

178

THE  
BIBLE  
365 A

LETTER →

Cline Bridge  
Marion  
4' Rise  
12' Span  
20' Clear Road Way  
Bridge More 40' East  
New Channel, to be dug.

Completed

2

Spears Bridge

Red River

4'-6" Rise

12' Span

30° Skew

22' Clear Road Way

Present Road 30' between  
fences

floor poured June 8-1937

4

on job April 15 50 bags Bags Cement

5

Repair on Steel bridge  
on Lodge Rd.

4 plates  $14\frac{1}{2} \times 14 \times \frac{1}{4}$ "  
with 1" II End to hold  
hook  
3 - 1"  $\phi$  Rods with threads  
and hook. 24'-0"

67  
4' Ext on Each Side

~~40'~~ Ret Wall on NW  
av. height 4' to 6'

Free Bridge 72

Outside Cased	I	19"
Inside	"	15"
Width	"	12"

C to C of I<sup>s</sup> = 56"

Rise 72'

Span 20' 0"

Top abt width = 20"

Present  
Wing 5' 0"

Completed

Rawlings Bridge  
Middle

Rise 7'-2"

Roadway 14'-0"

45° New 15' Wing Needed on SE

75 Channel Ex. on Side Bridge

15° Wing on NE 5', fast slope

191

Road

191

Rise 8'

Span 16'

Abut 17' wide

NE + NW 45° - 6'

Parker Bridge

4' Rise

20' Span

Clay Twp.

Channel Straightening

20' Clear Roadway

~~NEW~~

100 CU. Yds EXC

NEW Rise 6'

22' Roadway

22' Span

Footings 3' Wide

2'-6" Deep



15

Westerfield Bridge 15  
Center Top

8 Upright Compression Members  
and on the rod on N.E. Corner

Cable Steel Bridge  
Franklin twp.

Paint Job

Davis Bridge  
Paint Job

Grifford Twp.

Kendall Bridge

Paint Job

Liberty twp.

18f

Aug - 1936

Chester + Bessie Martin

19f

Completed ~~name~~

Inside of hub Rail  
widen 5' to inside hub Rail  
8" hub

hub Rail 6" high

slate thickness 1'-0"

Rise 4'-6"

Dip 12'

about 18" thick

NE wing due North 5' long  
hole for 16" or 18" tile and dip

NW wing 6' long due West  
with road

22

23

Simmons Bridge

Old Bridge

Rise → 5' 6"  
Span → 18' 0"  
Roadway → 15' 6"

---

New Bridge

30° skew

20' along Center of Road.

Roadway Clear 22'

Long bridge

57 Sacks  
Cement.

$$\begin{array}{r} 11.93 \\ 6.95 \\ \hline 59.65 \\ 10237 \\ 7158 \\ \hline 82,3136 \end{array}$$

28<sup>95</sup>

29<sup>95</sup>

← 24 →  
E End

0+0

0+09

0+98

1+44

2+36

2+49

312

-

+

+

BM

104.77 4.77 109.54

0+0

0+09

0+98  
1+44

2+36

2+49

1.89

102.88

110.90 7.52 118.42

W. End. 2+36

1+44

0+98

E. End. 0+09

S. Side

312

100.55

4.22

100.60

4.17

99.50

98.00

98.52

6.25

98.32

6.45

Top

106.20

4.20

105.42

4.98

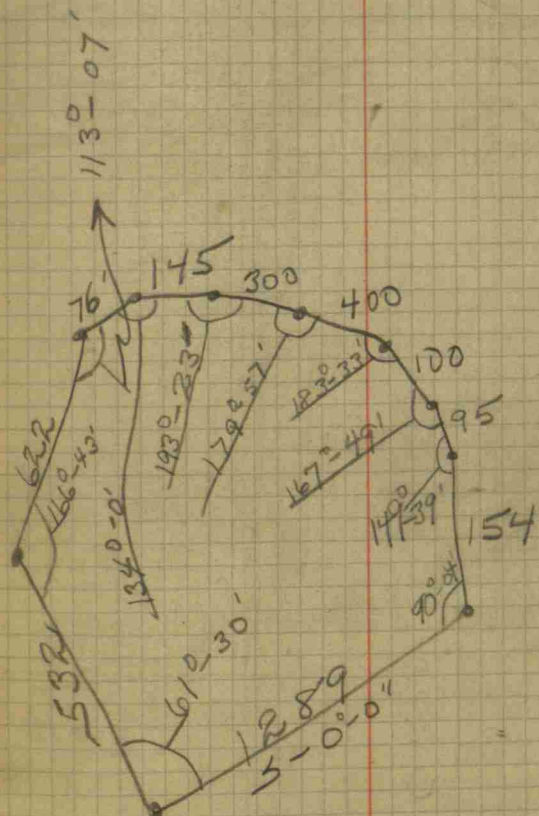
107.60

2.80

108.22

2.18



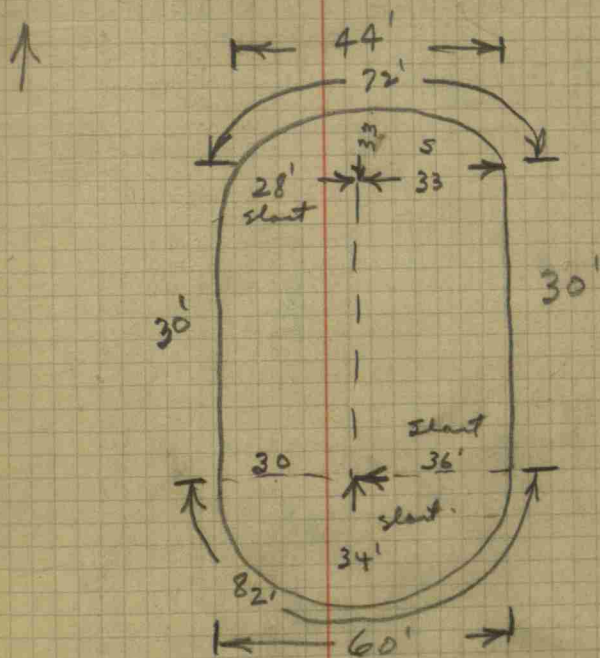


NW<sup>4</sup> NW<sup>4</sup> Sec 14-17-2N  
 Cor.

