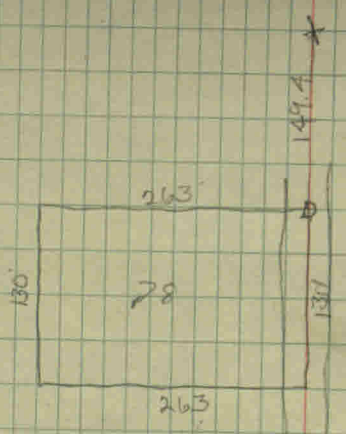
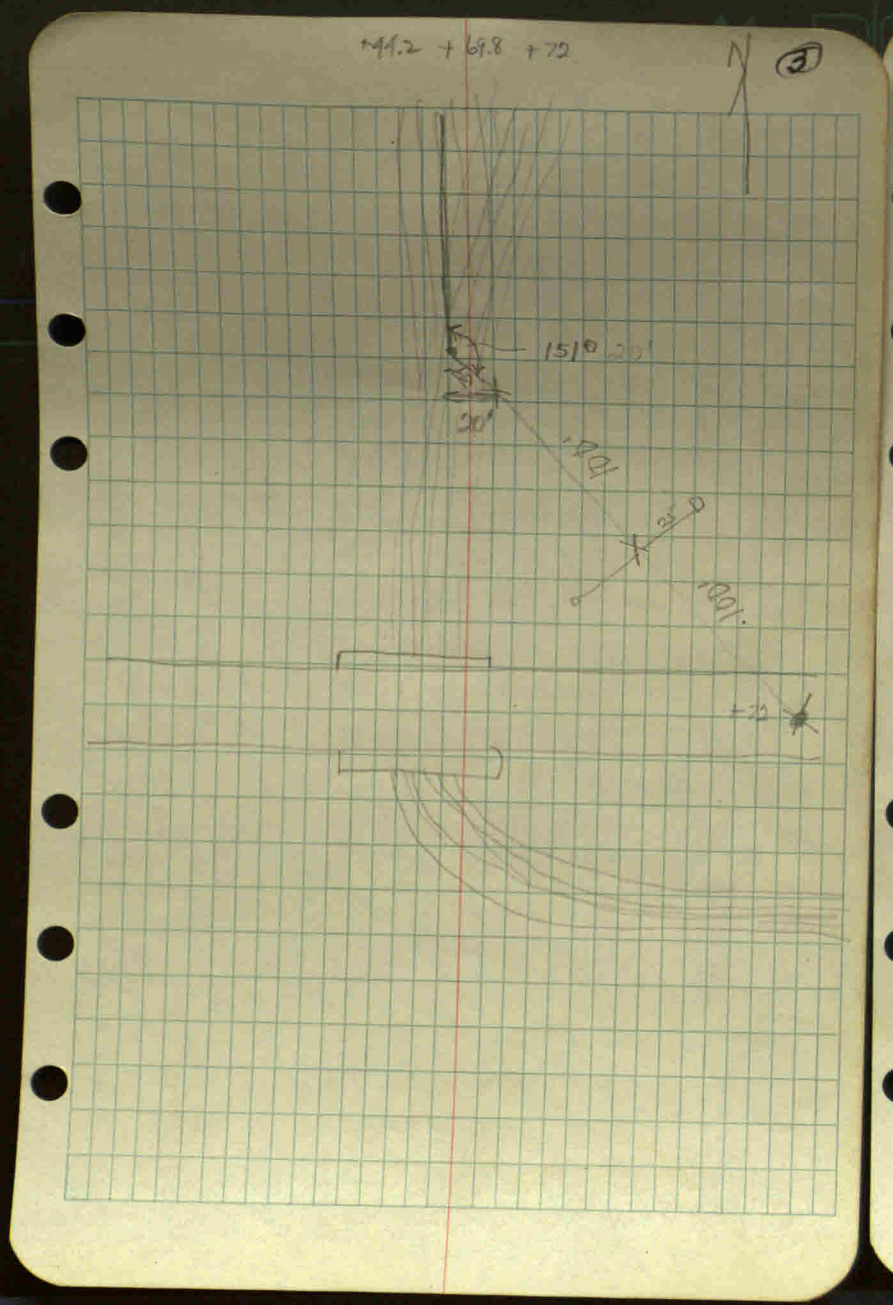
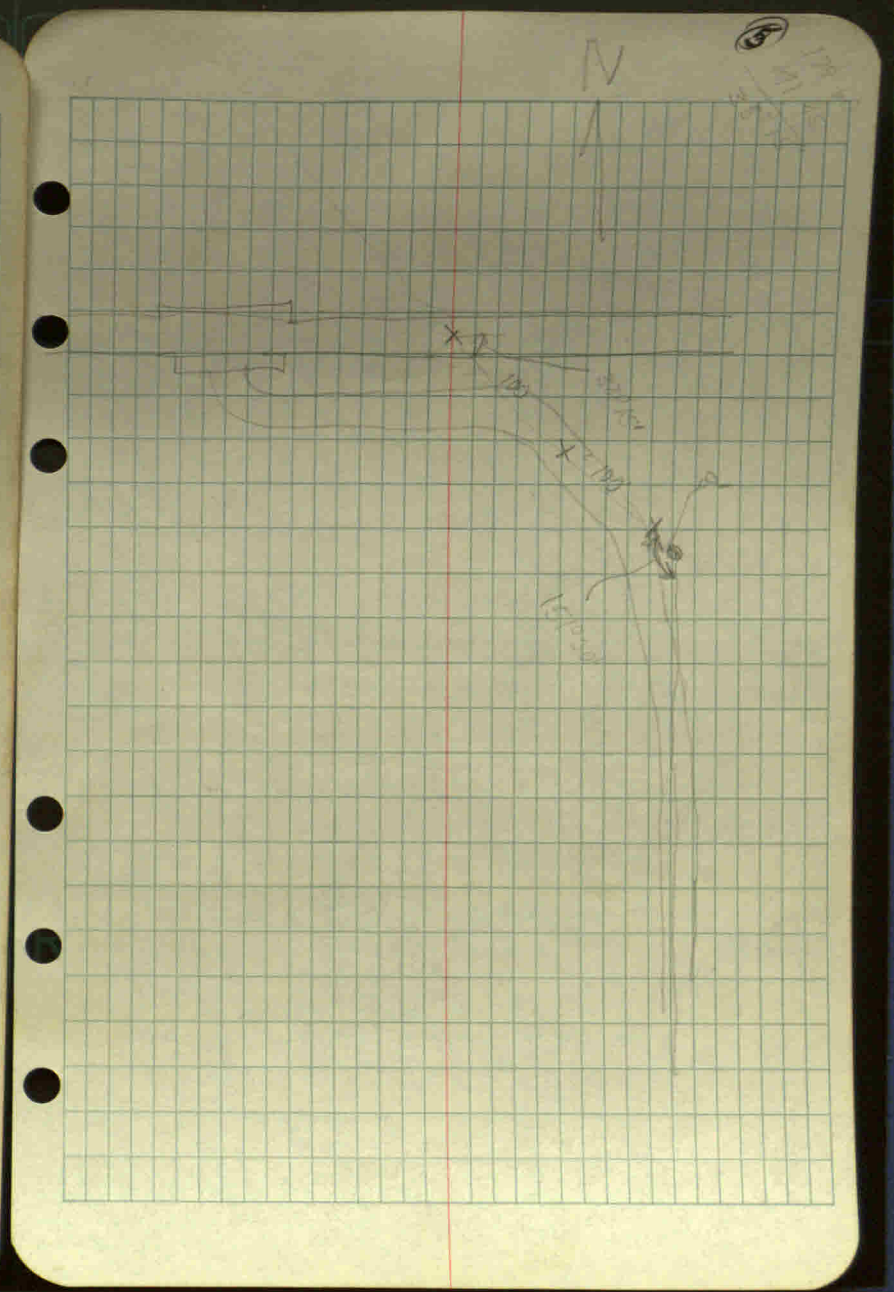
INDEX

