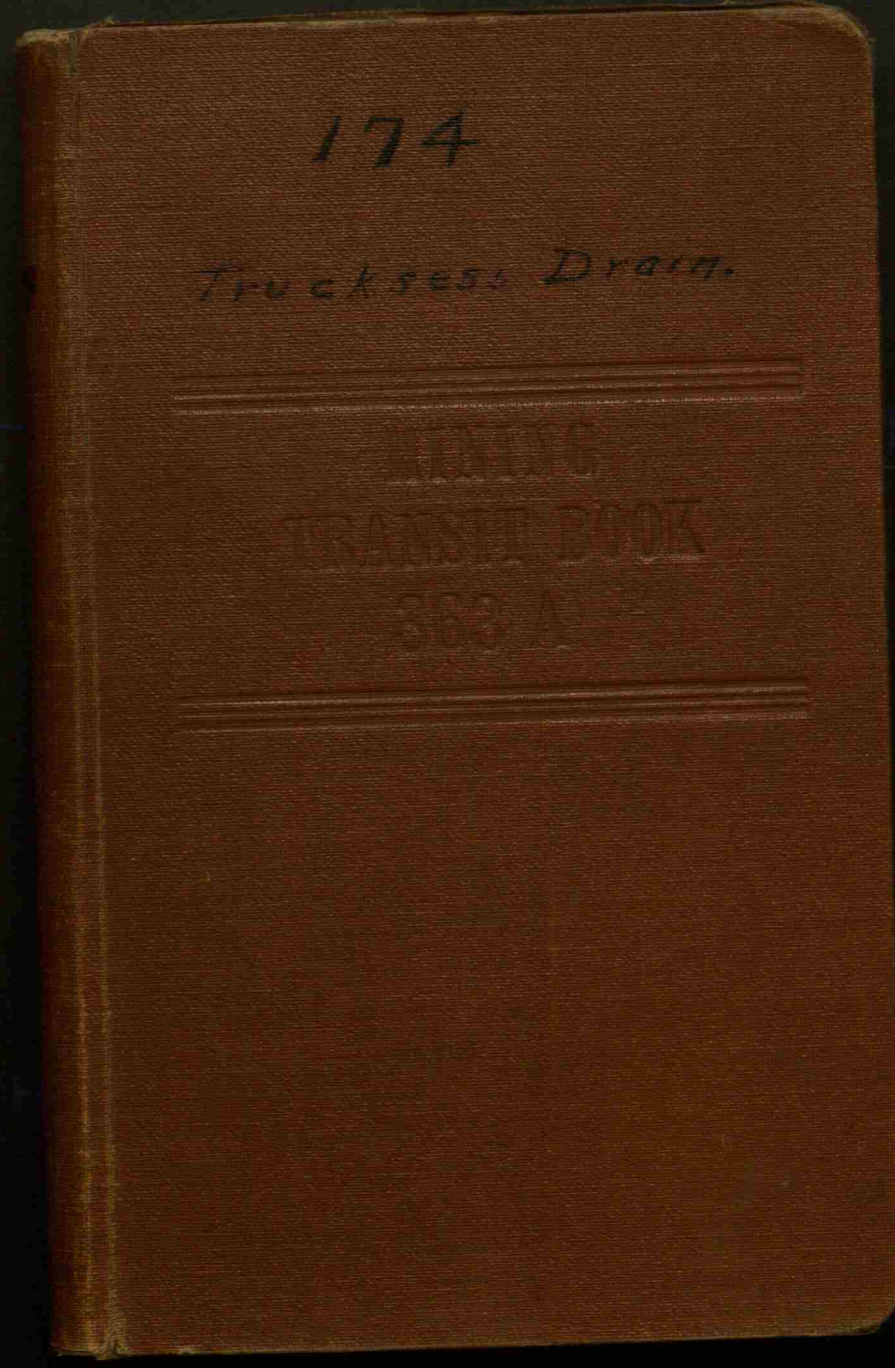


LR

A3 11x17 LR A3 11x17

← A3 →

← 11x17 →



174
Trucksess Drain.

MINING
TRANSIT BOOK
368 A

← ER →



2

+	∩	-	BM
3.62	108.62		100.00 →

4.24	100.69	7.17	96.45
------	--------	------	-------

3.00	97.74	5.95	94.74
------	-------	------	-------

1.62	97.16	2.20	95.54
------	-------	------	-------

4.85	91.24	10.77	86.39
------	-------	-------	-------

1.26	89.98	Per. BM	
------	-------	---------	--

Trucksess Ditch
below outlet of tile

3

West End of Main Head Wall

FL. Tile N. of Ditch = $\frac{95.97}{7.65}$ 29725
Top " " " " = 6.38

FL. 100' N. = $\frac{96.37}{7.25}$

Top 100' N = 5.98

250' North ^{at fence} = 5.38

Ditch $\frac{93.89}{6.33}$ - 12+0

Ditch $\frac{90.41}{7.33}$ - 8+25

FL. Tile at R.R. = $\frac{82.00}{9.24}$ sta. 0+0
Ditch $\frac{94.94}{6.36}$ sta. 3+0

017 SW cor. West End of North Headwall.

4

Check

+	∓	-	BM
4.86	91.24		86.99
2.95	83.39	9.80	81.44
3.81	82.14	6.06	77.33
1.26	91.24	1.26	89.98
9.20	96.18	9.86	86.38
6.06	99.29	2.95	93.23
		3.81	95.48

$$\begin{array}{r} 863.90 \\ 486 \\ \hline 867.76 \end{array}$$

5

Ditch

98.84 sta. 6+70
10.95

Old Desc. of Line of ⁵¹/₄₅₁
 6 French E. Trucksess Drain
 Beg at NE corner Sec. 11-16-1E
 Thence S 2650'
 " W 1200'
 " S5°W 250'
 " S20°W 400' and terminate at
 Stake 45 of what is known as
 the Christopher Trucksess Drain

⁵⁵/₄₂₀ Continuation of Drain as
 The Christopher Trucksess Drain
 Thence S 265'
 " S28°W 200'
 " S50°W 300'
 " S20°W 780'
 " S47°W 170'
 " S29°W 200'
 " S45°W 300'
 " S61°W 530'
 " S4°W 350'
 " S27°W 160'
 " S8°W 160'
 " S 780'
 " S28°W 160'
 " S40½°W 180'
 " S22°W 230'

