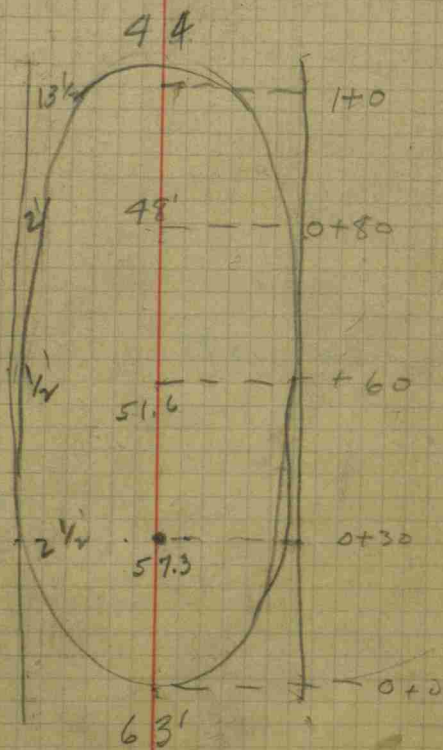


2 Saddle Gravel - Sullivan Farm

+ A -

B. 77



4. Saddle Shovel

	+	∓	-	B.M
	10.79	100.79		100.-

0+0

0+30

0+60

0+80

1+0

9.72	118.79	1.72	109.07
------	--------	------	--------

0+30

0+60

0+80

33
100
5

Gd.	Peak	Gd.
-----	------	-----

11.38	22 1/2 99.55	63
99.41	11.24	10.93
		99.86

99.86
10.93

99.95
10.94

99.99
10.80

100.01
10.78

25'
2.19 116.60

116.44 25'
2.35 26' 117.39
1.40

114.89 19'
4.10 21' 115.10
3.69

6

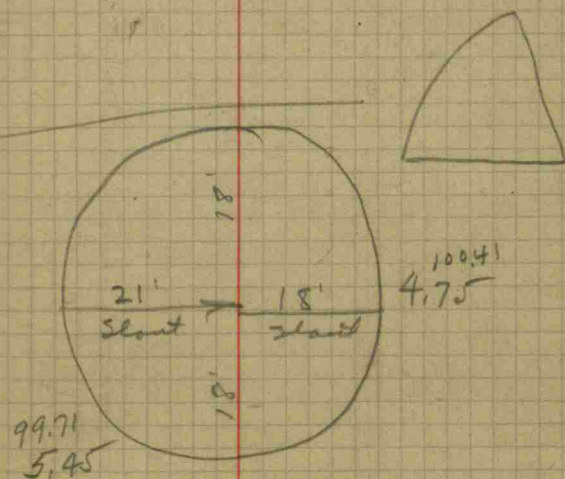
Saddler Gravel

118.79

105.16

7

East pile

Peak 110.19
8.60

87 cu.

8

Saddler Travel

T

5.16 105.16 100.00

0730

0760

0780

170

8

100.21
4.95

100.42
4.74

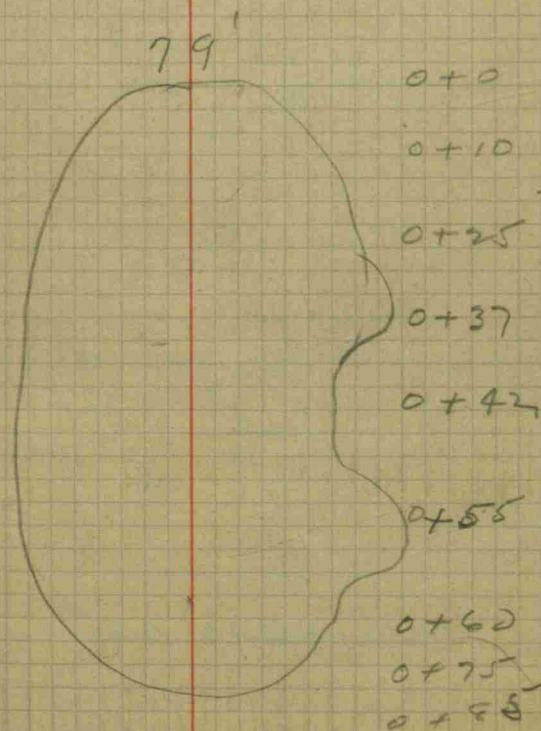
100.45
4.71

100.40
4.76

AR

RA

Saddle Gravel -
 Dauphin - Marion Co.



79'

FA

+	T	-	BM.	Stamp
10.32	110.32		100.00	

0+0

0+10

0+25

0+37

0+42

0+55

0+60

0+75

0+85

10.74	120.93	0.13	110.19
-------	--------	------	--------

Dayent - Marion Co

29	79
98.77	98.42
11.55	11.90

21 1/2	29 1/2	39 1/2	50 1/2	79
104.23	105.58	104.32	98.62	98.04
6.09	4.74	6.00	11.70	12.28

