

199

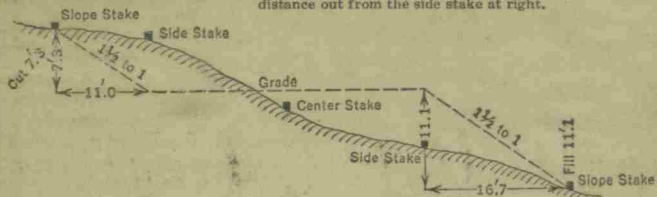
BRIDGES

K. E.
MINING
TRANSIT BOOK
363

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING

Roadway of any Width. Side Slopes 1 1/2 to 1.

In the figure below: opposite 7 under "Cut or Fill" and under .3 read 11.0, the distance out from the side stake at left. Also, opposite 11 under "Cut or Fill" and under .1 read 16.7, the distance out from the side stake at right.



Cut or Fill	Distance out from Side or Shoulder Stake										Cut or Fill
	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.0	0.2	0.3	0.5	0.6	0.8	0.9	1.1	1.2	1.4	0
1	1.5	1.7	1.8	2.0	2.1	2.3	2.4	2.6	2.7	2.9	1
2	3.0	3.2	3.3	3.5	3.6	3.8	3.9	4.1	4.2	4.4	2
3	4.5	4.7	4.8	5.0	5.1	5.3	5.4	5.6	5.7	5.9	3
4	6.0	6.2	6.3	6.5	6.6	6.8	6.9	7.1	7.2	7.4	4
5	7.5	7.7	7.8	8.0	8.1	8.3	8.4	8.6	8.7	8.9	5
6	9.0	9.2	9.3	9.5	9.6	9.8	9.9	10.1	10.2	10.4	6
7	10.5	10.7	10.8	11.0	11.1	11.3	11.4	11.6	11.7	11.9	7
8	12.0	12.2	12.3	12.5	12.6	12.8	12.9	13.1	13.2	13.4	8
9	13.5	13.7	13.8	14.0	14.1	14.3	14.4	14.6	14.7	14.9	9
10	15.0	15.2	15.3	15.5	15.6	15.8	15.9	16.1	16.2	16.4	10
11	16.5	16.7	16.8	17.0	17.1	17.3	17.4	17.6	17.7	17.9	11
12	18.0	18.2	18.3	18.5	18.6	18.8	18.9	19.1	19.2	19.4	12
13	19.5	19.7	19.8	20.0	20.1	20.3	20.4	20.6	20.7	20.9	13
14	21.0	21.2	21.3	21.5	21.6	21.8	21.9	22.1	22.2	22.4	14
15	22.5	22.7	22.8	23.0	23.1	23.3	23.4	23.6	23.7	23.9	15
16	24.0	24.2	24.3	24.5	24.6	24.8	24.9	25.1	25.2	25.4	16
17	25.5	25.7	25.8	26.0	26.1	26.3	26.4	26.6	26.7	26.9	17
18	27.0	27.2	27.3	27.5	27.6	27.8	27.9	28.1	28.2	28.4	18
19	28.5	28.7	28.8	29.0	29.1	29.3	29.4	29.6	29.7	29.9	19
20	30.0	30.2	30.3	30.5	30.6	30.8	30.9	31.1	31.2	31.4	20
21	31.5	31.7	31.8	32.0	32.1	32.3	32.4	32.6	32.7	32.9	21
22	33.0	33.2	33.3	33.5	33.6	33.8	33.9	34.1	34.2	34.4	22
23	34.5	34.7	34.8	35.0	35.1	35.3	35.4	35.6	35.7	35.9	23
24	36.0	36.2	36.3	36.5	36.6	36.8	36.9	37.1	37.2	37.4	24
25	37.5	37.7	37.8	38.0	38.1	38.3	38.4	38.6	38.7	38.9	25
26	39.0	39.2	39.3	39.5	39.6	39.8	39.9	40.1	40.2	40.4	26
27	40.5	40.7	40.8	41.0	41.1	41.3	41.4	41.6	41.7	41.9	27
28	42.0	42.2	42.3	42.5	42.6	42.8	42.9	43.1	43.2	43.4	28
29	43.5	43.7	43.8	44.0	44.1	44.3	44.4	44.6	44.7	44.9	29
30	45.0	45.2	45.3	45.5	45.6	45.8	45.9	46.1	46.2	46.4	30
31	46.5	46.7	46.8	47.0	47.1	47.3	47.4	47.6	47.7	47.9	31
32	48.0	48.2	48.3	48.5	48.6	48.8	48.9	49.1	49.2	49.4	32
33	49.5	49.7	49.8	50.0	50.1	50.3	50.4	50.6	50.7	50.9	33
34	51.0	51.2	51.3	51.5	51.6	51.8	51.9	52.1	52.2	52.4	34
35	52.5	52.7	52.8	53.0	53.1	53.3	53.4	53.6	53.7	53.9	35
36	54.0	54.2	54.3	54.5	54.6	54.8	54.9	55.1	55.2	55.4	36
37	55.5	55.7	55.8	56.0	56.1	56.3	56.4	56.6	56.7	56.9	37
38	57.0	57.2	57.3	57.5	57.6	57.8	57.9	58.1	58.2	58.4	38
39	58.5	58.7	58.8	59.0	59.1	59.3	59.4	59.6	59.7	59.9	39
40	60.0	60.2	60.3	60.5	60.6	60.8	60.9	61.1	61.2	61.4	40

199

Stanley Skuttle
20 June 1944.

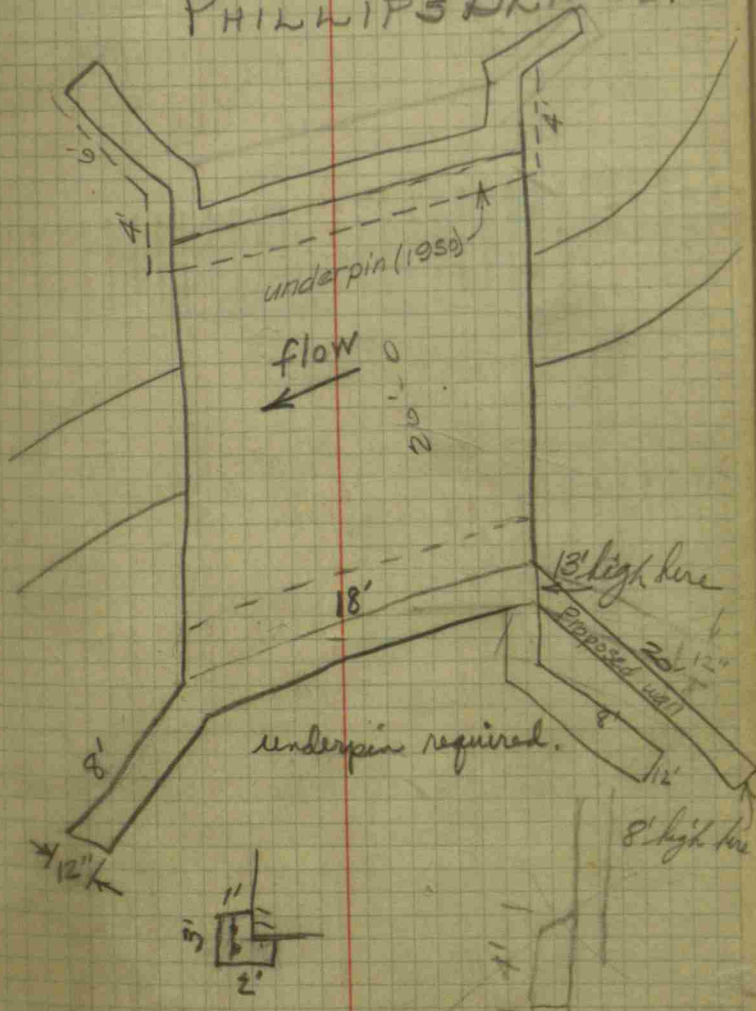
Present structure O.K. except
south abutment and wings need
underpinning.

1950 Repair
Underpin N abut - down 4'

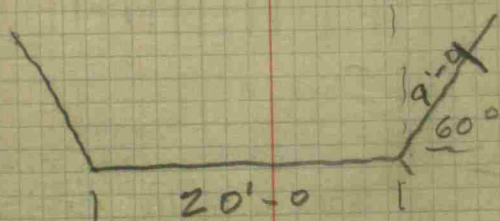
SE wall - 13' from top of footing
to road level at bridge & 8' high at
extremity with 3' deep footing

Near
W $\frac{1}{2}$ mi stone 20-15-2W
Concrete arch

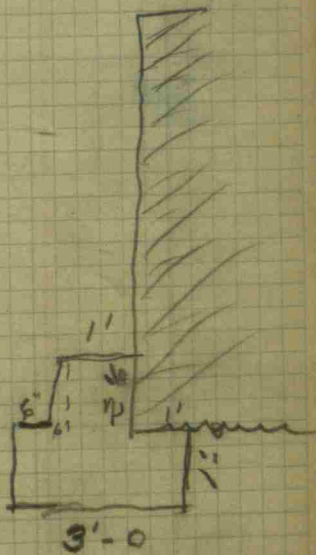
PHILIPPS BRIDGE



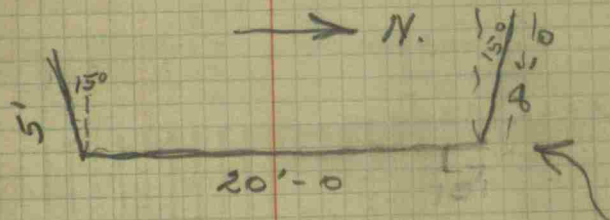
COSTIN BRIDGE
 NEAR SW. COR. 10-15-1E
 → N



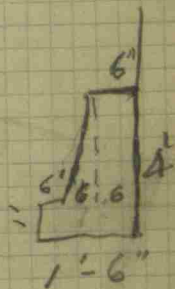
See page 58



FRANTZ BRIDGE



FRANTZ BRIDGE
NEAR CEM. S SE $\frac{1}{4}$
19-15-111.

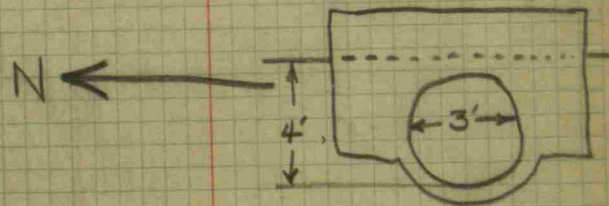
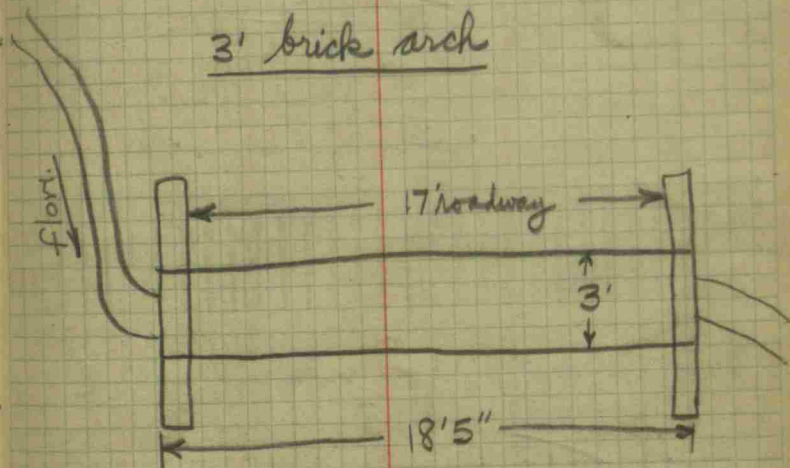


Stanley Skittle
20 June 1944.

The newly constructed bridge
should be built several
feet east of the present
site and should be built
on a skew of about 30° to right.

York Bridge
Near Cen S. SE⁴ 19-15-2W.

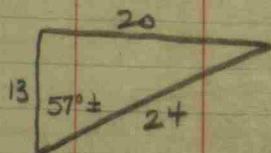
9



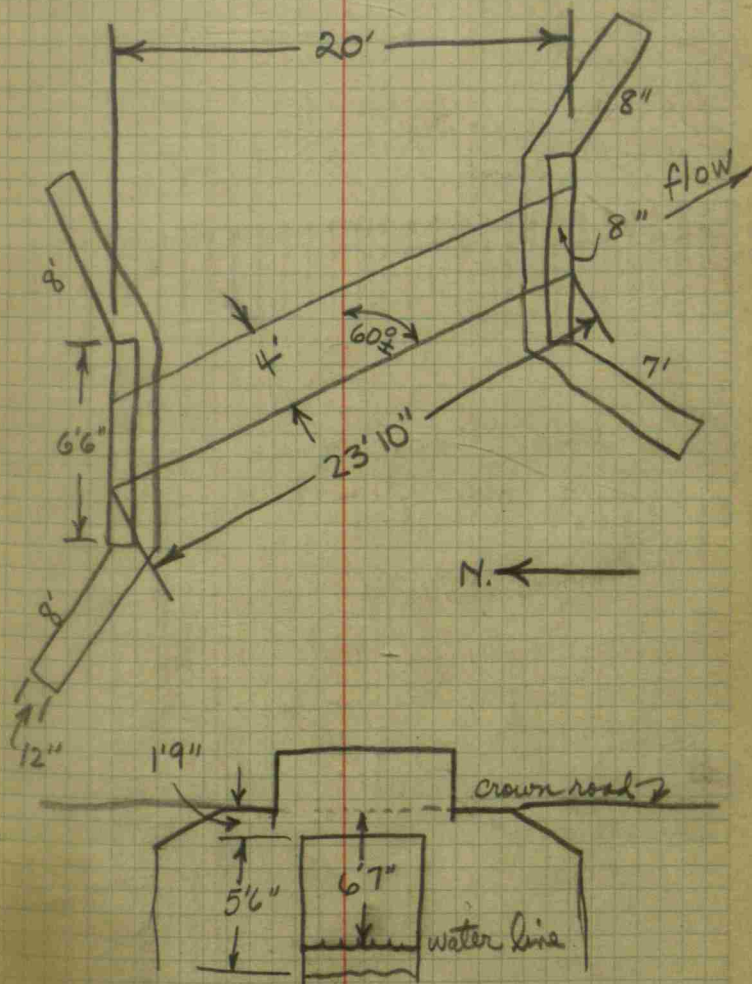
Stanley Shartle
21 June 1944.

