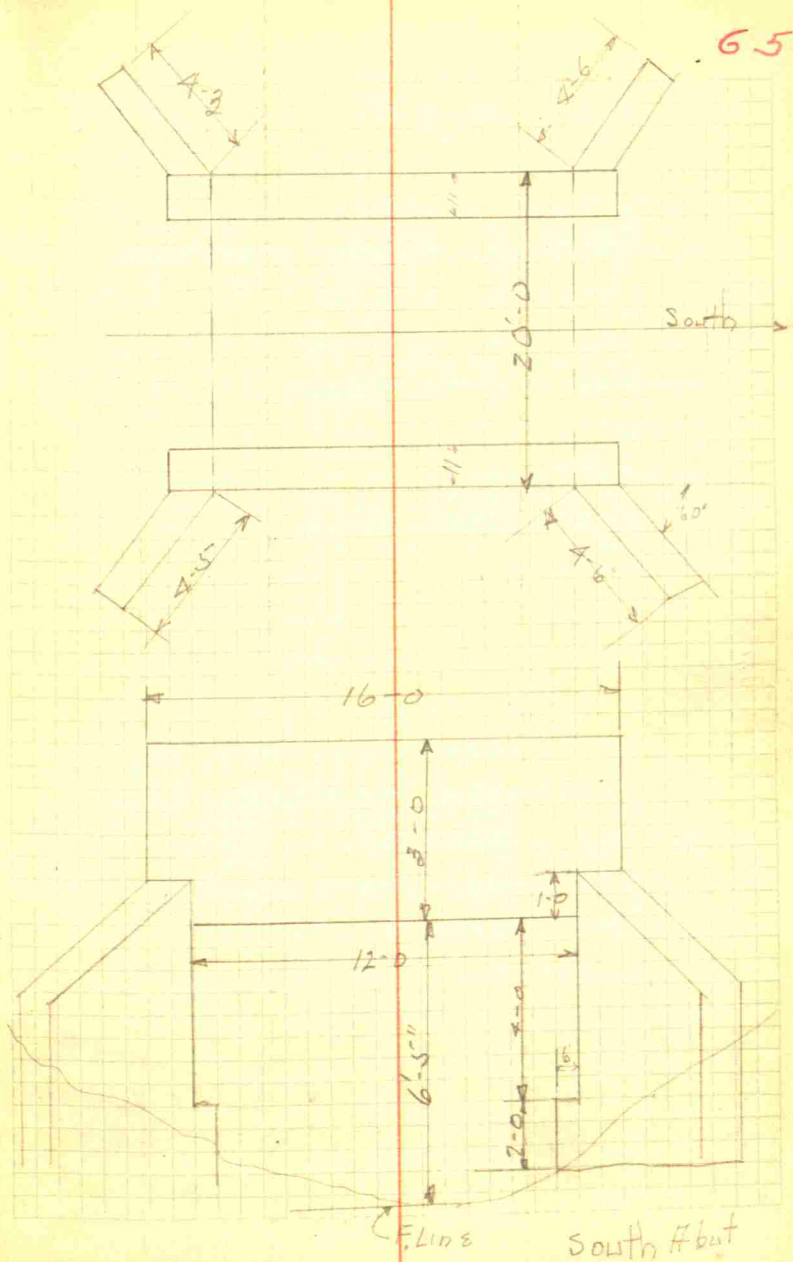
63



Under Pin East wall only

64. First Bridge South of steel Bridge
on Jamestown Road

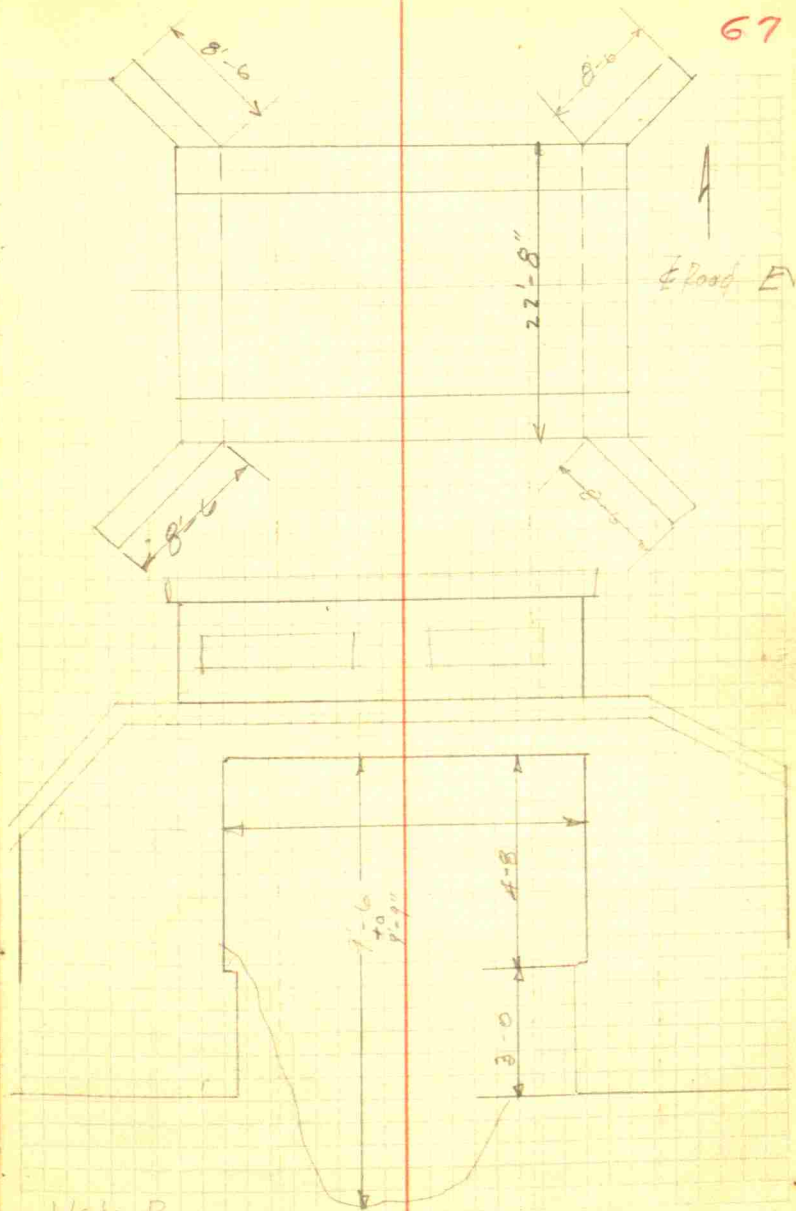
65



66

M. CORD #2

67

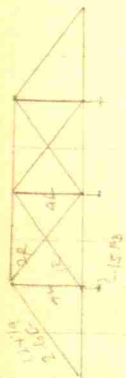


68

STEEL BRIDGE on County hwy

15'-6 1/4" out to out 6E on outside
16'-Timber

Height - 6'-9"
4 Panels



6E - 2" Flyer

6E

6E

6E

6E

6E

6E

6E

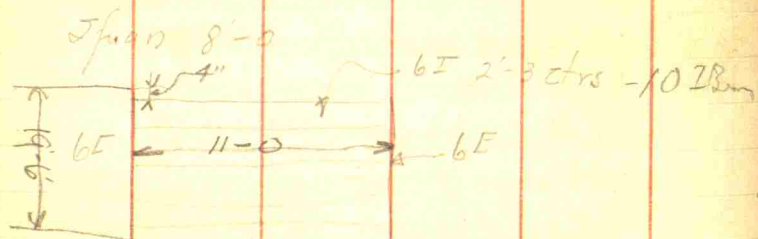
5'-2"

69

Mud silt at End 10' w x 10' h
Top of E + I Beams - 8' from Bottom of Mudsilt

70

Cane Bridge South of Hardswood



Hand Rails 24'-0

Height FL to Bottom Slab 4'-6"

Length - 20'-0

Have tile Ditch over on East side
coming from North -

71

King Bridge from Union

For box 4'-0 in 22 - 3'-0 in 22
 width of 20' 31'-8"
 20' - culvert or 22 for 26 roadway

42 HARVEY Bridge 30'-000
 30 11'-6 high
 13
 19
 11

7'-6

11'-6

72

Relocation. Ice River Trap Sec 22+15-17-20

BM				100
0	9.62	107.62		
T	1.25	98.87	12.00	97.62
100' S down			9.04	89.73
200' "			9.95	88.92
300' "			9.55	89.32
0+00				
0			1.25	77.62
T	9.85	107.47		
1+00				
2+00				
0			1.06	106.41
T	.66	107.07		
2+50				
3+00				
3+10				
3+50				
4+00				

