



LEVEL BOOK
DITCH

10

LEVEL BOOK 10

387.3

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THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

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CHICAGO

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P. 1

Eads Drain

Sta.	B.S.	H.I.	F.S.	elev.	Remarks
B.M. 1	3.82	103.82		100.00	Assumed elev.
T.P. 1	5.83	106.89	2.76	101.06	
T.P. 2	5.61	108.75	3.75	103.14	Black Top
T.P. 3	2.72	110.45	1.02	107.73	
T.P. 4	0.67	110.37	0.75	109.70	in dirt road
T.P. 5	-0.34	107.57	2.44	107.93	"
T.P. 6	5.10	105.83	6.84	100.73	
B.M. 2	1.85	104.84	2.84	102.99	Point on NW corner of bridge near Richmond House
T.P. 7	4.84	104.46	5.22	99.62	in field of return to B.M. 1
T.P. 8	5.49	106.93	3.02	101.14	
B.M. 3			9.49	97.44	Top of culvert
T.P. 9	3.25	104.60	5.58	101.35	
T.P. 10	5.75	103.79	6.56	98.04	
T.P. 11	5.03	103.10	5.72	98.07	
B.M. 4			3.09	100.01	
check	49.94		59.08	-100.00	
	0.34		9.49		
	49.60		49.59		
check	-49.59				
check	0.01			0.01	

Winters in
Leak 0

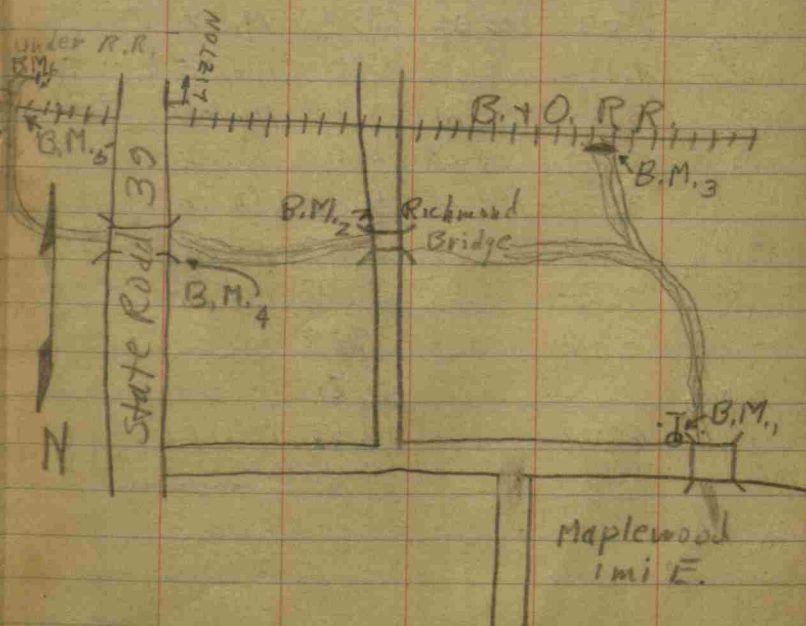
2-24-61
Foggy-Cold

Wet
level/rod

P. 2

Nail in Power Pole

Point on NW corner of bridge near Richmond House
of return to B.M. 1



3

Edds Drain

Sta.	B.S.	H.I.	F.S.	elev.	REMARKS
B.M. ₂	2.44	105.43		102.99	Richmond bridge 1/2 mi
T.P. ₁	5.01	107.60	2.84	102.59	
T.P. ₂	3.54	108.69	2.45	105.15	
B.M. ₄	4.28	109.91	3.06	105.63	Bridge on #39
T.P. ₃	8.94	115.91	2.94	106.97	N.W. cor. (base of railing wall on S. side)
T.P. ₄	4.43	119.43	0.91	115.00	
B.M. ₅	6.90	118.52	7.81	111.62	Nail at base of
T.P. ₅	6.56	120.79	4.29	114.23	E. side of power pole which is 1st pole E. of pole No. 145/40 on B+O.R.R.
B.M. ₆			7.54	113.25	Nail in base of
T.P. ₆	2.09	116.36	6.52	114.27	tree - 8" dia. East side tree is on fence about 150' N of end of ditch
T.P. ₇	4.11	118.59	1.88	114.48	return circuit
T.P. ₈	3.63	119.14	3.08	115.51	
T.P. ₉	4.32	118.05	5.41	113.73	
T.P. ₁₀	3.50	116.53	5.02	113.03	
T.P. ₁₁	4.15	116.23	4.45	112.08	
T.P. ₁₂	2.24	110.43	8.04	108.19	
T.P. ₁₃	3.16	105.68	7.97	102.52	
B.M. ₈			2.71	102.97	
Total	69.30		69.32	102.99	
	- 69.32				
check	- 0.02			- 0.02	

027

2-27-61

4

5

Eads drain Profile

Witney #4
Leak #20

4-18-61

6

Sta.	B.S.	H.I.	F.S.	elev.	dis. from Stake
0+00		102.75			
TOP OF STAKE			9.36	96.39	
BASE OF STAKE			5.17	95.58	
1st. Break			11.05	89.70	22'
E. of S.			12.75	88.00	26'
C. of S.			13.10	87.65	29'
E. of S.			12.84	87.91	32'
1st. Break			5.23	95.52	49.54'
0+00					
TOP OF STAKE			4.60	96.15	"
BASE OF STAKE			5.25	95.50	
1st. Break			14.00	86.75	19'
C. of S.			14.90	85.85	28'
E. of S.			14.7	86.05	33'
Bank			6.7	94.05	55'
T.P.	6.10	102.70	4.15	96.60	
2+00					
TOP OF STAKE			6.10	96.60	
BASE OF STAKE			6.86	95.85	
E. of S.			13.05	89.65	25'
C. of S.			13.60	89.10	27'
E. of S.			13.10	89.60	29'
Bank			6.43	96.27	42'