Old structure built 1913. Concrete box
4' x 5' built on 35° skew to left.

7'3" from crown roadway
to flowline stream

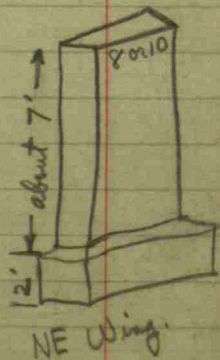


near SE cor 14-17-1E



Stanley Shartle
22 June 1944.

Present structure is of concrete and is built on a skew to the right. The northeast wing has fallen off the bridge. The newly constructed wing taking its place should be 8 or 10 feet long and 6 feet high from present water line up to top. Northwest wing needs repair or replacement.

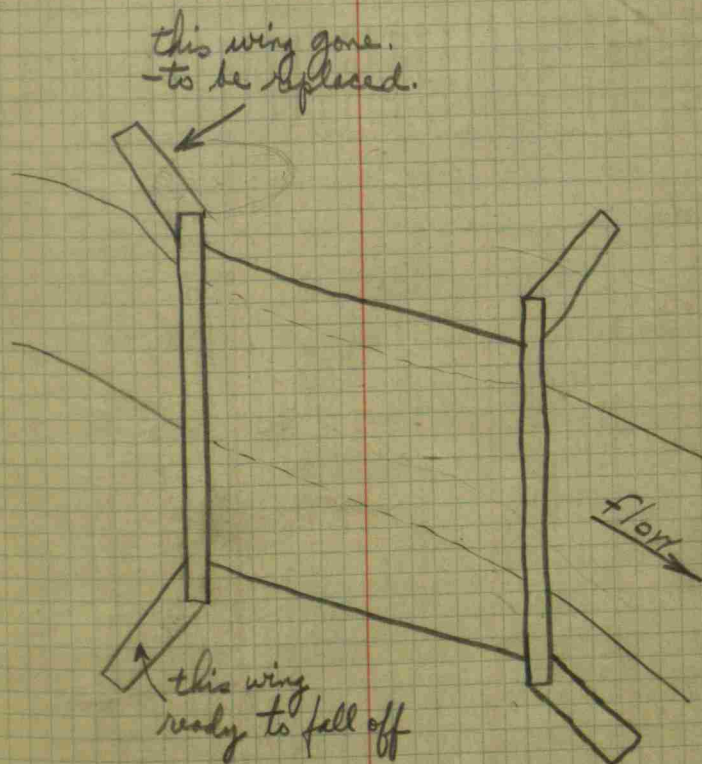


17

TUCKER BRIDGE

Near 5 1/2 mile stone 23-17-2M.

N ←



31st March 1945

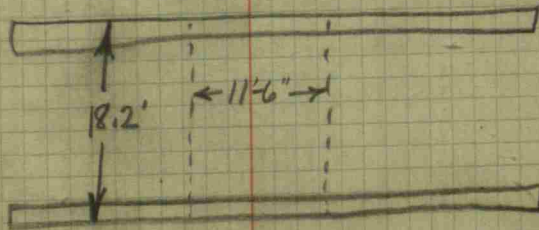
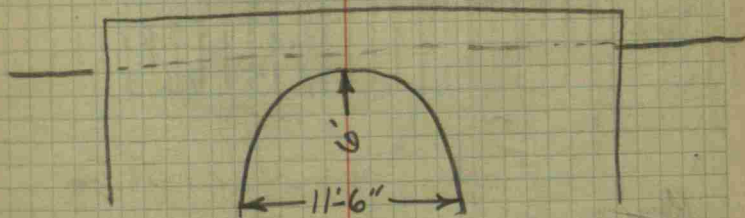
Major Franklin
Stanby Skettle

Underpin abutment on S- 4 feet deep.
" " on N- 3 feet deep.
Remove old floor.

800

SW¹/₄
3-15-1E

CARTHUESER 19
BRIDGE

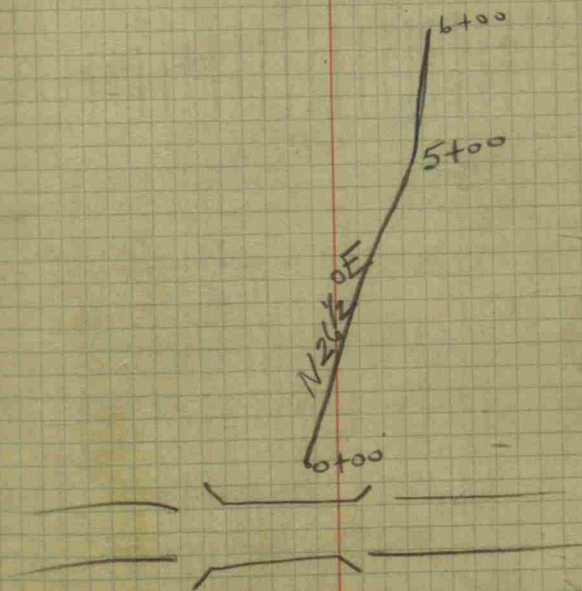


Sta.	B.S.	H.I.	F.S.	El.
0	10.74	100.00		89.26
1			4.16	95.84
2	6.04	104.30	1.74	98.26
3			7.55	96.75
4			4.83	99.47
5			8.83	95.47
6			11.15	93.15

Channel for Frantz Bridge

14. Aug. 1944.

Franklin
Shurtle



NE 1/4 27-14-2W.

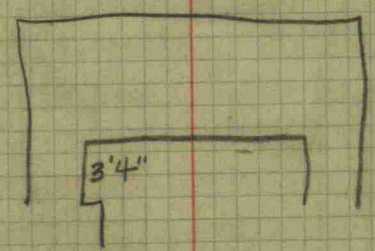
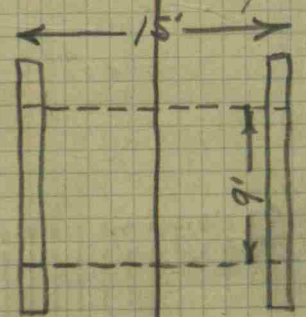
31 Mar. 1945

1948 Construction
R.M. Franklin
S.M. Skurtle

Widen to 20' roadway
Put 3' wings @ 45°

8X5 - Rfe Cove Box

Van Cosner Bridge
Franklin Twp.



31 Mar. 1945

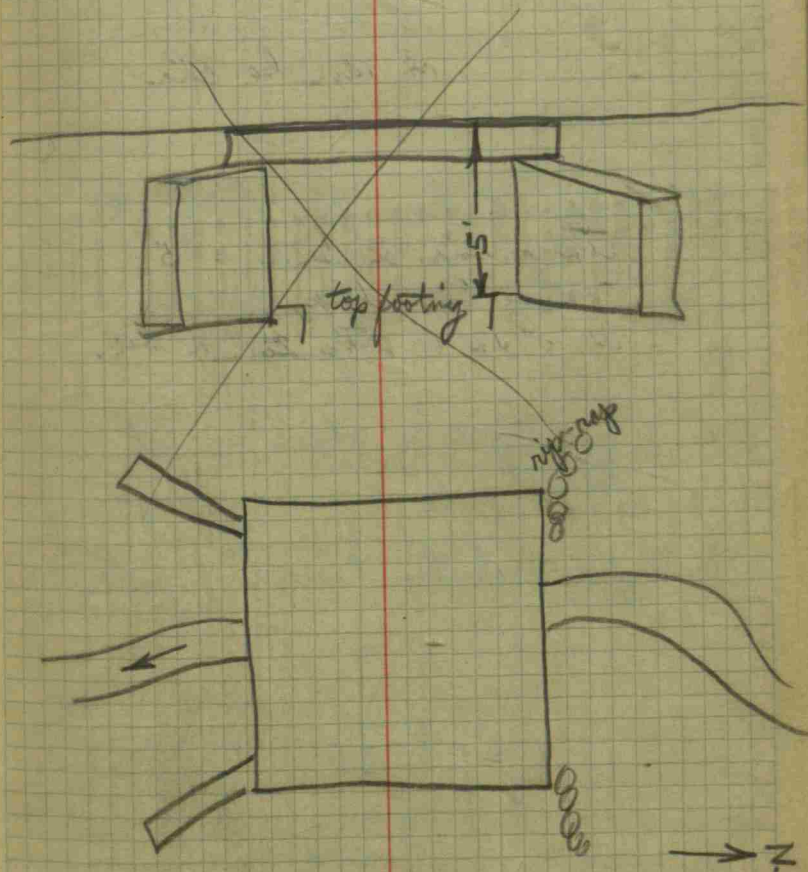
R. Major Franklin
Stanley Shurtle

New structure should be erected
about 33 ft east of present
bridge.

New struct should be 6x4 box
with 20 foot roadway.
Channel change estimated @ \$50.

24

Wise Bridge
Near $3\frac{1}{2}$ mile 7-14-2W.



Larrabee Bridge
Near Cen. 5-15-1E

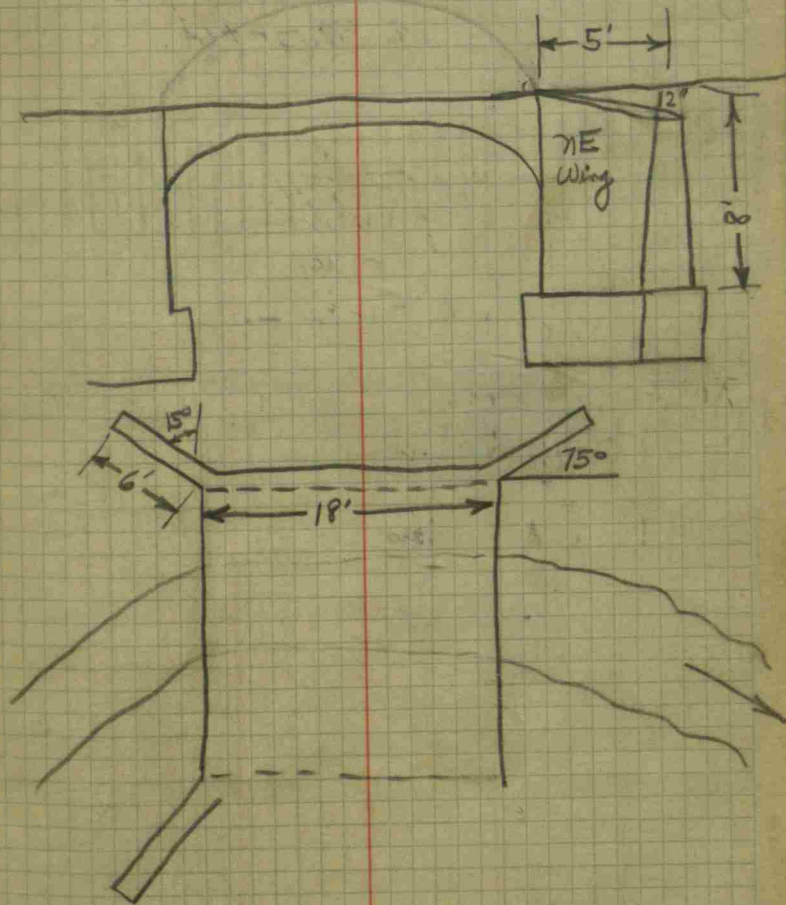
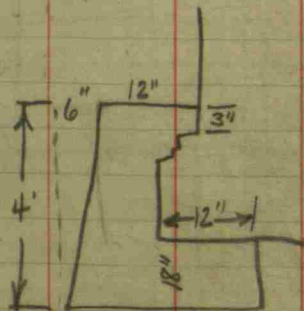
9 June 1945.

R. M. Franklin
S. M. Shurtle

NE Wing: 8' from top footing to
top wing. Length = 5'
Footing 18" deep, 2'-6" wide.
Wing 12" on top 24" on bot.