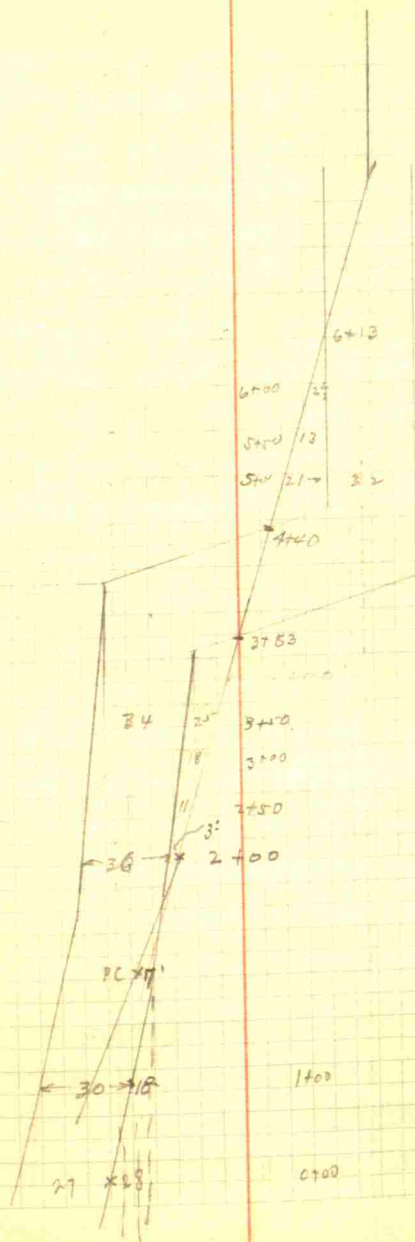
73

Nail in Pear tree 50' East Sta 2+25

E				€	W							
<u>41</u>	<u>38</u>	<u>34</u>	<u>31</u>	<u>24</u>	<u>16</u>	<u>8</u>	515.8	<u>6</u>	<u>12</u>	<u>19</u>	<u>21</u>	<u>40</u>
6.83	7.72	8.74	9.92	8.88	7.95	6.17	93.29	5.66	6.0	2.04	5	
102.25	115.81	15	89.95	91.02	90.22	92.10		93.21	92.87	96.83	93.87	
<u>33</u>	<u>18</u>	<u>13</u>	<u>8</u>					<u>2</u>	<u>16</u>	<u>20</u>	<u>27</u>	<u>49</u>
6.83	5.28	8.61	8.34					7.83	7.54	8.3	7.41	1.6
100.64	102.19	98.26	99.13					99.64	99.93	99.17	100.06	105.87
		<u>30</u>	<u>24</u>						<u>7</u>	<u>19</u>	<u>27</u>	<u>30</u>
		3.28	2.88						1.54	2.8	2	2.72
		104.11	104.59					105.81	105.93	105.67	105.47	104.75
											105.60	107.37
		<u>30</u>	<u>22</u>	<u>16</u>					<u>11</u>	<u>15</u>	<u>25</u>	<u>38</u>
		6.63	6.1	4.8					2.82	2.3	2.79	3.36
		100.44	100.97	102.27					104.25	103.17	106.29	103.71
		<u>30</u>	<u>23</u>	<u>20</u>	<u>12</u>				<u>18</u>	<u>22</u>	<u>23</u>	<u>24</u>
		11.0	10.38	10.4	3.72				6.6	5.7	4.21	3.64
		96.07	96.62	96.67	97.35				98.23	100.37	101.29	102.86
											103.32	
			<u>31</u>						<u>21</u>	<u>24</u>	<u>28</u>	<u>43</u>
			13.8						6.85	5.24	4.2	3.4
			93.27						100.22	101.47	102.87	103.67
			<u>30</u>						<u>24</u>	<u>26</u>	<u>32</u>	<u>40</u>
			11.84						4.4	4.65	5.8	5.67
			95.23						99.52	102.67	102.42	103.27
											103.46	
		<u>22</u>	<u>18</u>	<u>15</u>	<u>10</u>	<u>9</u>	<u>6</u>		<u>7</u>	<u>15</u>	<u>26</u>	<u>30</u>
		10.2	8.44	8.42	2.15	1.65	4.7		4.66	4.78	5.31	4.3
		98.25	99.52	98.22	98.65		101.42		107.17		102.77	
							99.97				102.17	
											102.41	102.29
											101.57	102.77

76

77



78

STAKES FOR TILE DITCH MALONEY

Sta	BS	HI	FS	Elev
	9.00	123.07		114.07
51+00				
50+00				
49+00				
48+00				
47+00				
o			4.24	118.83
T	3.20	122.03		
46+00				
45+00				
44+00				
43+00				
o			4.10	117.93
T	4.10	122.03		
42+00				
41+00				
40+00				
39+00				
T	9.99	124.06		114.07
53+00	(10.00)	(124.07)		
54+00				
55+00				

79

ROAD

Elev. Top of 8" Tile

Top Stake

F.L. Ditch

3.76	119.31	5.85	117.22
5.05	118.02	6.47	116.60
4.62	118.45	6.10	116.97
3.00	120.07	6.00	117.07
4.24	118.83	6.32	116.75
3.82	118.21	5.74	116.29
4.66	117.37	6.22	115.71
4.98	117.05	6.50	115.53
4.94	117.09	6.37	115.66
5.07	116.96	6.25	115.18
4.43	117.60	6.50	115.53
5.27	116.76	6.58	115.45
4.82	117.21	6.41	115.62
(5.40)	5.51 118.55	6.98	117.08
(4.15)	4.34 119.72	6.55	117.51
	4.31 119.73	6.36	117.70
4.19	119.88		

		124.06 (124.07)		
56 ^{to}				
57 ^{to}				
0				
π	4.77 (4.73)	124.23 (124.21)	4.60 (4.59)	119.46 (119.48)
58 ^{to}				
58 ^{to} 92	0.5 Wfd w/ stg gals			
60 ^{to}				
61 ^{to}				
62 ^{to}				
63 ^{to}				
	9.25	123.32		114.07
			5.12	118.20
	3.99	122.19		
			4.27	117.92
π	9.26	123.33		114.07
52 ^{to}				
51 ^{to}				
50 ^{to}				
49 ^{to}				
48 ^{to}				
47 ^{to}				
46 ^{to}				
π	3.52	121.82	5.03	118.30

See Page 84

Top stake			FoL Ditch	
(5.30) 5.31	118.75	118.77	6.85	117.21
(4.59) 4.60	119.46	119.48	6.40	117.66
5.05	119.18	119.19	6.52	117.71
(5.02) 4.27	119.96	119.93	6.16	118.07
(4.28) 4.97	119.26		6.60	117.63
			6.00	118.23
(4.89) 4.85	119.38	119.32	5.20	119.03
	3.30	120.93		
	2.82	121.41	5.10	119.23

stake		Ditch	
3.52		5.96	117.37
3.87		6.39	116.94
5.13	118.20	6.87	116.46
4.71	118.62	6.31	117.02
3.17	120.16	6.12	117.21
4.36	118.97	6.35	116.98
5.03	118.3	6.25	116.58

82

BM	BS	HI	FS	130.02
11+0	4.55	124.57		
10+00				
9+00				
0			6.58	129.99
+	4.03	132.02		
8+00				
7+00				
6+00				
5+00				
4+00				
0			4.58	127.44
+	3.86	131.30		
3+00				
2+00				
1+00				
0+00				
BM			4.72	126.58

East of Bayless Ditch

Grade	S. Stake	€	Cuts	H. Stake	cut
(124)	4.26	120.31	6.31 ✓	9.91	124.66
(123.5)	4.90	129.67	6.17 ✓	10.13	124.44
(123.0)	5.24	129.33	(6.33) ✓		
(122.5)	3.59	128.43	5.93 ✓	8.52	123.50
(122.10)	4.19	127.83	5.73 ✓	8.90	123.12
(121.70)	4.35	127.67	5.97 ✓	9.24	122.78
(121.30)	4.26	127.74	6.46 ✓	9.54	122.48
(120.90)	4.58	127.44	6.54 ✓	9.66	122.36
(120.50)	4.10	127.20	6.70 ✓	9.20	122.10
(120.10)	3.97	127.33	7.23 ✓	10.03	121.27
(119.70)	4.17	127.13	7.43 ✓	9.96	121.34
(119.30)	3.58	127.77	8.47	10.87	120.43

83

H. Stake	cut
6.05	4.52 ✓
5.44	5.63 ✓
6.58	4.99 ✓
4.14	5.38 ✓
4.69	5.23 ✓
4.73	5.59 ✓
4.89	5.83 ✓
5.08	6.04 ✓
4.72	6.08 ✓
4.59	6.61 ✓
6.05	5.55 ✓
5.18	6.82 ✓

84

4.47 131.05

126.58

121.82

45+00

44+00

43+00

42+00

41+00

40+00

40+33

85

127.38

Station

4.40 117.42

4.84 116.98

4.80 117.02

4.78 117.04

4.84 117.48

5.10 116.72

6.25. 2nd ditch Road

Dtdr

5.85 115.97

6.30 115.52

6.20 115.62

6.56 115.76

6.27 115.55

6.30 115.52

7.25 Top 6-Tile

114.57

126.58

4.47

131.05

127.38

3.67

86

Check on about Richardson

BM	BS	HI	FS	109.31
	4.59	113.90		
114+00				
115+00				
116+00				
117+00				
118+00				
119+00				
+ BM	3.05	112.36		109.31
113+00				
112+00				
111+00				
110+00				
109+00				
108+00				
⊙			4.32	108.04
⊥	3.22	111.26		
107+00				
106+00				
105+00				
104+00				
103+00				
102+00				
⊙			6.18	105.08
⊥	6.31	111.39		