26 1/2	37 1/2	50	55	60 1/2	71 1/2	95.50	79
X	X	104.12	104.67	104.92	98.72	98.50	79
		6.20	5.65	5.40	11.60	11.76	

32 1/2	50	52 1/2	57 1/2	60	79 1/2
X	106.55	106.43	109.82	110.02	98.52
	3.77	3.89	0.50	0.30	11.80

32 1/2	47 1/2	58	61 1/2	66 1/2	76 1/2
X	108.32	107.51	107.03	105.19	98.79
	2.00	2.81	3.29	5.13	11.55

33	46.5	53.5	57	65	75	82
Y	0.92	109.40	X	109.62	102.70	99.82
				0.70	7.62	10.50

33	48 1/2	58	66 1/2	77 1/2	89	
Y	1.10	109.22	X	109.02	102.02	99.82
				1.30	8.30	10.50

27	41 1/2	54	64	79
Y			100.32	100.32
			10.00	10.00

100.77	79
9.55	

14

T
120.93

0+10

0+25

0+37

0+42

0+55

0+60

0+75

0+85

15

Saddle - Gravel

26 1/2
115.53
5.40

37 1/2
113.15
7.78

29 1/2
118.33
2.60

32 1/2
118.18
2.75

29 1/2
119.38
2.55

32 1/2
118.23
2.170

29 33 53 1/2
119.13 118.83 114.03
180 2.10 6.90

57
114.48
6.45

28 33
118.43 119.33
2.50 1.60

58
112.01
8.92

14 1/2 27 41 1/2
107.13 110.23 108.23
13.80 10.70 12.70

54
105.93
15.00

16

	2108	102.65	100.00
070			
0+10			
0+25			
0+37			
0+42			
0+55			
0+60			
0+75			
0+85			
	5.42	105.42	100.00
0+85			

17

Liddle General - Dauphin

Line		
98.28		
4.40		
98.43	7 1/2	98.93
4.25		3.75
98.48	2	98.56
4.20		4.12
98.96	1/2	98.93
3.72		3.75
99.18	1/2	
3.50		3.50 99.18
99.85	1/2	
2.53		2.53 99.85
100.08	1	
2.60		100.08 2.60
100.33	1 1/2	
2.35		2.35 100.33
100.17	13	
2.56		2.56 100.17
	30 1/2	48
	103.62	99.62
1.80		5.80

John W. Lackey Drain
Eel River Twp

0+0

0+50

1+0

2+0

3+0

4+0

5+0

6+0

7+0

8+0

8+72 Crosses old open channel

9+0 Tile may be all right

10+0

10+44 S. edge old channel

10+64 N. " " "

11+0 End Repair.

Repair of 8" Dr. Tile on Grant Sellars
Farm, Eel River Twp.

Station numbers do not
correspond with Sta. numbers of
original Ditch.

Surveyed.

August 28, 1935.

Contract Let.

Sept. , 1935

20

Lackey Drain

on Highest

spot of

large rock

+	π	-	B.M.
5.66	105.66		100.00

0+0

0+50

0+88

1+0

2+0

3+0

4+0

5+0

6+0

6+22

6+65

7+0

8+0

8+72

9+0

near Sta 5+50

Stk.	Ground.	Open channel
------	---------	--------------

97.48

8.18

97.58

8.08

96.61

9.05

96.71

8.95

26' E 94.86

10.80

18' E

94.90 10.76

95.46

T.T.

10.22

Fl.

11.00

94.66

98.06

7.60

99.11

8.55

14' W 94.49

10.17

99.40

6.26

98.46

7.20

24' 95.82

9.84

100.47

5.19

99.32

6.34

22' 96.41

9.25

100.99

4.67

100.15

5.51

19' 96.61

9.05

101.94

3.72

101.08

4.58

17' 96.91

8.75

101.71

3.95

101.02

4.64

14' 98.11

7.55

102.64

3.02

100.07

5.15

100.08

T.T.

5.58

99.06

Fl.

6.60

add ch.

7.20 98.46

101.78

3.88

101.78

3.88

10' 98.86

6.80

103.16

2.50

102.36

3.30

12' W 100.16

5.50

4.80 100.86

103.66

2.00

102.66

3.00

13' E 101.78

3.88

105.66

21

94.66

22

	+	T	-	BM
1070		105.66		

10+54

11+0

23

sth

104.16
0.50

Gd.