NW. Wing: same as above except
length = 6'

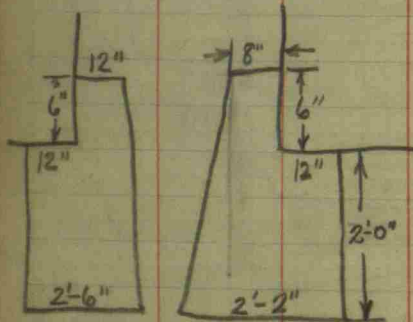
Underpin N. abutment with 4' footing



West Bridge
Near 1/2 Mile Stone 1-14-2W

9 June 1945

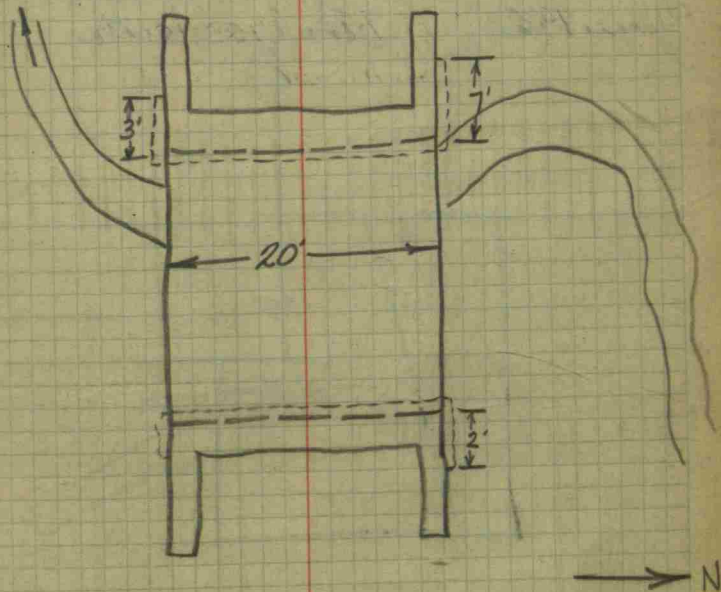
R. M. Franklin
S. M. Shartle



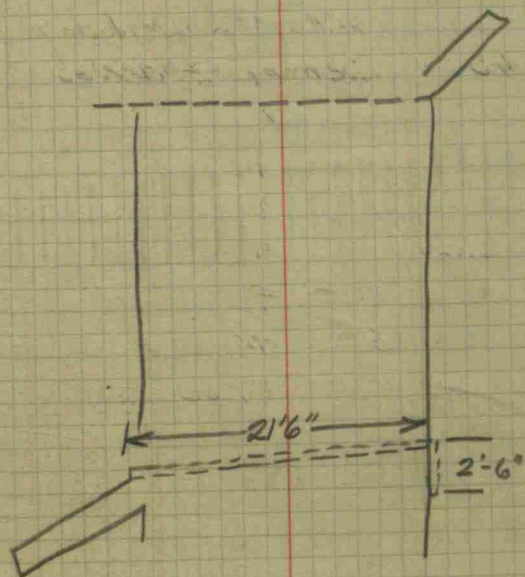
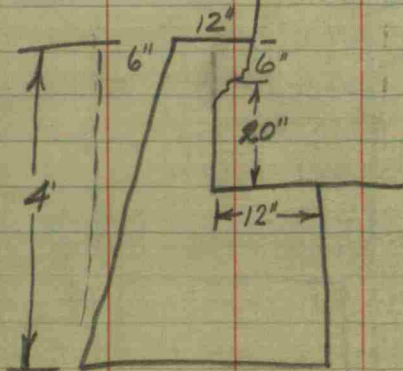
WEST
3'-6" deep

EAST

26



Osborn Bridge
Near S $\frac{1}{2}$ Mi. Stone 1-14-2W.
9 June 1945. Major Franklin
Stanley Shurtle



Chas Edmonson

Cen Sec 4 -14 -1 W

8X6 R+c. Box L = 22'-0.

\$100 150' Channel Change on North
30' Roadway

1947 Construction

B.S.	H.I.	F.S.	EL.	Location.
------	------	------	-----	-----------

2.37	100.00		97.63	B.M. top conc post 15' N of Cen 4-14-1 W.
		8.35	91.65	1 to at ditch
		6.00	94.00	1 to Ground at stake
		10.40	89.60	Flowline at bridge

5/12/47
Frymble
Spittle
Laypool

out for Present

29

Chas Edmonson

New Structure Located
50' W of Present - 30'-0 Rdwy
8'-0 From Top Rdwy To Top
of Footing - 10'-6 Span
150' Channel Change On South
300' " " " North
5'-0 Average Depth - 4'-0 Bot. Width

Jacktown or Clawson
Liberty & Franklin Twp.
W-Line Sec 17-14-1W
5 X 4 Rtc. Box L = 22'-0"
1947 Construction

Wise - Franklin Twp.

1947 Construction

Near $5\frac{1}{2}$ Mi. Sec 8-14-2W

8X5 Rfc Box L = 22'-0

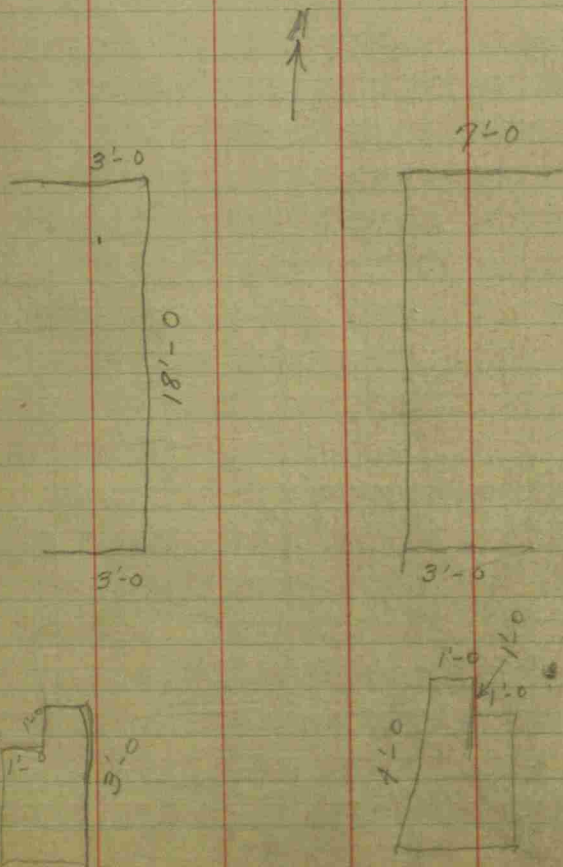
Channel Change 50' on North

150' on South 4'-0 Cut - 3'-0 Bot.

B.S.	H.I.	F.S.	EL.	Location
5.03	100.00			B.M. rail pole 814.
		8.88	91.12	ditch 50' N.
		6.48	93.52	ground 50' N.
		9.47	90.53	ditch @ bridge
		6.35	93.65	ground 40' N.
		9.60	90.40	" 40' S of ditch

in ditch

Rudd Clay Twp
 S. Line Sec 25-15-2W
 1947 Construction
 Underpin



out

Maba - Clay Trip.

~~E 1/2 Mile - 14' - 1 W~~

~~Channel Change & Piling~~

~~350' Long~~

~~16' Piling Driven 8' - 0~~

~~10' - 0 Bot. Width - 8' - 0 Cut~~

Adams - Fall River

1947 Construction

S.E. 1/4 Sec 29-17-2W

~~6X~~

~~12X6 Slotted~~ - Rdwy 36'

42" Fill Above Waterway

8X8 Ref. Box

Smith

Eel River 1947 Construction

Near Cen 5 of SE 1/4 Sec 20-17-2W

5X5 Rtc. Box L = 26'-0

Rdwy 33'-0 - Fill 3'-0

Gregor 1947 Construction

Brown Twp

Near SE Cor Sec 36-17-2E

7'-6" Top Footing To Top Floor

30'-0" Span Rwy 33'-0"

10" I Beams 25" C-C

Baumer Bridge Below Has

24'-0" Span

Haag Bridge Below (Private) 20'-0" Span

Ballard " " 21'-0" "

Wilde " " 1 Mile 27'-0" "

Present Structure -

7-10" I Beams - 4 $\frac{3}{8}$ " Flange

Pickerell - Liberty
Channel Change
Near E 1/2 Mi. Sec 30-15-1E
400' - 8'-0 Bot. Av. Cut 7'-0

9 May 1947.

R. M. Franklin

Stanley Startle

Ophir Claypool

Gilbert Bridge

29-15-2E

Guilford Twp.

1948 Construction

1X6 Rtc. Box

R/W between fences = 37'

Proposed roadway = 20'

~~Reeves Bridge~~

~~8-14-2E~~

~~Guilford Twp~~

~~8x5 Rfc. Conc Box~~

~~100' Channel Change~~

Mills BRIDGE

19-14-2E

Guilford TWP

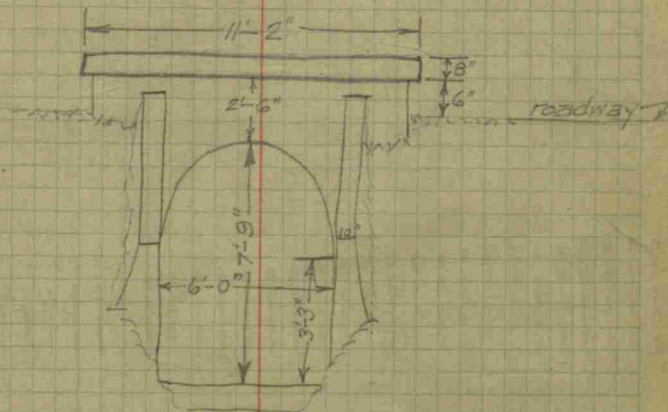
Cone Arch - Floor

1948 Construction

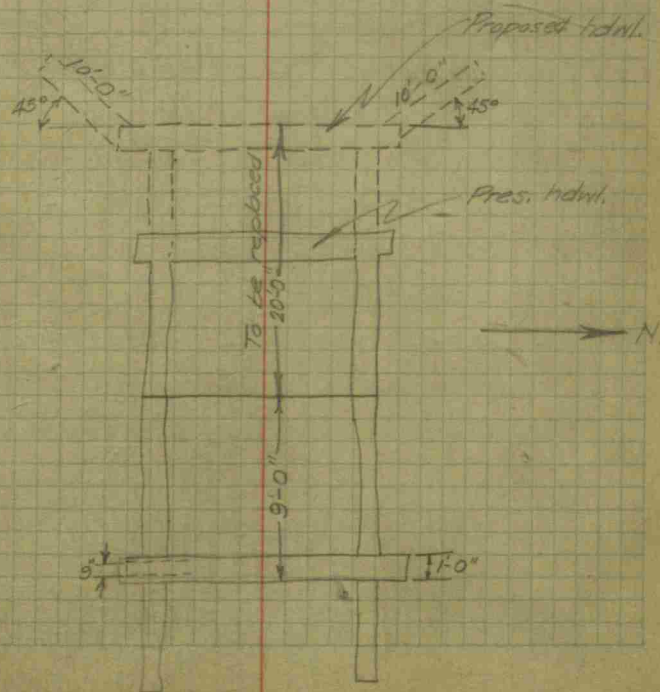
100' of Channel change

End of new wings to be 5'-0" high.

40



EAST ELEV.

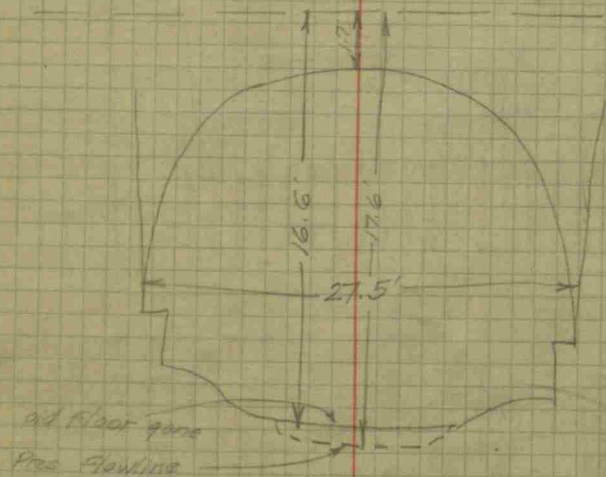
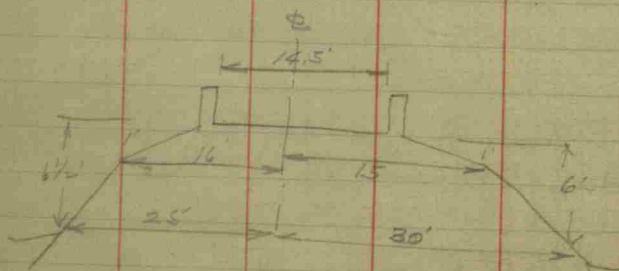


Wampner Bridge
24-15-1W
Center Twp.
8x6 Rfc Cove Box
1948 Construction

33' betw. fences

Whyte Bridge
Center Twp.

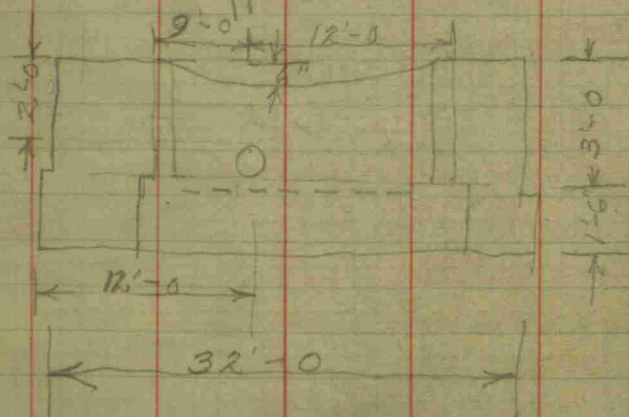
North of SE cor. 33-16-111
1948 Construction



3.7
3.3
11.7

42

Earl Cox Headwall
Chas. F. Martin Tile



43

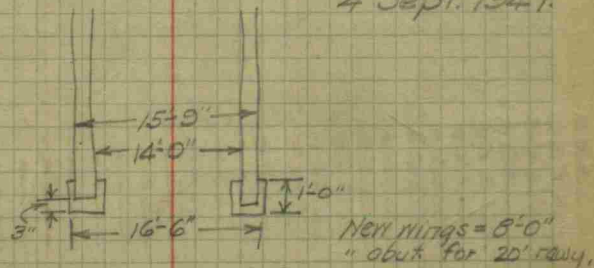
LOCKHART BRIDGE

over Mud Creek.