87

Height	End of Rail Stake	Ditch
4.78	109.12	10.74 108.16
4.51	109.39	10.40 108.80
5.26	108.64	10.20 108.70
4.92	108.98	9.89 109.01
4.16	109.74	9.58 109.32
		9.65 109.25
2.90	109.46	9.59 102.77
3.52	108.84	9.67 102.69
4.19	108.17	9.85 102.51
4.14	108.21	10.08 102.28
4.14	108.22	10.32 102.04
4.32	108.04	10.32 102.04
3.74	107.52	9.52 101.74
3.87	107.39	9.41 101.85
4.38	106.88	9.53 101.73
6.10	105.16	9.91 101.30
4.29	106.97	10.12 101.14
6.18	105.08	10.51 100.95

88

BS

NJ

FS

111.39

102+00

100+00

99+00

98+00

97+00

0

π

5.07

109.71

96+00

95+00

94+00

93+00

92+00

91+00

0

π

3.51

108.26

90+00

89+00

88+00

87+00

86+00

6.75 100.64

4.86 104.85

89

Stake

Stem

10.39 101.00

5.62 105.77

10.94 100.45

5.76 103.63

11.18 100.21

6.29 102.10

11.31 100.08

6.75 104.64

11.48 99.91

4.53 103.18

10.13 99.58

4.42 102.29

10.16 99.56

6.25 103.46

10.30 99.41

4.80 104.91

10.50 99.21

4.32 105.39

10.56 99.15

4.86 104.85

10.78 98.93

3.39 104.97

9.55 98.81

3.38 104.98

9.65 98.71

2.92 103.44

9.82 98.53

3.69 104.67

10.05 98.51

3.14 105.22

10.34 98.02

90

BARNETT DITCH -

BM	BS	HI	FS	Elev
π	1.82	101.82		100
23+00				
22+00				
21+00				
20+00				
19+00				
○			4.82	97.00
π	4.17	101.17		
18+00				
100 17+00				
15+00				
14+00				
○			4.23	96.94
π	4.06	101.00		
13+00				
12+00				
11+00				
10+00				
9+00				
8+00				
7+00				
6+00				
○			4.49	96.57
π	4.1	100.61		

91

Top of stake
on End E SE Cor Bridge

F.L. of Ditch

3.44	98.38	6.34 - 95.48
3.74	98.08	7.00 - 94.82 ✓
3.86	97.96	6.40 - 95.42 ✓
4.13	97.69	7.38 - 94.44 ✓
3.97	97.85	7.60 - 94.22 ✓
3.23	97.94	7.40 - 93.57 ✓
3.51	97.66	7.55 - 93.62 ✓
3.88	97.29	7.52 - 93.65 ✓
3.59	97.58	7.40 - 93.77 ✓
3.59	97.41	7.10 - 93.90 ✓
3.76	97.04	7.40 - 93.60 ✓
3.97	97.03	8.10 - 92.90 ✓
3.98	97.02	7.65 - 93.35 ✓
3.72	97.28	8.45 - 92.55 ✓
3.92	97.08	8.30 - 92.70 ✓
4.53	96.47	8.45 - 92.55 ✓
4.49	96.51	8.60 - 92.40 ✓

92

	BS	HI	FS	
BM		100.61		
5+00			3.89	96.72
BM				100
	3.00	103.00		
24+00				
25+00				
26+00				
27+00				
28+00				
⊙			3.63	99.37
⊓	5.66	105.03		
29+00				
30+00				
31+00				
32+00				
33+00				
34+00				
35+00				
⊙ BM			2.45	102.58
⊓	4.10	106.68		
36+00				
37+00				

93

	Stake		Ditch
	sto 4+75	S. Side Ditch - 12" Tree 30' South	
	4.76	95.85	7.84 - 92.77
			10.00 - 93.0
	3.82	99.18	7.55 - 95.75
	3.10	99.80	8.00 - 95.00
	3.71	99.29	8.25 - 94.75
	3.37	99.63	7.90 - 95.10
	4.83	100.20	9.60 - 95.43
	3.71	101.32	9.40 - 95.63
	3.41	101.92	8.85 - 96.18
	3.05	101.98	8.70 - 96.28
	3.71	101.32	8.16 - 96.87
	3.34	101.64	8.25 - 96.78
			8.30 - 96.73
	Nail in stump - 24+50		
	5.75	102.93	9.50 - 97.16
	5.17	101.51	9.30 - 97.36

96

BM	BS	HI	FS	
				10.1 31
			96.72	
	2.30	99.02		
4+00			4.88 - 101.60	
3+00			13.2 88.40	
2+00				
0			3.67 15.35 '2	
π	4.37	119.92		
1+00				
23-76				
0+00				
24+00				
0			4.03 95.67	
π	2.41	98.10		
25+00				
26+00				
27+00				
0			97 97.13	
π	4.50	101.62		
27+94	Mouth of	114.50	9.5 92.13	
28+00				
29+00				
30+00				

97

Stake		Ditch
Tree S side sta 4+75		
3.70	95.32	6.70 92.32
3.15	95.87 ✓	6.55 92.47
3.67	95.35 ✓	6.60 92.42
3.79	96.43 ✓	7.50 92.22
5.25	94.47 ✓	8.73 90.99
4.03	95.69 ✓	7.85 91.87
.98	97.12 ✓	6.75 91.35
1.08	97.02 ✓	6.70 91.40
.99	97.13 ✓	6.90 91.20
5.95	95.68 ✓	10.50 91.13
3.80	97.85	9.95 91.68
		10.40 91.23

106

BS	HI	FS
	106.71	
9+00		
+50		
10+00		
⊙		
⊕		5.06 101.65
+50	5.77	
11+00	107.42	
+50		
12+00		
+50		
13+00		
+50		
14+00		
+50		
15+00		
+50		
⊙		
⊕		6.56 100.84
BM ³	3.03	
	103.89	
16+00		3.75 100.12
+50		
17+00		
+50		

BASE POINTS
IN CIRCLES

107

Stake	Ditch
6.25 100.46 ✓	7.56 99.15 ✓
6.72 100.59 ✓	7.51 99.20 ✓
5.06 101.65 ✓	6.66 100.05 ✓
4.90 102.52 ✓	6.45 100.97 ✓
4.19 103.23 ✓	6.59 100.83 ✓
4.84 102.58 ✓	6.28 101.14 ✓
5.02 102.40 ✓	6.56 100.86 ✓
5.39 102.03 ✓	6.40 101.02 ✓
5.49 101.93 ✓	6.49 100.93 ✓
5.52 101.90 ✓	6.70 100.72 ✓
5.35 102.07 ✓	7.15 100.29 ✓
5.65 101.77 ✓	7.14 100.28 ✓
6.04 101.38 ✓	7.24 100.08 ✓
6.56 100.86 ✓	7.53 99.89 ✓
3.79 100.10 ✓	4.81 99.08 ✓
4.15 99.74 ✓	5.45 98.44 ✓
4.86 99.03 ✓	5.96 97.93 ✓
5.08 98.81 ✓	6.32 97.59 ✓

	BS	HI	FS	
18+00		103.59		
+50				
19+00				
+50				
20+00				
+50				
21+00				
⊙			5.10	98.79 ✓
⊕	4.85	103.64 ✓		
+50				
BMI A			4.70	98.94 ✓
22+00				
+50				
23+00				
+50				
24+00				
+50				
25+00				
+50				
26+00				
⊙			4.19	99.43 ✓
⊕	5.58	105.03 ✓		
+50				

Bottom Bolt
Cane Post
N. Side of Pile

	Stoke	Side Ditch at Road
5.17	98.72 ✓	6.48 97.41 ✓
5.22	98.67 ✓	6.17 97.72 ✓
5.18	98.71 ✓	6.28 97.61 ✓
5.42	98.47 ✓	6.39 97.50 ✓
5.16	98.73 ✓	6.17 97.72 ✓
5.21	98.68 ✓	6.38 97.51 ✓
5.10	98.79 ✓	6.32 97.57 ✓
4.84	98.80 ✓	6.09 97.55 ✓
4.83	98.81 ✓	6.06 97.58 ✓
4.97	98.67 ✓	6.03 97.61 ✓
5.07	98.57 ✓	6.27 97.39 ✓
4.72	98.92 ✓	6.21 97.43 ✓
4.85	98.79 ✓	6.15 97.49 ✓
4.69	98.95 ✓	6.12 97.52 ✓
4.59	99.05 ✓	5.61 98.03 ✓
4.42	99.22 ✓	5.26 98.38 ✓
4.19	99.45 ✓	5.46 98.18 ✓
5.82	99.21 ✓	7.07 97.96 ✓