7

Sta.	B.S.	H.I.	F.S.	elev.	dis. from top of stk
2+200			5.54	97.16	
at stk			6.51	96.19	
M.S.			12.60	90.10	10'
C.S.			13.38	89.32	16'
E.S.			11.85	90.85	21'
Bank			6.30	96.40	34'
B.M.	2.70	102.70		100.00	
2+237					
T.M. stk			5.91	96.79	
at stk			6.77	95.93	
F.S.			11.96	90.74	21'
C.S.			13.44	89.26	25'
F.S.			13.16	89.54	29'
Bank			7.46	95.24	35'
3+00					
T.M. stk	6.51	103.41	5.80	96.90	
at stk			6.52	96.89	
E.S.			12.20	91.21	21'
C.S.			12.30	91.11	23'
F.S.			12.15	91.26	26'
Bank			5.45	97.96	46'

Bottom
PipeBottom
Pipe

8

Sta.	B.S.	H.I.	I.S.	elev.	dis. from stake
4+00			5		
T.O. STK			5.74	97.67	
B.O. STK			6.46	96.95	
E.M.S.			12.13	91.31	19'
C.M.S.			12.50	90.81	21'
E.M.S.			12.20	91.21	25'
Bank			5.06	98.35	51'
5+00					
T.O. STK			4.98	98.43	
B.O. STK			5.62	97.79	
E.M.S.			11.40	92.01	19'
C.M.S.			11.80	91.61	21'
E.M.S.			11.22	92.19	23'
Bank	5.74	103.75	5.40	98.01	67'
6+00					
T.O. STK			5.66	98.09	
B.O. STK			6.43	97.32	
E.M.S.			11.10	92.65	20'
C.M.S.			11.55	92.20	23'
E.M.S.			11.02	92.73	25'
Bank			4.80	98.90	52'

11

Sta.	B.S.	I.I.F.	F.S.	Elev.	dist. from Stake?
6+360					
T.M. 5th			5.91	97.84	
B.M. 5th			6.68	97.12	
E. of S.			10.47	93.28	16'
C.M.S.			11.00	92.75	20'
E. of S.		103.7	10.40	93.35	26'
Bank	6.50	104.94	5.31	98.44	44'

TRIBUTARY

1+00					
T.M. 7th			3.51	101.93	
B.M. 5th			4.23	100.71	
E. of S.			11.50	93.44	20'
C.M.S.			11.55	93.39	25'
E. of S.			11.20	93.74	31'
Bank			5.03	99.91	45'

1+383

T.M. 5th			4.34	100.82	
B.M. 5th			5.22	99.94	
E. of S.			11.20	93.96	17'
C.M.S.			12.20	92.96	25'
E. of S.			11.30	93.86	29'
Bank			3.35	101.81	44'
B.M. 2	7.69	105.16	7.47	97.47	
T.P. 1	4.13	105.10	4.19	100.97	

12

13

Sta.	B. S.	H. I.	F. S.	elev.	Vis. from stalet
7+00			9.8		
T.M. Sth			9.84	95.26	
B.M. Sth			10.35	94.75	
E.M.S.			11.54	93.56	11'
C.M.S.			12.30	92.80	15'
F.M.S.			11.90	93.20	17'
B.M.S.			6.71	98.39	37'
8+00					
T.M. Sth			5.52	99.58	
B.M. Sth			6.30	98.80	
F.M.S.			10.38	94.72	19'
C.M.S.			10.31	94.79	22'
E.M.S.			10.40	94.70	27'
B.M.S.			5.80	99.38	41'
9+00					
T.M. Sth			5.35	99.75	
B.M. Sth			6.16	98.94	
E.M.S.			10.22	94.88	16'
C.M.S.			10.50	94.60	19'
F.M.S.			10.05	95.05	24'
B.M.S.	4.40	104.49	5.01	100.09	41'

14

15

	Sta	D.S.	H.T.	F.S.	elev	dis. From Bench
7	10+00					
T	T. of Sta.			4.87	99.62	
B	B.M. Sta.			5.59	98.90	
E	E.M.S.			8.70	95.79	15'
C	C.M.S.			9.40	95.09	19'
F	F.M.S.			8.90	95.59	26'
B	Bench			3.66	100.83	43'
8	11+00					
T	T.M. Sta.			4.40	100.09	
B	B.M. Sta.			5.16	99.33	
E	E.M.S.			8.50	95.99	15'
C	C.M.S.			8.70	95.79	17'
F	F.M.S.			8.30	96.19	23'
B	Bench	4.76	105.27	3.98	100.51	39'
9	11+188					
T	T. of Sta.			4.66	100.61	
B	B.M. Sta.			5.37	99.90	
E	E.M.S.			8.99	96.28	14'
C	C.M.S.			9.27	96.00	24'
F	F.M.S.			8.91	96.36	29'
B	Bench			4.92	100.35	41'
	B.M. 3			2.26	103.01	

16

Bridge

Sta.	B.S.	I.I.E.	F.S.	Elev.	dis from stake
11+241					
T.M.S.T.			3.68	101.59	
BM dho			4.45	100.82	
F.M.S.			9.20	96.07	8.0'
C.I.S.			9.72	95.55	13'
F.M.S.			9.20	96.07	24'
Bank			5.35	99.92	36'
B.M. ₃	2.82	105.81		102.99	
12+00			9.72		
T.M.S.T.			9.72	101.08	
F.M.S.			5.57	100.24	
F.M.S.			9.50	96.31	12'
C.I.S.			9.70	96.11	16'
F.M.S.			9.50	96.31	21'
Bank			5.38	100.43	33'
13+00					
T.M.S.T.			5.07	100.74	
B.I.S.T.			5.73	100.08	
F.M.S.			8.80	97.01	7'
C.I.S.			9.30	96.51	12'
F.M.S.			8.80	97.01	16'
Bank	5.42	107.12	4.11	101.70	31'

Bridge

19

	BS.	HI.	F.S.	elev.	1/5, iron stake
14+00					
TM stake			4.25	102.87	
BM stake			4.90	102.22	
FS			4.43	97.69	18'
CS			10.03	97.09	12'
FS			9.62	97.50	16'
Bank			4.61	102.51	32'

15+00					
TM stake			3.53	103.59	
BM stake			4.18	102.94	
FS			9.20	97.92	9'
CS			4.40	97.72	11'
FS			9.20	97.92	14'
Bank	4.57	108.29	3.40	103.72	31'
T.P.	7.04	110.44	4.89	103.40	