40 Sellers Gravel

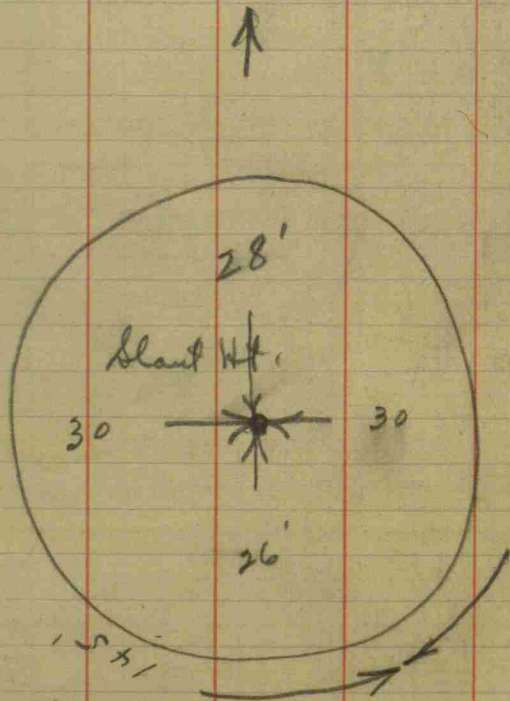
Sept 29, 1938

41 South Pile



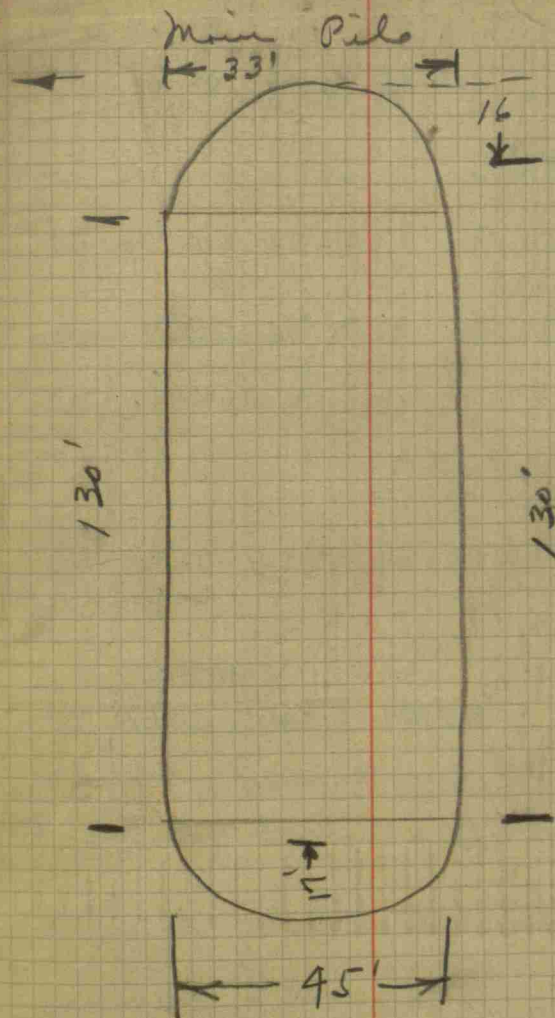
Sellers Hovel

Sept 29, 1938



circ - 145'

Sellers Private Pile



-	⊖	+	B.M
	110.33	10.33	100.00

1.28	118.01	8.96	109.05
------	--------	------	--------

11.60	109.98	3.57	106.41
-------	--------	------	--------

118.01  
110.00  
106.61

85

Gd N. end S. Pile -	11.48	98.85
Gd. SW end S. Pile -	11.28	99.05
Gd SE end S Pile -	11.00	99.33
Gd S. side main Pile	11.05	99.28
Gd N. side main Pile	11.10	99.13