Heminger

1




+41.2 + 69.8 + 72
N
151°
30°
+72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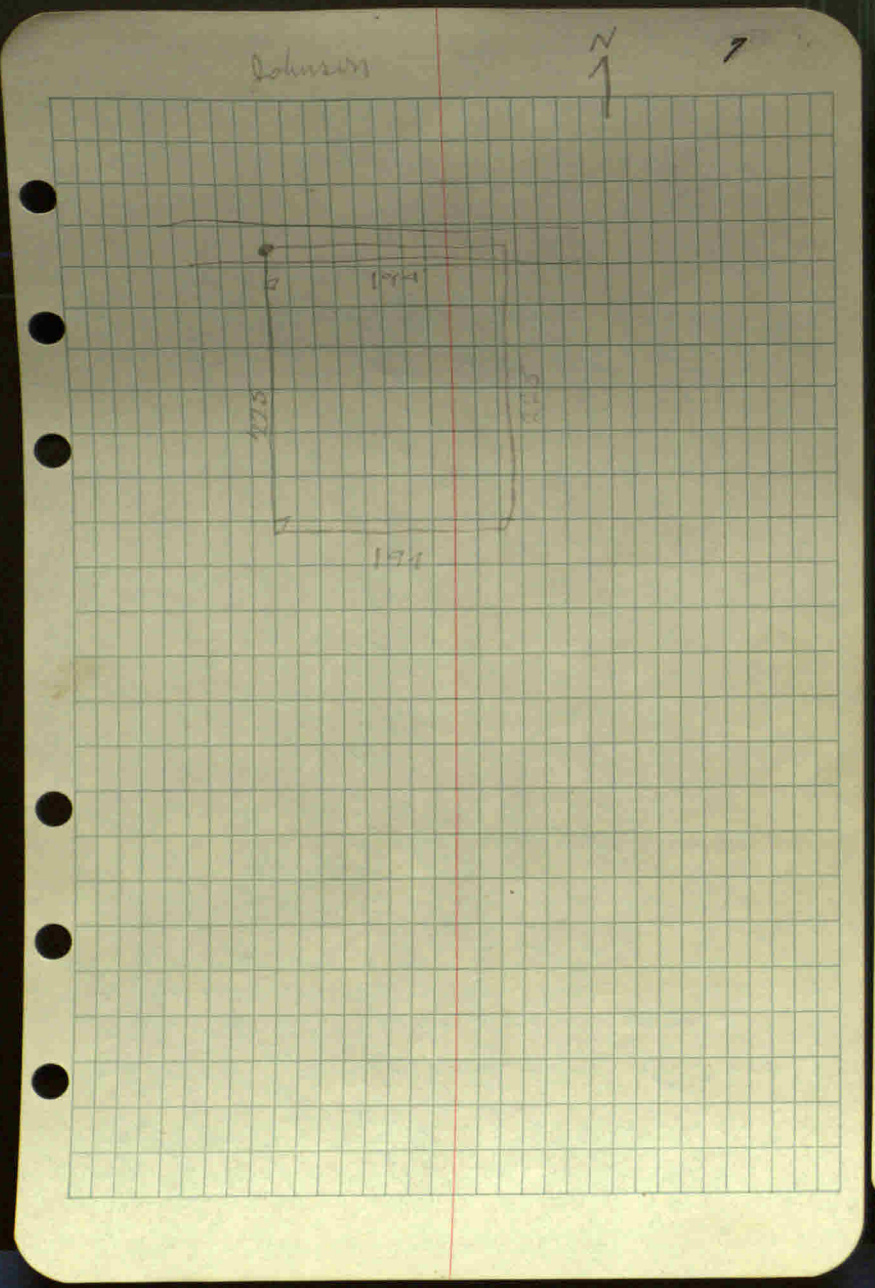
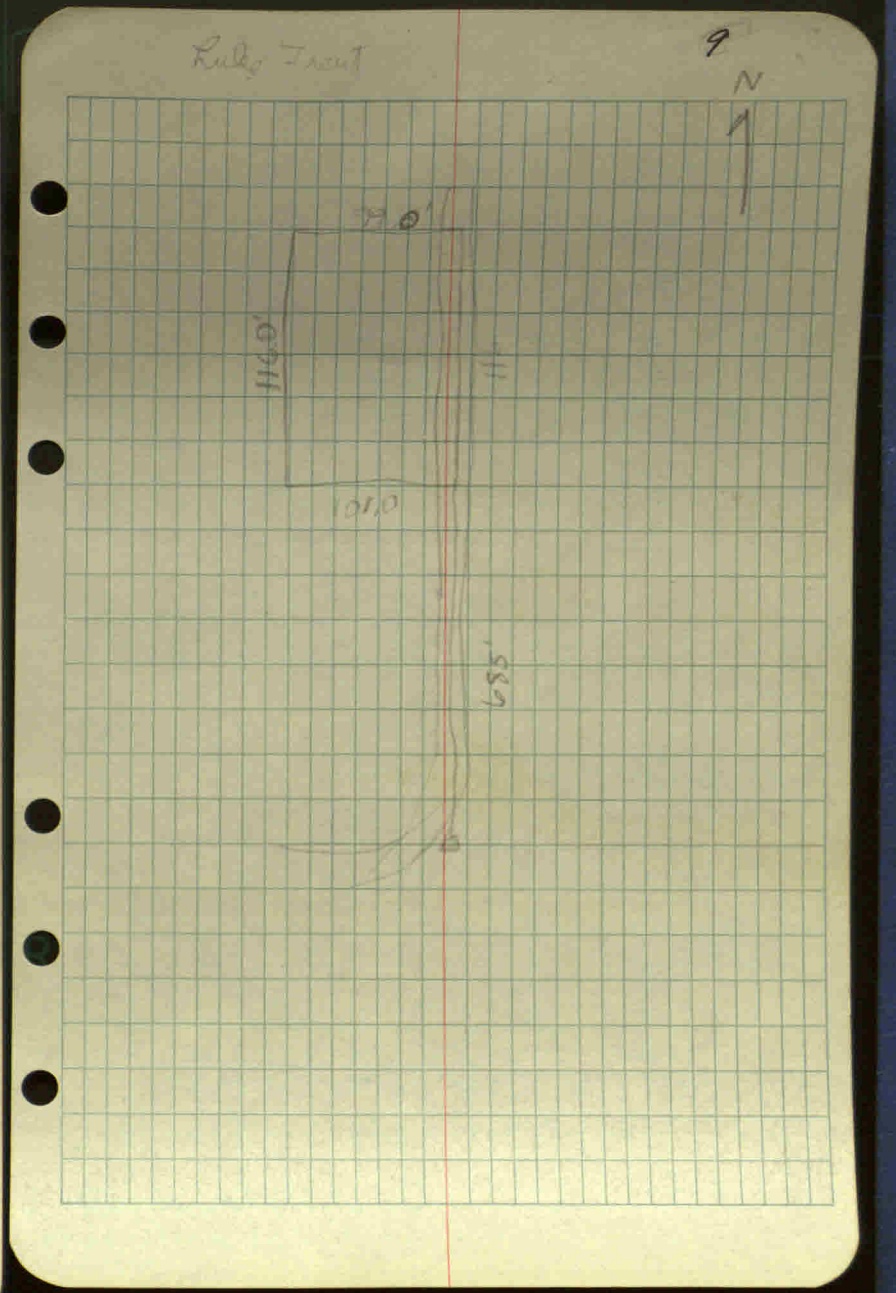
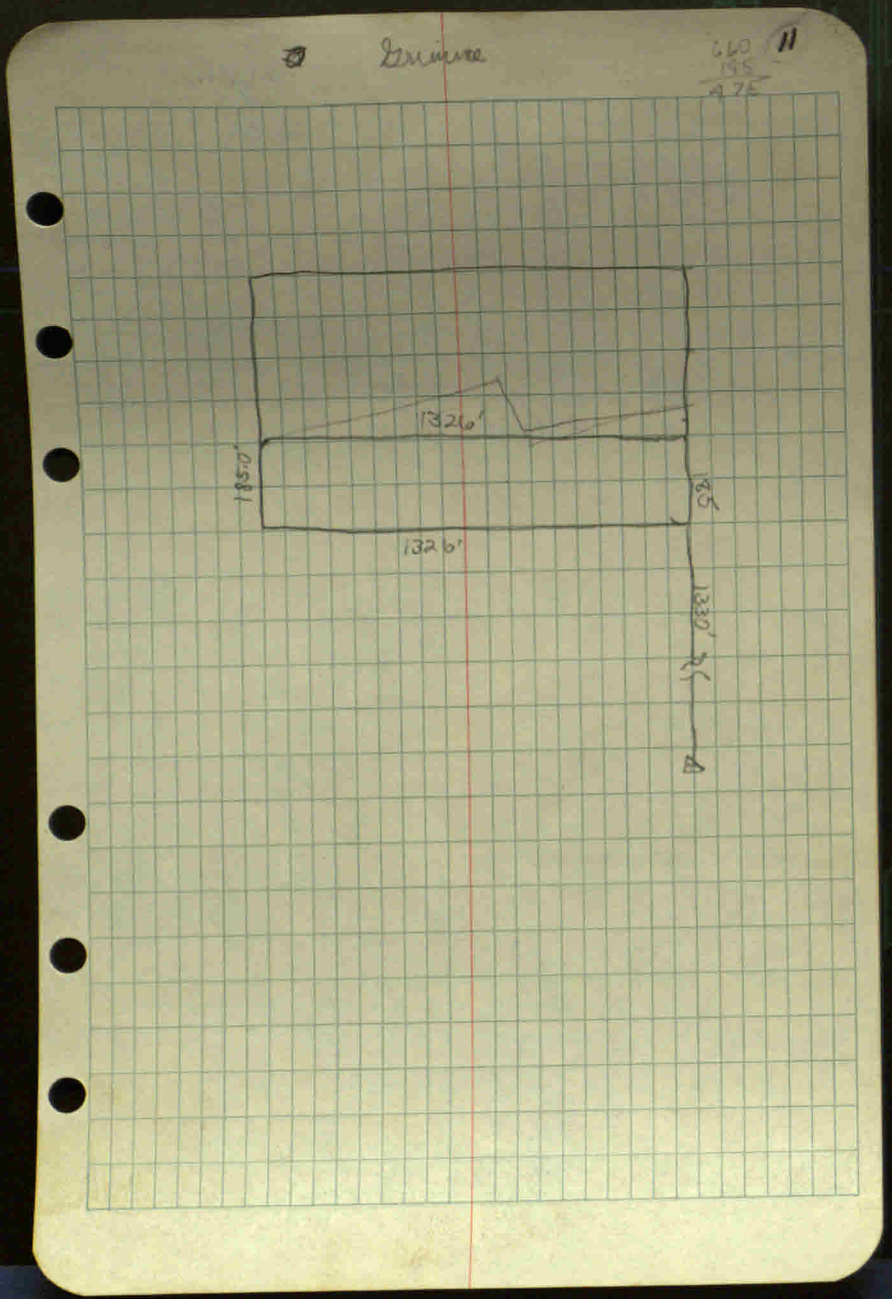