16+00					
TM stake			6.27	104.17	
BM stake			6.95	103.49	
FS			11.50	98.94	16'
CS			11.90	98.54	19'
FS			11.60	98.84	22'
Bank			5.37	105.07	29'

20

21

Sta.	B.S.	H.T.	F.S.	elev.	dist. in stake
17+00					
T of stake			5.18	105.26	
B of stake			5.88	104.56	
E.M.S.			10.73	99.71	12'
C.M.S.			10.94	99.50	15'
E.M.S.			10.60	99.84	20'
Bank			6.20	104.24	30'
T.P.	6.10	108.88	7.66	102.78	
18+00					
T of stake			2.90	105.98	
B of stake			3.40	105.48	
E.M.S.			8.02	100.86	13'
C.M.S.			8.51	100.37	16'
E.M.S.			8.05	100.83	21'
Bank			3.39	105.49	29'
18+165			<u>3.33</u>		
T of stake	3.77	109.35	3.33	105.55	
B of stake			4.50	104.85	
E.M.S.			8.20	101.15	17'
C.M.S.			8.90	100.45	22'
E.M.S.			8.15	101.20	26'
Bank			4.50	104.85	36'
E Flawline			8.45	100.90	
W Flawline			8.50	100.85	

Bridge

22

23

Sta	B.S.	HI	F.S.	elev.	dis
184247					
T.M. stk.			2.50	106.85	
B.M. stk.			3.18	106.17	
F.S.			7.98	101.37	14'
C.M.S.			8.79	100.56	20'
F.S.			8.21	101.14	28'
Bank.			4.56	104.79	41'
B.M.			3.72	105.63	
19400					
T.M. stk.			1.48	107.87	
B.M. stk.			2.18	107.17	
F.S.			7.75	101.60	17'
C.M.S.			8.07	101.28	20'
F.S.			7.73	101.62	23'
Bank.			3.96	105.39	34'
T.P.	6.80	113.99	2.16	107.19	
20400					
T.M. stk.			5.34	108.60	
B.M. stk.			6.01	107.98	
F.S.			11.40	102.59	20'
C.M.S.			12.20	101.79	23'
F.S.			11.50	102.49	26'
Bank.			7.30	106.69	41'

24

Sta.	B.S.	I.T.	F.S.	elev.	dis. from stake
21+00					
T.M. stk.			9.53	109.46	
B.M. stk.			5.22	108.77	
E.M.S.			10.70	103.29	18'
C.M.S.			11.30	102.69	22'
E.M.S.			10.90	103.09	26'
Bank.	7.38	115.75	5.62	108.37	39'
22+00					
T.M. stk.			3.88	111.87	
B.M. stk.			4.96	111.29	
E.M.S.			11.70	104.05	20'
C.M.S.			12.0	103.75	24'
E.M.S.			11.60	104.15	27'
Bank.			6.64	109.11	41'
23+00					
T.M. stk.			4.00	111.75	
B.M. stk.			4.65	111.10	
E.M.S.			11.00	104.75	16'
C.M.S.			11.26	104.49	20'
E.M.S.			10.70	105.05	23'
Bank.			6.01	109.74	37'
T.P.	3.69	115.45	3.99		

27

Sta.	B.S. Hit	F.S. elev	dist. from setback
29400			
T.M. stk		2.12 113.33	
B.M. stk		2.70 112.75	
F.M.S.		9.20 106.25	20'
C.M.S.		9.70 105.75	25'
F.M.S.		9.20 106.25	27'
Bank		4.81 110.64	39'
25700			
T.M. stk	1.81 114.21	3.05	
B.M. stk		2.44 111.77	
F.M.S.		7.5 106.71	15'
C.M.S.		7.8 106.41	19'
F.M.S.		7.5 106.71	23'
Bank		3.6 110.61	35'
257135			
T.M. stk	8.24 119.59	2.86 111.35	
B.M. stk		9.75 110.84	
F.M.S.		12.32 107.27	15'
C.M.S.		12.52 107.07	22'
F.M.S.		12.52 107.07	25'
Bank		9.28 110.31	33'
Flowline		12.26 107.33	
Flowline		12.16 107.43	
B.M. 4		7.96 111.63	

28

Culvert S. side
RR
N. side
RR P.P.

29

Fads Drain

Sta.	B.S.	H.I.	F.S.	elev	dis. from stake
B.M.	8.08	119.70		111.62	
25+216	8.00				

V.P.

26+00

T. of stk.			6.54	113.16	
B. of stk.			7.17	112.53	
E. of S.			12.79	106.91	8'
C. of S.			13.4	106.30	16'
E. of S.			12.2	107.50	20'
BANK			7.4	112.30	30'
V.P.	7.18	120.34	6.54	113.16	

27+00

T. of stk.			7.71	112.63	
B. of stk.			8.38	111.96	
E. of S.			12.89	107.45	9'
C. of S.			13.60	106.74	14'
E. of S.			13.0	107.34	18'
BANK			9.07	111.27	27'

Wiltonger #4
Leak #

4-11-61

30

Sta.	B.S.	I.F.	F.S.	elev.	dis. from stake
T.P.	9.65	120.92	9.07		
27+314					
V. of stk.			7.68	113.24	
B. of stk.			8.45	112.47	
E. of s.			13.40	107.52	13'
C. of s.			13.80	107.12	15'
E. of s.			13.40	107.52	19'
Bank.	4.32	117.03	8.21	112.71	32'
28+00					
V. of stk.			3.77	113.26	
B. of stk.			4.47	112.56	
E. of s.			9.41	107.62	11'
C. of s.			10.0	107.03	14'
E. of s.			9.45	107.58	18'
Bank			4.9	112.13	30'
T.P.	6.00	117.26	5.77	111.26	
29+00					
V. of stk.			3.27	113.99	
B. of stk.			4.12	113.14	
E. of s.			9.65	107.61	14'
C. of s.			10.08	107.18	16'
E. of s.			9.60	107.66	19'
Bank.			4.34	112.92	30'
T.P.	5.16	117.79	4.63	112.63	

intersection
of stream makes Right of

Sta.	B.S.	H.I.	F.S.	elev.	dis. from stake
30+00					
T. Stake			2.54	115.25	
B. Stake			3.24	114.55	
E.S.			9.20	108.59	13'
C.S.			9.68	108.15	17'
E.S.			9.20	108.59	22'
Bank			4.50	113.29	31'
T.P.	4.48	117.27	5.00	112.79	