110

136

HE

F6

106.03

27+00

750

28+00

750

29+00

750

30+00

750

0

π

3.98

104.81

4.20 100.83 ✓

31+00

750

32+00

→ 8715

S Hand

4.33 100.48

Final Jan 3 1900

99.49

90.26

9.23

LETTER

111

S Hand

S Hand

5.16 99.87 ✓

6.46 98.57 ✓

4.86 100.17 ✓

6.25 98.78 ✓

4.43 100.60 ✓

6.02 99.01 ✓

4.20 100.83 ✓

5.69 99.34 ✓

4.07 100.96 ✓

5.36 99.67 ✓

4.28 100.75 ✓

5.36 99.67 ✓

3.92 101.11 ✓

5.07 99.94 ✓

4.20 100.83 ✓

5.19 99.84 ✓

4.86 99.95 ✓

5.83 98.98 ✓

5.31 99.50 ✓

6.60 98.21 ✓

5.32 99.49 ✓

6.62 98.17 ✓

112

	BS	HI	FS	
BM ⁷⁺²⁵	2.52	103.92		101.40
			10.5	93.42

	BS	HI	FS	
BM ⁷⁺²⁵	3.45	104.85		101.40
			10.21	94.64
			10.04	94.81

	BS	HI	FS	
BM ⁷⁺⁵⁰	3.45	102.39		98.94
			6.37	96.02
			6.57	95.82
			7.15	95.24

113

Top 8' tile sta 3+50

$$\begin{array}{r} 93.42 \\ 83 \\ \hline 92.59 \end{array}$$

Top 8' tile sta 11+00

$$\begin{array}{r} 94.64 \\ 83 \\ \hline 93.81 \end{array}$$

" " " sta 14+00

$$\begin{array}{r} 94.81 \\ 83 \\ \hline 93.98 \end{array}$$

Top 8' tile sta 23+50

$$\begin{array}{r} 95.82 \\ 83 \\ \hline 94.99 \end{array}$$

" " " sta 21+50

$$\begin{array}{r} 96.02 \\ 83 \\ \hline 95.19 \end{array}$$

st 18.00

$$\begin{array}{r} 95.24 \\ 83 \\ \hline 94.41 \end{array}$$

114

N.C. Brown Ditch check

6-15-33

	BS	HI	FS	Stake	Elev
BM#1	2.57	102.57			100
4+00				4.55	98.02 ✓
+50				3.58	98.99 ✓
5+00				2.57	100.0 ✓
0			2.57	100.	
⌊	5.97	105.99 ✓			
5+50				5.19	100.80 ✓
6+00				4.64	101.32 ✓
+50				4.38	101.61 ✓
7+00				4.36	101.63 ✓
BM#2			4.54	101.45 ✓	
+50				4.37	101.62 ✓
8+00				4.85	101.14 ✓
+50				5.21	100.72 ✓
9+00				5.46	100.53 ✓
+50				5.33	100.66 ✓
10+00				4.27	101.72 ✓
+50				3.39	102.60 ✓
11+00				2.68	103.31 ✓
0			2.68	103.31 ✓	
⌊	4.04	107.35 ✓			
11+50				4.64	102.71 ✓
12+00				4.86	102.49 ✓
+50				5.23	102.12 ✓

115

116

	BS	HI	FS	Stake	Elev
		107.35			
13+00				5.25	102.00 ✓
+50				5.38	101.97 ✓
14+00				5.22	102.13 ✓
+50				5.51	101.84 ✓
15+00				5.72	101.42 ✓
+50				6.42	100.93 ✓
BM#3			7.14	100.21 ✓	
16+00				7.22	100.13 ✓
o			7.22	100.13 ✓	
π	3.65	103.78 ✓			
+50				4.01	99.77 ✓
17+00				4.70	99.08 ✓
+50				4.93	98.85 ✓
18+00				5.03	98.75 ✓
+50				5.06	98.72 ✓
19+00				5.02	98.76 ✓
+50				5.28	98.50 ✓
20+00				5.02	98.76 ✓
+50				5.09	98.69 ✓
21+00				4.96	98.82 ✓
o			4.96	98.82 ✓	
π	4.82	103.64 ✓			
BM#4			4.65	98.99 ✓	

117

118

BS	HI	FS	Stake	Elev
	103.64			
21+50			4.87	98.77 ✓
22+00			4.92	98.72 ✓
+50			5.01	98.63 ✓
23+00			5.10	98.52 ✓
+50			4.98	98.66 ✓
24+00			4.88	98.76 ✓
+50			4.75	98.88 ✓
25+00			4.65	98.97 ✓
+50			4.34	99.20 ✓
26+00			4.23	99.41 ✓
+50			4.13	99.51 ✓
27+00	Lost			
+50			3.17	100.47 ✓
0				
π	5.84	3.17	100.47 ✓	
28+00			5.45	100.56 ✓
+50			5.05	101.26 ✓
29+00			4.92	101.37 ✓
+50			5.13	101.18 ✓
30+00			4.75	101.56 ✓
+50			5.08	101.23 ✓
31+00			5.93	100.38 ✓
+50			6.39	99.80 ✓
32+00			6.39	99.80 ✓
Brogas		5.39	100.92	

98.94 119

98.99

3.51 103.50

22

4.71 98.79

23

4.67 98.83

FLT. In

9.66 93.84

93.39

Glen at 32+00

4.70 98.80

98.80

4.00

94.80

93.84

81.96

.12

.12

.12

98.19

1.40

94.19

93.84

35

120

Sadler Gravel P/c - Pritchard

2.38 102.38

0+00

0+45

0+57

0+82

1+00

1+20

1+37

1+55

1+97

0

K

11.59 113.37

0+45

0+57

100

121

P.T.

BM Nail in Hickory Tree 150' - SE

0
8.65
92.73

0	5	17	21
9.24	9.9	4.2	1.7
93.14	92.98	98.18	100.68

9	2	17	20
9.53	9.25	2.2	7.5
92.85	93.13	100.18	101.73

0	4	9	18
9.25	8.7	5.7	7
93.13	93.68	96.68	101.78

0	6	12	22
8.45	9.3	6.1	6
93.93	94.08	96.28	101.78

0	12	24
8.7	5.8	1.4
93.98	96.58	100.98

0	4	14	18
8.25	7.6	3.8	7
94.13	94.78	98.58	101.48

0	5	15
8.0	8.1	1.7
94.38	94.78	100.68

0
8.65
93.73

31	26
6.2	2.1
109.07	111.27

24	31	38
9.0	5.0	2.0
104.37	109.37	111.37

122

0+82

1+00

1+20

1+37

1+55

O

K

0+45

0+57

0+82

1+00

1+20

Toolbox

1+37

1+55

O

K

113.27

9.47

121.65

3.10

113.10

119

112.18

116.5

110.00

123

<u>34</u>	
4	✓
112.97	

<u>38</u>	<u>42</u>
3.2	1.5
110.17	111.87

<u>41</u>	
7.3	✓
104.07	

<u>36</u>	
2.2	✓
111.17	

<u>35</u>	
.8	✓
112.57	

<u>39</u>	<u>41</u>	<u>46</u>	
7.8	6.9	10.7	✓
113.85	114.75	110.95	

<u>39</u>	<u>41</u>	<u>42</u>	
8.1	8.2	11.7	✓
113.55	113.45	109.95	

<u>41</u>	<u>51</u>	
9.	11.	✓
117.65	110.65	

<u>48</u>	
12.9	✓
108.75	

<u>40</u>	<u>43</u>	<u>45</u>	<u>53</u>	
8.4	7.6	7.6	11.4	✓
113.35	114.05	114.05	110.25	

<u>40</u>	<u>43</u>	<u>45</u>	<u>47</u>	<u>56</u>	<u>58</u>	
5.3	3.5	2.2	1.6	9.2	10.3	✓
116.35	118.75	119.45	120.05	112.45	117.35	

124

0+45

113.10

0+57

0+82

1+00

1+20

1+37

1+55

⊙

K

4.19

105.40

11.89 101.21

0+45

0+57

0+82

1+00

1+20

125

<u>56</u>	<u>62</u>	
8.6	9.5	✓
104.5	103.6	

<u>56</u>	<u>63</u>	
6.3	10.4	✓
106.8	102.7	

<u>63</u>		
7.6		✓
105.5		

<u>60</u>		
9.3		✓
103.8		

<u>53</u>	<u>61</u>	
9.2	11.8	✓
103.9	101.3	

<u>64</u>		
9.3		✓
103.8		

<u>68</u>	<u>74</u>	
7.3	10.5	✓
105.8	102.6	

<u>86</u>		
9.6		✓
95.8		

<u>70</u>	<u>82</u>	
5.4	8.6	✓
100.	96.8	

<u>23</u>		
9.0		✓
96.4		

<u>67</u>	<u>80</u>	
6.1	9.8	
99.3	95.6	

<u>82</u>		
9.8		
95.6		

126

1+37

1+55

105.40

127

<u>76</u>	<u>83</u>	
6.8	9.2	✓
98.6	96.2	

91
4.0

96.40

128

Ek on Barnett Ditch

Bm

100

K

3.94 103.94

24+00

11.7 92.24

29+00

10.90 93.00

34+00

9.90 94.04

0

2.91 101.03

K

5.56 106.59

39+00

11.4 95.19

42+00

10.7 95.89

0

3.97 102.62

K

5.59 108.21

47+00

11.5 96.71

49+50

10.6 97.61

0

4.33 103.88

K

5.67 109.55

53+00

11.3 98.25

BM

4.85 104.70

56+00

10.4 99.15

3.00 105.65 56+55

129

38100 T. Inf. ...

130

SADLER GRAVEL PILE (Pritchard)