Size of Tile

10" - 0+00 to 26+00
 12" - 26+00 to 45+00
 — Fall —
 .20 - 0+0 to 16+0 } 3.20
 .30 - 16+0 to 22+0 } 1.80
 .15 - 22+0 to 30+0 } 1.20
 .20 - 30+0 to 38+0 } 1.60
 .40 - 38+0 to 42+0 } 1.60
 .05 - 42+0 to 45+0 } .15
 Total Fall - 9.55

8

Thence	S 89° W	130'
"	S 65½° W	210'
"	S 31° W	230'
"	S 7° W	220'
"	S 4½° W	360'
"	S 15½° W	200'
"	S 44° W	300'
"	S 69° W	500'
"	S 23° W	470'
"	S 72° W	80'
"	S 64° W	967'

and terminating
20' North and 30' West of the
Center on the South of the
SE⁺ of Sec. 15-16-1E

9

Size of Title

12" - 0+0 to 6+0
14" - 6+0 to 49+32
16" - 49+32 to 94+32

S

Harry Sumpter } Feb. 13. -
Oscar Hyten } 2½ hrs.

Feb. 15.
Harry Sumpter 7½
Oscar Hyten 5½

Feb. 19.

Line

0+0
 6+25.5 4" tile archhole Concrete band
 13+20 Wash S. line & Truckers N. line
 26+63 Truckers S. line
 26+50 Def. R. $89^{\circ}00'$
 38+50 Def. L. $72^{\circ}15'$
 38+63 Truckers S. line of 80 a. tract
 45+22 Truckers S. line & N. line of
 old. I.N. 9 & E. Zinc Co.
 45+46.5 N. end. T.N. 9 & E. Bridge
 45+61 Def. R. $0^{\circ}38'$
 45+64 S. end T.N. 9 & E. Bridge
 45+94 N. end P. & E. Bridge
 46+03 N. rail
 46+08 S. rail
 46+16.5 N. Switch rail
 46+21.5 S. Switch rail
 46+31 S. end P. & E. Bridge
 46+39 S. R/w P. & E. Fence.
 50+41 Def. L. $27^{\circ}50'$
 50+57 N. side Pav't
 50+99 S. " Pav't
 51+12 S. Fence of Rd. Pav't.
 51+07 S. end 3' x 2' box Haul. 12' long.

T.H. 9 & E. Bridge

8' Span } Concrete Flat top
 5' Rise }

P. & E. Riv. Big Four Bridge

Stone Arch.

N. end

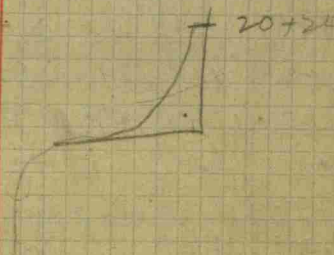
S. end



Rise N. end. 3'

Rise S. end. 3'

(45+0)



50+41 - Inlet basin N side of rd with
2' square

with $3\frac{1}{2}' \times 3\frac{1}{2}'$ inlet with 6" tile inlet down
to main tile

14

136+36 Def R. $44^{\circ}30'$
 139+89 Def L $16^{\circ}52'$
 143+70 Def L $40^{\circ}03'$
 147+21 Def R. $23^{\circ}47'$
 152+44 Def R $15^{\circ}05'$
 155+67 Nichols W. line and Medich
 156+49 Def. L $40^{\circ}30'$
 160+48 Def. R. $34^{\circ}12'$
 164+32 End.

15

139+89 - 603' E. to E of N&S Rd.

139+89 - end of tile
SE corner.

162+10 - 154 ft. E. to Nichols
SW. corner

164+18 - N. fence line of R.R.

95 to 14" tile comes into main

16

Curve Notes

Two Simple Curves.

$$PC = 21+61$$

$$PI = 23+50$$

$$PT = 25+39$$

8

$$PC = 27+61$$

$$PI = 29+50$$

$$PT = 31+39$$

$$\Delta = 44^{\circ}-30'$$

$$E = 37'$$

$$D = 12^{\circ}-29'$$

$$T = 189$$

$$L = 359$$

$$R = 442$$

One Simple Curve.

$$PC = 21+60$$

$$PI = 26+50$$

$$PT = 31+40$$

$$\Delta = 89^{\circ}-0'$$

$$D = 11^{\circ}-30'$$

$$T = 490'$$

$$L = 773.8$$

$$R = 498.2$$

$$E = 200'$$

17

$$PC = 39+89.3$$

$$PI = 36+37$$

$$PT = 37+89.7$$

$$\Delta = 29^{\circ}-51'$$

$$E = 20'$$

$$T = 152.7$$

$$D = 10^{\circ}$$

$$R = 573-L = 298.5$$

$$PC = 38+80$$

$$PI = 42+22$$

$$PT = 45+69$$

$$\Delta = 33^{\circ}-15'$$

$$E = 50'$$

$$D = 5^{\circ}$$

$$T = 342.2$$

$$L = 665$$

$$R = 1146$$

18

Feb. 18, 35

+	-	BM	#
8.06	108.06	100.00	#1
4.56	111.95	106.89	#2
8.99	119.87	105.93	#3
3.87	116.79	112.92	#3
4.64	115.29	110.60	#3
4.03	112.84	108.81	#3
		3.54	#4
4.53	116.64	112.11	#4
6.23	118.14	111.93	#4
6.30	120.31	114.01	#4
9.81	123.14	113.33	#4
4.24	122.45	118.21	#4
0.67	119.32	118.65	#4
4.50	118.84	114.31	#5
		4.66	#5
6.52	126.10	119.58	#5
1.40	122.67	121.27	#5

19

BM. EL. 89.98 on SW. Cor.
West End North Hwd. Sta. 169+32

B.M. EL. 100.00 on West End
of Main Hwd. Sta. 139+89

B.M. EL. 105.93 on South End of
Wing on East Side Road Sta. 127+45

112.11
4.68

B.M. EL. 109.30 Iron spike in tulip
tree 100' N on Armstrong W. line.