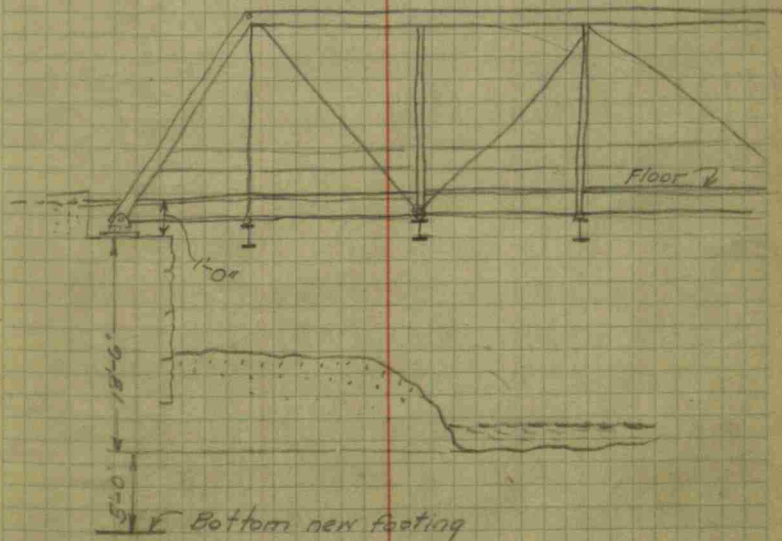
Franklin
Shurtle

1947 Construction

4 Sept. 1947.

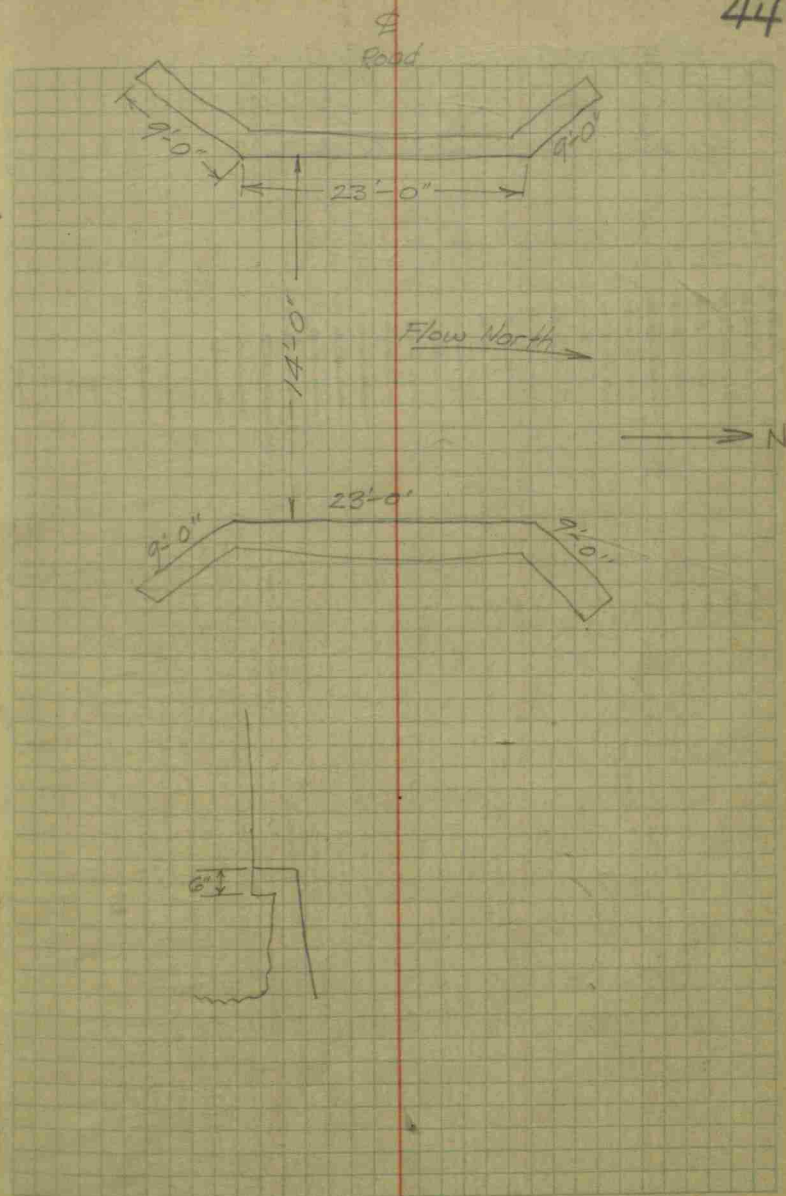


° PLAN °



W. Abut.

HEDGE BRIDGE
1948 Underpin repair
concrete bridge
W. of E $\frac{1}{2}$ Mi. Stone 36-17-W
24 June 1948
Middle Twp.



REYNOLDS BRIDGE
N $\frac{1}{2}$ Mi. 25-17-1W. Middle Twp.
1948 New Construction

8 x 8 R. C. Box
Length 22'-0"

Tucker Bridge
Ox B R. C. Box
20' Roadway
Skew 30° Rt.
W. of NE cor 16-16-1W

1948 Construction

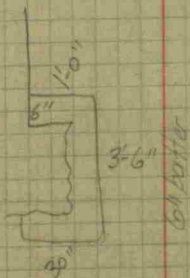
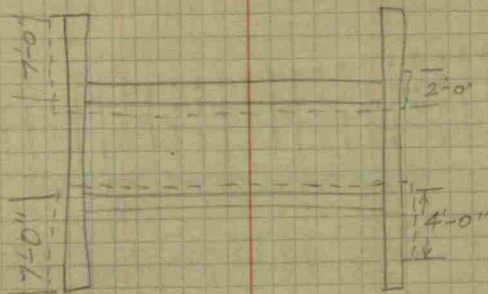
CHADD BRIDGE
20' Length
Hdwl. Wings 7'-0"
8' waterway
Underpin repair

W 19-16-2W

POSTPONED

47

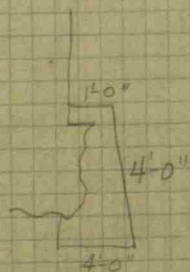
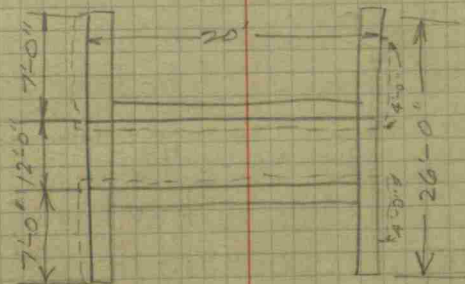
E
Rd



ROOKER BRIDGE
N. Line of 30-16-2N

Underpin

• POSTPONED •



ELLIS BRIDGE
W. of NE cor. 32-16-2W

Postponed!

Stuart Bridge

W. of E 1/2 Mi. S. 15-2W

Waterway 12'

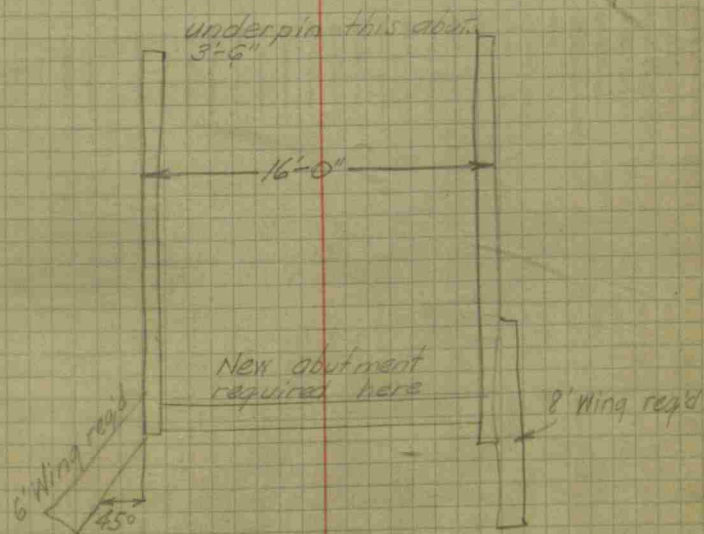
Height 6'

Roadway 20'

Marion Twp.

ROBARDS BRIDGE
 N $\frac{1}{2}$ Mile 14-14-2W
 1948 Repair
 Clay Township

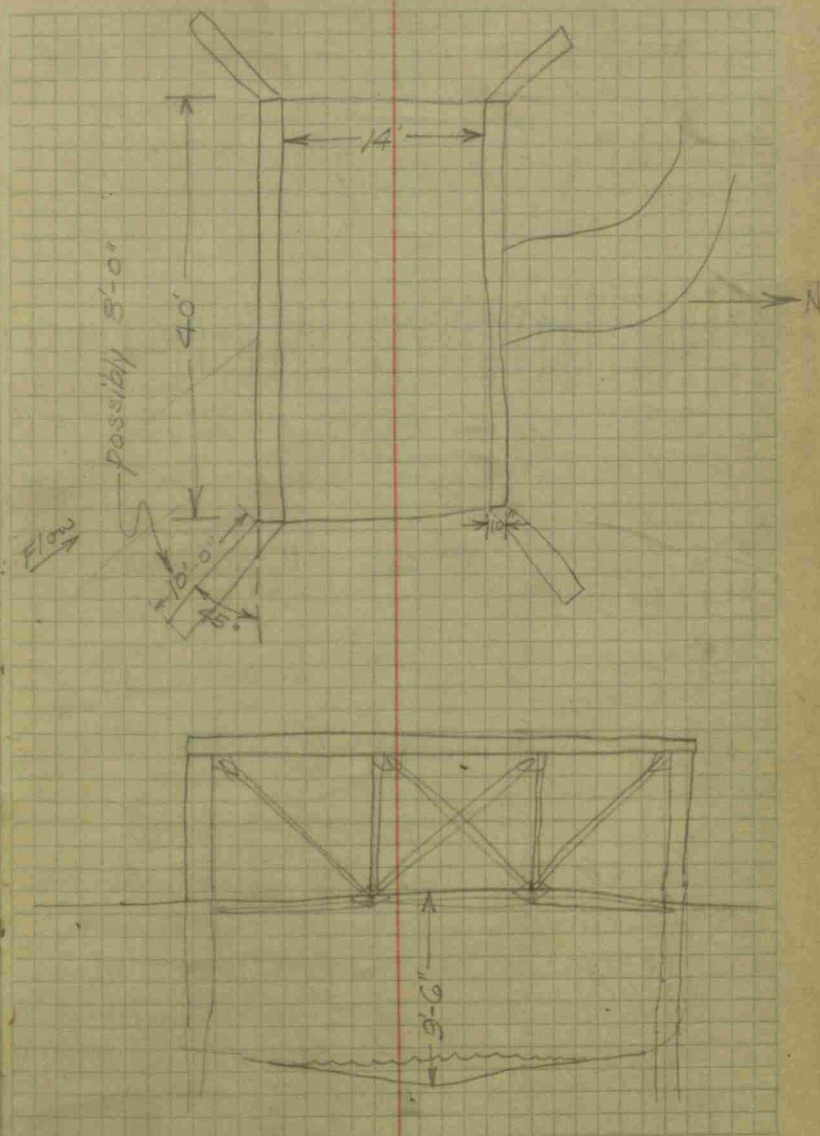
Top of footing to bottom
 slab = 9'-0"