Johnson
N
1
1974
1974
1974


Ruby Trout
9
N
1969
1969
1969
1969


1326'
1850'
185'
1326'
1330'

12

Residential Bridge

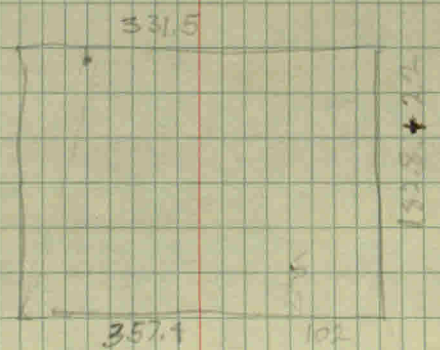
	+	I	−	elev
BM# 1				100.00
	2.80	102.80		
⊙			6.95	95.85
	3.23	99.13		
BM# 2			3.57	95.56
	2.95	98.51		
BM# 3			1.15	97.06
	1.15	98.51		
BM# 2			2.95	95.56
	3.19	99.05		
⊙			3.20	95.85
	6.90	102.75		
BM# 1			2.75	100.00

NAIL in tele phone pole N side Sta 10+20

NAIL in tele phone pole N side Sta 17+80

NAIL in Walnut tree N side Sta 22+80

Fred Worrell



18

Broadstreet Bridge -P

STA	+	π	−	elev.
BM#1				100.00
	4.36			
10+00				
⊖			5.52	
	4.60			
11+00				
⊙			5.32	
	4.58			
12+00				
⊙			4.16	
	2.56			
13+00				

19

25.0	16.0	13.5	10.4	8.0	→1.0	12.0
4.42	4.59	6.17	5.11	5.03	4.63	5.17
19.5	17.5	25.0				
5.92	4.79	4.42				
25.0	18.0	13.0	9.5	7.0	→1.2	11.0
4.32	4.16	6.20	4.76	4.89	4.56	5.00
18.5	19.5	17.0	25.0			
5.08	5.60	4.68	4.23			
25.0	18.0	13.0	12.0	7.5	→1.0	12.0
4.29	4.50	5.79	5.01	5.15	4.89	5.39
15.0	17.0	25.0				
5.85	4.99	5.17				
25.0	16.5	13.0	8.0	6.0	→1.0	13.0
4.90	5.25	4.38	4.85	4.75	4.87	5.07

21

M.D	16.0	18.0	25.0
4.78	5.30	7.69	9.81

23

Plainfield Presbyterian Church

(-S)

14.14 East NE
Bottom of Storm Sewer - in Laundry Room

16.10 West (Top of 8" sewer)
Sanitary Sewer 27.75 from
Back Line / North - South

Water - 1.3' E of N-S Base
7.2' S of E-W "

27

Griswold Road

Nov 2, 1961

Grade at Wall street, railroad crossing
@ 30±" St

28

Sta.	+S	H	-S	Elev
B.M. #1	2.24			
~~75'~~ 50' E				
~~150'~~ ~~100'~~ E				
~~225'~~ ~~150'~~ E				
300' E				
E of G.				
W of G				
~~225'~~ ~~300'~~				
		Railroad		
50+36	4.49	109.14		104.65
50' E				
300' E				

29

N side		S side	
No	Ditch	Ditch	Cut
	Ditch		
	5.11		5.73
	4.74		5.40
	5.45		5.82
	5.80		6.08
	~~5.~~ 5.02		5.75
	4.25		5.59
	4.92		5.04
103.87	5.27	103.20	5.94
101.37	7.77	101.81	7.33

31

S side

103.90	6.60
103.67	6.87
8" pipe	
102.70	7.80
104.70	5.80
105.95	4.55

FIELD NOTES
RENO CROSSING

Index

76' Pipe

std	B.S.	H.I.	F.S.	elev.
B.M.	2.42	211.71		209.29
Flow line			7.21	204.50

5-31-61
A.M. - Rain
P.M. - Sunny

①

A.M. - removed 2-500 gal. tanks. -
Filled with grade 'B' Borrow
P.M. - Replaced Field tile structure
No. 14 with 8" C.M.P.

Catch Basins

Sta.	B.S.	H.I.	F.S.	elev.
B.M. 2	2.03	912.25		910.22
Basin #2			4.55	907.70

Septic tank outlet Found
Connected into C.B. #2

6-1-61
Sunny - Warm

Catch Basins

#1 Cut 12" Below top stake

#2 Cut 11" Below top stake

#3 Cut 4.5' Below top Stake
For F.I. of pipe

#4 Cut 12" Below top Stake

* all cuts will be to top of concrete of C.B.

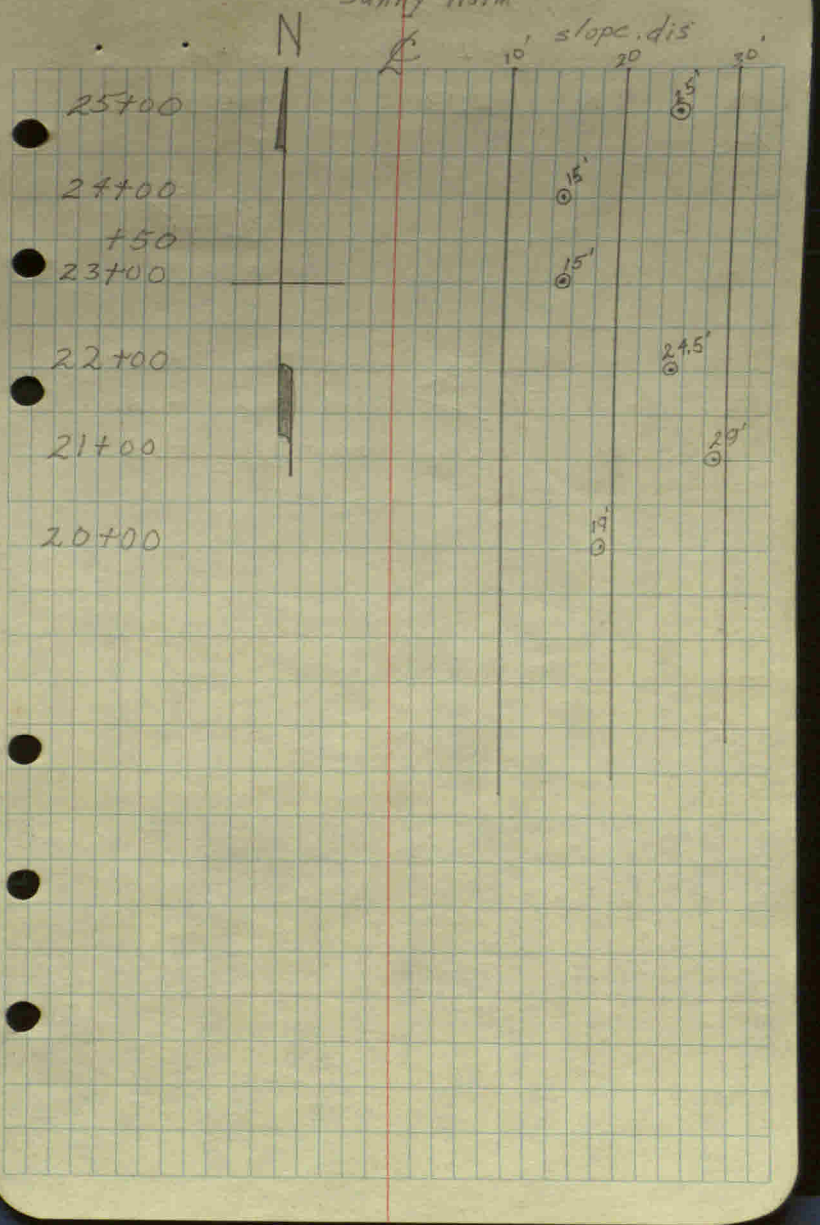
Grade Stakes.

sta. 21+00 - 23+00

sta.	B.S.	H.I.	F.S.	elev.
B.M.4	3.65	912.94		909.29
23+00			3.63	909.31
22+00			.96	911.98
21+00			-.56	913.50
20+00			-.53	913.47

23+00 Fill 6.75' above top stk.
22+00 Fill 5.50' above top stk.
21+00 Fill ~~7.00~~ 8.10' above top stk.