119.58
2.87

B.M. EL. 114.18 on NW cor. of square.
Wall apron about Sta. 7+0

116.28
6.39

B.M. EL. 116.28 on the O in O¹⁰⁰
in C.B. South side State Rd
Sta. 5+0

110.09
12.58

FL T. 14

20

+	∧	-	BM	
	122.67			#7
5.87	126.09	2.45	120.22	
		5.49	120.60	#8
3.64	125.78	4.00	122.09	
		5.66	120.12	#9
6.01	126.23		120.22	Ch. in
4.41	126.17	4.47	121.76	Road
4.14	125.92	4.39	121.78	N+S
4.27	124.61	5.58	120.34	
		8.38	116.23	

Feb. 19,
35.

6.75	122.98		116.23	
10.64	130.62	3.00	119.98	
5.66	129.61	6.67	123.95	
5.71	129.18	6.14	123.77	
		5.36	123.82	#10

95.46

21

BM. E.L. 120.22 55' E. end of South Head
of Rail Road bridge Sta 26+31

BM. E.L. 120.60 N.E. corner of North Head
rail of Sta 26+5 Bridge Sta 25+46

BM. E.L. 120.12 on head of nail in
port of tree at Sta 26+75

← on nail in tree in N+S gut
Highway E.L. 116.23

113.18

9.20

elevation in gully

BM. E.L. 123.82 On E. End of South Head
175' West of 0+0

22

+

π

-

BM.

BM
Check

W.

F 23

0+0

129.18

1+0

2+0

3+0

4+0

5+0

6+0

5.65 128.25 6.58 122.60

6+25

7+0

8+0

9+0

STK

123.08

61

125.38

38

125.93

325

125.88

33

124.08

51

122.38

68

122.58

66

122.13

Gd

7.05

123.98

Gd

6.7

123.68

Gd

5.6

123.42

Gd

5.75

122.23

Gd

6.95

121.08

Gd

8.1

121.23

Gd

7.95

119.05

9.20

122.40

585

122.33

592

122.83

542

120.90

Gd

7.35

121.05

Gd

7.2

121.45

Gd

6.8

119.93

T.T.

9.25

119.08

F.T.

10.1

24	+	π	-	BM
		128.25		
110+0				
111+0				
12+0				
13+0				
	5.55	127.36	6.44	121.81
14+0				
15+0				
16+0				
17+0				
18+0				
19+0				
20+0				
	2.68	123.60	6.94	120.92

W	Stk	E 25
	123.85	121.45
	4.9	6.8
	124.23	121.95
	4.02	6.3
	123.25	121.95
	5.00	6.3
	121.80	120.45
	6.95	7.8
		117.30
		10.95
	121.41	120.26
	5.95	7.1
	124.16	123.06
	3.2	4.3
	123.86	122.56
	3.5	4.8
	123.01	121.71
	4.85	5.65
	121.36	120.41
	6.00	6.95
	120.01	119.76
	7.35	7.6
		116.76
		10.60
	120.96	119.66
	6.40	7.7

26

+ T T BM

123.60

2310

20+75

2110

2210

2310

2410

2910

2810

2710

26+50

2610

2510

3.52
120.08
120.12

w

STK

27

119.10
Grd 100'
4.5

119.82
3.78

118.85
Grd
4.75

116.50
T.T.
71

118.10
Grd 75'
5.5

118.55
5.05

117.90
Grd
5.7

116.30
T.T.
7.3

118.40
Grd 75'
5.2

119.70
3.9

118.95
Grd
4.65

118.90
Grd 100'
4.7

119.65
3.95

118.80
Grd
4.8

118.85
200' Grd
4.75

119.25
Grd 176'
4.85

119.70
3.9

118.60
Grd
5.0

~~119.10~~
118.95

119.85
4.25

117.90
Grd
5.8

114.85
T.T.
8.75

120.80
2.8

119.60
Grd
4.0

120.00
3.6

118.85
Grd
4.75

119.75
3.95

118.95
Grd
4.65

119.95
3.65

118.80
Grd
4.8

119.70
3.9

118.70
Grd
4.9

28	+	$\bar{\lambda}$	-	BM.
30+0	3.30	123.42		120.12
31+0				
31+				
32+0				
33+0	4.00	122.14	5.28	118.14
34+0				
35+0				
35+50				
36+0				
37+0				
38+0				
38+50				
40+0				

X	5+R	5	29
118.12 Gd 100' 5.3	118.97 45	117.67 Gd 5.75	
117.97 Gd 50' 3.45	118.45 4.97	117.42 Gd 6.0	
		TT 8.55	
	118.82 4.6	117.62 Gd 5.9	
	118.17 5.25	116.98 Gd 6.44	
	119.54 2.6	118.34 Gd 3.8	
	119.29 2.85	118.12 Gd 4.02	
		TT 7.9	114.24
	118.76 3.38	117.64 Gd 4.5	118.24 20' 3.9
	118.04 4.1	117.14 Gd 5.1	117.19 50' 4.96
	117.24 4.9	116.29 Gd 5.85	116.49 100' 5.65
	117.64 4.5	116.69 Gd 5.45	116.44 140' 5.7
		TT 8.9	TT 113.24 +35
			E 116.44 5.7