30+31.6

T. Stake			8.20	113.07	
B. Stake			4.98	112.29	
E.S.			6.65	110.62	23'
C.S.			6.80	110.47	24'
E.S.			6.65	110.62	25'
Bank			5.00	112.27	33'
B.M.			4.06	113.21	

35

Arno Bridge Profile

Sta.	B.S.	H.I.	F.S.	elev.	Dist. from Stake
B.M.	10.65				Tree-spike black top
				4.53	
47+00				4.79	
47+50				4.83	
48+00				5.03	
48+60				5.89	
W. end bridge				4.76	
E. end bridge				4.87	
B.M. on footing				12.68	
51+00				4.82	
T.P.,	8.97			4.82	
52+00				8.54	
52+50				8.23	
53+00				7.67	
53+50				6.84	
54+00				5.64	
54+50				5.10	
55+00				4.15	
55+75				2.87	
56+00				2.45	
56+50				1.69	
57+00				0.91	
T.P.,	5.30			0.91	
				2.32	black top
T.P.,	4.32			12.20	
B.M.				11.30	

36

C.C.P. & St. L. RR

	B.S.	H.I.	F.S.	elev.
B.M.	2.76	102.76		100.00
0+00				
T. of stk.			2.29	100.47
B. of stk.			2.89	99.87
Ditch			5.18	97.58
1+00				
T. of stk.			4.35	98.41
B. of stk.			5.18	99.87
Ditch			6.81	95.95
2+00				
T. of stk.			4.42	98.34
B. of stk.			4.42	98.34
Ditch			4.42	98.34
3+00				
T. of stk.			4.63	98.13
B. of stk.			5.43	97.33
Ditch			6.31	96.45
4+00				
T. of stk.			4.83	97.93
B. of stk.			5.27	97.49
Ditch			6.20	96.56
5+00				
T. of stk.	5.23	102.18	5.81	96.95
B. of stk.			6.49	95.69
Ditch			7.64	94.54

1263' to County Road

1317' to R/W #74

B.S. H.I. F.S elev.

6+00				
TMStk		6.04	96.14	
BMStk		6.54	95.64	
Ditch		7.80	94.38	
7+00				
TMStk		5.93	96.25	
BMStk		6.34	95.84	
Ditch		7.67	94.51	
8+00				
TMStk		5.16	97.02	
BMStk		5.74	96.44	
Ditch		7.14	95.04	
9+00				
TMStk		3.83	98.35	
BMStk		4.59	97.59	
Ditch		5.90	96.28	
10+00				
TMStk		2.79	99.39	
BMStk		3.37	98.81	
Ditch		4.21	97.97	
11+00				
TMStk	2.27	102.67	1.78	10040
BMStk				
Ditch				

B.S. H.F. F.S. CkV.

12700

T.M.S.K.

4.10 98.57

B.M.S.K.

4.66 98.01

Ditch

5.26 97.41

13700

T.M.S.K.

4.82 97.85

B.M.S.K.

5.44 97.23

Ditch

6.15 96.52

C. Road.

4.88 97.79

14700

T.M.S.K.

4.33 98.34

B.M.S.K.

4.96 97.71

Ditch

6.57 96.10

R.W.

T.M.S.K.

4.25 98.42

B.M.S.K.

4.80 97.87

Ditch

7.24 95.43

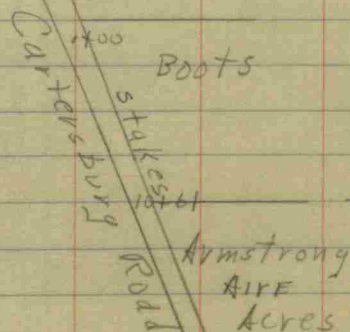
45 Route to Armstrong

Sta.	B.S.	H.I.	F.S.	elev	
B.M.	3.65	103.65		100.00	nail
0+00					
T.MstK.			4.15	99.5	
Ditch			6.52	97.13	
2+00					
T.MstK.			4.60	99.05	
Ditch			6.56	97.09	
4+00					
T.MstK.			3.70	99.95	
Ditch			5.80	97.85	
6+00					
T.MstK.	3.37		4.02	99.63	
Ditch			6.02	97.63	use B.M. H.I.
8+00					
T.MstK.			4.04	98.96	
Ditch			5.84	97.16	
10+00					
T.MstK.			5.03	97.97	
Ditch			6.09	96.91	
10+61					
T.MstK.			4.57	98.03	
Ditch			7.82	95.18	

5-26-61
sunny-cold
45°

46

DANVILLE



47

Reset stakes on
Boots to Armstrong

Sta.	B.S.	H.I.	F.S.	elev.
B.M.	3.85	103.85		100.00
0+00			4.80	99.05
2+00			4.62	99.23
4+00			3.54	100.31
6+00	2.90	103.17	3.58	100.27
8+00			3.55	99.62
10+00			4.92	98.25
10+61			5.10	98.07

48

49

	BS	T	FS	Elev.	N Headon culvert 39 X G Rd
BM	4.95			200.00	
SE 141		204.95	5.09	199.86	
SW " 1			5.84	199.11	
NW " 1			5.72	199.23	
NE " 1			4.81	200.14	
NE " 2			4.28	200.67	
NW " 2			6.78	198.17	
NW " 3			7.83	197.12	
NE " 3			6.45	198.50	
B.M.	2.16	202.16		200.0	
Cen S 7			1.61	200.55	
" N #1			1.14	201.02	
" N #2			2.85	199.31	
" N #3			3.76	198.40	
NE 4			5.71	196.45	
Cen 4			6.23	195.93	
NW 4			6.79	195.37	
NW 5			6.7	195.46	
Cen 5			7.62	194.54	
NE 5			7.24	194.92	
NE 6			7.20	194.96	
Cen 6			5.56	196.60	
NW 6			4.54	197.62	