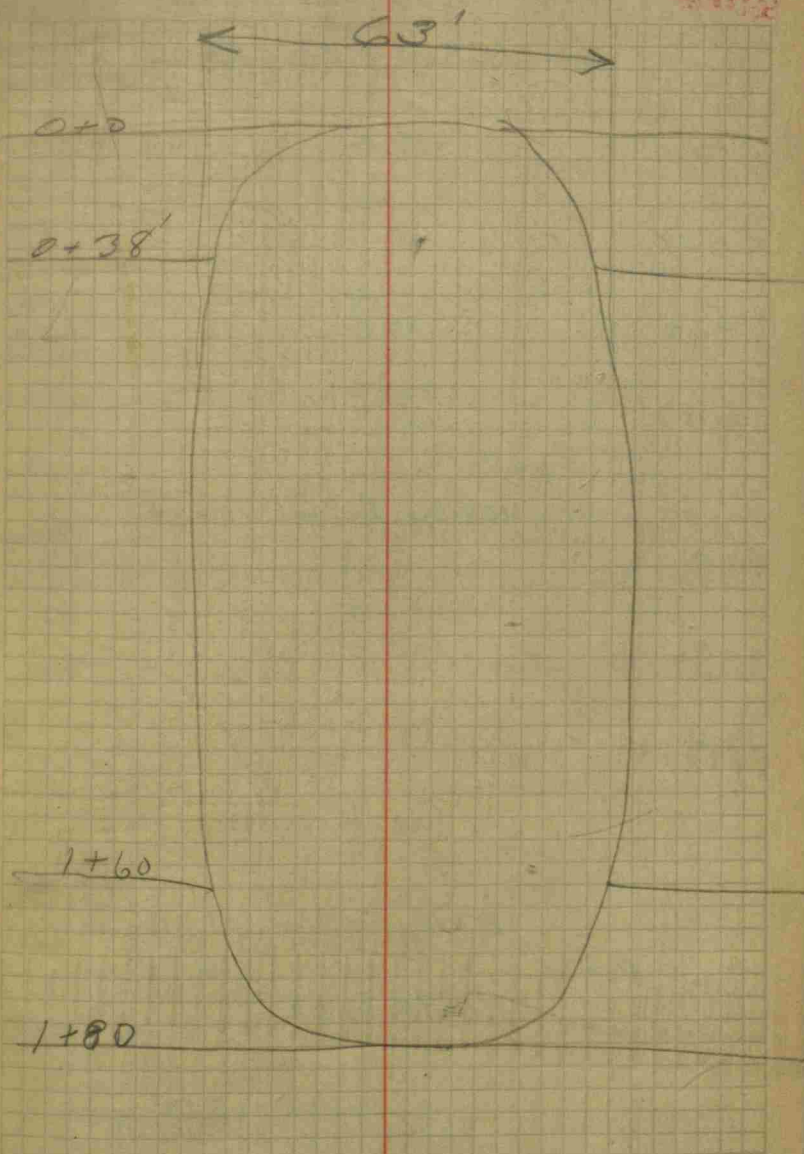
(Gd. at North Pile) - 11.65 98.68  
Sullens.

Top Sullens Pile	4.35	113.66
W. end top main	2.65	115.36
E. end top main	4.26	113.75
N. end top S. Pile	1.95	116.06
S. end top S. Pile	1.08	116.93

B.M. check 10.02

46

Pritchett Gravel



	-	+	B.M.
	101.81	1.81	100.00

0+0

0+38

1+60

1+80

0+0

0+38

1+60

1+80

102.36	2.36	100.00
--------	------	--------

107.36	7.36	100.00
--------	------	--------

0.62

117.94	11.20	106.74
--------	-------	--------

2

$$\begin{array}{r} 96.96 \\ \underline{20.30} \end{array}$$

West Side.

96.96

4.85

95.65

5.16

94.74

7.07

94.69

7.12

East Side

97.45

4.91

97.41

4.95

95.21

7.15

95.16

7.20

117.26		
0+38	→	0.68

118.60

1+60	→	4.31
------	---	------

115.68

2.06

4.50 → 113.44

113.24

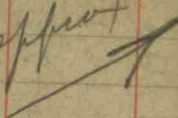
4.70

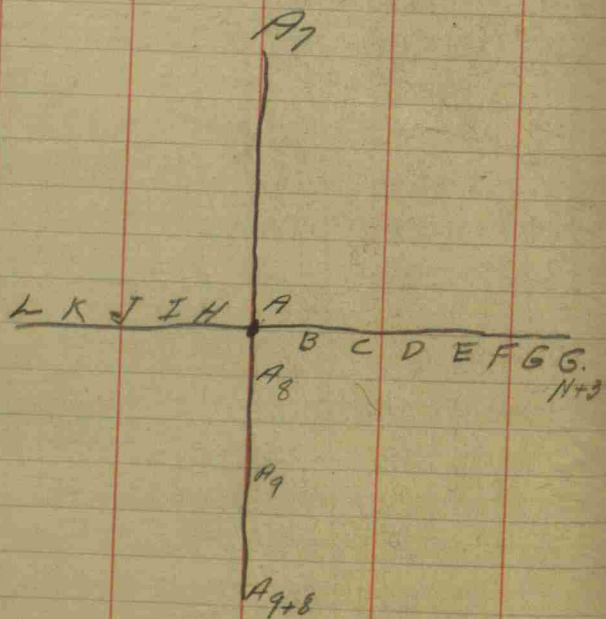
12  
July 14<sup>th</sup> - 1937

Chester Parsons

Model

50

afford 



51

July 16<sup>th</sup> - 1937

B.M. on Nail in 10" diameter tree at S.E. corner of gravel pile near base of tree E1. 20.00

Check B.M. 19.98

A	39.89	B	33.77	C	27.23
A <sub>1</sub>	37.24	B <sub>1</sub>	32.45	C <sub>1</sub>	26.34
A <sub>2</sub>	35.34	B <sub>2</sub>	29.35	C <sub>2</sub>	23.93
A <sub>3</sub>	31.78	B <sub>3</sub>	25.95	C <sub>3</sub>	19.17
A <sub>4</sub>	25.68	B <sub>4</sub>	21.57	C <sub>4</sub>	15.75
A <sub>5</sub>	19.38	B <sub>5</sub>	17.74	C <sub>5</sub>	13.13
A <sub>6</sub>	12.37	B <sub>6</sub>	14.75	C <sub>6</sub>	8.65
A <sub>7</sub> Gd	5.50	B <sub>7</sub> Gd	5.57	C <sub>6</sub> +6W Gd	5.78
A <sub>8</sub>	34.60	B <sub>8</sub>	31.91	C <sub>8</sub>	26.43
A <sub>9</sub>	27.38	B <sub>9</sub>	25.71	C <sub>9</sub>	23.44
A <sub>9</sub> +8E Gd	22.53	B <sub>9</sub> +8E Gd	21.65	C <sub>9</sub> +7E Gd	19.29