32

+

A

-

BM

50+0

121.01

50+41

50+

51+

4.78
116.23

52+0

53+0

54+0

5.93 120.30 6.69 114.37

55+0

56+0

57+0

58+0

59+0

33

5+6

114.36 113.36 111.33

6.65 7.65 9.68

115.89 113.66 114.97

5.62 7.35 6.54

116.23
Top Con. Par. 4
4.78119.01
Top Con. Inlet
7.0

112.31

8.7

116.66

4.25

114.26

6.75

114.36

6.65

114.60 112.65 TT 110.70

57 7.65 9.6

114.17 112.56

6.13 7.79

114.45 113.21

5.85 7.09

115.20 113.10

5.1 7.20

114.46 113.35

5.84 6.95

34

+

K

-

BM

120.30

60+0

61+0

62+0

63+0

5.19

12006

543

119.87

64+0

65+0

66+0

67+0

67+70

68+0

69+0

70+0

5.88
119.12

W

Stk

E35

114.40 113.20

59 7.1

114.55 113.40 109.55

575 6.9 10.75

115.80 113.20

95 7.1

114.90 113.100

54 7.3

114.86 112.91

52 7.15

114.11 112.86

595 7.2

113.66 112.51

64 7.55

113.41 112.26

665 7.8

112.86 112.01

72 8.05

113.12 112.06

694 8.00

112.91 111.51

715 8.55

112.34 111.30

782 8.76

36

+	π	-	BM
174	115.92		119.18

70+75

71+0

72+0

73+0

74+0

75+0

76+0

77+0

78+0

3.31	119.78	5.45	110.47
------	--------	------	--------

79+0

79+89

80+0

80+50

w

SK

E 37

108.102
T.T.
7.9

111.70	110.82
4.22	5.10

112.92	111.17
3.00	4.75

112.74	110.72
3.18	5.2

111.50	110.57
4.42	5.35

111.72	110.32	107.12
4.20	5.6	T.T.
		8.8 + 25

111.62	110.17
4.3	5.75

110.92	109.74
5.0	6.18

110.97	109.57
5.45	6.35

110.16	109.23	
3.62	4.55	106.73
107.88	108.88	T.T.
3.90	4.9	7.05

110.08	109.03	
3.7	4.75	106.64
		T.T.
		7.14

+

Λ

-

BM

118.74

80+75

81+0

82+0

83+0

84+0

84+48

2.81 112.28 9.31 109.97

85+0

85+25

86+0

87+0

87+83

w

stk

109.77 109.03
4.01 4.75109.93 108.98
3.95 4.80109.88 108.98
3.9 4.8109.86 108.88
3.92 4.9109.60 108.78
4.18 5.0109.48 108.63
4.20 5.15109.08 108.28
3.2 4.0105.88
6.4109.13 108.33
3.15 3.95108.73 108.03
3.55 4.25108.33 107.53
3.95 4.75

40

+

 $\bar{\Delta}$
112.28

BM

89+0

89+0

90+0

91+0

92+0

3.98 111.73 4.53 107.75

93+0

94+0

95+0

95+56

96+0

96+20

96+75

W

SHC

5 41

108.39 107.62
39 4.66108.28 107.43
400 4.85108.08 105.08
420 5.01 TT 7.20108.08 107.13
420 5.15107.75 106.98
453 5.30107.49 106.58
425 5.15107.55 106.53 104.68 104.78
418 5.2 TT 7.05 6.95107.62 104.40 103.03
411 5.5 TT 7.33 FLT 8.7107.00 104.42 106.83 TT
473 5.4 7.91 (+5)107.20 116.23
453 5.6109.40 102.96
TT FT
733 8.77104.13
TT
7.6

42

+

A

-

BM

111.73

9710

97+50.

9810

98+65

2.82 111.05 3.50 108.23

9910

10010

100+54

10110

10210

10310

10410

4.62 113.12 2.55 108.50

3.82
109.30

51K

43

10752 106.58
4.21 5.15103.98
TT
7.7510771 106.81
4.02 4.9210823 106.71
3.50 5.0210825 106.85
2.8 4.210797 106.95
3.58 4.610747 106.38
3.58 4.6710763 106.25
3.42 4.810719 106.45
3.86 4.610815 106.75
2.9 4.3510851 106.60 101.19
2.54 4.45 9.86

44

+

A

-

B/M

113.12

105+0

106+0

107+0

107+80

3.04

112.34

109.30

108+0

109+0

110+0

111+0

112+0

4.93

111.14

6.13

106.21

113+0

114+0

SHK

45

107.30 106.12

5.82 7.0

107.12 105.97

6.00 7.15

106.97 105.74

6.15 7.38

102.72
TT
10.40

107.69 105.49

4.65 6.85

106.24 105.39

6.1 6.95

105.54 105.14

6.8 7.2

116.37 105.14

5.95 7.2

106.19 104.99

6.15 7.35

106.19 104.89

5.00 6.25

105.24 104.79

5.9 6.35

46

+

 π

-

BM

111.14

119+19

115+0

115+50

116+0

117+0

117+80

118+0

119+0

120+0

5.22

110.20

6.14

105.00

121+0

122+0

123+0

4

5+K

5⁴⁷105.04 104.54
61 6.6105.54 104.64
56 6.5101.19
T.T.
9.95105.04 104.49
61 6.65105.24 104.44
59 6.7104.74 104.39
64 6.75104.94 104.39
62 6.75104.72 104.26
642 6.88104.99 104.19
615 6.95105.02 103.82
52 6.4105.32 103.57
49 6.65104.07 103.32
615 6.9

48

+ 7 - BM

110.22

12410

12510

12610

12610

2.97

10890

105.93

12810

12910

13010

13110

13210

13310

13410

110.22
10.72
99.50480
105.93
105.93108.70
108.50

51K

101.19
99.52
49
1.67

10425 104.40

537 5.82

103.59 102.67

663 7.55

99.52

TT

10.7

103.50 102.87

672 7.35

103.70 102.89

652 7.38

Road

3.45

3.00

3.10 5.20

104.35 103.80

4.55 5.1

10300 102.30

59 6.6

10270 101.92

62 6.98

102.20 101.65

67 7.25

102.47 100.90

648 8.00

98.40

TT

10.8

98.65

TT

10.25

10210 101.10

68 7.8

10185 100.40

705 8.5

50

+ ̂ - B/M

108.90

135+0

13

136+0

3.29 103.99 8.20 100.70

136+36

137+0

138+0

+50

139+0

+60

139.92

51

StK

101.49 100.10

7.11 8.8

110.71 99.65

8.19 9.25

100.89 99.29

3.7 4.7

100.19 99.04

3.8 4.95

99.61 98.59

4.38 5.4

99.49 97.69

4.5 6.3

97.74 96.34

7.1 7.65

6.25 7.65

97.96 96.17

6.63 7.82

97.73

97.09

6.26

6.90

+ A - BM

3.92 103.92 100.00

139+92

140+0

141+0

142+0

3.54 101.60 5.86 98.06

143+0

143+70

144+0

145+0

146+0

147+0

2.61 100.24 3.97 97.63

147+21

148+0

Stk.