R. Hendricks

6-2-61

Wind 50
80° 15 mph

	BS	T	Cloudy	FS	Elev.
SE #7				5.36	196.80
Cen S 7				5.05	197.11
SW 7				4.73	197.43
NW 7				3.56	198.60
Cen N 7				4.13	198.03
NE 7				5.09	197.07
SE 8				4.19	197.97
Cen S 8				3.42	198.74
SW 8				3.1	199.06
NW 8				1.78	200.38
Cen N 8				1.76	200.04
NE 8				1.54	200.62
TP	6.05	207.47		0.74	201.42
NE 9				5.62	201.85
Cen N 9				5.5	201.97
NW 9				6.82	200.65
NW 10				6.94	200.53
Cen 10				5.29	202.18
NE 10				5.14	202.33
NE 11				4.06	203.41
Cen 11				5.47	202.00
NW 11				6.09	201.38
NW 12				4.41	203.06
Cen 12				5.22	202.25
NE 12				5.56	201.91

51

BM	B.S.	T	F.S.	Elev.
	5.11 ^{100.00}	105.11		100.00
Bottom of Culvert (3+60) ↘		Top Culvert	-2.00	98.00
0+00			10.96	94.15
T 1+00		5 FT. out	3.80	101.51
B 1+00			3.85	102.10
T 2+00			2.48	102.63
B 2+00		5 FT.	2.99	102.12
T 3+00			5.16	100.89
B 3+00			3.45	101.66
T 4+00			4.00	101.11
B 4+00			4.05	99.90
T 4+00			4.26	100.85
B 4+00		Bottom Ditch	7.36	98.64
T 4+00			4.80	100.31
B 4+00			6.80	99.20
T 4+70			4.41	100.70
B 4+70			7.40	98.60
TP	5.78		7.00	99.00
T 1+00			5.30	99.81
B 1+00			5.75	99.36
TP	5.08	105.61	6.17	99.83
T 1+00			5.30	99.81
B 1+00			5.51	100.10
T 2+00			3.92	100.97
B 2+00			6.44	99.17
T 2+00			4.57	100.32
B 2+00			5.44	100.17
T 3+00			4.02	100.87
B 3+00			6.35	99.26
T 3+54			4.55	100.34
B 3+54			5.11	100.44
T 3+54			3.46	101.43
B 3+54			5.91	99.70
TP	5.34		4.16	100.73
T 3+54			5.22	100.39
B 3+54			3.79	101.10
TP	5.28		5.62	99.99
100 ft. 3+60			4.12	100.77
			4.05	100.96
	106.50		3.79	101.10
	106.38		5.23	101.15

Wincker Heights 6-5-6!

52

Fair B.S.	T	F.S.	Temp. 85°
	6+00	101.01	
	6+00	102.18	
	6+00	101.69	
	5+00	100.82	
	5+00	102.78	
	5+00	100.03	
	5+00	102.09	
	4+00	100.94	
	4+00	102.38	
	4+00	100.35	
	4+00	101.76	
	4+00	101.06	
	4+00	102.19	
	4+00	100.35	
	4+00	101.61	
	3+00	101.16	
	3+00	102.23	
	3+00	100.58	
	3+00	101.49	
	3+00	101.70	
	3+00	102.81	
	3+00	100.35	
	3+00	102.15	
	2+00	102.35	
	2+00	103.65	
	2+00	100.79	
	2+00	103.04	
	2+00	101.37	
	2+00	102.50	
	2+00	100.96	
	2+00	101.91	
	1+00	101.54	
	1+00	102.44	
	1+00	100.89	
	1+00	101.87	
	1+00	102.11	
	1+00	103.37	
	1+00	100.95	
	1+00	102.75	
	0+00	101.64	
	0+00	102.16	
	0+00	101.45	
	0+00	101.58	
	0+00	102.19	
	0+00	102.16	
TP ₃	6.52		
		108.68	

	B.S.	I	F.S	Elev.
TP ₃	6.52	108.61	4.22	104.46
T 5+00	S		1.39	107.29
B 5+00			2.10	106.58
T 5+00	N		0.85	107.83
B 5+00			1.62	107.06
T 4+02	S	S 5.12	4.40	104.28
B 4+02			B 6.60	101.77
T 4+00	N	S 5.03	3.80	103.56
B 4+00			B 5.90	102.71
T 3+00	S	S 7.41	6.31	101.20
B 3+00			B 7.87	100.74
T 3+00	N	S 7.12	6.10	101.49
B 3+00			B 7.41	102.58
T 2+00	N	S 6.85	5.93	101.86
B 2+00			B 8.04	101.76
T 2+00	S	S 7.75	6.70	102.75
B 2+00			B 8.15	100.57
T 1+00	S	S 7.70	6.62	101.98
B 1+00			B 8.15	100.88
T 1+00	S	S 8.26	7.26	100.48
B 1+00			B 8.26	101.42
TP ₄	5.41	106.99	7.10	101.58
T 1+00	N	S 7.30	7.10	101.58
B 1+00			B 8.31	101.23
T 0+00	N	S 7.70	4.84	102.15
B 0+00			B 8.45	100.48
T 0+00	S	S 7.40	5.56	101.43
B 0+00			B 8.20	100.91
T 0+00	S	S 7.40	5.96	101.03
B 0+00			B 8.45	101.63
T 0+00	S	S 7.40	6.66	100.33
B 0+00			B 8.20	100.33
T 0+00	S	S 7.40	5.72	101.27
B 0+00			B 8.20	100.86

B.M
7.00
Elev. 99.99

55

	B.S.	π	F.S.	Elev.	
B.M.,	3.46	203.46		200.00	Spike in pole SE Cor. 10th St.
			6.22	197.24	S. end of Culvert
Top of Stake 31+50			6.18	197.28	N. end of Culvert
Ditch			4.38	199.08	
33+00			5.66	197.80	
Dit			4.15	199.31	
35+00			6.38	197.08	
Dit			3.98	199.48	
TP ₁			7.28	196.18	
			5.66	197.80	
	3.57	201.31			
36+00			3.18	198.13	
Dit			6.00	195.31	
38+00			4.84	196.47	
Dit			7.67	193.64	
B.M.,	3.38	203.38		200.00	
			6.57	196.31	Culvert 1st House
Top of Stake 31+00			6.03	197.35	Bottom of Culvert
30+00			4.25	199.13	
Dit			3.78	199.60	
			5.63	197.75	
			7.95	195.43	Bottom of Catch Basin NW Corner 10th St.