D	21.87	E	14.97
D <sub>1</sub>	21.17	E <sub>1</sub>	14.46
D <sub>2</sub>	17.20	E <sub>2</sub>	12.98
D <sub>3</sub>	14.04	E <sub>3</sub>	8.37
D <sub>4</sub>	9.61	E <sub>4</sub>	5.47
D <sub>5</sub>	8.65	E <sub>5</sub> Gd	4.87
D <sub>6</sub> -Gd	4.72	E <sub>4</sub> +7N-Gd	3.81
D <sub>8</sub>	19.04	E <sub>8</sub>	13.87
D <sub>9</sub>	17.79	E <sub>9</sub>	12.71
D <sub>9</sub> -8E Gd	14.51	E <sub>9</sub> +6N-Gd	9.73
		E <sub>9</sub> +4E Gd	10.91



①	71.14				
F	9.74	G	6.67	H	37.38
F <sub>1</sub>	10.38	G <sub>1</sub>	6.68	H <sub>1</sub>	36.32
F <sub>2</sub>	8.65	G <sub>2</sub> Gd	4.87	H <sub>2</sub>	34.15
F <sub>3</sub>	5.71	G <sub>1</sub> +6 N. Gd.	4.78	H <sub>3</sub>	28.13
F <sub>3</sub> +6 N. Gd.	4.03			H <sub>4</sub>	23.29
		G+3 N. Gd.	5.81	H <sub>5</sub>	17.28
F <sub>8</sub>	10.11			H <sub>6</sub>	10.67
F <sub>8</sub> +6 E. Gd.	-9.40			H <sub>7</sub> Gd.	4.78
		G <sub>8</sub> Gd.	7.45		

H<sub>8</sub> 33.97  
H<sub>9</sub> 26.20  
H<sub>9</sub>+8 E. Gd 22.07

① I	31.70	55	① J	24.16	① 24.67
I	31.28		J <sub>1</sub>	24.62	
I <sub>1</sub>	31.10		J <sub>2</sub>	25.30	
I <sub>2</sub>	33.04		J <sub>3</sub>	22.46	
I <sub>3</sub>	25.54	① 16.26	J <sub>4</sub>	16.18	
I <sub>4</sub>	-20.60		J <sub>5</sub>	11.81	① 12.36
I <sub>5</sub>	-15.04		J <sub>6</sub>	-6.40	
I <sub>6</sub>	-8.58		J <sub>6</sub> +3 W-Gd	4.41	
I <sub>6</sub> +8 W-Gd	-4.08		J <sub>8</sub>	-23.93	
			J <sub>8</sub> +9 E-	20.81	Gd.
I <sub>8</sub>	-29.65	① 30.22			
I <sub>9</sub>	-24.00				
I <sub>9</sub> +4 E-	-21.30	Gd.			
I <sub>9</sub> +8 S-	-21.16	Gd.			

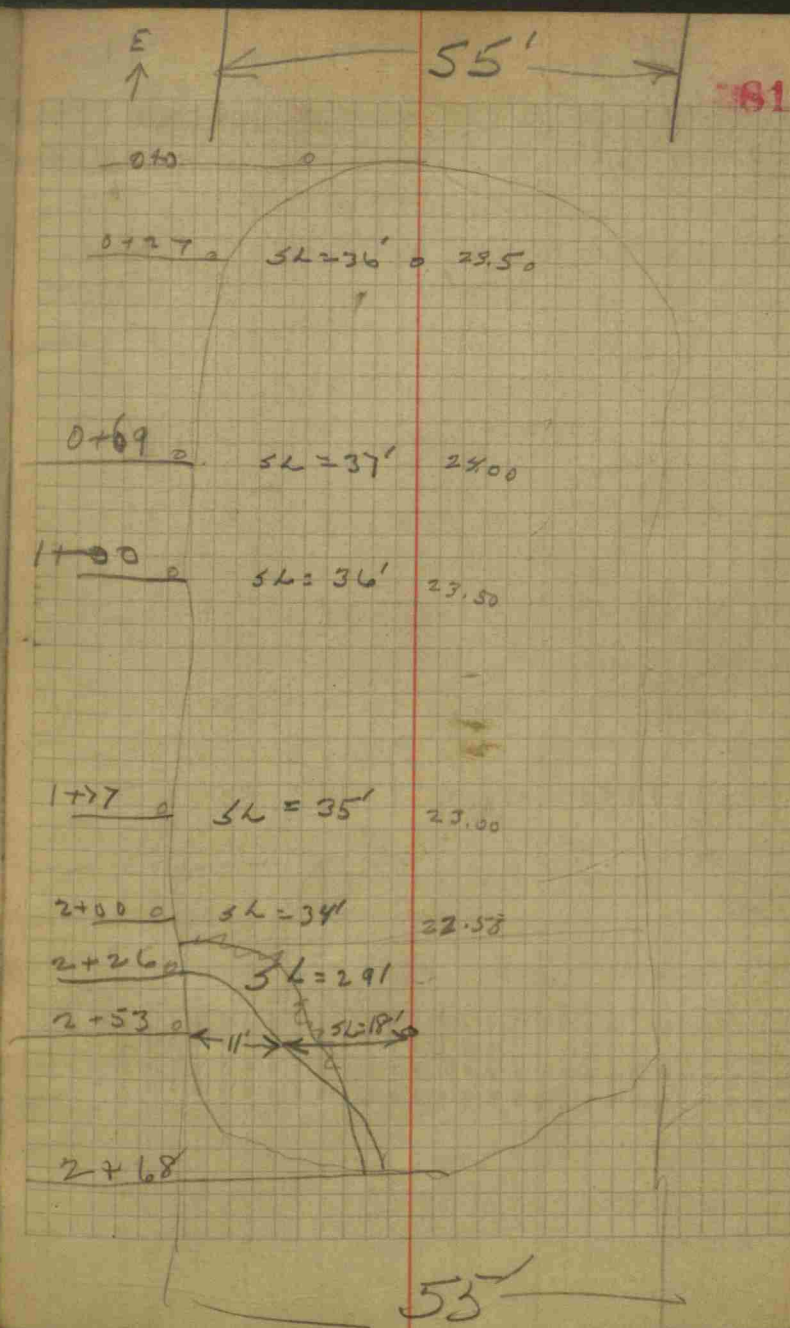
56  
K 16.35  
K<sub>1</sub> 17.76  
K<sub>2</sub> 19.70  
K<sub>3</sub> 15.93  
K<sub>4</sub> 12.20  
K<sub>5</sub> 7.30  
K<sub>4</sub>+8S Gd. 7.30  
K<sub>5</sub>+6S Gd. 5.10  
K<sub>5</sub>+7W Gd. 4.26  
K<sub>8</sub> 17.34  
K<sub>8</sub>+6E Gd. 16.40  
K<sub>8</sub>+8S Gd. 11.46