97.09 96.42

97.66 6.26 6.93 7.20 7.75 7.5

97.42 96.72 96.74 96.22 96.63 98.76
6.13 7.2 7.18 7.7 7.3 5.698.62 98.22 97.47 97.52 96.02 95.77 96.42 98.76 98.12
5.3 5.7 6.45 6.4 7.9 8.15 7.5 5.6 5.897.77 96.95 96.2 97.72 98.97
5.2 2.2 5.1 1.2 2.3
6.15 6.97 8.45 7.7 6.2 4.9597.15 97.00 95.85 96.50 96.20 97.06 96.20
1.0 8 3 5 15 15 25
4.15 4.3 6.25 5.1 5.4 4.54 5.4097.70 97.25 97.06 95.25 96.00 95.60 97.00 97.40
3.9 4.35 4.54 6.35 6.6 6.0 4.6 4.297.85 97.10 95.06 94.76 95.16 96.00 96.70
3.75 4.00 6.55 6.85 6.35 5.6 4.997.96 96.75 96.55 94.65 94.30 94.65 95.75 96.85
4.24 4.85 5.05 7.05 7.3 6.95 5.85 4.7597.15 96.50 94 17 20 23 25 30
4.45 5.1 5.7 7.1 7.5 7.25 5.6 5.2597.40 95.50 96.01 94.05 95.50 94.45 95.95 95.85
3 45 5.5 5 7 10 20 25
4.20 6.1 5.59 7.55 8.10 7.15 5.65 5.7597.60 97.00 97.44 96.64
2.16 3.25 3.8 4.7
95.27 94.74 95.04 95.54 94.59
3.18 10 25 30
4.87 5.5 6.2 5.7 5.65

+ X - BM

100.29

149+0

149+20

150+0

150+50

151+0

152+0

152+99

152+65

153+0

6.87 100.29 6.87 93.37

154+0

154+70

155+0

94.89	93.87	93.94	93.94	93.66
stK	sd	5	20	30
5.35	6.35	6.30	6.30	6.6

92.64
 to stream 7.6

94.14	93.54	93.14	94.00	94.19
stK	sd	10	17	30
6.1	6.7	7.1	6.25	6.1

92.04
 to stream 8.4

94.04	93.69	92.44	93.04	93.14
stK	sd	10	20	30
5.9	6.56	7.3	7.2	7.1

93.82	93.24	93.24	93.24	94.00
stK	sd	10	20	30
6.92	7.0	7.0	6.9	7.25

94.40	93.84	93.04	92.84
stK	sd	10	25
6.81	7.4	7.2	7.4

91.94
 to stream 8.3

93.54	92.74	92.74	92.84
stK	sd	10	30
6.7	7.5	7.5	7.4

93.03	92.29	92.14	91.89
stK	sd	10	25
7.21	7.95	8.1	8.35

91.24
 to stream 9.00

92.64	92.00	91.64	91.24	91.24	91.89
stK	sd	10	25	30	30
7.60	8.25	8.60	9.0	9.0	8.35

56

+ T - BM

100.29

156 to

156+99

157 to

157+50

158 to

158+70

159 to

87.38 95.96 9.66 90.58

160 to

160+98

161 to

162 to

163 to

57

92.34	91.59	91.54	91.39	90.74
5+K		10	25	30
7.9	8.65	8.7	8.9	9.50

91.02	90.39	90.34	91.79	91.11	91.19
5+K		5	15	30	40
6.20	6.85	7.9	8.45	9.05	9.05

92.00	91.12	91.04	90.89	90.79
5+K		5	15	20
9.65	9.06	9.20	9.35	9.45

89.14

Q stream 11.1

91.07	90.29	90.14	90.25
5+K		10	25
9.17	9.25	10.1	9.9

88.94

Q stream 11.30

90.59	89.94	89.74	89.59
5+K		10	20
9.65	10.3	10.50	10.65

89.26	88.66	88.46	87.96	87.66	87.76
5+K		5	10	15	25
6.6	7.3	7.5	8.0	7.3	7.2

89.31	88.70	88.26	87.96	87.06	87.31	87.76
5+K		5	10	15	20	30
6.65	7.21	7.7	8.0	8.9	9.65	8.2

88.56	87.91	87.35	86.86	87.36
5+K		5	10	25
7.4	8.05	9.61	9.1	9.6

88.11	87.46	87.26	87.31	86.86
5+K		10	25	35
7.85	8.5	8.7	9.65	9.1

87.14	86.81	86.81	85.96	85.81
5+K		10	25	35
8.80	9.45	9.75	10.0	10.15

58

+

⌘

-

BM

95.96

164+0

169+32

1.69

91.62

89.98

169+32

59

86.36	86.71	85.81	85.46	85.26
5.1K	15	25	30	
9.6	10.25	10.15	10.5	10.7

85.51	84.76	84.11
5.1K	6	
10.95	11.2	11.96

82.32	82.02	82.72	84.01	85.02
8	10	13	16	20
9.30	9.60	8.80	7.61	6.60

Fl. of CIPPA 9.55

60

	+	π	-	BM
	4.12	127.94		123.82

0+55

3+0

6+25

	5.26	128.15	5.05	122.89
--	------	--------	------	--------

17+0

20+0

		7.16		121.04
--	--	------	--	--------

61

119.54	
TT	
8.4	2.6 broken out
119.24	118.99
T.T.	F.T.
8.7	9.55
118.54	
TT	
9.5	
118.34	
9.6	

9+0

117.10	
TT	
11.05	
116.67	116.04
TT	TT
11.48	12.11

Broken file

62

+	+	-	BM
2.25	126.14		123.86

16+0

15+0

14+0

FL City Sewer	8.3'
Top "	7.0'

63

117.04

TT

9.07

117.10

9.01

121.40

5.71

4.71

117.09

TT

9.02

72

—	π	+	B.M.
			99.72
	108.17	8.45	
11.35			96.82
	105.67	8.85	
11.95			93.72
6.63			99.04
	102.07	3.03	
10.50			91.57