6-1-61
Sunny-Warm
(3)



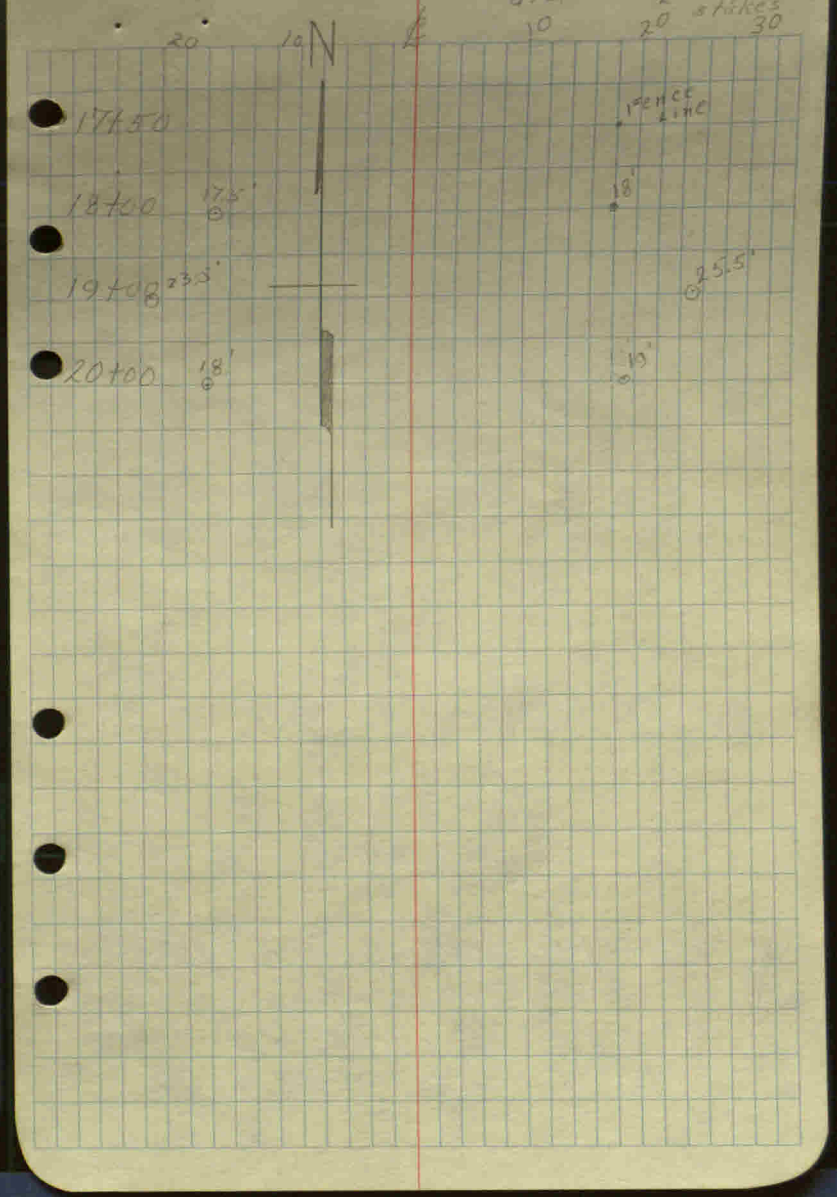
Grade Stakes
Sta. 17+50 - 20+00

Sta.	B.S.	H.I.	F.S.	elev.
B.M.$_3$	7.98	912.13		904.15
17+50				905.08
18+00				905.75
19+00				913.28
20+00				913.47

Sta. 18+00 Fill 0.20' above top stake
Sta. 19+00 Fill ~~5.26~~ 5.20' above top stake
Sta. 20+00 Fill 2.60' above top Stake

6-2-61
Sunny-Hot

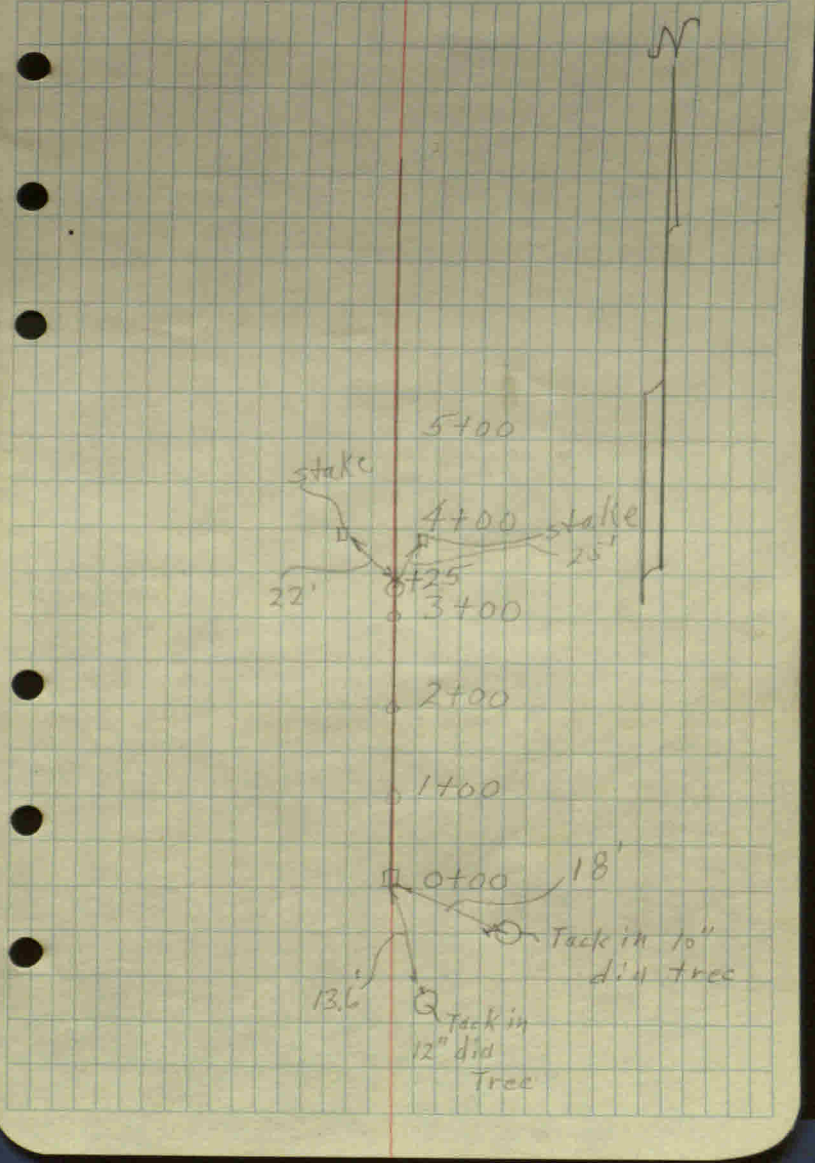
④



Base line For Borrow Pit

6-2-61
Sunny-Hot

(5)



Borrow Pit levels #1

Sta.	B.S.	H.I.	F.S.	elev.	Remarks
B.M.	11.80	111.80		100.00	assumed elev.

6-5-61
Sunny - Hot

⑥

	1+50	1+00	+50	0+00 = Baseline
3+00	110.97 / 0.83	109.66 / 3.14	104.07 / 4.73	100.35 / 11.45
2+50	110.53 / 1.47	109.20 / 2.10	106.17 / 5.63	99.78 / 11.82
2+00	108.76 / 2.04	110.04 / 1.76	105.79 / 5.85	94.91 / 12.39
1+50	107.99 / 1.81	109.47 / 2.33	105.28 / 6.52	98.53 / 12.27
1+00	107.78 / 4.02	107.13 / 4.67	106.06 / 5.74	78.50 / 13.30
0+50	106.42 / 5.38	105.32 / 6.48	103.63 / 8.17	99.30 / 12.50
+25 0+00	104.50 / 27.30	103.57 / 8.27	101.97 / 9.83	78.75 / 13.34

N

B.M. - Nail in tree 3' up From base
50' E. of Sta 1+50 - 2' dia tree

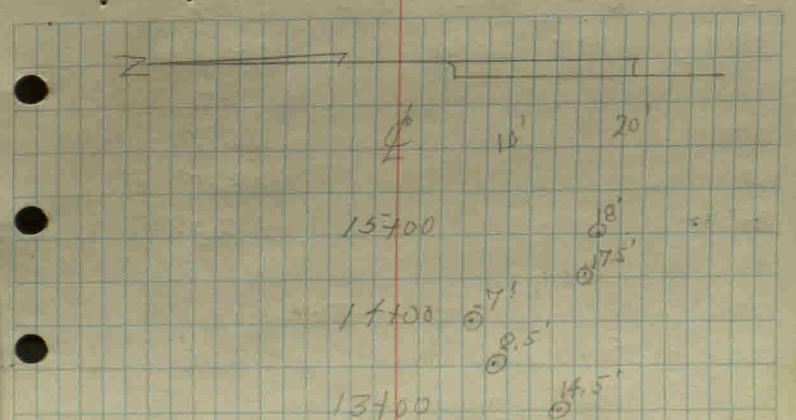
Line S-1 Grade & Slope Stakes

Sta ~~B.S.~~	B.S.	H.I.	F.S.	elev.
~~B.M.~~				~~910.22~~ ~~910.39~~
B.M. ✱	3.17	913.39		
15+00				913.28
14+50				912.45
14+00				910.89
13+50				909.34
13+00				909.41

~~Fill~~ 0.30 below
13+00 Fill ~~1.15~~ above top Stake
13+50 Fill 0.80 above top Stake
14+00 Fill 2.35 above top Stake
14+50 Fill ~~2.70~~ 2.90 above top Stake
15+00 Fill 1.65 above top stake

6-5-61
Sunny - Hot - P.M.