L+1S -Gd. 9.12  
L 9.91  
L+2S Gd. 8.95  
L<sub>1</sub> 10.12  
L<sub>2</sub> 13.65 (0-14.52)  
L<sub>2</sub>+7.5Gd 8.44  
L<sub>3</sub> 10.54  
L<sub>3</sub>+5S Gd 6.98

7.00  
2.50  
4.20 57

60 Cline Gravel Pit  
 Measured Feb. 4, 1938  
 by Armstrong  
 + Newman

25	22	23
25	22	23
50	44	46
625	74	76
56	27.5	
36	27.5	
37.6	197.5	
08	192.5	
1276	550	
756	756.25	
540		
1		
44	140	



$$\begin{array}{r} 736 \\ 253 \\ \hline 989 \end{array}$$
$$\begin{array}{r} 553 \\ 04 \\ \hline 1012 \end{array}$$
$$\begin{array}{r} 1.0 \\ 2.2 \\ \hline 4.2 \end{array}$$
$$\begin{array}{r} 5.42 \\ 4.13 \\ \hline 1.3 \end{array}$$
$$\begin{array}{r} 736 \\ .003 \\ \hline .2208 \end{array}$$
$$\begin{array}{r} 736 \\ 253 \\ \hline 989 \\ 9834 \end{array}$$

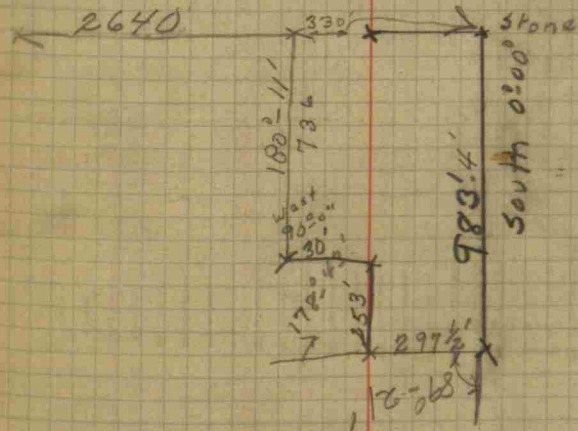
2.975

$$\begin{array}{r} 728 \\ 02 \\ \hline 730 \end{array}$$

69

all angles as with  
South = 0°00' 69

Clayton



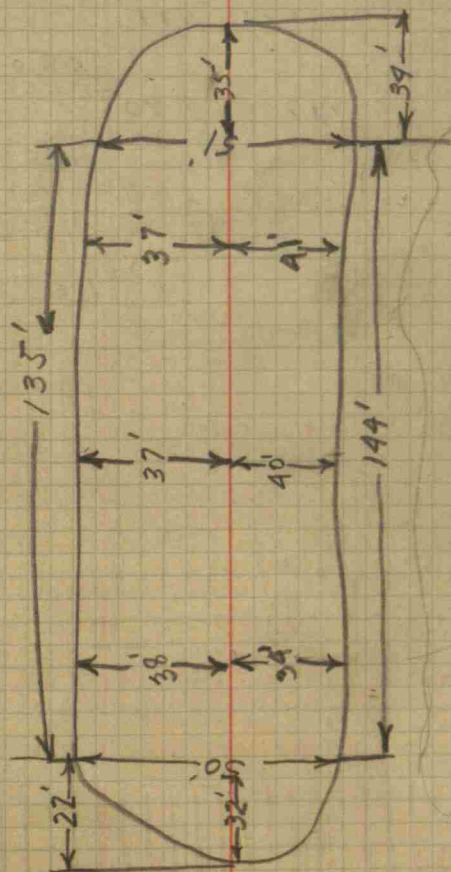
Albertson Gravel Pile

Lincoln Twp.

M. Newman

Mar. 10, 1939.

Cloudy-Cool.