Griswald Road 10-13-61
Rod: Ted Cloudy Temp. 76

56

	B.S.	π	F.S.	Elev.	
			2.77	200.61	28+80
			5.09	198.29	Dit.
			2.46	200.92	28+00
			5.36	198.02	Dit.
			2.40	200.98	26+00
			4.90	198.48	Dit.
			3.38	200.00	TP ₂
	5.01	205.01			
			4.90	200.11	24+00
			6.51	198.50	Dit
			4.70	200.31	22+00
			5.62	199.39	Dit
			4.69	200.32	TP ₃
	5.62	205.94			
			4.34	201.60	20+00
			5.56	200.38	Dit.
			3.87	202.07	18+00
			5.27	200.67	Dit.
			4.56	201.38	16+00
			5.73	200.21	Dit.
			3.81	202.13	14+00
			4.10	201.84	TP ₄
	4.77	206.61			
			5.80	200.81	Dit.

57

	B.S.	π	F.S.	Elev.
12+00			4.26	202.35
Dit.			6.20	200.41
10+00			4.45	202.16
Dit.			5.65	200.96
8+00			3.41	203.20
Dit.			4.99	201.62
6+00			3.25	203.36
Dit.			4.68	201.93
TP ₅			3.69	202.92

5.53 208.45

4+00			4.29	204.16
Dit			5.17	203.28
2+00			4.20	204.25
Dit.		-	5.67	202.78
0+00			3.05	205.40
Dit.			4.56	203.89

58

59 Tharp Drain

Sta + A - elev
RM #3 97.44

TP 15.34 112.78

TP 11.31 101.47

6.18 107.65

8+63

TP 5.23 102.42

4.76 107.18

12+63

TP 6.19 100.99

6.60 107.59

16+63

TP 5.59 102.70

3.82 105.82

20+63

TP 4.19 101.63

4.76 106.39

K D. Wright
P Leak & Taylor

3-16-62

060

Cloudy 32°

R L

0 23 40 92 47 58 71

6.80 7.81 13.31 14.10 13.81 6.99 3.57

100.75 99.84 94.34 93.65 14.45 93.81 100.66 103.78

93.20

0 9 21 27 31 43 50

4.87 5.33 11.69 12.39 11.90 6.57 5.92

102.31 101.85 95.49 94.79 95.28 100.64 101.26

0 15 28 35 39 41 53 61

4.83 5.53 11.92 12.84 11.82 10.35 6.22 6.11

102.76 102.06 95.67 94.70 95.77 97.24 101.37 101.18

0 11 23 24 33 35 42 53

4.71 5.24 9.99 10.80 9.99 8.83 7.06 3.98

101.11 100.56 95.83 94.92 95.83 96.99 98.76 101.84

29+63

TP

3.14

106.61

2.92

103.47

28+63

TP

5.4

6.53

107.23

5.91

100.70

32+63

33+42

B.M.#7

Center Headwall directly above
flowline of outlet tile.

J.R.L.

7.49 99.74

0	4	22	29	32	34	44	52
4.71	5.19	9.71	11.15	10.55	9.32	4.84	7.07
101.68	101.20	6	95.29	95.51	97.07	101.55	102.32

0	5	17	23	27	37	44
4.53	5.30	10.30	11.10	10.05	5.20	4.57
101.78	101.31	96.31	95.51	96.56	101.41	102.01

0	6	20	25	29	39	42
4.52	5.25	10.65	10.95	10.48	4.91	4.72
102.71	101.95	96.58	96.25	96.75	102.32	102.51

11.23

96.00

0667

Eads Ditch

6-9-62

STA	+	π	-	ELEV
Bm ¹	3.43			100.00
		103.43		
TP ¹			6.92	96.61
	4.04	100.65		
TP ²			4.90	95.75
	4.95	100.70		
TP ³			7.71	92.99
	5.96	98.95		
0+00			2.74	96.21
1+00			4.79	94.16
2+00			4.52	94.43
3+00			3.59	95.36
TP			4.54	94.41
	6.21	100.62		
4+00			4.35	96.27
5+00			3.70	96.92
6+00			4.58	96.04
TP			5.65	94.97
	4.49	99.86		
7+00			3.00	96.86
8+00			3.44	96.42
TP			2.25	97.61
	3.14	100.75		

L. Taylor

CLEAR + WARM

0668

P. Larry + Steve H.

STA	+	π	-	ELEV
12+00			3.94	96.81
TP			4.60	96.15
	4.95	101.10		
16+00			3.59	97.51
TP			4.77	96.33
	5.65	101.96		
TP			4.57	97.37
	4.52	101.91		
20+00			3.97	98.04
22+00			4.74	97.13
TP			4.93	96.98
	4.90	101.88		
24+00			4.26	97.62
TP			4.15	97.73
	6.47	104.20		
27+60			3.79	100.41
TP			6.25	97.95
	5.15	103.10		
31+60			4.01	99.09
TP			4.63	98.47
	5.15	103.62		
35+60			4.24	99.38
TP			5.69	97.93
	5.55	103.48		
39+60			4.24	99.24

69

STA	+	π	-	FLEV
TP			5.11	98.37
	5.93	104.30		
42+60			4.80	99.50
Bm ²			1.90	102.40

070

71

STA	EADS	DRAIN	G-5-62 Three Osters LARRY	F.S.	ELEV.
B.M'	3.44	103.44			100.00
TP			6.03		97.41
	3.50	100.91			
TP			6.99		93.97
	6.55	100.52			
0+00			3.75		
1+00			5.76		
2+00			5.49		
3+00			4.55		
TP			4.55		96.97
	5.42	102.39			
4+00			4.54		
5+00			3.83		
6+00			4.72		
7+00			3.95		
TP			3.95		99.44
	3.74	102.18			
8+00			4.20		
B.M'		100.98	1.20		
TP			2.73		