(7)



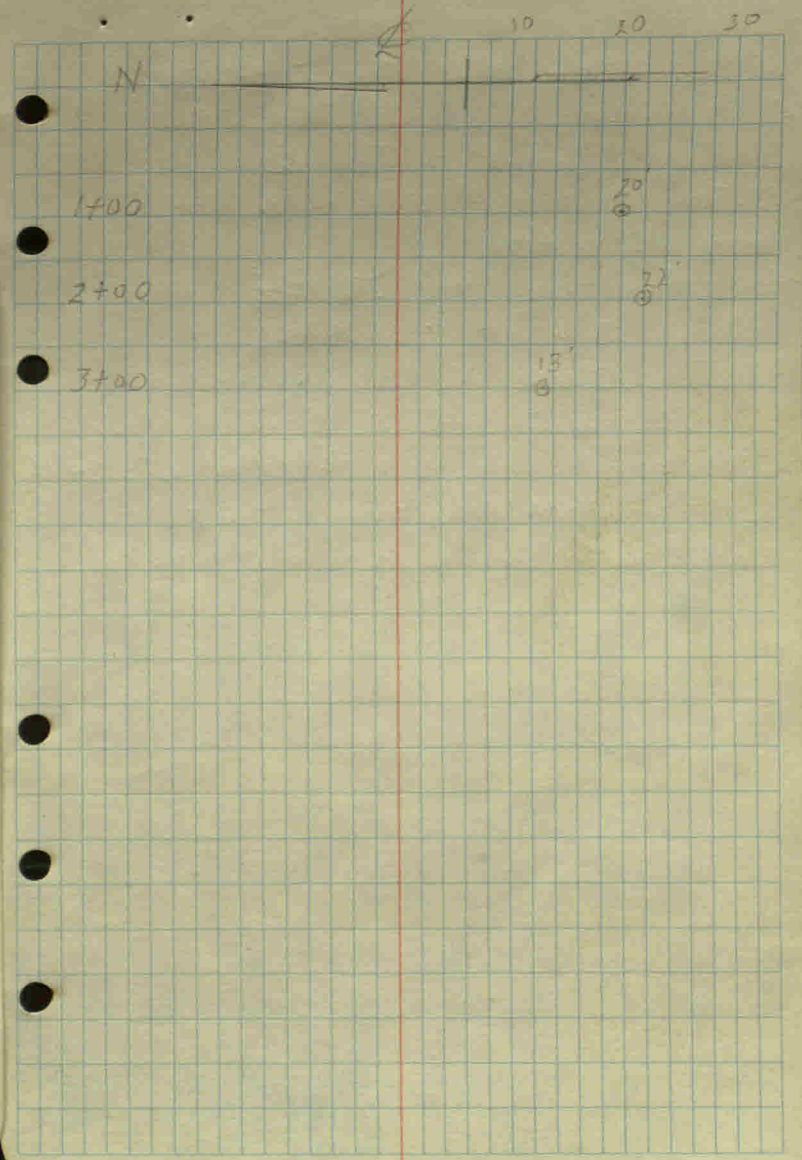
Grade & slope stakes Line 3-2

Sta	B.S.	H.I.	F.S.	elev
B.M.$_3$	5.93	910.08		904.15
1+00				900.71
2+00				902.75
3+00				902.37

1+00 Fill 9.75' above top stake
2+00 Fill 5.40 above top stake
3+00 Match Road

6-12-61
sunny - H.T

(B)



Special Notes

1. Mr. Armstrong Here June 7, 4:00 P.M.
2. Granniger placed Fill June 7 - Rain delayed work to June 12
3. June 9, Art Hinzel & M. Armstrong here 10:30 A.M.
4. Mr. Armstrong Here June 13, 1961 to check Job at 9:30 A.M.
5. June 13, 1961 Railroad Supervisor arrived with Crew to Replace Rails
6. Wilbur Newlin Here 6-15-61 11:30 A.M.
7. 6-15-61 - Mr. Armstrong out on Job to check with Granniger about insurance

Sub Grade Stakes
Sta. 21+00 - Sta. 23+50

Sta.	B.S.	H.I.	F.S.	elev.
B.M.	5.2	914.49		909.29
23+50			6.16	908.03
23+00			6.10	908.39
22+50			~~4.33~~ 5.96	908.53
22+00			3.43	911.06
21+50			2.29	912.20
21+00			1.91	912.58

add 0.92' to elev. for finished Grade

6-12-61
Sunny - Hot
(10)

N

10 20

℄ Stakes set out 25' to mark station

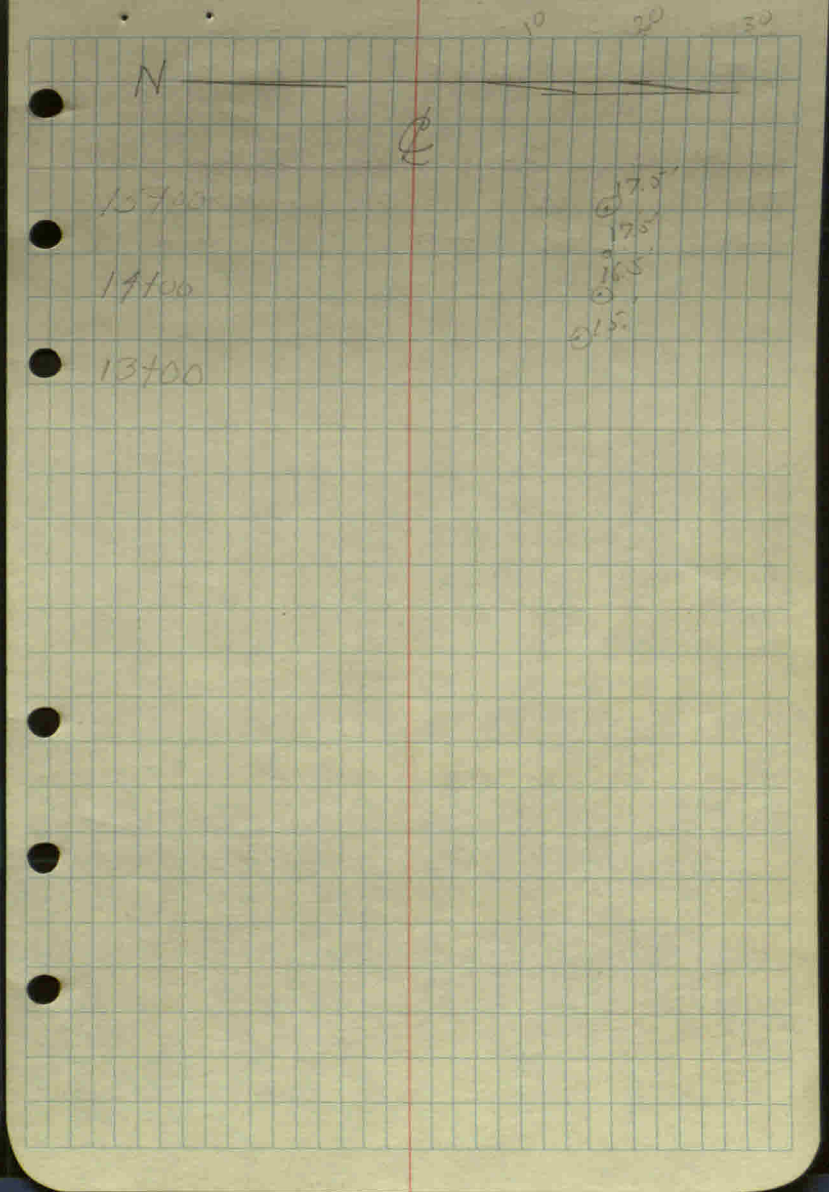
23+50
23+00
22+00
21+00

Sub Grade Stakes
Sta.-Aine S-1

Sta.	B.S.	H.I.	F.S.	elev.
B.M.	1.35	916.57		910.22
~~14+50~~				
~~14+00~~				
~~13+50~~				
~~13+00~~				
15+00			4.21	912.36
14+50			5.04	911.53
14+00			6.61	909.96
13+50			8.15	908.42
13+00			8.78	907.79

C-1 X 3-C1
Sunny-Hot

(11)



Borrow Pit No. 2.