89

-	+	BM	on Rock at Base of Pile
	108.44	8.44	100
.35			108.09
	107.89	9.80	
1.40			116.49
	123.44	6.95	
12.19			111.25
	111.58	.33	
11.58			100.00

 81  
 Elevation on  
 Albertson Gravel

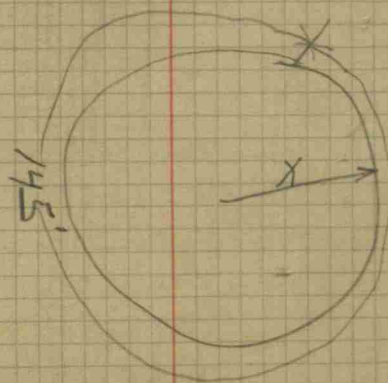
Top of Pile

120.62  
2.82121.69  
1.75121.30  
2.14

8:

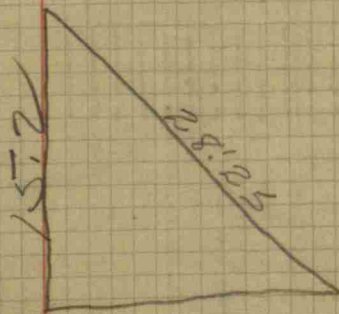
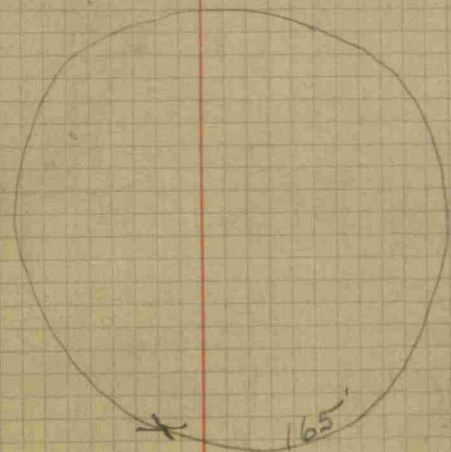
5  
784  
576  
208

85  
Ragsdale Gravel Pile

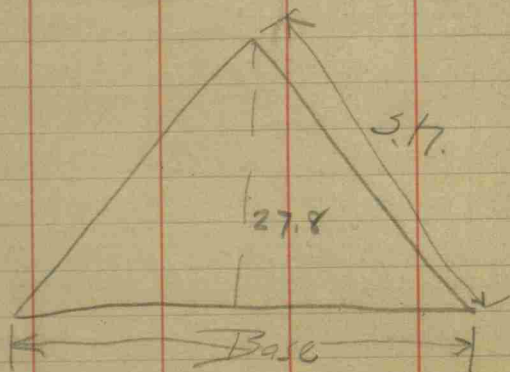


83  
slant height

$$\begin{array}{r} 26' \\ 30' \\ 28' \\ \hline 29 \\ 4 \overline{) 113} \quad 28 \\ \underline{8} \\ 33 \end{array}$$







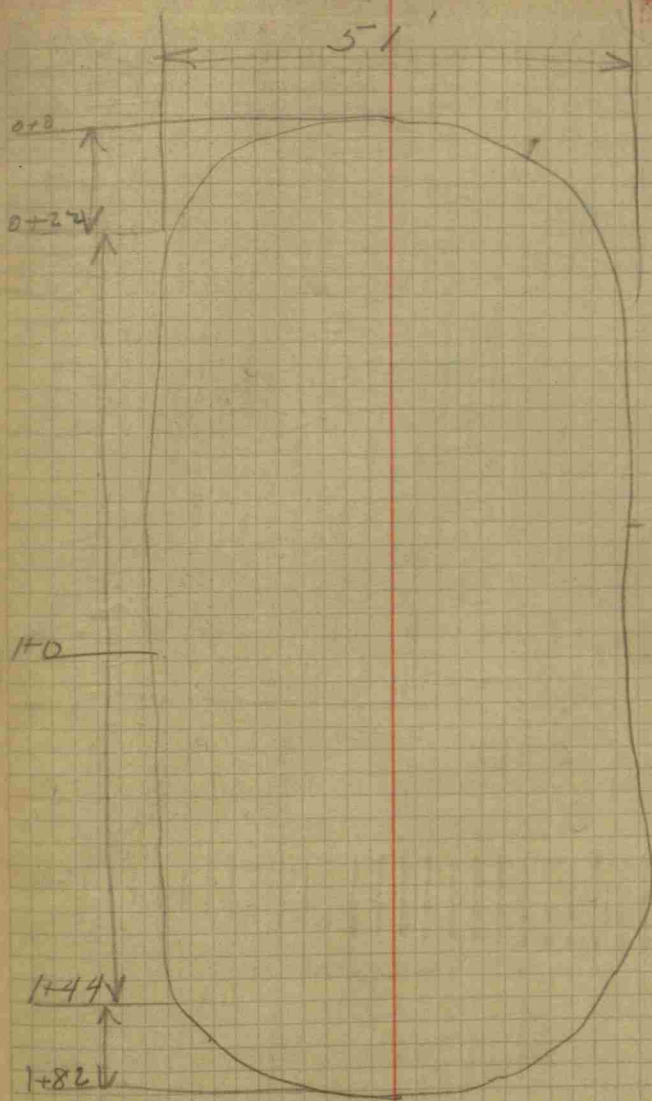
5.17

37  
37  
37  
32  
30

$$\begin{array}{r} 5 \overline{) 173} \\ \underline{15} \phantom{0} \\ 23 \phantom{0} \\ \underline{20} \phantom{0} \\ 3 \phantom{0} \end{array}$$
 34

91

62  
18  
44



92

4.