232-CIV 58

100

BM

T

3.20 103.20

C

A

O

T

11.11 104.83

B

D

O

T

11.5 119.54

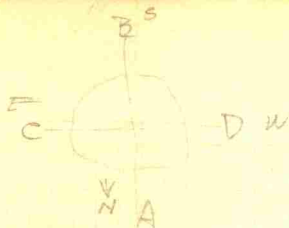
D-

B

C

A

7-31-33



0	11	19
11.2	6.2	2.1
92.0	99.0	101.1

0	10	15
10.2	4.5	1.4
93.0	98.9	101.8

0	12	12	12	27	28	33
12.2	10	8.5	7.5	7.2	3.2	1.5
92.93	94.3	96.33	97.33	100.53	101.63	104.33

0	10	18	28
10	10.2	9.1	1.1
91.43	94.93	97.73	103.73

41
3.9
115.64

43
0.2
115.34

38	40
9.2	9.2
110.34	115.24

37
4.2
115.34

131

132

SADLER

EAGLE

GUNNARD

7-31-35

BM

5.27

Top of ... 100

105.27

0400

1+13

1+43

1+62

O

K

1+62

1+43

1+13

0400

O

K

0400

1+13

1+43

1+62

11.78

115.11

2.94

102.33

11.50

102.61

3.88

106.49

133

$$\begin{array}{r} 97.17 \\ 1.1 \\ \hline 97.17 \end{array}$$

$$\begin{array}{r} 96.47 \\ 1.7 \\ \hline 96.47 \end{array}$$

$$\begin{array}{r} 93.97 \\ 3.9 \\ \hline 93.97 \end{array}$$

$$\begin{array}{r} 92.99 \\ 1.8 \\ \hline 92.99 \end{array}$$

$$\begin{array}{r} 102.91 \\ 12.1 \\ \hline 102.91 \end{array}$$

$$\begin{array}{r} 108.61 \\ 11.2 \\ \hline 108.61 \end{array}$$

$$\begin{array}{r} 110.51 \\ 10.4 \\ \hline 110.51 \end{array}$$

$$\begin{array}{r} 112.31 \\ 8.7 \\ \hline 112.31 \end{array}$$

$$\begin{array}{r} 97.69 \\ 11.6 \\ \hline 97.69 \end{array}$$

$$\begin{array}{r} 95.19 \\ 12.4 \\ \hline 95.19 \end{array}$$

$$\begin{array}{r} 94.09 \\ 13.2 \\ \hline 94.09 \end{array}$$

$$\begin{array}{r} 93.19 \\ 11.6 \\ \hline 93.19 \end{array}$$

134

BM

Saddle Gravel Pit (Sullivan Place)

Nail in Tree 100' East

100

6.44 106.44

0+16

0+32

0+44

0+60

0+76

0+87

O

T

10.66 116.32

0+87

0+76

0+60

0+44

0+32

0+16

8-1-33

116.67

135

$$\begin{array}{r} 0 \\ 44 \\ \hline 97.04 \end{array} \begin{array}{r} 12 \\ 1.9 \\ \hline 104.54 \end{array} \checkmark$$

$$\begin{array}{r} 0 \\ 9.6 \\ \hline 96.84 \end{array} \begin{array}{r} 7 \\ 4.3 \\ \hline 102.14 \end{array} \begin{array}{r} 13 \\ .9 \\ \hline 105.54 \end{array} \checkmark$$

$$\begin{array}{r} 0 \\ 9.6 \\ \hline 96.84 \end{array} \begin{array}{r} 14 \\ .4 \\ \hline 106.04 \end{array} \checkmark$$

$$\begin{array}{r} 0 \\ 9.1 \\ \hline 97.54 \end{array} \begin{array}{r} 12 \\ 1.3 \\ \hline 105.14 \end{array} \checkmark$$

$$\begin{array}{r} 0 \\ 8.3 \\ \hline 98.14 \end{array} \begin{array}{r} 12 \\ .6 \\ \hline 105.84 \end{array} \checkmark$$

$$\begin{array}{r} 0 \\ 9.1 \\ \hline 97.44 \end{array} \begin{array}{r} 12 \\ 1.0 \\ \hline 105.44 \end{array} \checkmark$$

$$\begin{array}{r} 24 \\ 3.6 \\ \hline 112.72 \end{array} \begin{array}{r} 31 \\ .3 \\ \hline 116.02 \end{array} \begin{array}{r} 43 \\ 3.2 \\ \hline 108.12 \end{array} \begin{array}{r} 47 \\ 11.3 \\ \hline 105.02 \end{array} \checkmark$$

$$\begin{array}{r} 19 \\ 6.4 \\ \hline 109.92 \end{array} \begin{array}{r} 27 \\ 1.0 \\ \hline 105.32 \end{array} \begin{array}{r} 33 \\ 4.0 \\ \hline 112.32 \end{array} \begin{array}{r} 43 \\ 11.0 \\ \hline 105.32 \end{array} \checkmark$$

$$\begin{array}{r} 18 \\ 7.4 \\ \hline 108.92 \end{array} \begin{array}{r} 27 \\ 1.0 \\ \hline 115.32 \end{array} \begin{array}{r} 43 \\ 12. \\ \hline 104.32 \end{array} \checkmark$$

$$\begin{array}{r} 26 \\ 6.2 \\ \hline 110.12 \end{array} \begin{array}{r} 26 \\ 2.8 \\ \hline 113.52 \end{array} \begin{array}{r} 40 \\ 11.6 \\ \hline 104.92 \end{array} \checkmark$$

$$\begin{array}{r} 20 \\ 8.0 \\ \hline 118.32 \end{array} \begin{array}{r} 34 \\ 4.6 \\ \hline 111.92 \end{array} \begin{array}{r} 34 \\ 11.9 \\ \hline 104.42 \end{array} \checkmark$$

$$\begin{array}{r} 19 \\ 7.0 \\ \hline 109.32 \end{array} \begin{array}{r} 28 \\ 12.9 \\ \hline 103.42 \end{array} \checkmark$$

136

0

116.32

10.17

106.15

π

1.53

107.68

0+87

0+76

0+60

0+44

0+32

0+16

137

57

10.6

97.08

56

10.6

97.08 ✓

56

10.9

96.78 ✓

51

10.9

96.78 ✓

45

11.2

96.48 ✓

38

11.2

96.38 ✓

138

92 1/2 8-1-33 West Pile
 SADLER GRAVEL PILE GULLEY FARM
 Top^{ENT} Conc Post 150-SW 100

π	5.08	105.08		
0+20				
0+31				
0+38				
0+51				
0+72				
0			.84	104.24
π	10.18	114.42		
0+73				
0+51				
0+38				
0+31				
0+20				
0			10.85	103.57
π	2.78	106.35		
0+20				

139

0/	14			
9.9	1.3			
95.18	103.98			
0/	14			
9.9	1.0			
95.18	104.08			
0/	14			
9.8	.7			
95.28	104.38			
0/	14			
9.6	.2			
95.48	104.88			
0/	12			
9.6	1.0			
95.48	104.08			
2.3	3.5			
2.2	10.6			
112.22	103.82			
2.2	2.7	3.9		
3.4	.7	8.9		
111.02	113.72	105.52		
2.6	3.8			
2.5	10.3			
111.92	104.12			
2.6	3.8			
2.9	10.			
111.52	104.42			
2.6	3.8			
2.8	10.9			
111.62	103.52			
4.9				
10.6				
95.75				

140

0+31

106.35

0+38

0+51

0+73

141

50

70

96.35

50

10.5

95.85

54

10.6

95.75

47

10.4

95.95

142

Hufford Gravel Pile

BM

1.95 101.75

0+26

0+36

0+45

0+52

0+68

0+74

0+81

0+95

1+06

1+19

0

π

11.78 112.26

1+19

1+06

8/18/23

Stump ^{100'} End
100

0	<u>12</u>	
10.1	1.4	✓
98.65	100.35	

0	<u>12</u>	
10.1	1.7	✓
98.65	100.05	

0	<u>12</u>	
10.6	1.8	✓
91.15	100.95	

0	<u>12</u>	
10.9	2.6	✓
90.35	99.15	

0	<u>12</u>	
10.2	2.1	✓
91.55	99.65	

0	<u>9</u>	<u>14</u>	
10.1	4.6	1.2	
101.65	97.15	101.55	✓

0	<u>12</u>	
10	1.1	✓
91.75	100.65	

0	<u>12</u>	
10.5	1.8	✓
91.25	99.95	

0	<u>12</u>	
10.7	2.6	✓
91.05	99.15	

0	<u>9</u>	
18.9	2.3	✓
92.85	99.45	

<u>26</u>	<u>28</u>	<u>30</u>	<u>42</u>	
1.7	2.9	3.2	11.5	✓
110.56	109.36	109.06	100.76	