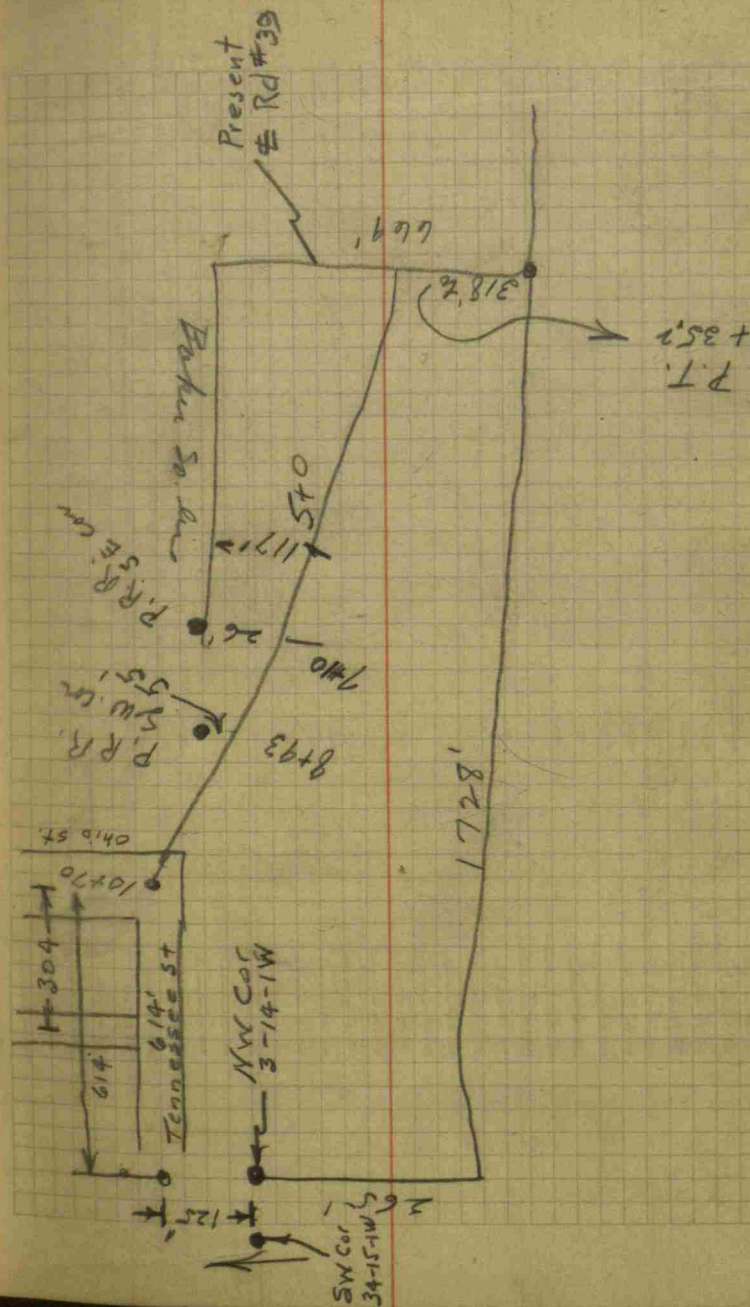
104.73
1.43Ti 102.96
2.70104.56
1.10

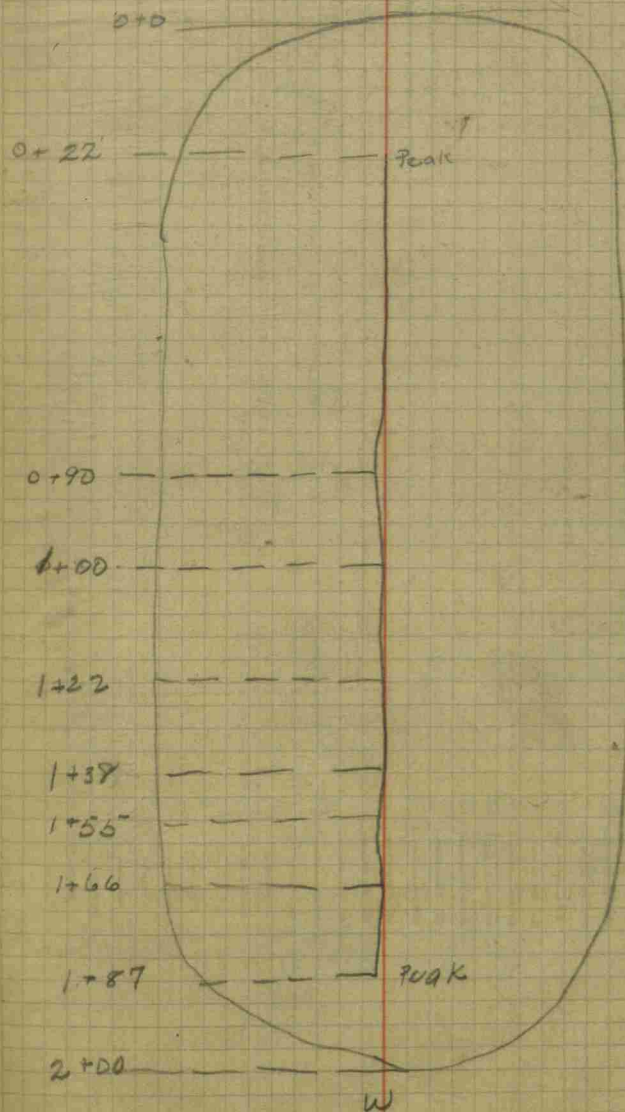
old ch.

25 102.44
3.22Fl. 102.76
3.409' 102.96
2.70

Clayton Rd #39 Relocation
Proposed

Corner Stone 38' East
of P. R. R. SW corner.