4.55

4.55

$6\frac{1}{2}$ "

$\begin{array}{r} 11.12 \\ 25 \\ \hline 10.87 \\ 6.25 \\ \hline 4.62 \end{array}$

11.12

6.25

93  
5' drop

11.22

4.71

$\begin{array}{r} 471 \\ 5 \\ \hline 9.71 \\ .55 \\ \hline 10.26 \end{array}$

403

$$\begin{array}{r} 10.35 \\ 6.00 \\ \hline 4.35 \end{array}$$

5

4.10

3.75

$$\begin{array}{r} 4.35 \\ 3.75 \\ \hline .60 \end{array}$$

$$\begin{array}{r} 10.90 \\ 9.30 \\ \hline 1.60 \end{array}$$

4020

$$\begin{array}{r} 7.50 \\ \hline 53.75 \end{array}$$

52.75

10.90

46.20

4.80

0.10

1.10

52.30

5.35

105

105

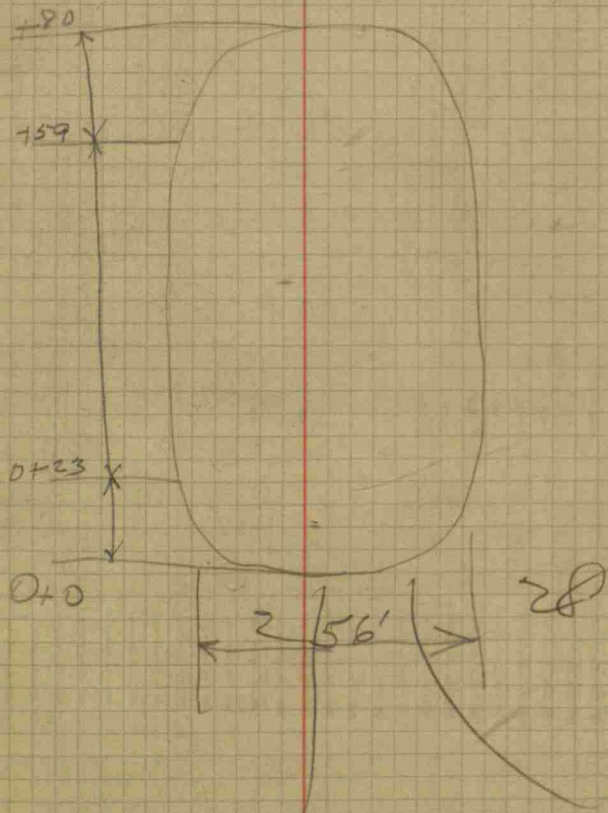
$$\begin{array}{r} 9.79 \\ 4.83 \\ \hline 4.96 \end{array}$$
$$\begin{array}{r} 8.62 \\ 1.16 \\ \hline 9.79 \end{array}$$

8.70

$$\begin{array}{r} 9.86 \\ 5.63 \\ \hline 4.23 \end{array}$$
$$\begin{array}{r} 9.70 \\ 1.16 \\ \hline 9.86 \end{array}$$

80108

80109



# 11

Sullivan Gravel

W

471

010

0130

1+40

1+70

E

# 15

116

-  $\pi$  + BM

104.47 4.47 100.01

width of pile = 40'

0+0

0+30

1+40

1+70

Side Rule 117

100.03  
4.4499.80  
4.6798.32  
6.1596.11  
8.30

118

-	+	BM
	102.86	2.86
		100

0+0

0+30

1+40

1+70

-	+	BM
	110.60	10.66
		100.00

-0.16

~~0+30~~

119.41 8.97

110.44

~~1+40~~

0+30

1+40

North Side

119

Sullivan

Tit

98.46

+4.40

99.15

3.71

97.78

5.08

95.03

7.83

Top Pile

116.80

2.61

113.70

5.71

Ave Height

115.88

4.14

5.02

2.84

2.49

2.58

4.15



100

	-	+	BM
0+0		105.06	5.06 / 100.00
1+0			
2+0			
3+0			
4+0			
5+0			
6+0			

Stk	Gd	f/
99.39		95.86
5.67		9.20
<del>99.15</del>		
5.90	5.40	625
99.63	99.16	
5.43	5.90	
99.90	99.56	
5.16	5.50	
100.11	99.67	
4.95	5.39	
99.96	99.56	
5.10	5.50	
99.32	99.06	
5.74	6.00	

300 East on top, to 94.96  
 10.10  
 94.42  
 fl. = 10.64

128

$$\begin{array}{r} 54 \\ 37 \\ \hline 136 \\ 102 \\ \hline 156 \\ 784 \\ \hline 372 \end{array}$$