<u>30</u>	<u>35</u>	<u>48</u>	
1.10	2.9	11.2	✓
112.16	109.36	101.06	

143

144

112.26

0+95

0+81

0+74

0+68

0+52

0+45

0+36

0+26

0

π

0+26

0+36

0+45

0+52

0+68

1.75

102.24

11.77 100.49

145

<u>30</u>	<u>33</u>	<u>45</u>	
4	2.3	9.9	✓

111.86 109.96 102.36

<u>27</u>	<u>30</u>	<u>36</u>	<u>44</u>
1.4	1.6	4.9	10.5

110.86 110.66 107.36 101.76 ✓

<u>22</u>	<u>28</u>	<u>40</u>	
4.3	2.8	11.3	✓

107.96 109.46 100.96

<u>27</u>	<u>31</u>	<u>35</u>	<u>42</u>
2.4	5.1	6.8	11.1

107.86 107.16 106.46 101.16 ✓

<u>27</u>	<u>41</u>		
2.4	12.2		✓

109.86 100.06

<u>25</u>	<u>27</u>	<u>32</u>	
3.5	3.3	11.9	✓

108.76 108.96 100.36

<u>25</u>	<u>27</u>	<u>38</u>	
2.5	2.8	11.4	✓

109.76 109.46 100.86

<u>26</u>	<u>31</u>	<u>36</u>	<u>43</u>
3.1	5.7	7.3	11.5

109.16 106.56 104.96 100.76 ✓

<u>28</u>			
10.9			
91.34			✓

<u>52</u>			
12.1			
90.14			✓

<u>52</u>			
12			
90.24			✓

<u>54</u>			
11.3			
90.94			✓

<u>59</u>			
11.7			
90.54			✓

146

102.24

0+74

0+81

0+95

1+06

1+19

BM

0+03

+20.5

+37

+40

End

RR Small Pda Geo Henry

28 10028

100

147

5711.7 ✓
90.546110.7 ✓
101.54609.7 ✓
92.54609.6 ✓
92.645610.6 ✓
91.64

9	3	13	17	E End
6.3	8.0	2.7	6.1	
93.98	97.28	97.28	94.18	

9	3	13	17
6.2	5.3	3.3	6.7
94.08	96.58	96.98	93.58

5	3	14.5	18.5
13.8	8.5	3.7	7.6
93.78	96.78	96.58	92.68

148

4 P. 1/2

3M

36

45

100

100
TIME METER

445 104.65

0+04

0+22

+55 39

+55

+79

+88

End

27. Big file

3M

.28

100.28

100

Lomb. Big file

0+03

+16

+50

+66.5

+79

+93

+98 EHA

149

7	2	23	24
92	5.0	5.6	12.5
95.45	99.65	99.05	91.15

N End

0	7	27	37
93	2.5	5.4	12.1
95.35	100.15	99.25	91.55

0	7	26.5	28.5
95	4.7	4.9	12.8
95.15	99.95	99.75	91.35

0	8	26	31.5
97	4.7	5.0	12.1
94.95	99.95	99.65	91.95

0	7.5	24	32.5
96	5.1	5.1	12.8
95.05	99.55	99.55	91.35

0	3	16	24	SENA
98	5.2	4.5	10.9	
92.55	96.65	95.75	89.35	

0	3/4	19.5	27.5
97	3.5	4.5	10.8
93.15	96.75	95.75	89.95

0	3	20	22
97	3.9	4.5	10.7
93.25	96.55	95.75	89.55

0	4	23	31
96	4.1	5.0	11
92.65	96.15	95.25	89.25

0	4	24	22
98	5.0	5.4	11.4
91.45	95.25	94.35	88.25

0	5	23	26.5
97	4.5	5.7	11.9
91.55	95.25	94.55	88.35

150

#3P1-ε

877

38

25

100

Top
Burr Hill

2.76

102.76

0x00

+11

shut
+24Loon
+24

+36

+45

+50

+59

+65

+77

+83 Ed

151

0	2	8	12	18	22
6.3	6.2	6.2	7.0	7.4	9.3
96.76	97.56	96.56	95.76	95.36	93.46

0	3	7	10	21	25
5.8	4.3	3.3	4.8	7.3	9.6
96.96	98.46	97.46	97.96	95.46	93.16

0	4	10	14	22
5.2	2.9	3.2	5.4	9.5
97.56	99.86	99.86	97.26	93.26

0	4	7	15	24	33
5.5	3.5	2.6	2.9	5.5	9.4
97.26	97.26	100.16	99.86	97.26	93.26

0	5	16	22
4.5	2.1	2.8	9.6
97.26	100.66	99.96	93.16

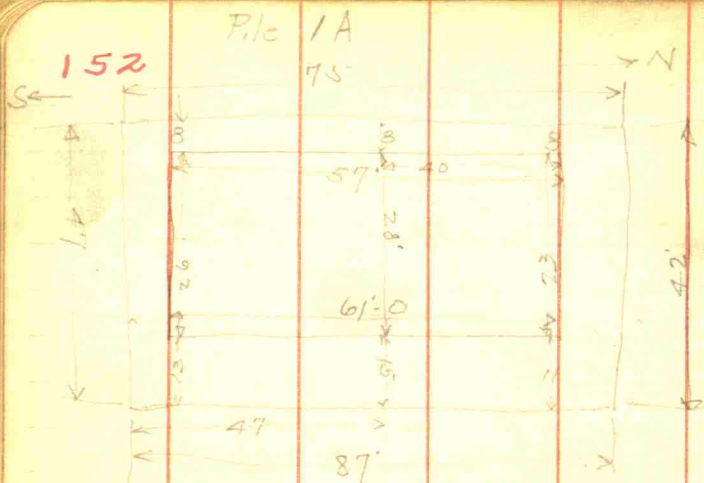
0	5	12	13	20	23	30	33
4.1	2.5	2.5	3.5	4.8	6.2	8.4	10
97.46	100.26	100.26	99.86	97.96	96.56	94.26	92.76

0	5	12	21	23	29	32
4.2	2	3.5	5.5	6.5	7.8	9.8
97.56	99.76	99.26	97.26	96.26	95.96	93.96

0	4	12	22	26	27
4.2	4.5	3.2	6.4	7.6	8.8
96.56	98.26	99.56	96.36	95.19	93.96

0	5	14	17	22	23
4.7	4.6	4.5	6.2	7.4	8.5
96.06	98.16	97.26	96.56	95.26	94.26

0	4	11	15	19	22
7.6	6.6	5.2	5.4	7.6	8.4
95.16	96.16	97.56	97.36	95.16	94.56



NE Cor	B = 12.08	T = 4.5	H = 8.52
C. E Side	B = 13.5	T = 4.7	H = 8.8
SE Cor	B = 14.0	T = 5.4	H = 8.6
SW Cor	B = 10.9	T = 5.1	H = 5.9
C. W Side	B = 10.2	T = 4.4	H = 5.8
NW Cor	B = 10.2	T = 4.7	H = 5.5

153

Row #2 - P.L. 794 - 100 -	694
#1-A " Est	150
#3 " Est 250 - 100 -	150
RR "	330
	1324
	45
	6620
	5296
	59580