Return check

91.57 $\frac{\$}{\text{Creek at Outlet}}$

	102.07	10.50	
1.15			100.92
	113.06	12.14	
5.50			107.56
	117.56	10.00	
.62			116.94
	121.99	5.05	
1.32			120.67
	126.87	6.20	
6.12			120.75
	126.75	6.00	

Trucksess Ditch Cont. 73

12.35 - $\frac{\$}{\text{open Ditch}}$ 11.95 $\frac{\$}{\text{open Ditch}}$

$$\begin{array}{r} -91.57 \\ 10.50 \end{array} \frac{\$}{\text{Creek at Outlet}} \text{ Sta. 0+00}$$

74

-

x

+

BM

126.75

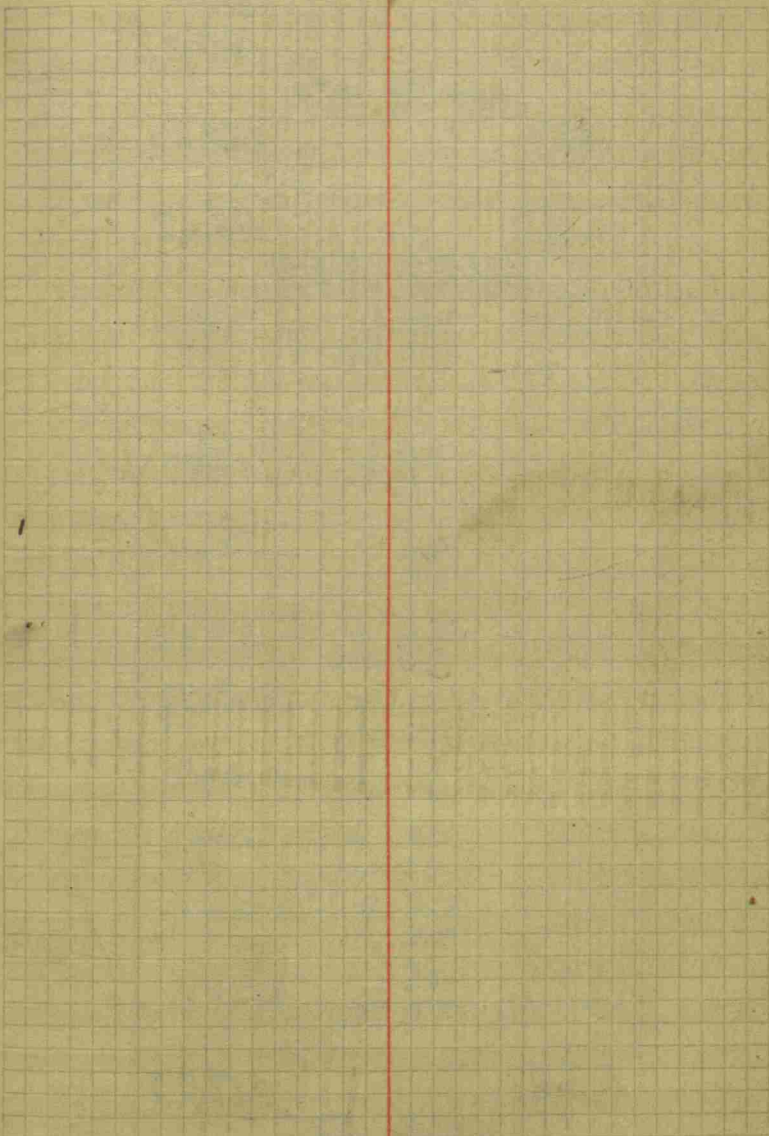
5.45

121.30

Temp BM.
at RR.

Trucksess Ditch Cont.

75



76

-	π	+	BM
			120.22
	124.92	4.70	
4.31			120.61
6.75			118.67
	121.27	2.60	

3,30

123.22	5.25	117.97
--------	------	--------

June 28th 1939 77

0+00	5.05	at tile
	116.22	

1+00	3.90
	117.37

2+00	4.30
	116.97

3+00	4.38
	116.89

4+00	4.90
	116.37

5+00	4.15
	117.12

6+00	4.30
	116.97

7+00	4.30
	116.97

8+00	3.30
	117.97

78

- π + BM

123.22

6.55

123.82

7.15

116.67

79

9+00

6.20

117.02

10+00 6.48

116.74

11+00 5.70

117.52

12+00 4.80

118.42

13+00 5.15

118.07

14+00 5.70

117.52

15+00 5.80

117.42

16+00 6.30

116.92

17+00 5.10

116.72

18+00 7.20

116.62

19+00 7.85

115.97

20+00 9.50

114.32

21+00 10.15

113.67

22+00 10 50
113 32

23+00 10 75
113 07

24+00 11 60
112 22

25+00 12 20
111 62

7 15
116 67

[Faint handwritten text at the bottom of the notebook, possibly bleed-through from the reverse side.]

84

-	+	BM
		120.22
	126.32 6.10	
4.60		121.72
	125.57 3.85	
4.28		121.29
	125.71 4.42	
3.47		122.24
	126.44 4.20	
5.10		121.34
	125.14 3.80	
4.40		120.74
	124.69 3.95	

B.M. at
Railroad

7.03		117.66
	122.53 4.87	

June 29th 1939.

85

120.62
5.70

119.23

5.46 E Rd at culvert

112.96

11.73 Fl. line of Culvert

114.21

8.32 El. of Ditch

	-	+	BM
			112.96
	124.46	11.50	
3.70			120.76
	125.06	4.30	
3.70			121.36
	126.71	5.35	
4.47			122.24
	125.74	3.50	
4.42			121.32

Fl. line of
calvert.