$$\begin{array}{r} 28 \\ 28 \\ \hline 274 \\ 56 \\ \hline 784 \end{array}$$

$$\begin{array}{r} 59 \\ 23 \\ \hline 36 \end{array}$$

210

723

440

1163

$$\begin{array}{r} 19.3 \\ 14 \\ \hline 772 \\ 93 \end{array}$$

270.2

$$\begin{array}{r} 440 \\ 1866 \end{array}$$

$$\begin{array}{r} 5404 \\ 36 \\ \hline 32424 \end{array}$$

$$\begin{array}{r} 2640 \\ 2640 \\ \hline 3520 \end{array}$$

$$\begin{array}{r} 32424 \\ 16212 \\ \hline 194544 \end{array}$$

$$\begin{array}{r} 3520 \\ 37040 \end{array}$$

27 | 194 54.4 | 723

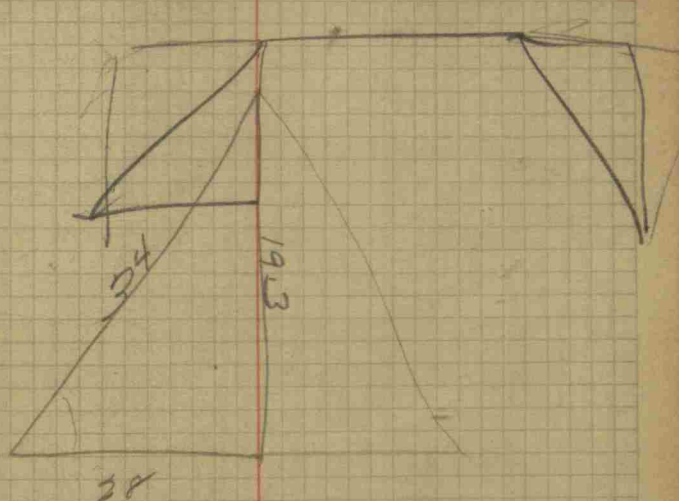
540.4

22

$$\begin{array}{r} 10808 \\ 10808 \\ \hline 11888.8 \end{array}$$

440

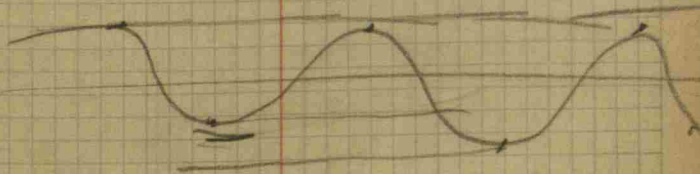
100  
95



723

371

1094



132

5.15

6.00

11.15

6.65

4.50

133

142

Mar	23	Office	
"	24	"	
"	25	Guilford + Liberty	65 mi
"	26	Brown Lincoln	
		Middle -	72 mi
"	27	True, Long, Simmons	
		Bridges	81 mi
"	28	Sunday	
		Rich	
"	29	Ditch	21 mi
		True	
"	30	True Bridge + WPA	42 mi
"	31	Sullivan Bridge + China	68 mi
April	1	Long + True + WPA	36 mi
"	2	Office	
"	3	Elk River Union Sup	49 mi
"	4	Sunday	
"	5	Union on Dick Bridge	22
"	6	" " " "	" "
"	7	Office	
"	8	Office	
"	9	Long + True + Parker B.	65
"	10	" " " "	65

143

April 11 Sunday

12 Sick

13 Long + True + Parker Bridge 65

	65
	72
	81
	21
	42
	68
	36
	49
	22
	22
	65
	65
	65
	83
	72
	65
	65
	71
	879
	05
	4445
	39
	48.35
	65
	49.00

78  
05  
290

889  
78  
967

April 14 Long + Parker Bridges and  
Clay Loop PB min 10 mi

April 15 Long Bridge + Parker 72 mi

" 16 Long + Forde C bridge 65 mi

" 17 + Sullivan's branch 11 78 mi

" 19 " " " 71 mi

" 20 Ferris + Long Bridge + WPA 27 mi

" 21 Parker Bridge + Cyclist's bridge 51 mi

" 22 Parker + Ferris + Long Bridge + Lucine 69 mi

" 23 Parker + Ferris Bridge + Lucine 72 mi

24 Office

26 Parker + Simmons HWP 65

27 " " " 65

28 " " " 65

29 " " " 65

30 " " " 65

1 " " " 65

3 Lucine branch " " 85

4 Parker Simmons " 65

5 " " " 65

6 " " " 65

Mason  
Lover

22  
23  
50

25  
39

morning to day

morning to John Bardine to day

Morning + Bardine to day

65

1.5

0.5

65

146

7	Parker Ferry + WPA	72
8	" " "	65
10	" " "	65
11	Waston Island + WPA	52
12	Parker Ferry + WPA	65
13	" " "	60
14	" " "	60
15	" " "	60
17	" " "	60
18	Parker Clinic + Piers	73
19	WPA, Gully + Piers	83
20	" "	92
21	" "	72
22	Indianapolis + WPA	82
		<hr/>
		1661

147

	30
Garry	<del>27</del> hr
Bob	
Newman	4 hr
Don	12 hr

148

Mar. 11-38	Richard G. York	3 1/2 hr
	Noble Mason	5 hr
	Self	5 hr

---

12-38	York	3
	Green	3
	Self	3

---

14-38	York	7 1/2
	Green	7 1/2
	Self	7 1/2

149

152

6'-8" + one Band - allie  
22'-8" - 1-50 banks - } Smith  
30'-8" - 1-Costin - }

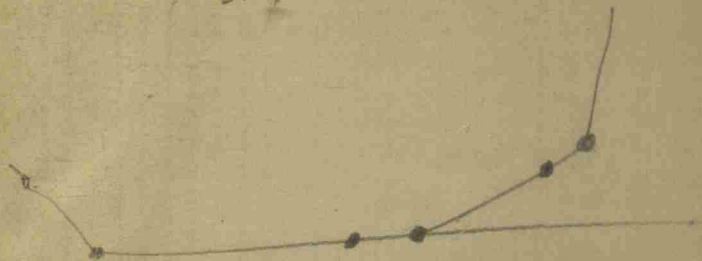
PAGE 3



Copie Walls Labels  
 Aug 26 '39 Newman

El. tile at 50. Drive	6.92
100' No.	6.53
50' No. (Head of tile)	6.98
50' No.	7.49
100' No	7.63
50' No	8.00
50'	8.74
50'	9.10
35+-	9.50

950  
 698  
 252



$$1750 \times \left(\frac{5}{8}\right) =$$

Cu. Yds

$$\begin{array}{r} 1094 \\ 8 \overline{) 8750} \\ \underline{6} \phantom{0} \\ 275 \\ \underline{72} \\ 30 \end{array}$$

North line  $\rightarrow$  10.31 ch.  
 S line  $\rightarrow$  9.465 + 2.28 ch

Ms-90.6

60  
 $\frac{2}{1200}$

Handwritten calculations and notes, including a large vertical line and various scribbles.

9500

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
 ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.  
 FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.