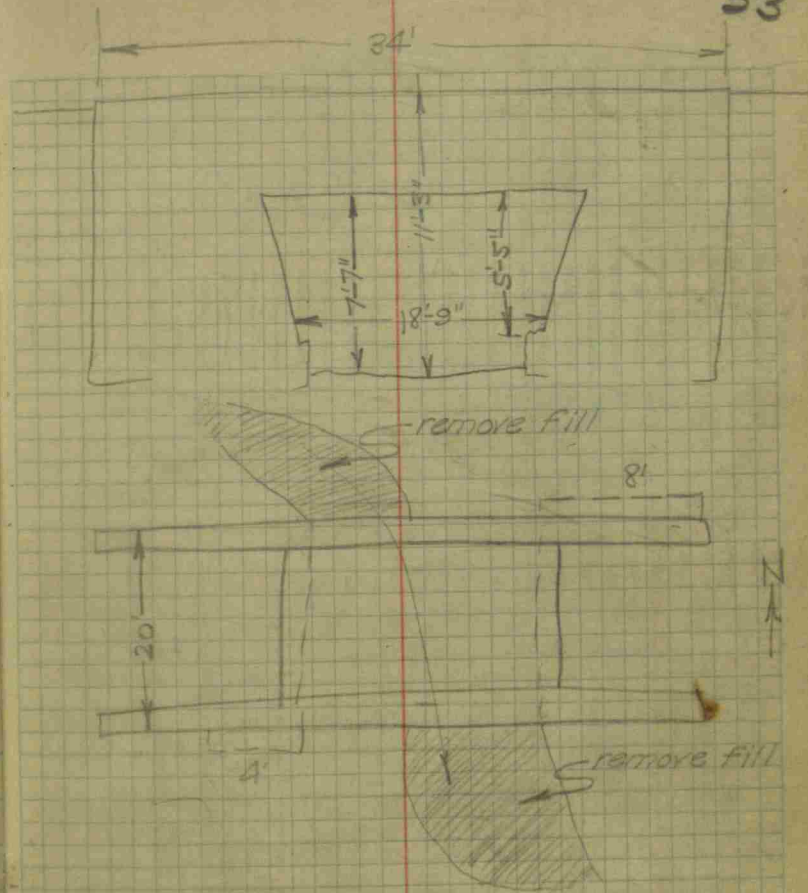
HOLTSCLAW BRIDGE

Franklin & Shattle
4 June 1949

Bottom of footings 3' below flowline



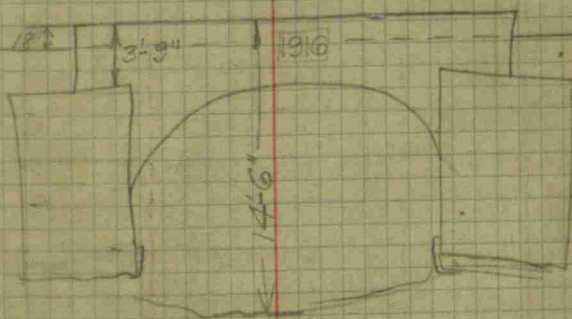
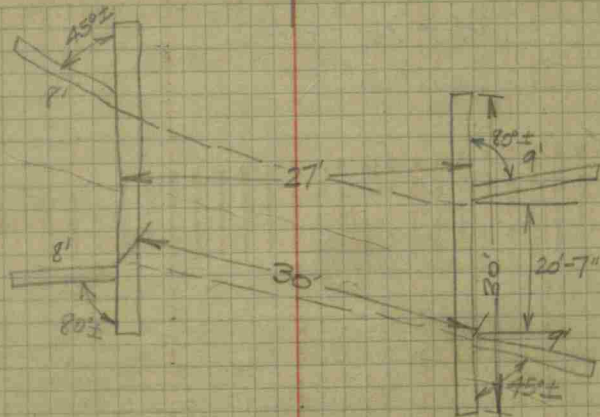
Graham Bridge
§ Sec. 21-16-1E
Lincoln Twp.
Nov. 21, 1949
Shurtle & Mason



Albertson Bridge
Near Cen. E. Cen. Sec. 16-16-1E
Lincoln Twp.
Nov. 21, 1949 Shurtleff & Mason

44-54.84

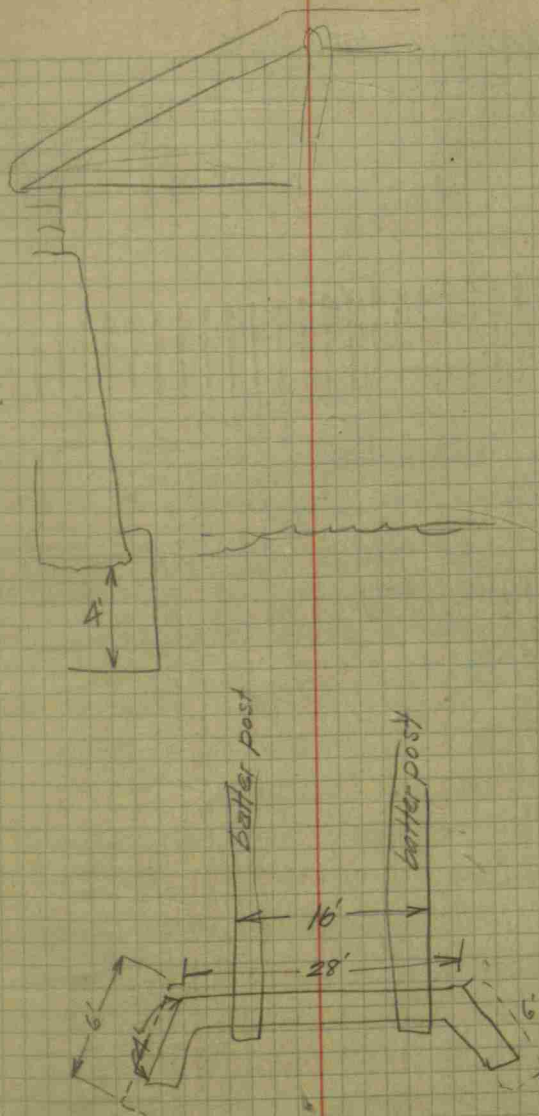
54



Lebanon Road Bridge
34-16-1W

Franklin + Shortle
30 Apr. 1950

55

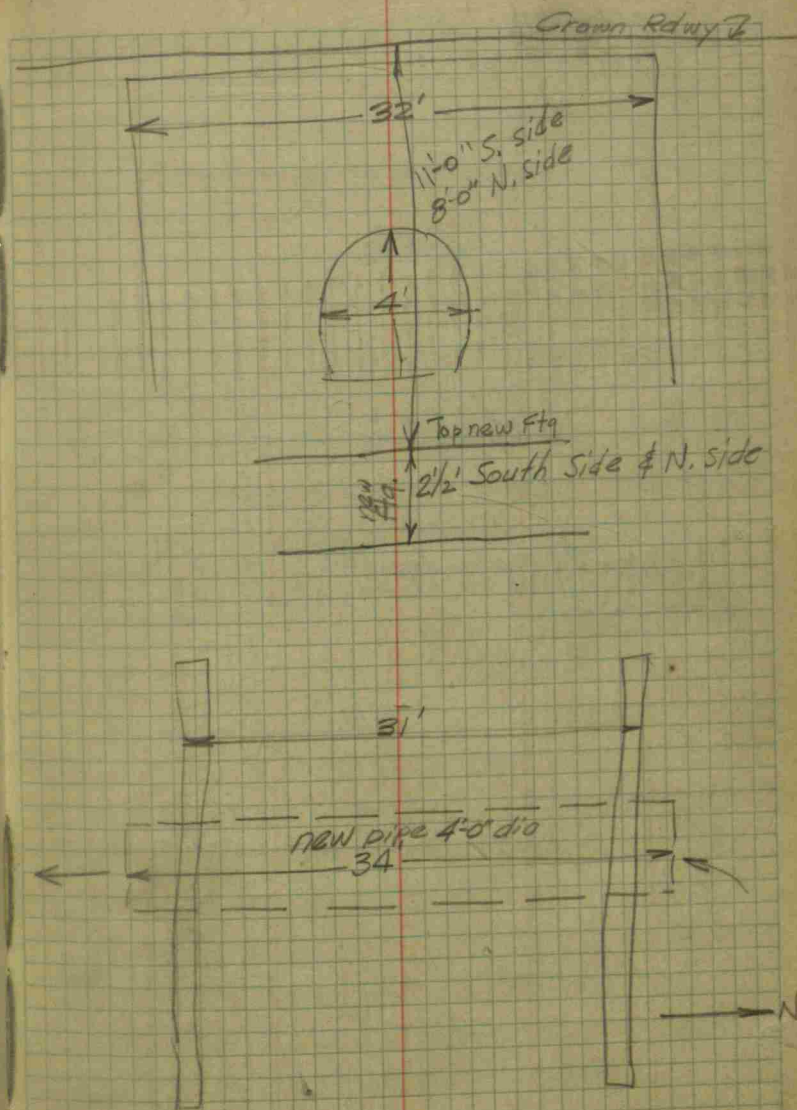


Walton Bridge
28-15-24

Franklin & Shartle
30 Apr. 1950 (Rain)

Re-examined by Shartle 1/31/53
Structure in very bad condition and
needs to be replaced. May be safe for
public use for some time yet if structure
is not subjected to severe conditions.
Recommend that this be put on list of
culverts to be built.

56



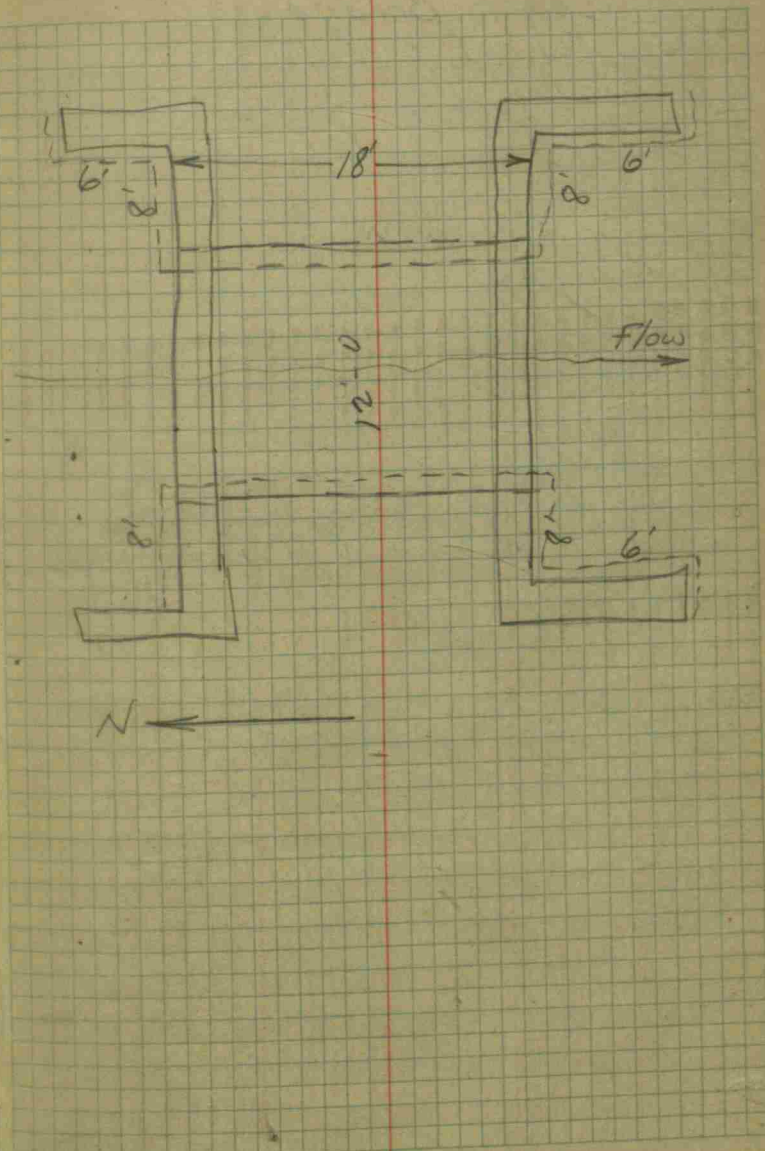
Gregory Bridge
24-14-2W

Franklin & Shurtle
30 Apr 1950 (rainy)

Underpin both sides and all wings
except NW.

Underpin to come up 1 ft on abut and
go down 4 ft.

57



Costin Bridge
 near SW cor 10-15-18
 (See page 6)

Franklin & Shurtle
 30 Apr. 1950

80' low
 16' to top of footing at bridge
 8' " " " " " at W end of well

16' to flowline

Footing should go down 3'

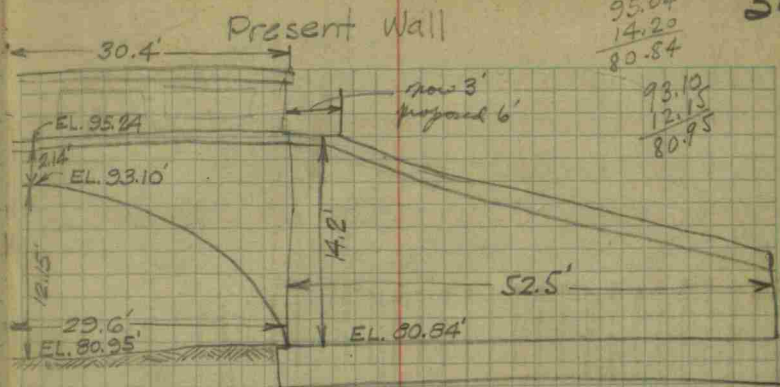
Avon Bridge repair
About 40 R. S. of E² Mi. 3-15-1E

Shurtle
Gossett
Shafer

25 April 1951.

Removal of present wing, spandrel, & kestrail		\$600
100 cu. yds. Channel change @ #1.25		\$125
Dry excavation	cu yds @ \$1.50	
Wet excavation	cu yds @ \$8.00	
Class A concrete in place	cu yds @ \$50.00	
Class E concrete in place	cu yds @ \$45.00	
Reinforcing steel	lbs. @ \$0.13	
Placing riprap	sf yds @ \$6.00	
Backfilling		