Sta	B.S.	H.I.	F.S.	Elev.
B.M.	11.17	111.17		100.00

B.M. is a Spike in a Scrub Tree on W.W. edge Borrow Pit 65 ft. S of Sta. 17+75

6-14-41 (12)
Cloudy - Warm

B = Base Line

			103.57 / 7.60	106.65 / 4.00
		101.40 / 9.77	103.99 / 6.18	107.17 / 3.20
		104.67 / 6.50	105.97 / 5.20	108.07 / 3.10
99.77 / 8.10	103.03 / 5.14	104.77 / 6.40	105.97 / 5.20	106.67 / 4.50
100.97 / 10.20	104.67 / 7.50	102.42 / 8.75	104.12 / 7.05	103.51 / 7.66
98.64 / 12.53	97.17 / 12.00	100.17 / 11.00	102.57 / 8.60	101.94 / 9.23

B.M.

Sub Control Check
Sta. 17+50 - 20+00

Sta.	R.S.	H.I.	F.S.	Elev.
B.M.	C.64	916.86		910.22
17+50			12.50	904.16
18+00			11.71	~~904.93~~
18+50			9.92	~~906.74~~
19+00			7.21	~~909.65~~
19+50			5.33	~~911.53~~
20+00			4.38	~~912.48~~

6-15-61
Cool - Cloudy

Borrow Pit #2

Std	B.S.	H.I.	F.S.	elev.
B.M.	7.61	107.61		100.00

6-17-61
sunny-warm

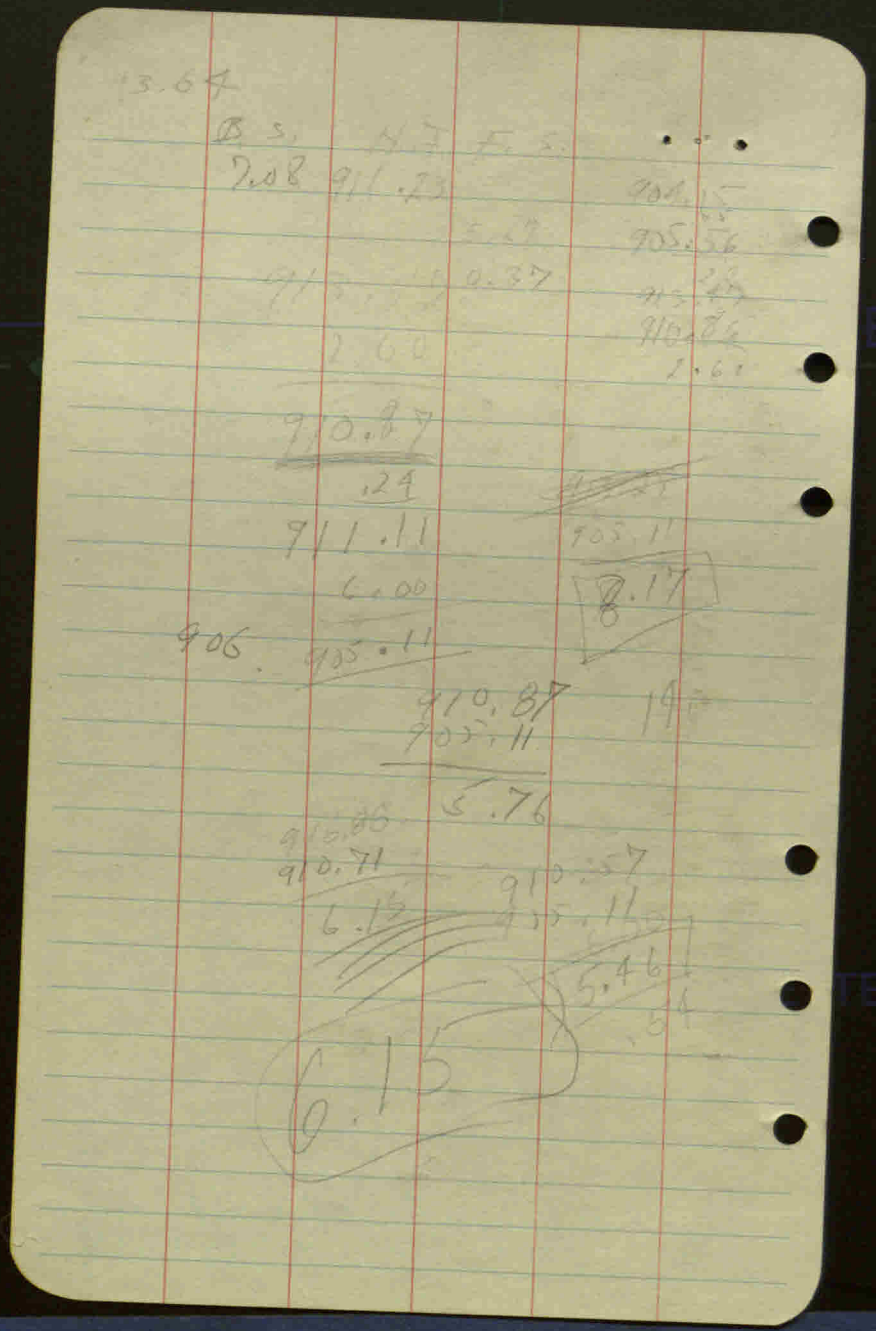
200	150	100	50	25 + 10 + 0	
		103.36 / 4.25	103.47 / 5.94		0+00
	101.21 / 5.41	101.41 / 6.20	102.24 / 4.90	103.51 / 4.10	0+25
	100.41 / 7.20	101.36 / 6.25	102.31 / 4.80	103.31 / 4.10	0+50
100.13 / 7.48	101.11 / 6.50	101.56 / 6.05	102.91 / 4.70	102.99 / 4.62	1+00
98.81 / 8.80	99.56 / 8.05	100.81 / 6.70	101.26 / 6.35	101.51 / 6.10	1+50
98.61 / 9.60	99.07 / 8.65	99.37 / 7.64	100.90 / 6.71	102.39 / 5.30	1+75
					2+00

Borrow Pit #1

Sta	B.S.	H.I.	F.S.	elev.
B.M.	9.86	109.86		100.00

6-17-61
Sunny - warm

	150	100	50	0	
					0+00 +05
	105.36 / 4.50	103.46 / 6.20	101.86 / 8.0	4.50	+50
	105.22 / 4.64	104.71 / 5.15	103.06 / 6.80		1+00
	106.36 / 3.50	106.11 / 3.75	103.43 / 6.43		+50
	104.91 / 2.95	106.86 / 3.00	104.16 / 5.70		2+00
	108.00 / 1.86	106.76 / 3.10	103.36 / 6.50		+50
					3+00



7-17-61 SUNNY hot! 1:00 - 2:00 33

BM #4				909.29	
	5.00	914.29			
23+60					
23+00					
22+95					
22+00					
21+57					
				912.69	
⊙			1.65	~~1.69~~	
	4.19	916.83			

35

21+57				
21+50				
⊙			4.03	912.80
	5.03	917.83		
21+50				
20+81				
BM #3				909.15
	7.93	912.08		
18+00				

908.98	908.88	909.15	909.02
0	9.0	13.1	30.0
5.31	5.41	5.14	5.27

908.10	908.95	908.00	908.95	909.29	909.36
28.0	22.0	19.0	16.0	10.0	0.0
6.19	5.89	6.29	5.39	5.05	4.93

909.17	909.58	909.73
10.0	22.0	37.0
5.12	4.71	4.56

909.50	909.29	909.59	909.79
0.0	10.0	25.0	37.0
4.79	5.00	4.70	4.50

905.94	906.08	911.18	911.55	911.83	911.58
33.0	28.0	15.0	10.0	0.0	10.0
8.35	8.21	3.11	2.74	2.96	2.71

911.33	907.61	907.91
13.0	21.0	26.0
2.96	6.68	6.38

905.45	905.52	911.92	912.49	912.69	912.37
35.0	30.0	15.0	10.0	0.0	10.0
8.54	8.77	2.37	1.85	1.60	1.92

909.92	908.72
31.0	56.0
6.91	8.11
905.39	905.89
36.0	28.0
11.99	10.94

912.18	912.52	912.78	912.48	912.39	907.67
14.0	10.0	0.0	10.0	15.0	28.0
5.65	5.31	5.05	5.35	5.11	10.16

907.51
34
10.32

906.00	907.29	912.80	913.16	913.49
60.0	07.0	15.0	13.0	0.0
11.83	10.59	5.03	4.67	4.39

909.12	905.67	905.88	906.08	905.87	905.71
21.0	19.0	9.0	0.0	10.5	19.0
7.96	6.41	6.20	6.00	6.21	6.37

904.55	904.83
21.0	26.0
7.53	7.25

18+32

18+50

899.90	903.58	904.31	906.96	907.23	
92.0	81.0	50.0	10.0	0.0	
12.18	8.50	7.77	5.12	4.85	
899.58	903.63	904.69	907.91	908.17	908.00
98.0	83.0	58.0	10.0	00	10.0
12.50	8.95	7.99	4.17	3.91	4.08
907.75	904.73	904.61			
16.0	23.0	31.0			
4.33	7.25	7.17			