Cloudy & cool

72

73

STA	B.S.	I.Z.	F.S.	ELEV.	REMARKS
B.M.	1.17	101.17		100.00	
TP			3.75	97.42	
	3.65	101.07			
TP ²			6.04		
	4.10	99.13			
0+00			2.35	96.78	
1+00			4.27	94.76	
2+00			4.09	95.04	
3+00			3.15	95.98	
TP			3.15	95.98	
	5.53	101.51			
4+00			4.67	96.84	
5+00			3.97	97.54	
6+00			4.87	96.64	
7+00			4.10	97.41	
TP			4.10	97.41	
	3.91	101.32			
8+00			4.38	96.99	
B.M.		99.96	1.36	99.96	100.00
TP			4.06	95.94	
	4.18	100.16			
12+00			4.16	96.00	
16+00			3.47	96.69	
TP			3.47	96.69	
	5.14	101.95			

BM

4.81 CUT

74

STA	B.S.	I.Z.	F.S.	ELEV.	REMARKS
20+00			4.67	97.18	
TP			4.67	97.18	
	4.00	101.18			
22+00			4.85	96.33	
24+00			4.35	96.83	
TP			4.35	96.83	
	5.14	101.97			
27+00			2.38	99.59	
Temp 20+00 B.M.			99.95	1.94	17" above and corner post 20+00
TP			1.94	100.03	
	2.44	102.51			
31+60			4.23	98.45	
35+60			3.92	98.59	
TP			3.92	98.59	
	3.96	102.55			
39+60			4.06	98.49	
43+60			3.95	98.70	
TP			3.95	98.70	
	4.65	103.35			
B.M. ²			1.71	101.64	

75

Eads Drain the steady!

STA	B.S.	+	F.S.	ELEV.
B.M. ²	3.32			
TP ¹			4.95	
	8.47			
TP ²			4.27	
	6.45			
TP ³			4.28	
	1.23			
TP ⁴			5.73	
	3.40			
TP ⁵			7.80	
	4.72			
B.M. ¹			3.62	
TP ¹			4.72	
	7.74			
TP ²			3.50	
	5.94			
TP ³			1.21	
	4.10			
TP ⁴			6.55	
	4.64			
TP ⁵			8.41	
	4.75			
B.M. ²			3.45	

76

77

THAIR DEBIN

6-11-62 Lee

cloudy & warm LARRY
STEV

STA.	B.S.	H.I.	F.S.	ELEV.
B.M. ²	9.65	107.09		97.44

4+00			5.32	101.77
7+82			6.59	100.50
B.M. ³			9.65	97.44

78

179

EADS ZINCH
6-20-62TAGE
OSTOVE
1 LARRYCLEAN
COOL

STA	B.S.	H.I.	F.S.	ELEV.
B.M. 3	2.23			102.99
		105.22		
46+41			3.75	101.47
48+00			4.19	101.03
TP			4.06	101.16
	3.73	104.89		
52+00		-	4.12	100.77
56+00			2.15	102.74
TP			2.15	102.74
	5.98	108.72		
60+00			5.19	103.53
TP			6.35	102.37
	6.72	109.09		
64+00			5.02	104.07
68+00			3.87	105.22
TP			3.87	105.22
	5.05	110.27		
72+00			4.37	105.90

e80

BM 4	4.92	105.45
BM 4	4.72	105.55

81

Eads Ditch 6-28-62

STA	B.S.	H.I.	F.S.	Elev.
B.M. 3	13.92	111.36		97.44
TP			6.25	105.11
	3.60	108.71		
8+63			7.08	101.63
12+63			5.47	103.24
TP			5.47	103.24
	4.23	107.47		
16+63			4.05	103.42
20+63			5.85	101.62
TP			5.85	101.62
	5.25	106.87		
24+63			4.43	102.44
28+63			4.34	102.53
TP			4.34	102.53
	9.96	107.49		
32+63			3.76	103.73
33+43			5.03	102.46
B.M. 7			7.63	
				99.86

82

83

F.S Elev
102.99

101.47
94.43
7.04

102.99
1.95
104.94
3.91
101.47

3.47

9.17 104.94
9.17
95.77

0 4
94 3
10.5

TOP
OF
STAKE

84

99.09

4.65 = 99.09

94.24

4.95

103.74

103.79

8.95

94.24

599.50

9.50

94.18

103.74

103.79

8.95

3.27

96.59

100.47

94.43

102.99

6.0494.43

8.56

102.99

96.59

104.94

104.47

6.40

3.47

104.94

94.43

10.5

85

CLEAR
&
COOL

EADS Ditch 7-9-62

Loc 7

LARRY I
STEVE O

STA.	B.S.	H.I.	F.S.	ELEV.
B.M. 4	4.92	110.45		105.63
74+47			3.60	106.95
76+00			2.33	109.12
80+00			1.92	109.53
TP			1.92	108.53
	5.18	113.71		
84+00			4.28	109.13
88+00			1.87	111.04
92+00			2.00	111.71
TP			5.20	108.51
	3.95	112.46		
B.M. 1			6.86	105.60

86

87

EADS Ditch 7-20-62

STA.	B.S.	H.I.	F.S.	ELEV.	Lee Steve Harry
B.M. 4	6.94			105.63	
TP ¹		112.57	4.03	108.54	
	5.03	113.57			
TP ²			1.65	111.92	
	4.12	116.04			
94+00			3.84	112.20	
96+00			2.65	113.39	
TP ³			2.65	113.39	
	3.14	116.55			
100+00			3.89	112.66	
101+35			4.92	111.63	
B.M.			4.96	111.69	

88

105.63

93 Ditch

6-13-62

Clear

+

WARM

STA	B.S.	H.T.	F.S.	ELEV.	REMARKS
R.M.	3.60			100.00	
		103.60			
0+00					
2+00					
4+00					
TP			3.86	99.74	
	7.09	106.83			
6+00					
8+00					
TP			4.72	102.11	
	2.27	104.38			
10+00					
TP			8.12	96.26	
	2.14	98.40			
12+00					
TP			6.16	92.24	
	0.33	92.57			
14+00					
16+00					

94

TP OF BTK.	Bottom of Ditch
4.13	5.50
4.32	5.76
3.86	5.12
4.76	6.10
4.72	6.15
5.13	6.22
5.24	6.43
2.56	3.96
4.24	5.96

N. side Road

18" Above Ground on Telephone APPROX. STA 0+00

95

	B.S.	H.I.	F.S.	Elev.
S STA				
164.97				
TP			3.00	89.57
	7.49	97.06		
TP			0.96	96.10
	8.95	104.55		
TP			3.33	101.22
	2.50	103.72		
A B.M.			3.78	

96

TOP OF S.I.K.