E
Cline FL

- π + BM
 21.37 11.37 10.00

0+0

0+22

0+90

1+0

1+22

1+38

1+56

1+66

1+87

2+0

5+0
 12.90
 8.47
 9.92
 12.45

9.55
 11.82

8.87
 12.50

11.95
 9.47

11.35
 10.02

12.16
 9.21

11.57
 9.90

11.47
 9.90

11.05
 10.32

23'
 12.90
 8.47

11'
 12.40
 8.97

3'
 11.90
 9.47

5'
 11.92
 9.45

6 1/2'
 11.60
 9.77

*

19'
 12.50
 8.87

21
 2.26
 19.11

10 1/2'
 11.46
 9.91

29'
 12.23
 9.14

26 1/2'
 0.80
 20.57

29 1/2'
 0.00
 21.37

62'
 13.30
 8.07

62'
~~12.90~~
 9.87

	-	π	+	BM
	0.61	21.37		20.76
		29.49	8.73	
0+22				
+90				
1+00				
1+22				
1+38				
1+55				
+66				
1+66				
1+87	12.20			17.29
		17.87	0.58	

top
7.102.5'
5.70
2.29
27.202.80
26.693.31
26.183.59
25.9027.48
2.106.60
22.895.25
24.24

+	\bar{X}	-	BM
---	-----------	---	----

17.87

0+0

+22

+90

1+0

1+22

1+38

1+55

1+66

1+87

5.46 14.56

8.77 9.10

BM Check
 12.00
 4.56

63	63
9.00	9.44
8.87	8.43

53	63
9.45	9.44
8.42	8.43

52 $\frac{1}{2}$	63
9.05	9.04
8.82	8.83

54 $\frac{1}{2}$	62 $\frac{1}{2}$
9.15	9.34
8.72	8.53

60	62 $\frac{1}{2}$
9.35	9.37
8.52	8.50

57 $\frac{1}{2}$	62 $\frac{1}{2}$
9.91	9.04
8.96	8.83

54 $\frac{1}{2}$	62 $\frac{1}{2}$
8.84	8.70
9.03	9.11

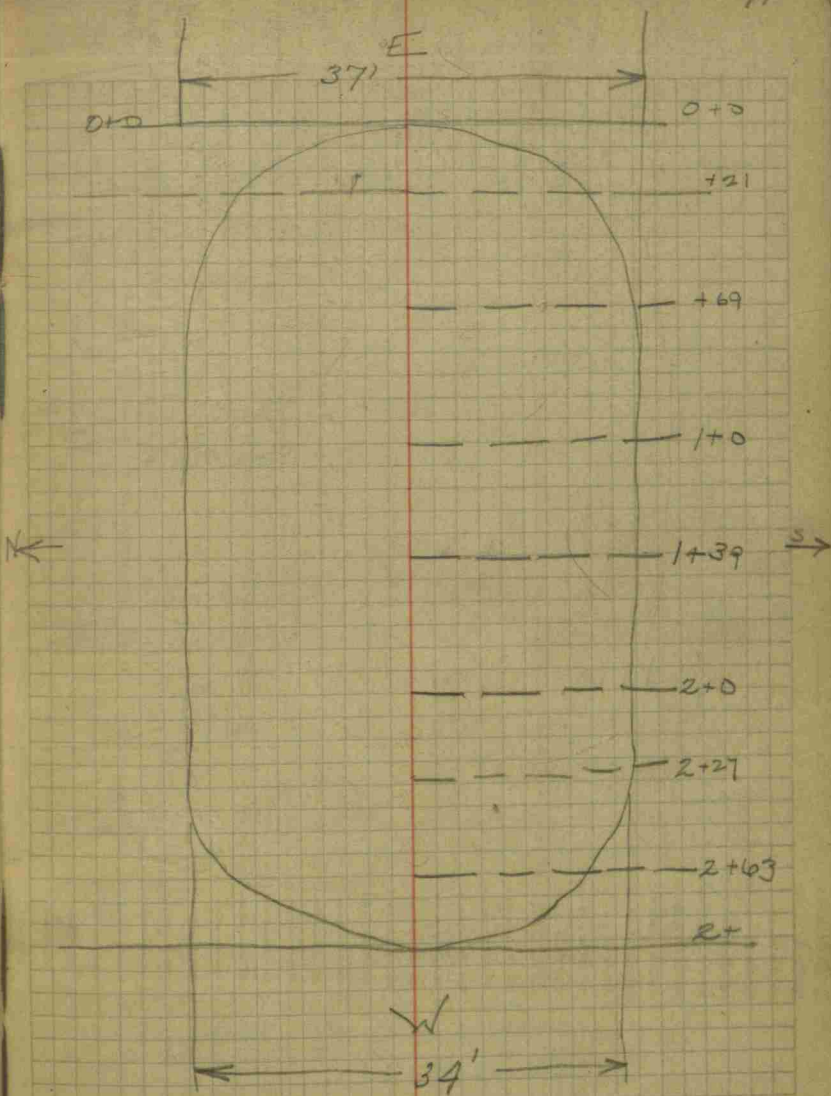
52 $\frac{1}{2}$	62
8.95	8.72
8.92	9.15

48	62
9.01	8.95
8.86	8.92

40

Gully Pit

41



44

	+	∑	-	BM
	1.10	101.57		100.47

2+78

2+63

2+27

2+0

1+39

1+0

0+69

0+21

0+0

N. Side 059.10

45

7	6	17	34
3.40	6.26	7.02	6.21
98.17	95.31	94.55	95.36

34
7.46
94.11

35
5.20
94.37

35.5
5.27
96.30

36
2.25
99.32

36.5
2.00
99.57

36.5
1.80
99.77

37
2.10
99.47

46

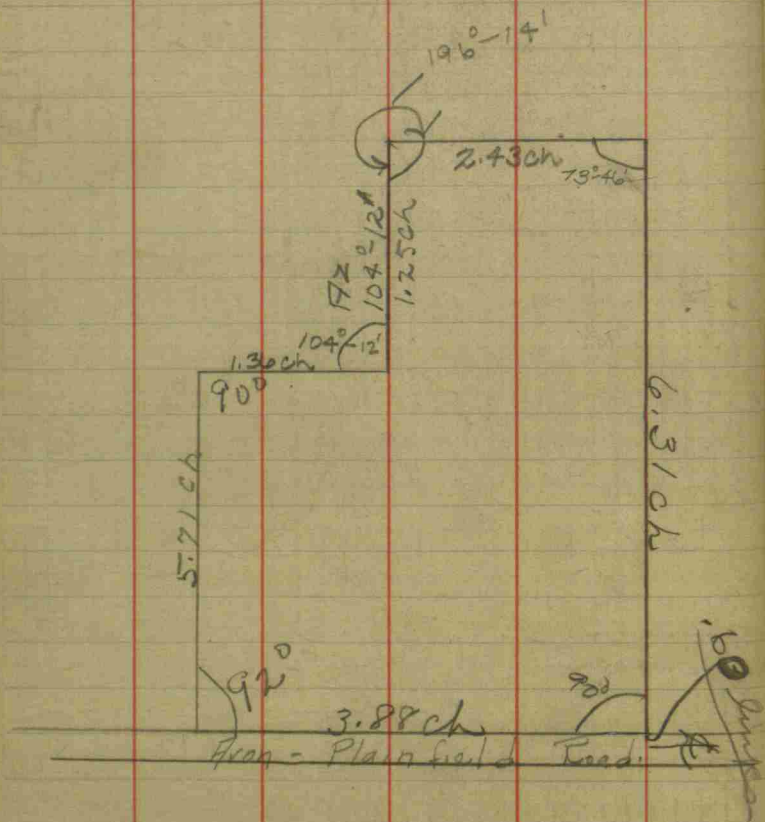
	+	*	-	B.M. 100.00
	8.84	113.15	0.41	104.31
0+21				