-	π	+	BM
			120.60
	124.52	392	
475			119.77
	122.47	270	

3.00

124.47

500

119.47

0+00	5 25 117 22
1+0	4 25 118 22
2+0	4 00 118 47
3+0	4 85 117 62
4+0	4 68 117 79
5+0	4 38 118 03
6+0	4 96 117 51
7+0	3 40 119 07
8+0	4 22 118 25
9+0	4 20 118 27
10+0	3 00 118 47

- π + BM

12447

980

120.79

6.12

114.67

11+0	4 65	
	119 82	
12+0	5 60	
	118 87	
13+0	5 65	
	118 82	
14+0	6 15	
	118 32	
15+0	6 20	
	118 27	
16+0	6 25	
	118 22	
17+0	8 40	
	116 07	
18+0	9 20	
	115 27	
19+0	9 30	
	114 57	
20+0	6 30	
	114 49	
21+0	6 25	
	114 54	
	112 89	
	7 90	Fl. line
	118 16	
	2 63	± Grant

94

BM CHECK

			120.22	
	125.18	496		
4.58			120.60	
5.45			119.73	Rock BM
4.58			120.60	
			112.96	BM at Fl. line tile
	123.49	10.53		
5.20			118.29	Grant St.
			121.30	BM at RR on Grant
	126.25	4.95		
4.20			122.05	
	126.15	4.10		
5.50			120.65	
	124.55	3.90		

3:00 PM 6/29/39

95

118.28
6.27 Grant

112.95
11.60 Fl. line tile

98

Steve Maloney Tile
June 17, 1943 M. Newman
S. Maloney

-	π	+	B.M
	104.11	4.11	100.00

5.85			98.26
------	--	--	-------

106.31	8.05		
--------	------	--	--

0.50			105.81
------	--	--	--------

106.21	2.40		
--------	------	--	--

9985
9001
2.83

96.02
97.22

1.20
99

0+0 Culvert at Hdwr. 809

0+25 7.39

7.08

6.89

6.39

6.30

5.85 98.26

7.48 98.73

900 99.20

836 99.95 E. SIDE RD

815 W. SIDE RD

100

-	+	BM
3.23		104.76
113.93	8.95	
5.50		108.43
115.28	6.85	
2.05		113.23
115.28	2.05	
8.06		107.22

101

Jim H. Hogan
 Steve Maloney
 Prop Mine

8.06 107.22 4 1/2"

Nash Drain

July 7, 1941

Cross pres. tile 138+50
 " " " 136+30
 " " " 135+50

356 1/2 ft S. of E of Rd
 running West N. of
 Hufferd Bridge

cross Pres. tile 130+0

128+65 W. R/W Avon-Brownsburg Rd
 128+30 E " " " "
 128+02 E R/W " " " "

Line Run 15' on East of tile

near
 Cross pres tile 127+0
 " or near " " 123+0

cross pres. tile 104+0

July 9, 41 Follow old tile 104+0 to 100+54

near pres tile 98+65 to 95+0

94+84 - 14" tile from East

93+0 Extra Def. to L

cross pres tile about 82+0

near " " " 76+0

cross " " " 73+0

" " " 68+60

" " " 62+0

cross and near pres tile 56+0
 " " " " 53+0

$$\begin{array}{r} 140+14 \\ 94+84 \\ \hline 45+08 \end{array}$$

$$\begin{array}{r} 45+1439+84 \\ 121+0 \\ \hline 18+84 \end{array}$$

$$\begin{array}{r} 121+00 \\ 9480 \\ \hline 2616 \\ 1- \end{array}$$

$$\begin{array}{r} 1882 \\ 24 \\ \hline 1906 \end{array} \quad 1806 \times 24$$

$$\begin{array}{r} 140+0 \\ 121+0 \\ \hline 19+0 \end{array}$$

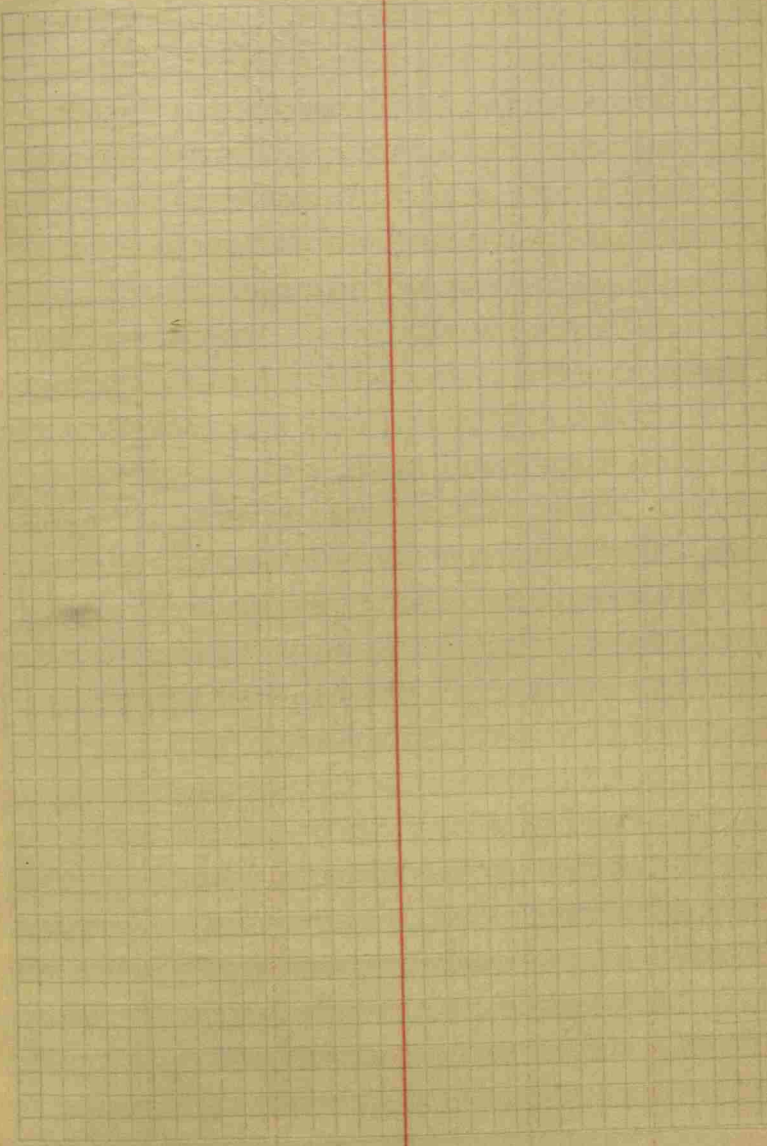
$$\begin{array}{r} 1890 \\ 14 \\ \hline 1904 \end{array}$$

$$\begin{array}{r} 1904 \times 24 \\ 2616 \times 22 \\ \hline 4520 \end{array}$$

104

46+76 S. Ryw P&E Ry

105



152

— π + BM

11.25 1.25 10.