154

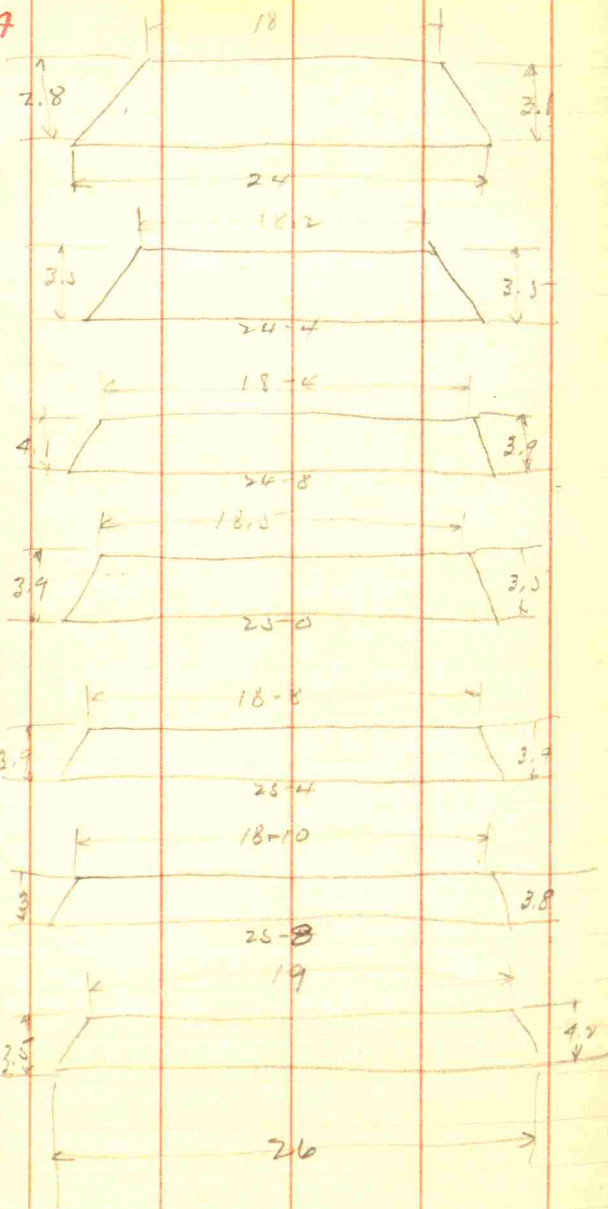
$$\begin{array}{r} 21.25 \\ 3.5 \\ \hline 106.25 \\ 63.75 \\ \hline 74.375 \end{array}$$

$$\begin{array}{r} 21.75 \\ 3.7 \\ \hline 152.25 \\ 65.35 \\ \hline 70.425 \end{array}$$

$$\begin{array}{r} 78 \\ 78 \\ \hline 458 \end{array}$$

$$\begin{array}{r} 22.25 \\ 3.4 \\ \hline 89.00 \\ 67.50 \\ \hline 73.050 \end{array}$$

$$\begin{array}{r} 3.85 \\ 2.25 \\ \hline 19.25 \\ 77.0 \\ \hline 84.25 \end{array}$$



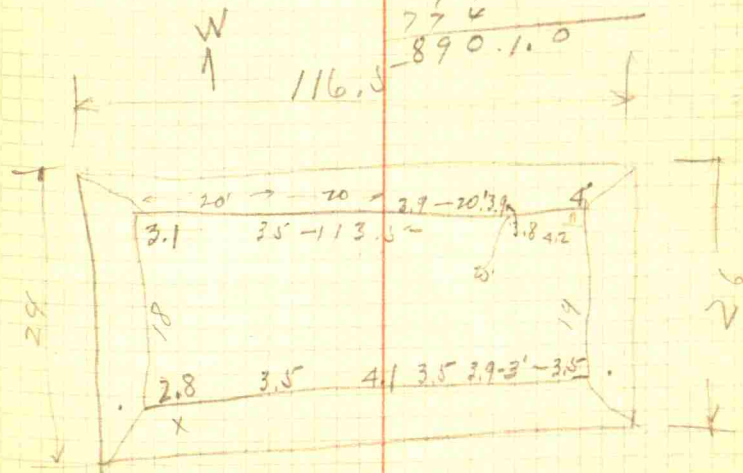
/ A = 150

R.R. D.K.

155

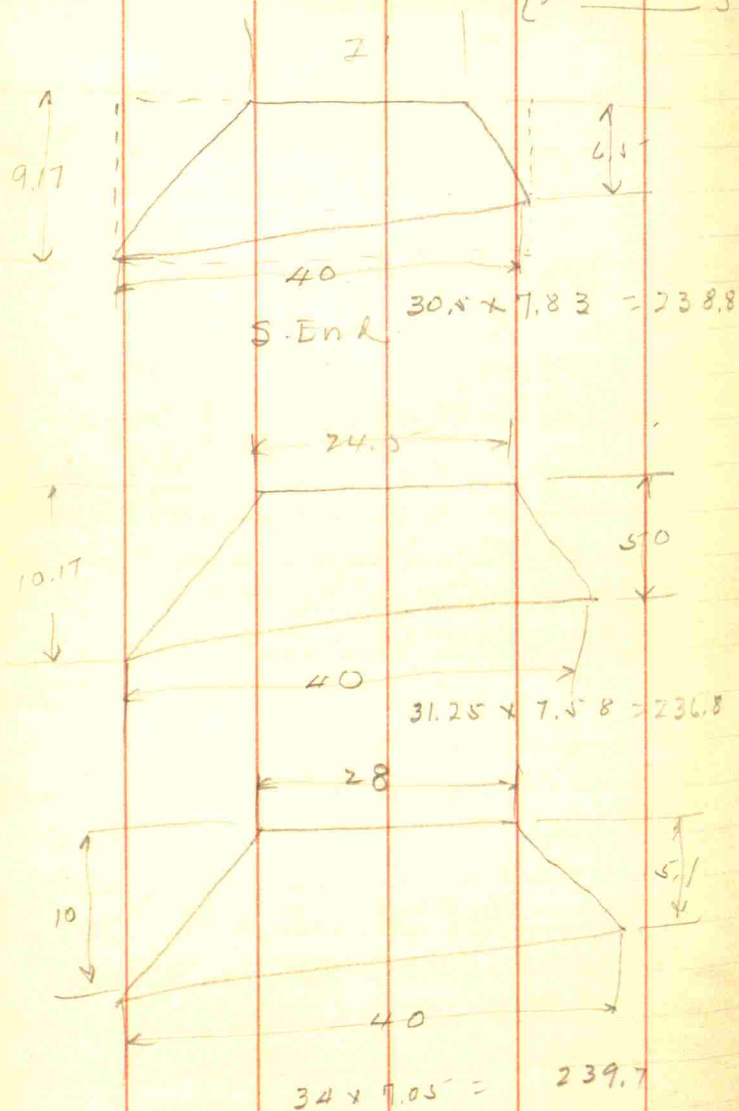
21 x 3	=	63
21.25 x 3.5	=	74.375
21.5 x 4	=	86.0
21.75 x 3.7	=	70.47
22 x 3.9	=	85.8
22.25 x 3.4	=	75.6
22.5 x 3.55	=	86.6

$$\begin{array}{r} 71541.82 \\ \hline 77.4 \\ \hline 115 \\ \hline 3870 \\ 774 \\ \hline 774 \\ \hline 890.10 \end{array}$$



$$\begin{array}{r} 27 \quad 89016330 \\ 81 \\ \hline 80 \\ 81 \end{array}$$

156

2 of Middle Pile
from 1st Est

#3 Pile 150 cu ft

SE Bot

TOP	13.67
	4.5
	9.17

Mid E. side Bot

TOP	14.67
	4.50
	10.17

NE Corner Bot

TOP	14.5
	4.5

	31.25
	7.58
	236.875
	13625
	21875
	236.875
	238.8
	239.7
3	715.375
	238.45

27	2144	2500	(794.1)
	189		
	254		
		90	
		239.70	

157

NW Corner Bot

	9.6
	4.5
	5.1

Mid W. side Bot

	9.5
	4.5
	5.0

SW Corner Bot

	11.0
	4.5
	6.5

	7.83
	30.5
	3915
	2809
	238.8.10

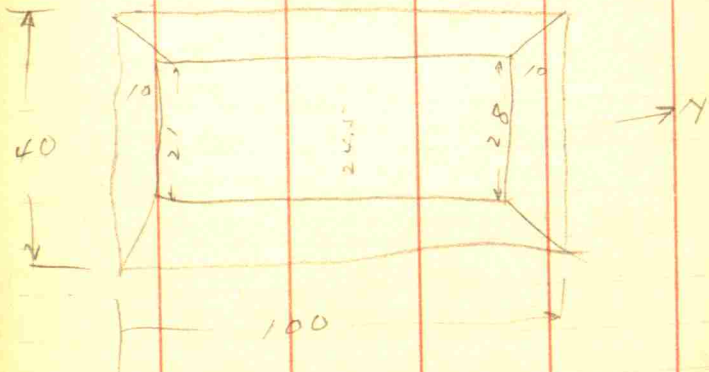
	7.05
	30
	2115
	239.70

158

$$\begin{array}{r}
 PC \quad 6 + 27.2 \\
 \hline
 PI \rightarrow 6 + 89.96 \\
 \hline
 \quad 1 + 25 \\
 \hline
 PT \quad 8 + 14.96
 \end{array}$$

$$\begin{array}{r}
 PC: 6 + 27.2 \\
 1^{\circ} - 09 \quad 6 + 50 \\
 3^{\circ} 39 \quad 7 + 00 \\
 6^{\circ} 09 \quad 7 + 50
 \end{array}$$

$$\begin{array}{r}
 6 + 27.2 \\
 \hline
 1 \quad 25 \\
 \hline
 7 + 52.2
 \end{array}$$



$$\begin{array}{r}
 23 \\
 \hline
 115 \\
 \hline
 60 \\
 \hline
 90
 \end{array}$$