0+69				
1+0				
1+39				
2+0				
2+27				
2+63				

top of pile

47

1825
2.00
111.15
1800
3.40
109.75
1775
4.45
108.70
1775
2.78
110.45
1750
5.97
107.18
1750
6.81
106.34
17.25
6.21
106.94

H. Mason



658 Fairfield Ave.
Indianapolis

52 N
↑

Sullivan
Gravel
Pit

0+0

0+31

60'-0" wide.

0+71

0+83

1+0

53

54

+ 5.35
 π 105.35

- BM 100.0

on stake
 at N. Side of
 Pile
 EL. 100

0+0

0+31

0+61

0+71

0+83

1+0

0.08 105.27
 12.30 117.57

0+31

0+61

0+71

0+83

Ground of Pile

55

E

W

5.95
 99.40

5.65
 99.70

6.05
 99.30

6.05
 99.30

6.25
 99.10

6.40
 98.95

4.5
 5.92
 99.43

2.8
 6.00
 99.35

4.6
 6.22
 99.13

6.30
 99.05

7.8
 6.25 6.40
 99.10 98.95

2.7
 6.05 6.25
 99.50 99.10

5.1
 100.25

5.3
 6.60 6.50
 98.75 98.85

6.65
 98.70

117.07
 0.60

114.76
 2.81

114.67
 2.90

114.73
 3.14

7
 7.60
 109.97

12
 5.70
 111.87

56

+ X - BM

117.57

0+17

0+24

0+38

3.65 / 03.65

100.0

0+0

0+17

0+24

0+38

0+56

Pik #2
34' wide

57

8.45
109.12107.17
10.40111.72
5.85W
↑

N

6.15
97.506.10
97.556.15
97.505.82
97.835.70
97.956.00
97.655.95
97.706.00
97.605.85
97.805.60
98.05

John Garvey Pitch Inspection

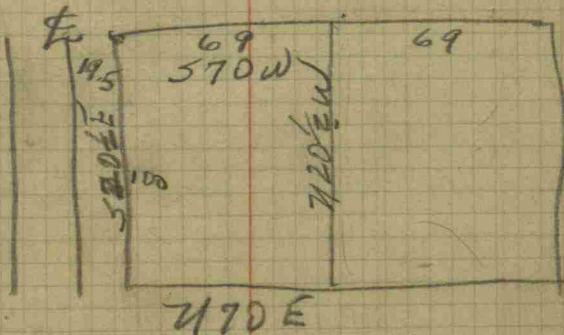
Allot.

County - OK
 Geo Davis - OK
 Henry Zerr - Back of Barn not cleaned
 Virgil Muse - OK
 Thos. Bullock - OK
 John McPheeters - OK
 Carrie - OK
 P. Luteritz - OK
 Chester Briggs - OK
 Wm Banta - OK however d/d jammed
 up on account of Head
 Gertrude Head - Not cleaned
 Park Thornburg - OK
 Bro - OK
 Mary Bersot - Not cleaned
 Thos Colliso - 1/2 cleaned
 Mary Bersot - Not clean
 Herbert Tansel - Fair
 Sarah Hession - Fair
 Hen drick's Co. OK

69
69
19.5
157.5

Survey for
P. B. L. P. G.