7-18-61 Cloudy - WARM 8:00 - 40

BM#3				909.15
	8.75	912.90		
18+80				
19+00				
19+50				
0			0.51	912.39
	1.17	913.56		
19+70				

41

909.33	909.27	908.02	906.50	906.63	
0	10.0	33.0	59.0	86.0	
3.57	3.63	4.88	6.40	6.27	
903.15	903.85	909.90	910.15	910.26	910.22
30.0	24.0	14.0	10.0	0.0	10.0
9.75	9.05	3.00	2.75	2.64	2.68
909.99	904.39	904.13			
16.0	29.0	35.0			
2.91	8.51	8.77			
907.74	903.10	911.77	912.06	912.39	912.35
34.0	28.0	14.0	10.0	0.0	10.0
10.16	9.80	1.13	0.84	0.51	0.55
912.06	904.28	903.87			
15.0	29.0	37.0			
0.84	8.62	9.03			
902.36	903.29	912.91	912.58	912.79	913.00
60.0	43.0	20.0	12.0	9.0	0.0
11.20	10.32	1.15	0.98	0.77	0.56
913.01	912.44	903.60	903.78		
18.0	15.0	30.0	39.0		
0.55	1.12	9.96	9.78		

20+00				
0+20				
0+50				
0			3.49	910.07
	0.77	909.30		
1+00				

911.90	913.02	912.39	912.41	913.19	913.39	
60.0	27.0	10.0	0.0	10.0	14.0	
1.66	0.64	0.17	0.15	0.12	0.22	
913.23	910.62	910.39				
16.0	24.0	31.0				
0.33	2.94	3.17				
902.92	903.83	912.34	912.69	913.13	913.28	
9.0	38.0	19.0	15.0	0.0	14.0	
10.63	10.23	1.22	0.87	0.43	0.83	
913.20	911.81	911.87				
33.0	36.0	39.0				
0.36	1.75	1.69				
902.17	902.53	911.83	912.11	912.35	912.80	
37.0	30.0	14.0	11.0	2.0	7.0	
11.39	11.03	1.73	1.45	1.21	1.26	
911.89	903.92	903.77				
10.0	26.0	31.0				
1.67	9.69	9.79				
898.46	898.90	908.01	907.60	908.59	908.49	
34.0	28.0	12.0	9.0	0.0	8.0	
10.84	10.40	1.29	1.70	0.76	0.81	
908.28	900.85	900.85				
11.0	25.0	31.0				
1.02	8.45	8.45				

2+00

BM # 2 910.22

4.12 914.34

15+00

14+50

14+00

910.39	907.92	907.39
12.0	20.0	25.0
9.00	6.92	7.00

909.90	909.49	908.96	907.57	907.58
0.0	12.0	21.0	55.0	61.0
4.44	4.85	5.38	6.77	6.76

908.01	908.19	909.12	909.09	909.41	909.09
19.0	13.0	10.0	8.0	0.0	9.0
6.33	6.20	5.22	5.05	4.93	5.25

908.90	907.96	907.70
11.0	15.0	22.0
5.49	6.88	6.64

908.79	908.60	908.10	908.23
0.0	9.0	13.0	19.0
5.56	5.74	6.24	6.11

908.43	908.41	908.48	908.72	908.59	908.23
19.0	13.0	9.0	0.0	9.0	13.0
5.91	5.93	5.86	5.62	5.75	6.11

908.39
18.0
6.00

908.92	908.55
0.0	11.0
5.42	5.79

896.90	897.28	902.17	902.19	902.78	902.61
27.0	21.0	11.0	9.0	0.0	9.0
12.10	12.02	7.13	6.81	6.52	6.69
902.22	896.83	896.75			
13.0	23.0	32.0			
7.08	12.47	12.55			
911.39	911.11	912.55	912.93	913.02	912.77
22.0	17.0	12.0	8.0	0.0	9.0
2.95	3.23	1.79	1.41	1.32	1.57
912.37	906.94	906.99			
12.0	25.0	29.0			
1.97	7.40	7.40			
910.90	909.34	911.84	912.08	912.12	911.87
22.0	17.0	10.0	8.0	0.0	10.0
3.49	5.00	2.50	2.26	2.21	2.47
911.06	906.82	906.79			
14.0	29.0	30.0			
3.28	7.52	7.55			
907.90	907.58	910.67	910.87	910.90	910.62
21.0	18.0	11.0	9.0	0.0	9.0
6.49	6.76	3.67	3.47	3.49	3.72

14+00

13+66

13+50

13+25

13+00

12+85

R A4 LETTER

← LETTER →

R A5 HALF LETTER

U. S. # 40.

50

STA.	B.S.	H.I.	⑤ F.S.	ELEV.	CORRECTION COLUMN FOR State Highway Bench mark
1731			1.02	92.01	833.73
1730			0.55	92.48	834.20
T.P.			0.62	92.41	834.13
	4.10	96.51			
1729			4.00	92.51	834.23
1728			4.12	92.39	834.11
1727			4.30	92.21	833.93
1726			4.45	92.06	833.78
1725			4.40	92.11	833.83
1724			4.20	92.31	834.03
1723			3.95	92.56	834.28
1722			3.65	92.86	834.58
1721			3.35	93.16	834.88
T.P.			3.42	93.09	834.81
	5.60	98.69			
1720			5.18	93.51	835.23
1719			4.86	93.83	835.55
1718			4.52	94.17	835.89
1717			4.10	94.59	836.31
1716			3.90	94.79	836.51
1715			4.12	94.57	836.29

52

STA.	B.S.	H.I.	④ F.S	ELEV.	CORRECTION COLUMN FOR STATE HIGHWAY BENCH MARK
1753			4.40	86.03	827.75
1752			4.20	86.23	827.95
1751			4.05	86.38	828.10
1750			3.80	86.63	828.35
T.P.			3.90	86.53	828.25
	5.20	91.73			
1749			4.90	86.83	828.55
1748			4.70	87.03	828.75
1747			4.50	87.23	828.95
1746			4.32	87.41	829.13
1745			4.38	87.35	829.07
1744			4.55	87.18	828.90
1743			4.82	86.91	828.63
1742			5.29	86.49	828.21
1741			5.60	86.13	827.85
1740			6.00	85.73	827.45
T.P.			6.05	85.68	827.40
	7.35	93.03			
1739			7.65	85.38	827.10
1738			7.80	85.23	826.95
1737			7.45	85.58	827.30
1736			6.62	86.41	828.13
1735			5.45	87.58	829.30
1734			4.22	88.81	830.53
1733			3.04	89.99	831.71
1732			1.90	91.13	832.85

54

STA.	B.S.	H.I.	③ F.S.	ELEV.	Correction Column for State Highway Bench mark
1773			5.26	90.13	831.85
1772			4.82	90.15	831.87
1771			4.50	90.83	832.55
1770			4.35	90.98	832.70
1769			4.30	91.03	832.75
1768			4.32	91.01	832.73
T.P.			4.42	90.91	832.63
	4.62	95.53			
1767			4.70	90.83	832.55
1766			4.90	90.63	832.35
1765			4.98	90.55	832.27
1764			4.95	90.58	832.30
1763			4.86	90.73	832.45
1762			4.59	90.94	832.66
1761			4.55	90.98	832.70
1760			4.82	90.71	832.43
1759			5.42	90.11	831.83
T.P.			5.50	90.03	831.75
	0.40	90.43			
1758					
1757			2.45	87.98	829.70
1756			3.42	87.01	828.73
1755			4.10	86.33	828.05
1754			4.45	85.98	827.70

56

STA.	B.S.	H.I.	② F.S.	ELEV.	Correction Column for State Highway Bench mark
1793			3.70	95.92	937.64
1792			2.21	97.41	839.13
1791			1.00	98.62	840.34
T.P.			1.05	98.57	840.29
	5.60	104.17			
1790			4.75	99.42	841.14
1789			4.35	99.82	841.54
1788			4.41	99.76	841.48
1787			4.88	99.29	841.01
1786			5.62	98.55	840.27
1785			6.54	97.63	839.35
1784			7.35	96.82	838.54
T.P.			7.52	96.65	838.37
	1.92	98.57			
1783			2.70	95.87	837.59
1782			3.45	95.12	836.84
1781			4.25	94.32	836.04
1780			5.00	93.57	835.29
1779			5.70	92.87	834.59
1778			6.30	92.27	833.99
1777			7.50	91.07	832.79
T.P.			7.52	91.05	832.77
	4.28	95.33			
1776			5.21	90.12	831.84
1775			5.52	89.81	831.53
1774			5.65	89.68	831.40