Bottom ditch

2.84

5.45

97

CLEAR
WARM

JULY 25, 1962

ENOS ditch

Lee X
KENNY ϕ

STA.	B.S.	H.I.	F.S.	ELEV.
B.M. ⁵	4.02	115.64		111.62
102+16			4.95	110.69
104+00			2.52	113.12
108+00			3.38	112.26
TP			3.38	112.24
	4.80	117.06		
112+00			4.19	112.87
116+00			2.65	114.41
TP			2.65	114.41
	2.70	117.11		
120+00				
123+16			5.06	112.03
B.M. ^v			3.81	113.30

98

099

BATZ Ditch

9-20-62

CLEAR + Cool

BOS L. 6
LCC T. 7

100

STA	B.S.	H.I.	F.S.	Elev.	REMARKS	STA	B.S.	H.I.	F.S.	Elev.	REMARKS
B.M. 1	3.61			200.00	STAKES	36+00			6.01	205.51	STAKES
		203.61			Set						STAKES
TP 1			5.38	198.23	ON	TP 7			6.01	205.51	ON
	4.72	202.95			Right		6.92	212.93			Right
TP 2			4.64	198.31	Side	40+00			6.31	206.12	Side
	6.59	204.90			OF						OF
12+00			3.13	201.77	Ditch	TP 8			6.25	206.18	Ditch
							7.55	213.73			
TP 3			5.62	199.28		44+00			5.49	208.24	
	7.70	206.98			No						
16+00			6.14	200.89	STAKES	B.M. 2			4.41	209.32	
20+00			5.16	201.82	AT						
					0+00						
TP 4			5.16	201.82	4+00						
	7.20	209.82			8+00						
24+00			2.23	206.79							
TP 5			2.23	206.79							
	3.79	210.58									
28+00			6.89	203.69							
TP 6			3.06	207.53							
	4.00	211.52									
32+00			6.35	205.17							

101

OCT. 16, 62 BATZ

DHCh

Lee T

Bob O

George I

941

102

STA	B.S.	H.I.	F.S.	Elev.
B.M. 3	3.61	219.67		216.06
100+00			3.28	216.39
B.M. 3	3.63	219.69		
96+00			3.65	216.04
92+00			3.51	216.18
88+00			5.29	214.40
TP 1			5.29	214.40
4	5.10	219.50		
84+00			4.80	214.70
80+00			4.90	214.60
76+00			4.68	214.82
TP 2			4.68	214.82
8	3.34	218.16		
72+00			5.02	213.14
TP 3			5.02	213.14
	1.83	214.97		
68+00			3.40	211.57
TP 4			3.40	211.57
	5.62	217.19		
64+00			6.83	210.36
60+00			7.45	209.74

cloudy warm + windy Temp 68° Wind 20 MPH

103

BATZ Ditch 12-3-62

STA.	B.S.	H.I.	F.S.	Elev.
B.M. 4	2.92	222.47		219.55
T.P.			5.09	217.38
	5.00	222.38		
140+00			4.30	218.08
144+00			3.40	218.99
T.P.			3.40	218.98
	6.35	225.33		
149+00			5.24	220.09
152+00			4.10	221.23
154+00			4.70	220.63
T.P.			4.70	220.63
	6.50	227.13		
156+00			6.52	220.61
160+00			5.95	221.18
164+00			5.90	221.23
168+00			5.40	221.73
T.P.			5.40	221.73
	5.56	227.29		
172+00			6.35	220.94
176+00			3.85	223.44
180+00			4.00	223.29
184+00			3.30	223.99
T.P.			3.30	223.99
	3.45	227.44		
188+00			3.72	223.72
B.M.			2.81	224.63

104

1051

Batz Ditch 1-8-63

STA.	B.S.	H.I.	F.S.	ELEV.
B.M. ⁶	3.55	228.17		
186+00			3.71	224.46
T.P.			3.64	
	5.10			
184+00			5.31	224.82
188+00			5.86	223.83
192+00			4.65	224.98
TP			4.65	224.98
	3.14	224.12		
196+00			2.88	225.24
200+00			2.39	225.73
204+00			3.40	224.72
T.P.			3.40	

1061

109

Batz

Ditch 3-15-63

110

STA.	FAIR + mild	H.I.	F.S.	Boo ALCV.	Remain
B.m. 8	3.86			224.65	
		228.51			
T.P. 1			5.72	222.79	
	4.67	227.46			
230+00			3.85	223.61	
T.P.			3.85	223.61	
	3.50	227.11			
234+00			2.66	224.45	
238+00			2.40	224.71	
T.P.			2.40	224.71	
	5.70	230.41			
242+00			3.73	226.68	
246+00			5.18	225.23	
250+00			4.65	225.76	
T.P.			4.65	225.76	

139

1120

Grat
5+k

140

157

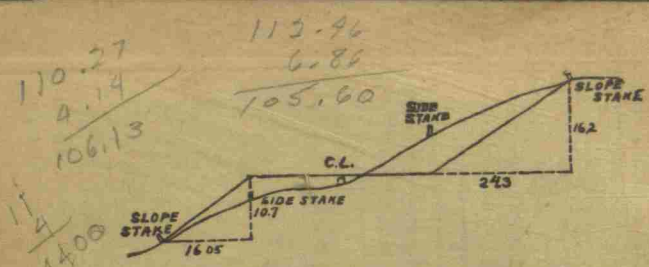
B.M.	P.S.	HI.	F.S.	Elev
	2.40	933.41	2.50	936.81
1	—		2.60	
T.P.	8.00			
BM	9.00		4.50	
BM	3.60			
2			6.80	
2	2.10			
B.M.			2.25	

158

Ground to right 4.95
Fence Post

Roof Curve

Hand of E Cone Roofing near Street



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

23
3.2
3.76
4.72
8.12
6.16
3.00
0.96
3.23

23
7.99
1.48
2.50
3.60
7.09
2.27
2.14
1.83

3.60
7.09
5.27
2.14
1.33

30.15
33.87