M. St.



$$\begin{array}{r} 20 \\ \hline 5.206 \\ \hline 6.20 \end{array}$$

4

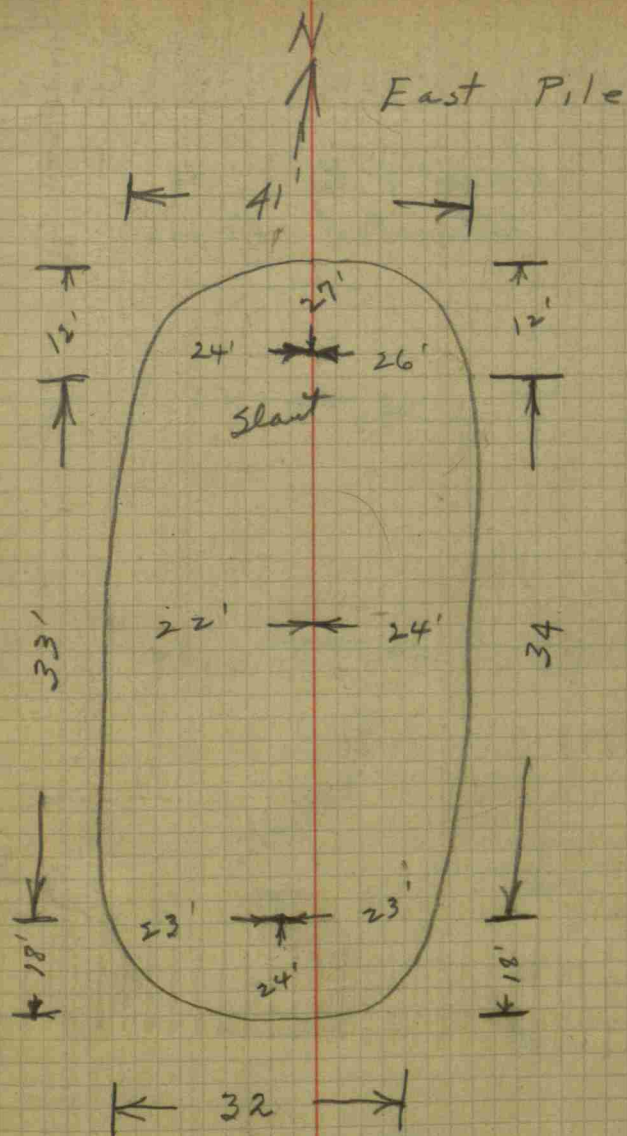
5.00

$$\begin{array}{r} 30 \\ \hline 1.20 \end{array}$$

90

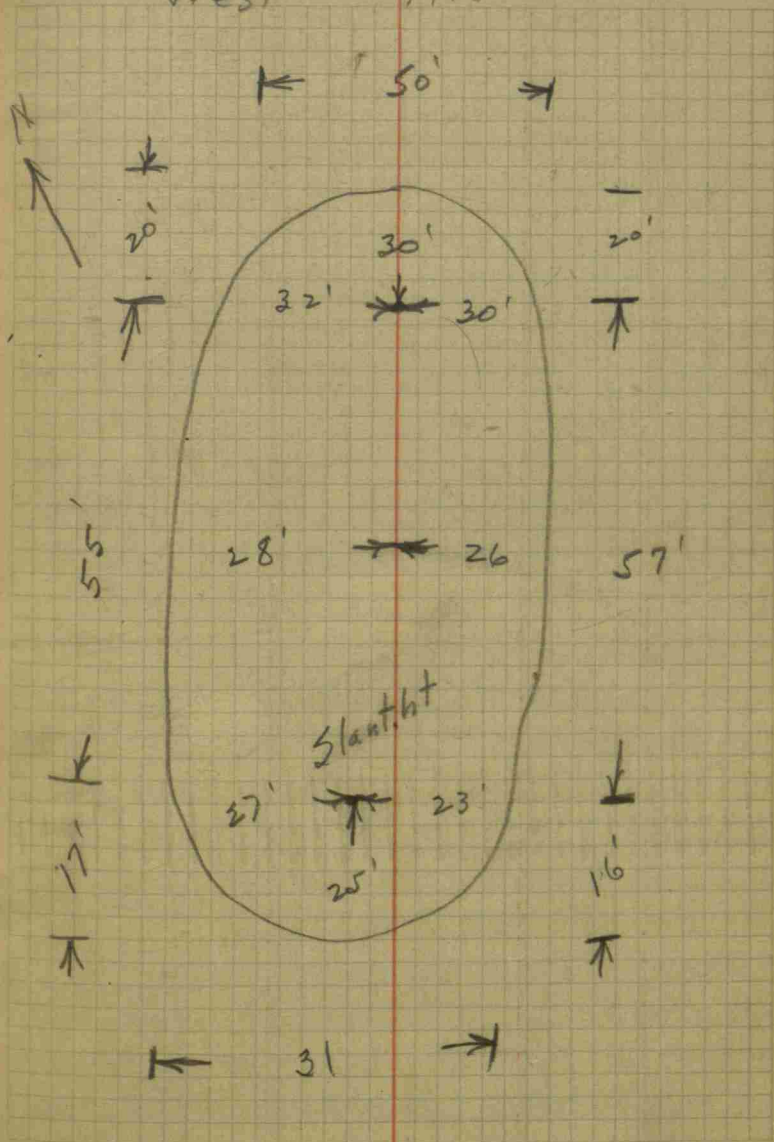
2.10

Sullivan Gravel
 Oct 7, 1938



Small Pile
Estimated 50 yds

West Pile



152

Surrey and Bldg. on North
side
Nov 2, 1937

-	+	BM
102.06	2.06	100.00

102.92	2.92	100.00
--------	------	--------

Made by
R. W. Armstrong
+
M. Newman

BM. E.I. 100.00 on
North wall to
Count Kannels
on
Curring wall on E. Side of

side Danville Square

153

92.36

1. 9.70

Partition
Wall

92.71

2. 9.35

10'-5" Partition
Wall

91.36

#3 10.70

Opposit Point
#2 to the East

91.40

#4 10.66

18'-5" Point #3

99.28

#5 3.64

on Sidewalk at E
edge of Bldg. on

99.43

#6 2.49

on Sidewalk at W
edge of Bldg.

158

λ	BMI
0.0	100.95
1.0	100

0.0

1.0

159

λ	BMI
0	2.50
500	97.30
0	10
295	10.60
93.50	8.5

0

500

0

295

93.50

10

2.50

97.30

10

10.60

8.5

160
5.28

.88
300
26400

12.86
264
0.22

0+0

12.86

1

11.98

✓

11.10

3

10.22

4

9.34

5

8.46

12.86
7.78
5.08

11.10

88

10.22

88

7.34

88

8.46

9.34

8.10

1.76

0+0

12.86

1+0

11.86

2

10.86

3

9.86

4

8.86

5

7.86

Natural Trigonometrical Functions.

Angle.	Sine.	Tan.	Sec.	Cosec.	Cotg.	Cosin.	Angle.	Sine.	Tan.	Sec.	Cosec.	C ^o t.	Cosin.
0	0	0	1	∞	∞	1	90	1	∞	∞	0	0	0
10	.0029	.0029		343.8	343.8	1	50	.1421	.1435	1.0102	7.040	6.968	.98986
20	.0058	.0058		171.9	171.9	.99998	40	.2014	.2032	1.0107	6.900	6.827	.98944
30	.0087	.0087		114.6	114.6	.99996	30	.2618	.2648	1.0111	6.766	6.691	.98902
40	.0116	.0116	1.0001	85.94	85.94	.99993	20	.3214	.3254	1.0115	6.636	6.561	.98858
50	.0145	.0145	1.0001	68.76	68.76	.99989	10	.3811	.3861	1.0120	6.512	6.435	.98814
1	.0175	.0175	1.0002	57.30	57.29	.99985	89	.4400	.4460	1.0125	6.394	6.314	.98769
10	.0204	.0204	1.0002	49.11	49.10	.99979	50	.4981	.5051	1.0129	6.277	6.197	.98723
20	.0233	.0233	1.0003	42.98	42.98	.99973	40	.5554	.5634	1.0134	6.166	6.084	.98676
30	.0262	.0262	1.0003	38.20	38.19	.99966	30	.6121	.6211	1.0139	6.059	5.976	.98629
40	.0291	.0291	1.0004	34.38	34.37	.99958	20	.6681	.6781	1.0144	5.965	5.871	.98580
50	.0320	.0320	1.0005	31.26	31.24	.99949	10	.7234	.7344	1.0149	5.885	5.789	.98531
8	.0349	.0349	1.0006	28.65	28.64	.99939	88	.7781	.7901	1.0154	5.769	5.671	.98481
10	.0378	.0378	1.0007	26.45	26.43	.99929	50	.8321	.8451	1.0160	5.665	5.576	.98430
20	.0407	.0407	1.0008	24.56	24.54	.99917	40	.8854	.9004	1.0165	5.575	5.485	.98378
30	.0436	.0437	1.0010	22.93	22.90	.99905	30	.9381	.9541	1.0170	5.488	5.396	.98325
40	.0465	.0466	1.0011	21.49	21.47	.99892	20	.9901	.1016	1.0176	5.403	5.309	.98272