1.70

9.55

9.55

4.83

4.72 Pres. Base Floor

2.50

2.22 Fl. Tile under
new Basement

1.67

83

2.50

1.00

1.22

520

9.98 3.93

605

ression levels 153

(9.55)

1.70 Basement window

1.00

1025 Fl. of Tile

.20

1105 waterline

538 Bank

900 ±

154

- π + BM

10.

10.23 .23

155

156

Quinn Drain

0+0 1400' x 24" - .07 full
 14+0 to 34+0 - 2000' x 22" (14+0-20+0) .10
 20+0 to 27+0 - .09
 27+0 to 34 - .08
 Deputy Nichols Sta. 32+0

Natural Trigonometrical Ratios.

Sec.	Cosec.	Cotg.	Cosin.	Angle.	Sine.	Tan.	Sec.	Cosec.	Cotg.	Cosin.
1.			1.	90	0					
	343.8	343.8	L.	50	8	.1392	.1405	1.0098	7.185	7.115
	171.9	171.9	.99998	40	10	.1421	.1435	1.0102	7.040	6.968
	114.6	114.6	.99996	30	20	.1449	.1465	1.0107	6.900	6.827
1.0001	85.94	85.94	.99993	20	30	.1478	.1495	1.0111	6.766	6.691
1.0001	68.76	68.75	.99989	10	40	.1507	.1524	1.0115	6.636	6.561
.0002	57.30	57.29	.99985	89	50	.1536	.1554	1.0120	6.512	6.435
.0002	49.11	49.10	.99979	50	9	.1564	.1584	1.0125	6.394	6.314
.0003	42.98	42.96	.99973	40	10	.1593	.1614	1.0129	6.277	6.197
.0003	38.20	38.19	.99966	30	20	.1622	.1644	1.0134	6.166	6.084
.0004	34.38	34.37	.99958	20	30	.1650	.1673	1.0139	6.059	5.976
.0005	31.26	31.24	.99949	10	40	.1679	.1703	1.0144	5.955	5.871
.0006	28.65	28.64	.99939	88	50	.1708	.1733	1.0149	5.855	5.769
.0007	26.45	26.43	.99929	50	10	.1736	.1763	1.0154	5.759	5.671
.0008	24.56	24.54	.99917	40	10	.1765	.1793	1.0160	5.665	5.576
.0010	22.93	22.90	.99905	30	20	.1794	.1823	1.0165	5.575	5.485
.0011	21.49	21.47	.99892	20	30	.1822	.1853	1.0170	5.488	5.398
.0012	20.23	20.21	.99878	10	40	.1851	.1883	1.0176	5.403	5.309
.0014	19.11	19.08	.99863	87	50	.1880	.1914	1.0181	5.320	5.226
.0015	18.10	18.07	.99847	50	11	.1908	.1944	1.0187	5.241	5.145
.0017	17.20	17.17	.99831	40	10	.1937	.1974	1.0193	5.164	5.068
.0019	16.38	16.35	.99813	30	20	.1965	.2004	1.0199	5.089	4.989
.0020	15.64	15.60	.99795	20	30	.1994	.2035	1.0205	5.016	4.915
.0022	14.96	14.92	.99776	10	40	.2022	.2065	1.0211	4.945	4.843
.0024	14.34	14.30	.99756	86	50	.2051	.2095	1.0217	4.877	4.773
.0027	13.76	13.73	.99736	50	12	.2079	.2126	1.0223	4.810	4.705
.0029	13.23	13.20	.99714	40	10	.2108	.2156	1.0230	4.745	4.638
.0031	12.75	12.71	.99692	30	20	.2136	.2186	1.0236	4.682	4.574
.0033	12.29	12.25	.99668	20	30	.2164	.2217	1.0243	4.620	4.511
.0036	11.87	11.83	.99644	10	40	.2193	.2247	1.0249	4.560	4.449
.0038	11.47	11.43	.99619	85	50	.2221	.2278	1.0256	4.502	4.390
.0041	11.10	11.06	.99594	50	13	.2250	.2309	1.0263	4.445	4.331
.0043	10.76	10.71	.99567	40	10	.2278	.2339	1.0270	4.390	4.275
.0046	10.43	10.39	.99540	30	20	.2306	.2370	1.0277	4.336	4.219
.0049	10.13	10.08	.99511	20	30	.2334	.2401	1.0284	4.284	4.165
.0052	9.839	9.788	.99482	10	40	.2363	.2432	1.0291	4.232	4.113
.0055	9.587	9.514	.99452	84	50	.2391	.2462	1.0299	4.182	4.061
.0058	9.309	9.255	.99421	50	14	.2419	.2493	1.0306	4.133	4.011
.0061	9.065	9.010	.99390	40	10	.2447	.2524	1.0314	4.086	3.962
.0065	8.834	8.777	.99357	30	20	.2476	.2555	1.0321	4.039	3.914
.0068	8.614	8.556	.99324	20	30	.2504	.2586	1.0329	3.994	3.867
.0072	8.405	8.345	.99290	10	40	.2532	.2617	1.0337	3.949	3.821
.0075	8.206	8.144	.99255	83	50	.2560	.2648	1.0345	3.906	3.776
.0079	8.016	7.953	.99219	50	15	.2588	.2679	1.0353	3.864	3.732
.082	7.834	7.770	.99182	40	10	.2616	.2711	1.0361	3.822	3.689
.088	7.661	7.596	.99144	30	20	.2644	.2742	1.0369	3.782	3.647
.090	7.496	7.429	.99106	20	30	.2672	.2773	1.0377	3.742	3.606
.094	7.337	7.269	.99067	10	40	.2700	.2805	1.0386	3.703	3.566
				82	50	.2728	.2836	1.0394	3.665	3.526
										74

Sec. Tan. Sine. Angle.

Cosin. Cotg. Cosec. Sec. Tan. Sine. Angle.