159

$$I = 4^{\circ} - 29' \quad D = 4^{\circ} 0'$$

$$T = \frac{224.3}{4} = 56 \text{ Ten}$$

$$L = \frac{4.4833}{4} = 112.08$$

$$\begin{array}{l}
 PC = 1 + 44 \\
 PT = 2 + 56
 \end{array}$$

$$\begin{array}{r}
 .56 \\
 \hline
 2 \\
 \hline
 1.12 \\
 \hline
 60 \\
 \hline
 7.20 \\
 \hline
 10-7
 \end{array}$$

$$I = 12^{\circ} - 30' \quad D = 10'$$

$$T_{\text{ten}} = \frac{627.6}{10} = 62.76$$

$$L = \frac{12.5}{10} = 125'$$

160

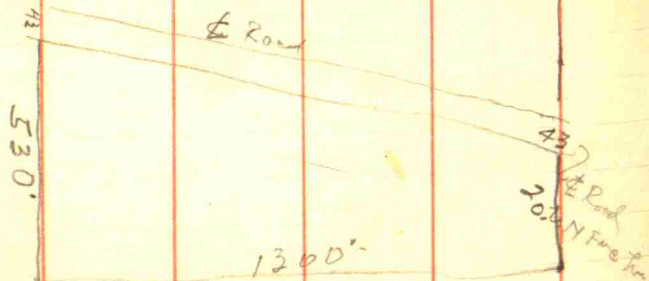
16.5

79
 1485-
 1155-
 1203.5-

63
 573
 2)636
 318
 1200
 75400
 318
 4)13400 (9.467)
 392040
 213600
 184240
 291600
 261360
 302400
 304920

530
 20
 2)55-8
 275
 1300
 82500
 275
 8.206
 43560) 357500
 348480
 90200
 87120
 288000
 261360

Mrs J. H. Lewis
 Dayton



9.467 dem
 8.206
 1.261

Natural Trigonometrical Ratios.

Angle.	Sine.	Tan.	Sec.	Cosec.	Cotg.	Cosin.	Angle.	Sine.	Tan.	Sec.	Cosec.	Cotg.	Cosin.
0	0	0	1.	∞	∞	1.	90	1.	0	0	∞	∞	0
10	.0029	.0029	1.0002	343.8	343.8	1.	50	.1392	.1405	1.0098	7.185	7.115	.99027
20	.0058	.0058	1.0019	171.9	171.9	.99998	40	.1421	.1435	1.0102	7.040	6.968	.98986
30	.0087	.0087	1.0044	114.6	114.6	.99996	30	.1449	.1465	1.0107	6.900	6.827	.98944
40	.0118	.0118	1.0081	85.94	85.94	.99993	20	.1478	.1495	1.0111	6.766	6.691	.98902
50	.0145	.0145	1.0031	68.76	68.76	.99989	10	.1507	.1524	1.0115	6.636	6.561	.98858
1	.0175	.0175	1.0002	57.30	57.29	.99985	89	.1536	.1554	1.0120	6.512	6.435	.98814
10	.0204	.0204	1.0002	49.11	49.10	.99979	50	.1564	.1584	1.0125	6.394	6.314	.98769
20	.0233	.0233	1.0003	42.98	42.96	.99973	40	.1593	.1614	1.0129	6.277	6.197	.98723
30	.0262	.0262	1.0003	38.20	38.19	.99966	30	.1622	.1644	1.0134	6.166	6.084	.98676
40	.0291	.0291	1.0004	34.38	34.37	.99958	20	.1650	.1673	1.0139	6.059	5.976	.98629
50	.0320	.0320	1.0005	31.26	31.24	.99949	10	.1679	.1703	1.0144	5.955	5.871	.98580
10	.0378	.0378	1.0007	26.45	26.43	.99939	88	.1708	.1733	1.0149	5.855	5.769	.98531
20	.0407	.0407	1.0008	24.56	24.54	.99931	50	.1738	.1763	1.0154	5.759	5.671	.98481
30	.0436	.0437	1.0010	22.93	22.90	.99923	40	.1768	.1793	1.0160	5.665	5.576	.98430
40	.0465	.0466	1.0011	21.49	21.47	.99915	30	.1794	.1823	1.0165	5.575	5.485	.98378
50	.0494	.0495	1.0012	20.23	20.21	.99907	20	.1822	.1853	1.0170	5.488	5.396	.98325
10	.0552	.0553	1.0015	18.10	18.07	.99897	10	.1851	.1883	1.0176	5.403	5.309	.98272
20	.0581	.0582	1.0017	17.20	17.17	.99891	87	.1880	.1914	1.0181	5.320	5.226	.98218
30	.0610	.0612	1.0019	16.38	16.35	.99883	50	.1908	.1944	1.0187	5.241	5.145	.98163
40	.0640	.0641	1.0020	15.64	15.60	.99875	40	.1937	.1974	1.0193	5.164	5.066	.98107
50	.0669	.0670	1.0022	14.96	14.92	.99866	30	.1965	.2004	1.0199	5.089	4.989	.98050
10	.0698	.0699	1.0024	14.34	14.30	.99856	20	.1994	.2035	1.0205	5.016	4.915	.97992
20	.0727	.0729	1.0027	13.76	13.73	.99846	10	.2022	.2065	1.0211	4.945	4.843	.97934
30	.0756	.0758	1.0029	13.23	13.20	.99836	86	.2051	.2095	1.0217	4.877	4.773	.97875
40	.0785	.0787	1.0031	12.75	12.71	.99826	50	.2079	.2126	1.0223	4.810	4.705	.97815
50	.0814	.0816	1.0033	12.29	12.25	.99816	40	.2108	.2156	1.0230	4.745	4.638	.97754
10	.0843	.0846	1.0036	11.87	11.83	.99806	30	.2136	.2186	1.0236	4.682	4.574	.97692
20	.0872	.0875	1.0038	11.47	11.43	.99796	20	.2164	.2217	1.0243	4.620	4.511	.97630
30	.0901	.0904	1.0041	11.10	11.06	.99786	10	.2193	.2247	1.0249	4.560	4.449	.97566
40	.0929	.0934	1.0043	10.76	10.71	.99776	85	.2221	.2278	1.0256	4.502	4.390	.97502
50	.0958	.0963	1.0046	10.43	10.39	.99766	50	.2250	.2309	1.0263	4.445	4.331	.97437
10	.0987	.0992	1.0049	10.13	10.08	.99756	40	.2278	.2339	1.0270	4.390	4.275	.97371
20	.1016	.1022	1.0052	9.839	9.788	.99746	30	.2306	.2370	1.0277	4.336	4.218	.97304
30	.1045	.1051	1.0055	9.567	9.514	.99736	20	.2334	.2401	1.0284	4.284	4.165	.97237
40	.1074	.1080	1.0058	9.309	9.255	.99726	10	.2363	.2432	1.0291	4.232	4.113	.97169
50	.1103	.1110	1.0061	9.065	9.010	.99716	84	.2391	.2462	1.0298	4.182	4.061	.97100
10	.1132	.1139	1.0065	8.834	8.777	.99706	50	.2419	.2493	1.0306	4.133	4.011	.97030
20	.1161	.1169	1.0068	8.614	8.556	.99696	40	.2447	.2524	1.0314	4.086	3.962	.96959
30	.1190	.1198	1.0072	8.405	8.345	.99686	30	.2476	.2555	1.0321	4.039	3.914	.96887
40	.1219	.1228	1.0075	8.206	8.144	.99676	20	.2504	.2586	1.0329	3.994	3.867	.96815
50	.1248	.1257	1.0079	8.016	7.953	.99666	10	.2532	.2617	1.0337	3.949	3.821	.96742
10	.1276	.1287	1.0082	7.834	7.770	.99656	83	.2560	.2648	1.0345	3.906	3.776	.96667
20	.1305	.1317	1.0086	7.661	7.596	.99646	50	.2588	.2679	1.0353	3.864	3.732	.96593
30	.1334	.1346	1.0090	7.498	7.429	.99636	40	.2616	.2711	1.0361	3.822	3.689	.96517
40	.1363	.1376	1.0094	7.337	7.269	.99626	30	.2644	.2742	1.0369	3.782	3.647	.96440
50							20	.2672	.2773	1.0377	3.742	3.606	.96363
							10	.2700	.2805	1.0386	3.703	3.566	.96285
							82	.2728	.2836	1.0394	3.665	3.526	.96206
							50						74

Cosin. Cotg. Cosec. Sec. Tan. Sine. Angla. Cosin. Cotg. Cosec. Sec. Tan. Sine. Angla.

#1 - 00 Cement step at Arbucks

Front Gate - 119.94

#2 - 00 Corner stone at sta - 32+30

117.29

#3 - 00 Corner stone at sta - 71+85.5

116.57

#4 - 00 Corner stone at sta 79+82 -

114.49

#5 - 00 corner stone at sta. 92+65 -

110.53

#6 - 00 N. End of East Rail of Culvert 150' South
of sta. 98+68 - 110.30

at Sta. 12.2 N. End

at Sta. 12.2 N. End
at Sta. 12.2 N. End
at Sta. 12.2 N. End

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.