59



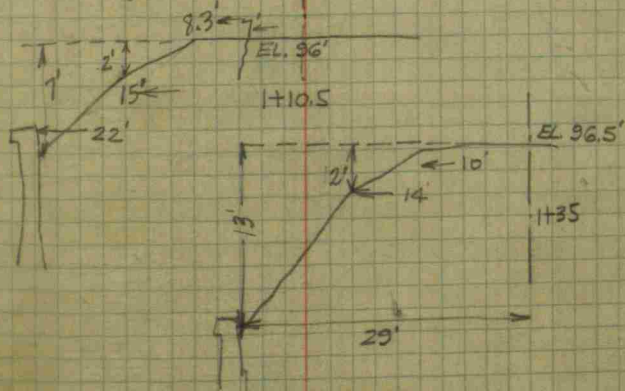
95.04
14.20
80.84

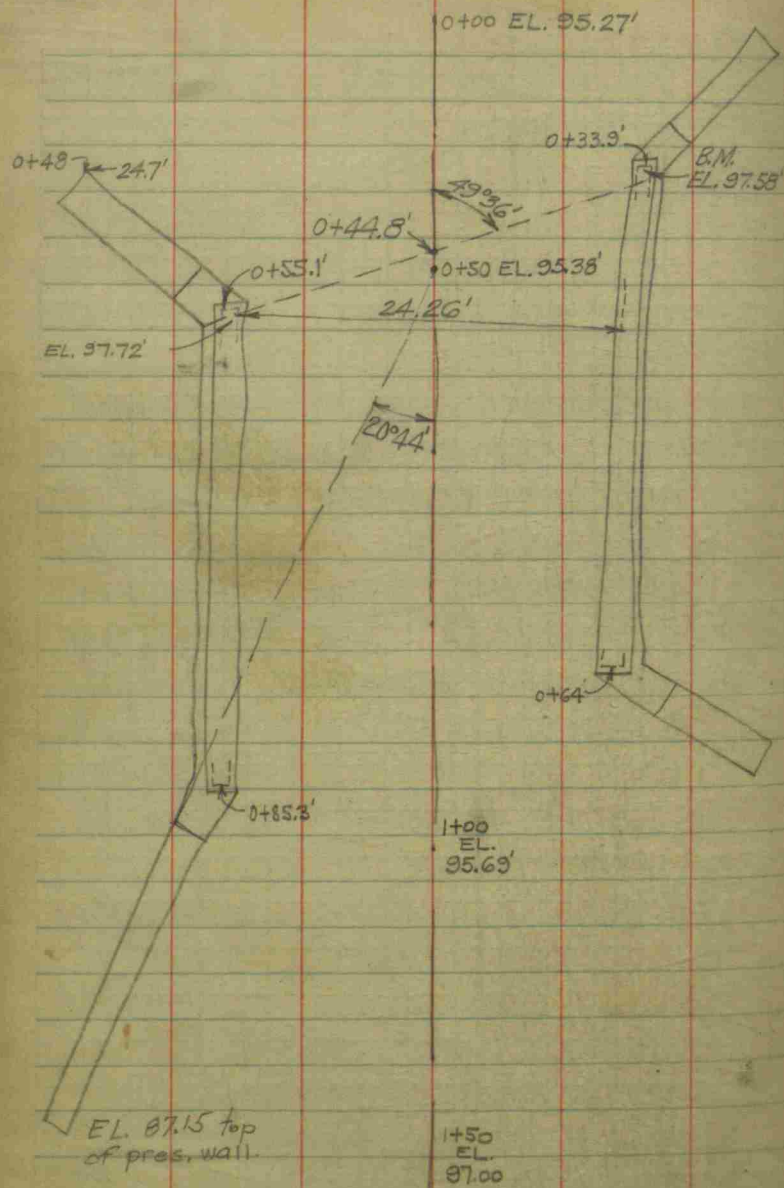
93.10
12.15
80.95



joint new spandrel to arching by
3/4" bars 1'-0" cc. on L.

408# coarse agg } 6 bags to yds
250 sand }
1 bag cement }

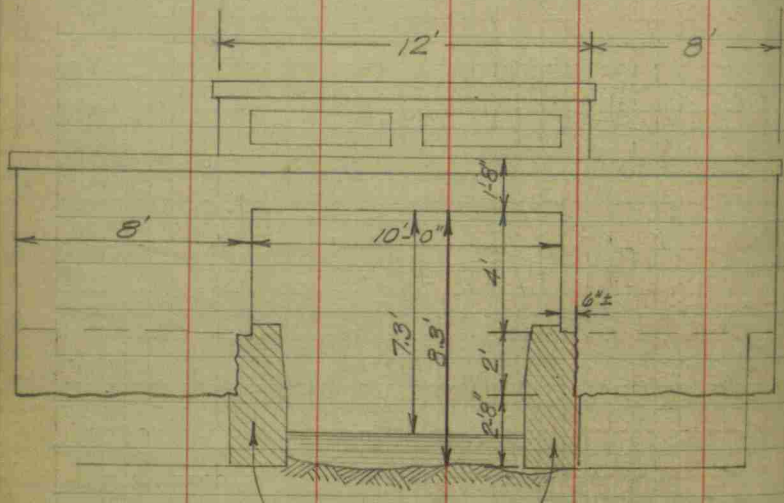




SHOCKLEY BRIDGE
Near 5th Mi. 18-17-1W Union Twp.

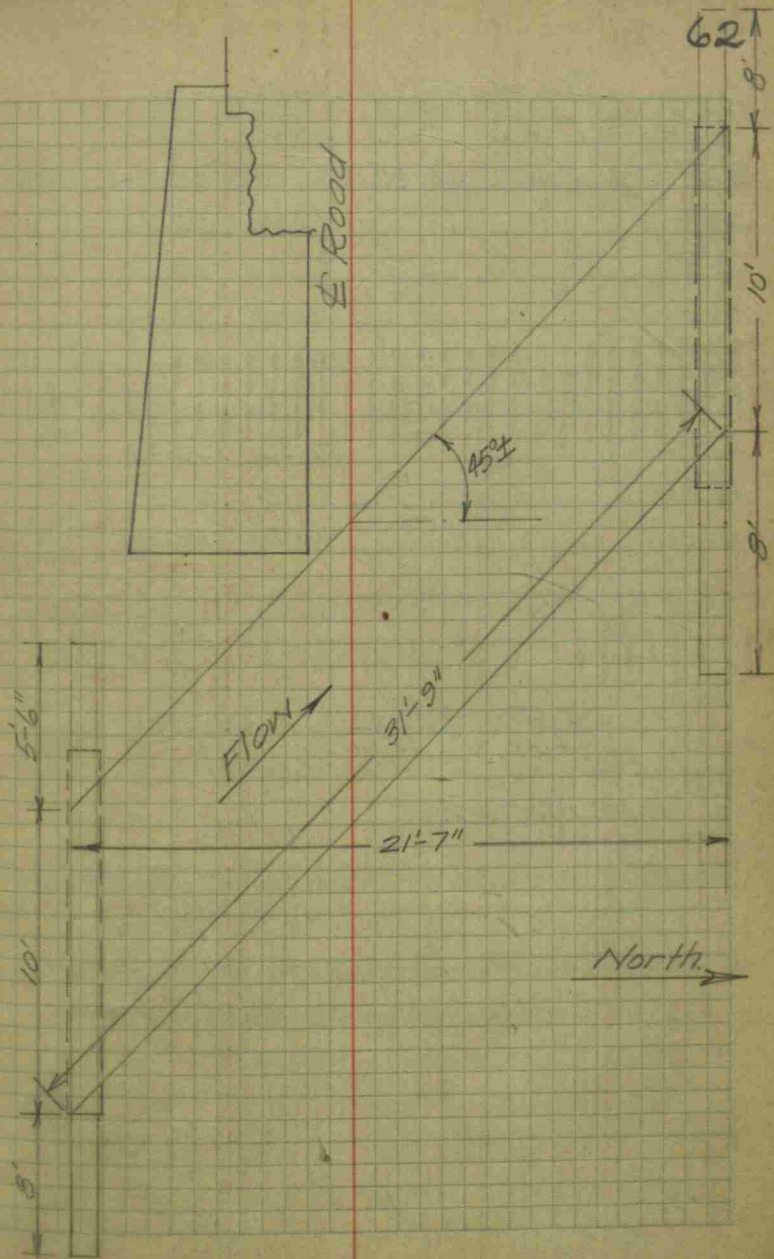
Shartle

May 13, 1951



Underpinning of 1931
to be removed.

NORTH END ELEVATION



Shockley Bridge

Sta.	B.S.	H.I.	F.S.	EL.
B.M.	2.50	64.80		62.30
28+00			12.40	52.40
29+00			12.20	52.60
30+00			11.60	53.20
30+30			4.13	60.67
30+60			3.88	60.92
31+00			11.30	53.50
32+00			11.10	53.70
33+00			10.70	54.10

	60.67	60.92	
	52.04	52.10	
N. end	8.63'	8.82'	S. end
8.00' approved.			

Spangler Ditch B.M. of 1930 on West NW wing of bridge.

Ceiling of box N end br.

" " " S " "

Computed from Spangler Ditch plans:
Floor @ N. end should be Elev. 52.04'

" " S. " " " " 52.10'

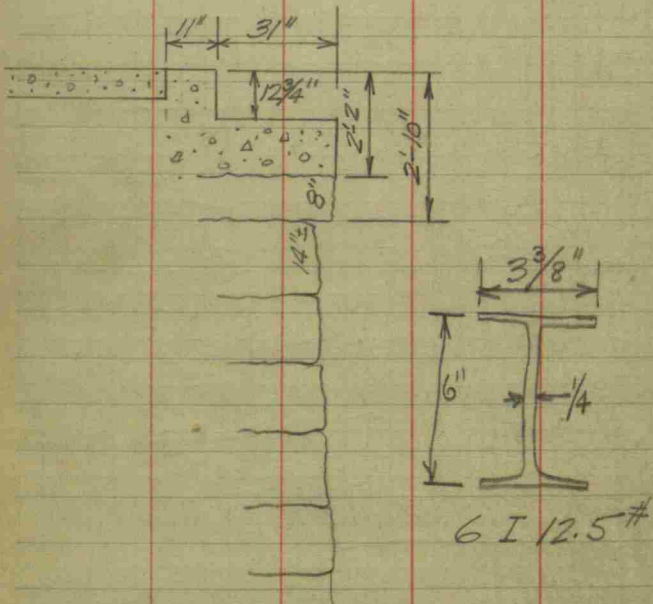
1400'± South (upstream) is flowline 16" D.T. with
Elev. of 55.85'

N end bridge on Spangler ditch = 30+30
0+00 = lower end of ditch

Weaver Bridge
 73± Rds. E. of Cen. Sec. 31-17-1E
 60' Pony Truss
 Failed July 16, 1951

Shartle

Jan. 29, 1952



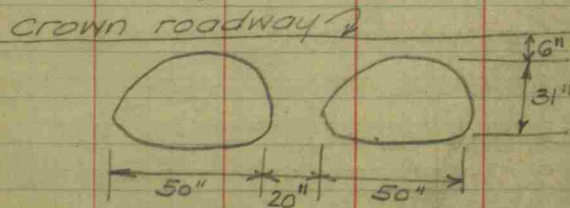
No. 1-1953 (New Const.)
Hadley Culvert
About 7 rods S. of NE. cor.
23-15-2W

Shurtle 1/31/53

Present structure: Timber beams on concrete abutments. Plank floor. Waterway 8 or 9' with height of about 3' to crown of roadway. No skew.

Watershed estimated to have an area of 175 acres. $C = \frac{1}{3}$.

Recommended: Two 12-gage pipe arches 22' long placed as follows:



4 sq. yds of lead-laid riprap obtained from the old structure shall be placed 12" deep at each end of the pipes instead of headwalls.

65

ESTIMATE

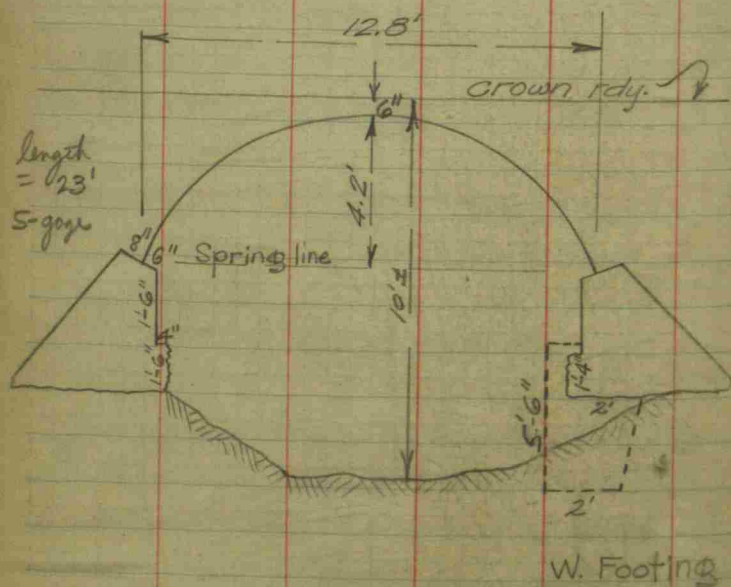
Pipe: C.M. Deformed 50x31	44 Lft.	\$14.00	\$616.00
Removal of Pres. Structure	1 L.S.	\$80.00	\$80.00
Prewarning signs	1 each	\$40.00	\$40.00
Std Barricades (Type A)	2 each	\$50.00	\$100.00
Placing lead-laid riprap 12"	8 sq	\$8.00	64.00
			<u>\$900.00</u>

Culvert No. 2-1953 (Repair)
 YEAGER BRIDGE
 @ Center 18-15-2W

Shartle 1/31/53

Watershed = 300 acres $C = \frac{1}{3}$

~~If present multi-plate arch is removed,
 I recommend either 36' of 66" dia. 10-gage
 C.M.P. which should be struttled during
 installation or a 5'x5' standard brinf.
 box culvert.~~



66

ESTIMATE

Class D concrete in structure	13.3 cu yd	\$80.00	\$1064.00
Reinforcing steel in structure	293 lbs.	\$0.15	\$43.95
Prewarning signs	2 each	\$40.00	\$80.00
Std Barricades (Type A)	2 each	\$50.00	\$100.00
			\$1287.95

SPECS.