50	.0494	.0495	1.0012	20.23	20.21	.99878	10	1.0414	1.0534	1.0181	5.320	5.226	.98218
3	.0523	.0524	1.0014	19.11	19.08	.99863	87	1.0921	1.1051	1.0187	5.241	5.145	.98163
10	.0552	.0553	1.0015	18.10	18.07	.99847	50	1.1421	1.1561	1.0193	5.164	5.066	.98107
20	.0581	.0582	1.0017	17.20	17.17	.99831	40	1.1914	1.2064	1.0199	5.089	4.989	.98050
30	.0610	.0612	1.0019	16.38	16.35	.99813	30	1.2401	1.2561	1.0205	5.016	4.915	.97992
40	.0640	.0641	1.0020	15.64	15.60	.99795	20	1.2881	1.3051	1.0211	4.945	4.843	.97934
50	.0669	.0670	1.0022	14.96	14.92	.99776	10	1.3354	1.3534	1.0217	4.877	4.773	.97875
4	.0698	.0699	1.0024	14.34	14.30	.99756	86	1.3821	1.4011	1.0223	4.810	4.705	.97815
10	.0727	.0729	1.0027	13.76	13.73	.99736	50	1.4281	1.4481	1.0229	4.745	4.638	.97754
20	.0756	.0758	1.0029	13.23	13.20	.99714	40	1.4734	1.4944	1.0236	4.682	4.574	.97692
30	.0785	.0787	1.0031	12.75	12.71	.99692	30	1.5181	1.5391	1.0243	4.620	4.511	.97630
40	.0814	.0816	1.0033	12.29	12.25	.99668	20	1.5621	1.5841	1.0249	4.560	4.449	.97568
50	.0843	.0846	1.0036	11.87	11.83	.99644	10	1.6054	1.6284	1.0256	4.502	4.390	.97502
5	.0872	.0875	1.0038	11.47	11.43	.99619	85	1.6481	1.6721	1.0263	4.445	4.331	.97437
10	.0901	.0904	1.0041	11.10	11.06	.99594	50	1.6901	1.7151	1.0270	4.390	4.275	.97371
20	.0929	.0934	1.0043	10.76	10.71	.99567	40	1.7314	1.7574	1.0277	4.336	4.219	.97304
30	.0958	.0963	1.0046	10.43	10.39	.99540	30	1.7721	1.8001	1.0284	4.284	4.166	.97237
40	.0987	.0992	1.0049	10.13	10.08	.99511	20	1.8121	1.8411	1.0291	4.232	4.113	.97169
50	.1016	.1022	1.0052	9.839	9.788	.99482	10	1.8514	1.8814	1.0299	4.182	4.061	.97100
6	.1045	.1051	1.0055	9.567	9.514	.99452	84	1.8901	1.9211	1.0306	4.133	4.011	.97030
10	.1074	.1080	1.0058	9.309	9.255	.99421	50	1.9281	1.9601	1.0314	4.086	3.962	.96959
20	.1103	.1110	1.0061	9.065	9.010	.99390	40	1.9654	1.9994	1.0321	4.039	3.914	.96887
30	.1132	.1139	1.0065	8.834	8.777	.99357	30	2.0021	2.0371	1.0329	3.994	3.857	.96815
40	.1161	.1169	1.0068	8.614	8.556	.99324	20	2.0381	2.0741	1.0337	3.949	3.821	.96742
50	.1190	.1198	1.0072	8.405	8.345	.99290	10	2.0734	2.1104	1.0345	3.906	3.776	.96667
7	.1218	.1228	1.0075	8.206	8.144	.99255	83	2.1081	2.1461	1.0353	3.864	3.732	.96593
10	.1248	.1257	1.0079	8.016	7.953	.99219	50	2.1421	2.1811	1.0361	3.822	3.689	.96517
20	.1276	.1287	1.0082	7.834	7.770	.99182	40	2.1754	2.2154	1.0369	3.782	3.647	.96440
30	.1305	.1317	1.0086	7.661	7.596	.99144	30	2.2081	2.2491	1.0377	3.742	3.606	.96363
40	.1334	.1346	1.0090	7.496	7.429	.99106	20	2.2401	2.2821	1.0386	3.703	3.566	.96285
50	.1363	.1376	1.0094	7.337	7.269	.99067	10	2.2714	2.3144	1.0394	3.666	3.526	.96206