Applicable provisions of Sec. E16 shall apply to the underpinning of existing footings, and the applicable provisions of Sec. E4 shall apply to the construction of the weir and apron.

Culvert No. 3-1953 (New Const.)
 Kentucky St. Bridge
 Danville, Ind.
 56 R. N. & 19 R. E. of SW. cor.
 E² NE⁴ 9-15-1W

Shurtle 1/31/53

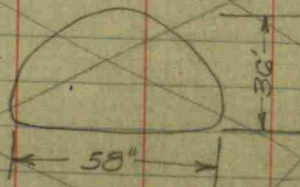
Estimated watershed = 110 acres $C = \frac{1}{3}$
 Use 54" R.C., C.I. or C.M. pipe for 4' x 3' standard
 reinforced conc. box culvert with W₂
 leadwells. (12-gage)

2 Conc. llwls W₂ reinf

Pipe should be 44' long.

Clean & straighten channel from bridge 30' W.

Or use one 12-gage pipe arch 44'
 long as follows:



~~Estimated cost of pipe arch only... \$470.00~~
~~Two connecting leads \$23.00~~
~~\$493.00~~

67

ESTIMATE

St. Barricade (Type A)	2	each	\$50.00	\$100.00
Warning signs	2	each	\$40.00	80.00
Pipe R.C., C.I. or C.M. 54"	44	Lft.	20.50	902.00
Removal of pvc. structure	1	L.S.	350.00	350.00
Class B. Conc. in structures	14.6	cys.	75.00	1095.00
Reinforcing steel in structures	940	lbs	0.15	141.00
Waterway Excavation	20	cys.	1.50	30.00
Clearing & Grubbing	1	L.S.	40.00	40.00
Sodding	50	cys	0.90	45.00
				<u>\$2783.00</u>

Contractor to replace subgrade but not base,
 combined base and surface, or surface courses.

Culvert No. 4-1953 (Repair)

BRIDGE

Near Cen. S. SE4 22-15-1E

Shartle 4/11/53

68

ESTIMATE

Ed. Barricades (Type A)	2 each	\$50.00	\$100.00
Class D. conc. in structures	20.8 cu yd	65.00	1352.00
Reinf. Steel in Structure	252 lbs	0.15	37.80
Blank grouted riprap	cu yd	7.00	
Repointing east abutment	1 L.S.	20.00	20.00
			<u>\$ 1509.80</u>

HENNIPMAN BRIDGE
 18 rods E. of N $\frac{1}{2}$ Mi. 32-16-2E
 Wash. Twp.
 Over Little White Lick Creek
 Shurtle 1/7/54

By careful investigation, I determine
 that this structure serves a watershed
 of 6.75 sq. miles or 4320 acres. Waterway
 area by Talbot's formula as follows:

$$a = \sqrt[4]{CV A^3}$$

Let $C = \frac{1}{3}$, then $a = 177.6 \pm$ or 178 sq ft
 waterway required.

Old Truss leg (worn deck) bridge 45'-10" long
 in place.

16'-4" betw trusses cto.c.

Clear waterway 45'

Ave high water 4.2' below floor rdwy.

Max. high water July 4, 1938, 0.5' below floor rdwy.

Structure in place to be removed:

2-16'	floor beams	12	I 50	1600 #
4-12	corner legs	9	II 26.8	1286
6-10	columns	6	I 12.5	750
6-46	stringers	6	I 12.5	3450
2-46	"	6	I 10.5	964
2-46	upper chord	3 $\frac{1}{2}$ x 2 $\frac{1}{2}$	T 9.8	902
4-15	lower "	3 $\frac{1}{2}$ x 2 $\frac{1}{2}$	L 9.8	588
2-16	"	2 $\frac{1}{2}$ x 2	L 5.5	176
4-3	verticals	2 x 2	# 12.8	154
144'±	diagonals	2 $\frac{1}{2}$ x 2	L 5.5	792
2-16	ext floor beams	5 x 5	L 16.2	518
4-12	leg diagonals	3 $\frac{1}{2}$ x 2 $\frac{1}{2}$	L 6.1	293
6-46	handrail chords	1 $\frac{1}{2}$ x 1 $\frac{1}{2}$	L 1.8	497
	handrail lattice, lateral bracing, plates, rivets			1200
				13172

or about 6 $\frac{1}{2}$ tons.

7 $\frac{1}{2}$ mi stone 32-16-1E - small stone found
 on top of a large stone 2'± deep. Replaced the
 small 4x8x11 stone on top of original.

Power pole S 50° W 32.02'

Base pole N 50° W 33.60'

Old wood cor. post S 45° E 27.24'

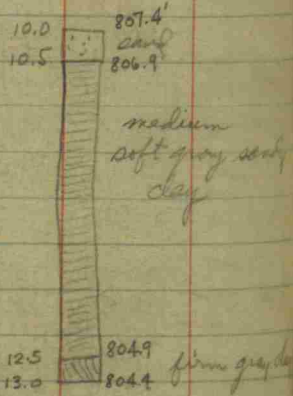
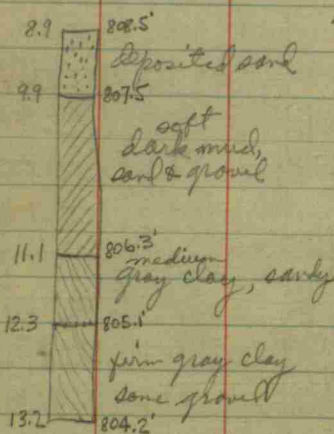
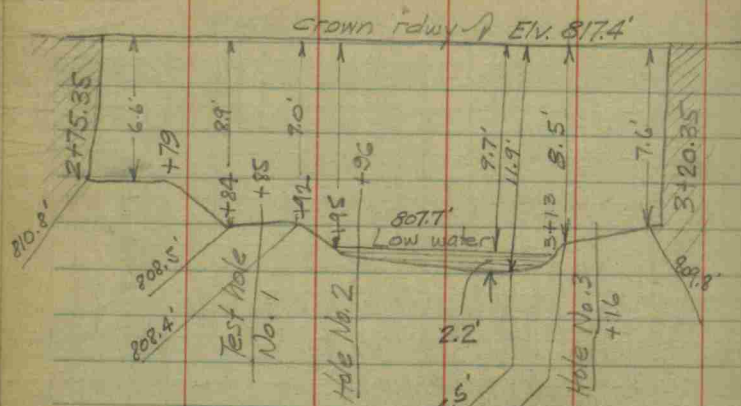
N. fence of road North 18.8'

2+74.65 center W. end center plank

2+74.85 F.F. stone midwall

2+75.35 W. edge clear waterway

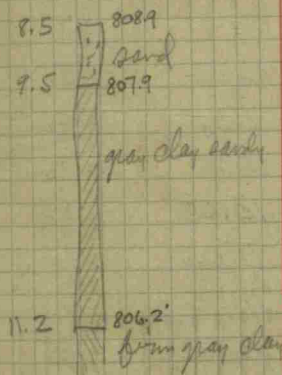
3+20.35 E " " "



All vert. meas. below roadway surface
E.V. at right.

71

Shartle } 1/25/54
Burrows } Fog
Graham }
Johnson }



#3

Estimated allowable bearing capacity 4 tons sq. ft.

Upstream from E structure

B.M. #1	0.23	818.94		818.71
Floor W end			1.63	17.31
" E. "			1.52	17.42
0+50			12.55	06.39
0+70			10.65	08.29
1+00			11.06	07.88
1+20			11.55	07.39
1+50			10.13	08.81
2+00			9.90	09.04
2+50			10.40	08.54
3+00			9.55	09.39
3+80			9.40	09.54
4+40			10.77	08.17
5+00			9.75	09.19
⊙	6.33	815.21	10.06	08.88
0+45	Downstream		7.70	07.51
1+00			8.13	07.08
1+50			8.23	06.98
2+00			8.72	06.49
2+25			8.15	07.06
3+00			9.00	06.21
4+25			8.40	06.81
5+00			9.00	06.21

B.M.#1	± Roadway		
	3.55	822.26	818.71
0+00		4.88	17.38
0+50		6.53	15.73
1+00		7.50	14.76
1+50		7.84	14.42
2+00		7.82	14.44
2+50		6.77	15.49
<u>-1-00</u>		0.50	21.76
2+74.65		4.96	17.30
3+20.35		4.85	17.41
3+50		4.60	17.66
4+00		3.95	18.31
4+50		3.01	19.25
5+00		2.01	20.25
5+50		1.39	20.87
6+00		1.13	21.13
6+50		0.89	21.37

Proposed
Cr. Rdwy.

0+00	817.38'
0+50	815.73'
0+75	815.30'
1+00	815.18'
1+25	815.80'
1+50	816.72'
1+75	817.47'
2+00	818.05'
2+25	818.47'
2+50	818.72'
2+75	818.80'
3+00	"
4+00	"
4+50	819.25'

G = -2.00%

P.V.I. 1+00

V.C. El. 814.80'

V.C. 50'

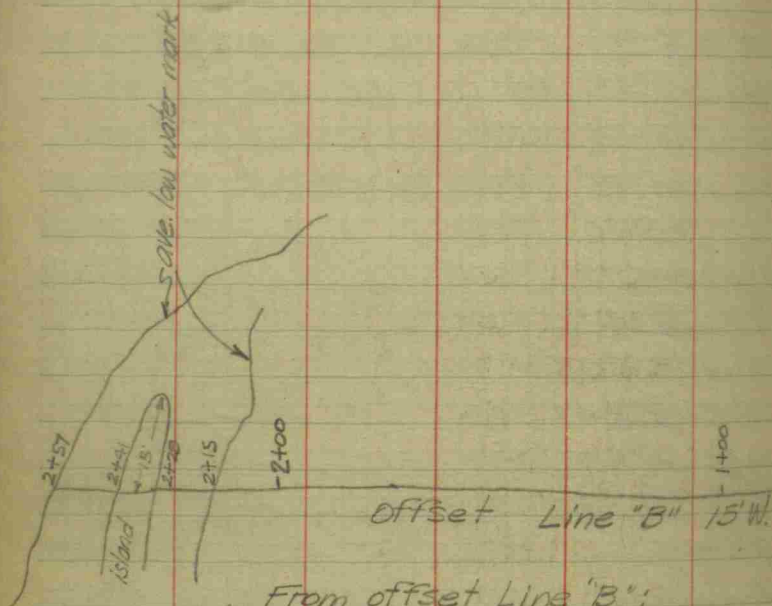
G @ P.R.V.C. = +4.00%

P.V.I. 2+00

V.C. El. 818.80'

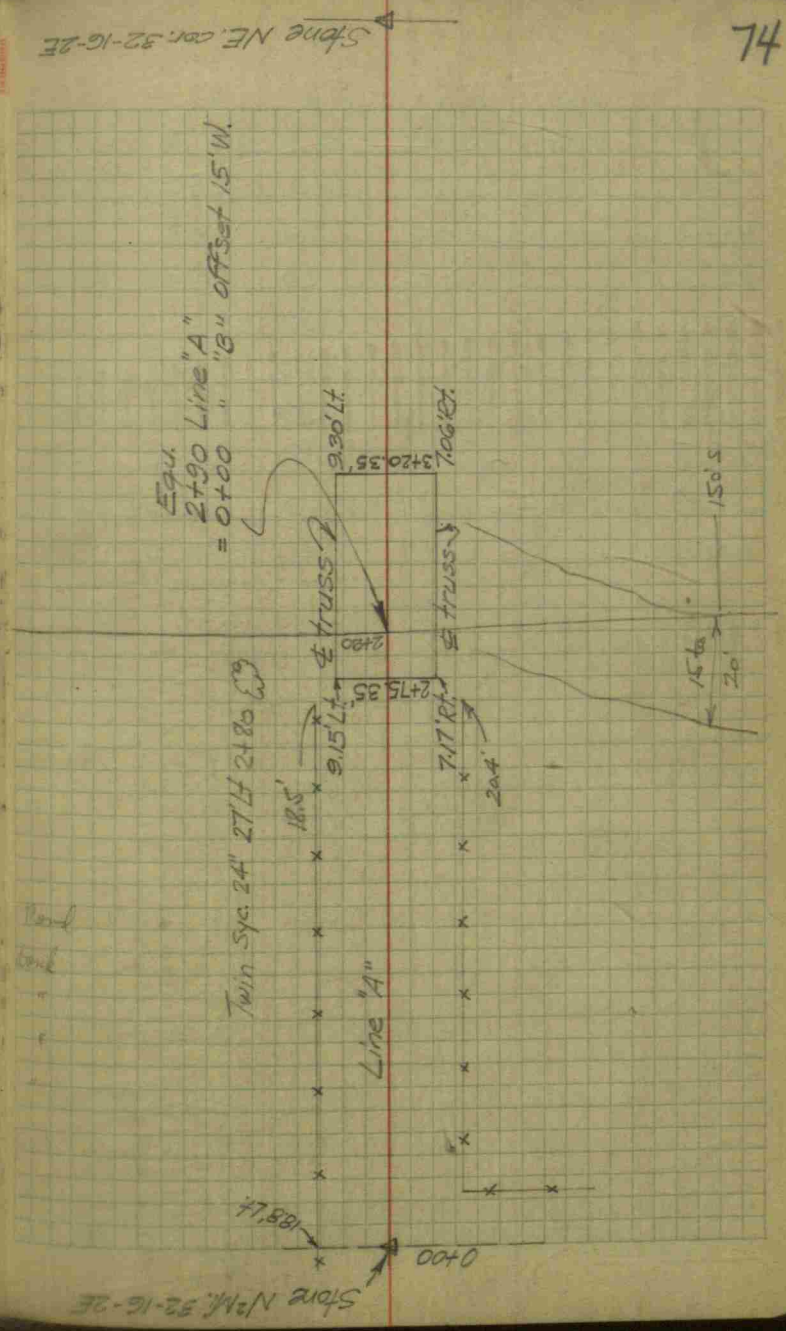
V.C. 150'

G = 0.00%



From offset Line "B":

Sta.	Top Bank	Bot Bank	W edge	E edge	Weg	Eq
2+00	9'	14'	37'	50'		
1+75	10	21	31	44		
1+50	16	22	22	29	50	59
1+25	17	17	17	31	65	65
1+00	22	22	22	39	65	
0+75	27	33	47	55	67	
0+50	22	27	33	49	64	
0+25	11	11	11	41		



	B.S.	H.I.	offset Line "B" F.S.	offset "B" EL.	Top back F.S.
B.M. #1	0.70	819.41			
0+25			8.40	811.01	8.70
0+50			7.50	811.9	7.50
0+75			7.20	812.2	6.90
1+00			7.30	812.1	6.60
1+25			7.00	812.4	6.60
1+50			6.80	812.6	6.80
1+75			6.90	812.5	6.90
2+00			7.10	812.3	7.50
2+10			7.40	812.0	

EV. B.M. = 818.71'

810.7

811.9

812.5

812.8

812.8

812.6

812.5

811.9

Windy, Fair
Jan 30, 1953

Levels- Clermont to Cen. N. Can. 8-15-2E
to est. elev. of B.M. #1 π SHARPLE
of Hennipman Bridge BURROWS
Survey. WATSON

			Miles
BM L50	6.81	833.13	0.0
	2.43	285	
	11.48	7.19	
	3.81	3.39	
	4.94	8.19	
	5.53	8.04	
	2.91	6.80	
	11.47	9.50	
	2.41	2.65	
	3.41	12.43	
BM #1		6.08	818.71
			818.64 2.1
	11.21	0.63	
	5.85	0.61	
	0.94	5.59	
	2.29	4.70	
	1.41	7.68	
	5.95	8.56	
	1.25	6.98	
	1.19	6.44	
	5.10	4.97	
	5.03	0.84	
B.M. #77		9.19	808.91
			808.75 4.4
			808.51
			0.16

76

Adjusted elev. in ink.

U.S.C. & G.S. B.M. L50-Clermont, Ind.

R.R. s.p.k. $N\frac{1}{2}$ Mi. 32-16-2E
p. pale SW cor "T" rd.

U.S.C. & G.S. B.M. #77
S. side C.C.C. & St. L. Ry. $\frac{1}{2}$ Mi. W. Co. line

4+00	$\frac{+1.2}{23}$	$\frac{+0.8}{20}$	$\frac{-1.9}{16}$	$\frac{-0.3}{13}$
3+50		$\frac{-4.5}{22}$	$\frac{-1.5}{16}$	$\frac{-0.6}{13}$
3+30			$\frac{-9.9}{27}$	$\frac{-0.3}{11}$
2+70			$\frac{-5.4}{18}$	$\frac{-0.4}{8}$
2+50	$\frac{-3.2}{23}$	$\frac{-3.6}{16}$	$\frac{-1.3}{11}$	$\frac{-0.4}{8}$
2+00		$\frac{-2.6}{19}$	$\frac{-1.7}{15}$	$\frac{-0.5}{12}$
1+50			$\frac{-1.1}{19}$	$\frac{-0.3}{11}$
1+00		$\frac{-1.4}{18}$	$\frac{0}{11}$	$\frac{-0.2}{8}$
0+50	$\frac{-1.7}{21}$	$\frac{-0.4}{17}$	$\frac{+0.3}{13}$	$\frac{0}{10}$

$Fill + 20\% = 764 \text{ cys.}$
 $Cut = 872$
 $Surplus = 108 \text{ cys.}$

$\frac{-0.4}{7}$	$\frac{0}{8}$	$\frac{-2.0}{14}$	$\frac{-0.5}{19}$	$\frac{+0.4}{23}$
$\frac{-0.3}{11}$	$\frac{-2.4}{16}$	$\frac{-2.8}{22}$		
$\frac{-0.2}{7}$	$\frac{-1.4}{12}$	$\frac{-4.5}{19}$		
$\frac{+0.2}{7}$	$\frac{-4.7}{17}$	$\frac{-4.8}{21}$		
$\frac{-0.5}{8}$	$\frac{-0.8}{10}$	$\frac{-3.4}{15}$	$\frac{-7.5}{20}$	
$\frac{-0.6}{12}$	$\frac{-1.8}{15}$	$\frac{-1.7}{20}$		
$\frac{-0.3}{8}$	$\frac{-0.2}{10}$	$\frac{-1.7}{20}$		
$\frac{-0.5}{8}$	$\frac{-0.4}{10}$	$\frac{-0.9}{13}$	$\frac{-1.3}{21}$	
$\frac{-0.4}{6}$	$\frac{-0.2}{9}$	$\frac{-1.0}{15}$		

637
 12
 1278
 128
 764
 77
 872
 764
 108

Levels for Jim Vaughn along N side

1145 road on

5/12/47 Franklin South - Chippewal

B.S.	H.I.	F.S.	EL.	
11.55	100.00		88.45	S. ditch
		7.75	92.25	top bank
		11.95	88.05	2nd ditch
		2.65	97.35	top bank
		8.70	91.30	3rd ditch
		5.75	94.25	N. ditch

$$I = 64^\circ$$

$$T = 300'$$

$$D =$$

$$L =$$

CURVE TABLES.

Published by KEUFFEL & ESSER CO.

HOW TO USE CURVE TABLES.

Table I. contains Tangents and External to a 1° curve. Tan. and Ext. to any other radius may be found nearly enough, by dividing the Tan. or Ext. opposite the given Central Angle by the given degree of curve.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Tan. opposite the given Central Angle by the given Tangent.

To find Deg. of Curve, having the Central Angle and External: Divide Ext. opposite the given Central Angle by the given External.

To find Nat. Tan. and Nat. Ex. Sec. for any angle by Table I.: Tan. or Ext. of twice the given angle divided by the radius of a 1° curve will be the Nat. Tan. or Nat. Ex. Sec.

EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle of Intersection or I. P. = $23^\circ 20'$ to the R. at Station 542+72.

Ext. in Tab. I opposite $23^\circ 20' = 120.87$
 $120.87 \div 12 = 10.07$. Say a 10° Curve.

Tan. in Tab. I opp. $23^\circ 20' = 1183.1$
 $1183.1 \div 10 = 118.31$.

Correction for A. $23^\circ 20'$ for a 10° Cur. = 0.16
 $118.31 + 0.16 = 118.47 =$ corrected Tangent.

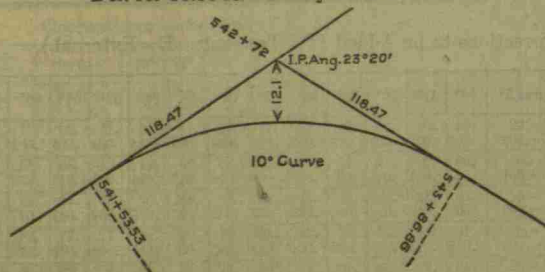
(If corrected Ext. is required find in same way)
 Ang. $23^\circ 20' = 23.33^\circ \div 10 = 2.3333 =$ L. C.

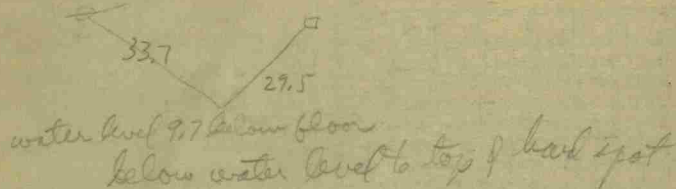
$2^\circ 19\frac{1}{2}' =$ def. for sta.	542	I. P. = sta.	542+72
$4^\circ 49\frac{1}{2}' =$ " " "	+50	Tan. =	1.18.47
$7^\circ 19\frac{1}{2}' =$ " " "	543	B. C. = sta.	541+53.53
$9^\circ 49\frac{1}{2}' =$ " " "	+50	L. C. =	2.33.33
$11^\circ 40' =$ " " "	543+	E. C. = Sta.	543+86.86
	86.86		

$100 - 53.53 = 46.47 \times 3' (\text{def. for 1 ft. of } 10^\circ \text{ Cur.}) = 139.41' =$
 $2^\circ 19\frac{1}{2}' =$ def. for sta. 542.

Def. for 50 ft. = $2^\circ 30'$ for a 10° Curve.

Def. for 36.86 ft. = $1^\circ 50\frac{1}{2}'$ for a 10° Curve.





$$\begin{array}{r} 3.0 + 9.7 = 12.7 \\ 3.4 + 9.7 = 13.1 \end{array}$$

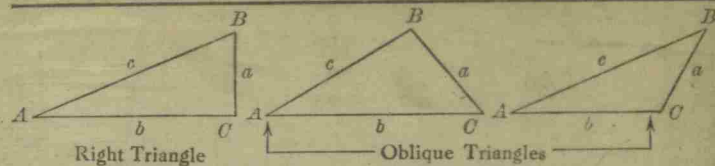
hand 11.1 below floor

$$\begin{array}{r} 7.65 \\ 5.1 \\ \hline 12.60 \end{array}$$

5.6
5.15
4.0
11.15

$$\begin{array}{r} 23.82 \\ 124.26 \\ \hline 148.08 \end{array} \quad \begin{array}{r} 17.3 \\ 3 \end{array}$$

TRIGONOMETRIC FORMULÆ



Right Triangle

Oblique Triangles

Solution of Right Triangles

For Angle A . $\sin = \frac{a}{c}$, $\cos = \frac{b}{c}$, $\tan = \frac{a}{b}$, $\cot = \frac{b}{a}$, $\sec = \frac{c}{a}$, $\operatorname{cosec} = \frac{c}{a}$

Given	Required	Formulas
a, b	A, B, c	$\tan A = \frac{a}{b} = \cot B$, $c = \sqrt{a^2 + b^2} = a \sqrt{1 + \frac{b^2}{a^2}}$
a, c	A, B, b	$\sin A = \frac{a}{c} = \cos B$, $b = \sqrt{c^2 + a^2} (c - a) = c \sqrt{1 - \frac{a^2}{c^2}}$
A, a	B, b, c	$B = 90^\circ - A$, $b = a \cot A$, $c = \frac{a}{\sin A}$
A, b	B, a, c	$B = 90^\circ - A$, $a = b \tan A$, $c = \frac{b}{\cos A}$
A, c	B, a, b	$B = 90^\circ - A$, $a = c \sin A$, $b = c \cos A$

Solution of Oblique Triangles

Given	Required	Formulas
A, B, a	b, c, C	$b = \frac{a \sin B}{\sin A}$, $C = 180^\circ - (A + B)$, $c = \frac{a \sin C}{\sin A}$
A, a, b	B, c, C	$\sin B = \frac{b \sin A}{a}$, $C = 180^\circ - (A + B)$, $c = \frac{a \sin C}{\sin A}$
a, b, C	A, B, c	$A + B = 180^\circ - C$, $\tan \frac{1}{2}(A - B) = \frac{(a - b) \tan \frac{1}{2}(A + B)}{a + b}$ $c = \frac{a \sin C}{\sin A}$
a, b, c	A, B, C	$s = \frac{a + b + c}{2}$, $\sin \frac{1}{2}A = \sqrt{\frac{(s - b)(s - c)}{bc}}$ $\sin \frac{1}{2}B = \sqrt{\frac{(s - a)(s - c)}{ac}}$, $C = 180^\circ - (A + B)$
a, b, c	Area	$s = \frac{a + b + c}{2}$, $\text{area} = \sqrt{s(s - a)(s - b)(s - c)}$
A, b, c	Area	$\text{area} = \frac{bc \sin A}{2}$
A, B, C, a	Area	$\text{area} = \frac{a^2 \sin B \sin C}{2 \sin A}$

REDUCTION TO HORIZONTAL

Horizontal distance = Slope distance multiplied by the cosine of the vertical angle. Thus: slope distance = 319.4 ft. Vert. angle = $5^\circ 10'$. From Table, Page IX. $\cos 5^\circ 10' = .9959$. Horizontal distance = $319.4 \times .9959 = 318.09$ ft. Horizontal distance also = Slope distance minus slope distance times (1 - cosine of vertical angle). With the same figures as in the preceding example, the following result is obtained. $\cos 5^\circ 10' = .9959$, $1 - .9959 = .0041$. $319.4 \times .0041 = 1.31$. $319.4 - 1.31 = 318.09$ ft. When the rise is known, the horizontal distance is approximately: the slope distance less the square of the rise divided by twice the slope distance. Thus: rise = 14 ft. slope distance = 302.6 ft. Horizontal distance = $302.6 - \frac{14 \times 14}{2 \times 302.6} = 302.6 - 0.32 = 302.28$ ft.