Cosin. Cotg. Cosec. Sec. Tan. Sine. Angle.

Cosin. Cotg. Cosec. Sec. Tan. Sine. Angle.

$$\begin{array}{r} 6.90 \\ 1.33 \\ \hline 8.23 \end{array}$$

$$\begin{array}{r} 12.86 \\ 8.23 \\ \hline 4.63 \end{array}$$

$$\begin{array}{r} 5.28 \\ 2.50 \\ \hline 7.78 \end{array}$$

$$\begin{array}{r} 6.90 \\ 1.17 \\ \hline 5.73 \\ 4.10 \\ \hline 1.63 \end{array}$$

$$\begin{array}{r} 8.10 \\ 4 \\ \hline 4.10 \\ 230 \\ 1.17 \\ \hline 1.33 \end{array}$$

$$\begin{array}{r} 16.5 \\ 32 \\ \hline 330 \\ 495 \\ \hline 528.0 \end{array}$$

$$\begin{array}{r} 528 \overline{) 600.} \\ \underline{528} \\ 720 \end{array}$$

$$1' - 1'' = 6$$

$$\begin{array}{r} 1.88 \\ 528 \overline{) 4,63.0} \\ \underline{4224} \\ 4060 \end{array}$$

$$\begin{array}{r} 12.36 \\ .50 \\ \hline \end{array}$$

$$\begin{array}{r} 786 \\ 690 \\ \hline 96 \end{array}$$

$$12.86$$

$$6.90$$

$$\hline 5.96$$

$$\begin{array}{r} 986 \\ 810 \\ \hline \end{array}$$

$$12.86$$

$$8.10$$

$$\hline 4.76$$

$$12.86$$

$$3$$

$$\hline 9.86$$

$$810$$

$$\hline 1.76$$

$$810$$

$$690$$

$$\hline 120$$

04
 0410
 + 25
 + 50
 560
 + 75
 + 85



233
 578

 811

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
 ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.
 FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.