U.S # 40 2-20-1928 ①

58 Lee T Bob D George

STA.	B.S.	H.I.	F.S.	ELEV.	Correction Column for State Highway Bench mark
B.M.'	0.42	100.42		100.00	
T.P.			12.85	87.57	
	0.25				
T.P.			8.75	79.07	
	3.65	82.72			
1809			6.32	76.40	818.12
1808			5.88	76.84	818.56
1807			5.47	77.25	818.97
1806			5.08	77.64	819.36
1805			4.90	77.82	819.54
1804			4.15	78.57	820.29
1803			3.55	79.17	820.89
T.P.			3.70	79.02	820.74
	8.85	87.87			
1802			7.82	80.05	821.77
1801			6.70	81.17	822.89
1800			5.38	82.49	824.21
1799			3.93	83.94	825.66
1798			2.23	85.64	827.36
1797			0.26	87.61	829.33
T.P.			0.40	87.47	829.19
	12.15	99.62			
1796			9.90	89.72	831.44
1795			7.78	91.84	833.56
1794			5.61	94.01	835.73

①

59

STA	B.S.	H.I.	F.S.	ELEV	
Bm'	0.42	100.42		100.00	
TP			12.85	87.57	
	0.25	87.82			
T.P.			8.75	79.07	
	3.65	82.72			
1809			6.32	76.90	819.42
1808			5.88	76.84	
1807			5.47	77.25	
1806			5.08	77.64	
1805			4.90	77.82	
1804			4.15	78.57	
1803			3.55	79.17	
TP			3.70	79.02	
	8.85	87.87			
1802			7.82	83.75 (80.05) (81.17)	818.07
1801			6.70	89.87	
1800			5.38	86.19 (82.49)	
1799			3.93	87.64 (83.94)	
1798			2.23	89.34 (85.64)	
1797			0.26	91.31 (87.61)	
TP			0.40	91.17 (87.47)	
	12.15	99.62 103.32			
1796			9.90	93.42 (89.72)	
1795			7.78	95.54 (91.84)	
1794			5.61	97.71	94.01

STA.	B.S.	H.I.	F.S.	ELEV.	
1793				95.92	
			3.70	99.62	837.64
1792				97.91	
			2.21	101.11	839.13
1791				98.62	
			1.00	102.32	840.34
T.P.				99.37	
		104.17	1.05	102.27	840.29
	5.60	107.87			
1790				99.42	
			4.75	103.12	841.14
1789				99.92	
			4.35	103.52	841.54
1788				99.76	
			4.41	103.46	841.48
1787				99.29	
			4.88	102.99	841.01
1786				98.35	
			5.62	102.25	840.27
1785				97.03	
			6.54	101.33	838.35
1784				96.12	
			7.35	100.52	838.54
T.P.				95.65	
		99.57	7.52	100.35	838.37
	1.92	102.27			
1783				95.87	
			2.70	99.57	837.59
82				95.12	
			3.45	98.82	836.84
81				94.32	
			4.25	98.02	836.04
80				93.57	
			5.00	97.27	835.29
1779				92.87	
			5.70	96.57	834.59
78				92.27	
			6.36	95.97	834.01
77				91.07	
			7.50	94.77	932.79
T.P.				91.05	
		95.33	7.52	94.75	832.77
	4.28	99.03			
1776				90.12	
			5.21	93.82	831.84
1775				89.81	
			5.52	93.51	831.53
1774				89.64	
			5.65	93.38	831.40

BM' T&P R/W marker approx sta 1792+00

STA.	B.S.	H.I.	E.S.	ELEV (3)	Correction Column H for State Hiway Bench Marks
1773			5.20	90.13 93.83	831.85
1772			4.82	90.59 94.21	832.23
1771			4.50	90.83 94.53	832.55
1770			4.35	90.98 94.68	832.70
1769			4.30	91.03 94.73	832.75
1768			4.32	91.01 94.71	832.73
T.P.		95.53	4.42	90.91 94.61	832.63
	4.62	99.23			
1767			4.70	90.93 94.53	828.85 832.55
1766			4.90	90.63 94.33	832.35
1765			4.98	90.55 94.25	832.27
1764			4.95	90.58 94.28	832.30
1763			4.80	90.73 94.43	832.45
1762			4.59	90.94 94.64	832.66
1761			4.55	90.98 94.68	832.70
1760			4.82	90.71 94.41	832.43
1759			5.42	90.11 93.81	831.83
T.P.		90.43	5.50	90.03 93.73	831.75
	0.90	94.13			
1758			0.10		
1757			2.45	91.68 87.98	829.70
1756			3.42	90.71 87.01	828.73
1755			4.10	90.03	828.05
1754			4.45	89.68	827.70

65

STA	B.S.	H.I.	F.S.	ELEV	④ Correction Column For State Highway Bench
1753			4.40	89.73	827.75
1752			4.20	89.93	827.95
1751			4.05	90.08	828.10
1750			3.80	90.33	828.35
T.P.			3.90	90.23	828.25
	5.20	95.43			
1749			4.90	90.53	828.55
1748			4.70	90.73	828.75
1747			4.50	90.93	828.95
1746			4.32	91.11	829.13
1745			4.38	91.05	829.07
1744			4.55	90.88	828.90
1743			4.82	90.61	828.63
1742			5.24	90.19	828.21
1741			5.60	89.83	827.85
1740			6.00	89.43	827.45
T.P.			6.05	89.38	827.40
	7.35	96.73			
1739			7.65	89.08	827.10
1738			7.80	88.93	826.95
1737			7.45	89.28	827.30
1736			6.62	90.11	828.13
1735			5.45	91.28	829.30
1734			4.22	92.51	830.53
33			3.04	93.69	831.71
32			1.90	94.93	832.85

67

STA.	B.S.	H.I.	F.S.	ELEV.	⑤ Correction Column For St. Bench Mark
[illegible]			1.02	95.71	833.73
1730			0.55	96.18	834.20
T.P.			0.62	96.11	834.13
	4.10	100.21			
1729			4.00	96.21	834.23
1728			4.12	96.09	834.11
1727			4.30	95.91	833.93
1726			4.45	95.76	833.78
1725			4.40	95.81	833.83
1724			4.20	96.01	834.03
1723			3.95	96.26	834.28
1722			3.65	96.56	834.58
1721			3.35	96.86	834.88
T.P.			3.42	96.79	834.81
	5.60	102.39			
1720			5.18	97.21	835.23
1719			4.86	97.53	835.55
1719			4.52	97.87	835.89
1717			4.10	98.29	836.31
1716			3.90	98.49	836.51
1715			4.12	98.27	836.29

81

Sta	+	⊼	-	elev
G1			1.97	103.30
			2.48	102.79
G2			4.95	100.32
G3			5.22	100.05
G4			5.36	99.91
H3			4.96	100.81
H2			3.07	102.20
H1			1.16	104.11
			1.73	103.54
I1			0.99	104.28
			1.52	103.75
I2			2.49	102.83
I3			3.72	101.55
I4			4.96	100.31
I5			5.39	99.88
I5+15			5.30	99.97
TP			2.27	103.00
	1.90	104.90		
			2.27	102.63
			4.02	100.88
			4.78	100.12
			5.40	99.50
Ditch +12.7			5.61	99.39
FL Line			7.05	97.85

79

sta	+	⊼	-	elev
			7.01	97.89
			7.09	97.81
BT+3			1.97	103.43
I+3			0.98	103.92
TP			1.15	103.75
	1.71	105.46		
			5.44	100.02

Sta.	+	π	−	elev
BM				100.00
	6.27	105.27		
B1			3.46	101.82
			2.94	102.33
B2			5.15	100.12
B3			5.36	99.91
C3			5.70	99.57
C2			5.18	100.09
C1			4.01	101.26
			3.38	101.89
D3			5.12	100.15
D2			4.86	100.41
D1			3.18	102.09
			3.80	101.47
E1			3.01	102.26
			3.56	101.71
E2			5.09	100.18
E3			5.76	99.51
F4			5.27	100.00
F3			5.93	99.39
F2			4.65	100.62
F1			2.17	103.10
			2.79	102.98

A - 20.7
B - 29.6
C - 30.3
D - 36.0
E - 41.7
F - 46.2
G - 51.0
H - 56.0
I - 59.1

θ 17°
10'
25" 7"

Sta	+	↑	−	elev	75
BM				100.00	
	5.01	105.01			
A1			2.99	102.02	
			3.24	101.77	
A2			3.84	101.17	
A3			3.94	101.07	
A4			4.03	100.98	
A4+15			4.77	100.24	
B4+15			4.60	100.41	
B4			4.97	100.04	
B3			5.53	99.48	
B2			5.00	100.01	
B1			3.53	101.48	
			2.70	102.31	
C1			3.38	101.63	
			3.93	101.08	
C2			5.05	99.96	
C3			5.56	99.45	
C4			5.13	99.88	
C4+15			4.91	100.10	
D4+15			5.03	99.98	
D1			5.19	99.82	
D3			5.20	99.81	

Ditch

	5.76	105.76	~~5.77~~	
H4+15			5.81	99.95
H4			5.89	99.87
H3			4.96	100.80
H2			4.11	101.65
H1			2.06	103.70
			2.67	103.09
I1			1.68	104.18
			2.36	103.90
I2			3.11	102.66
I3			4.23	101.53
I4			5.80	99.96
I4+15			5.70	100.06
E				
			3.46	102.30
			3.15	102.61
			2.15	103.61
			2.09	103.67
TP			2.63	103.13
	1.32	104.45		
			2.02	102.43
			3.78	100.67

			4.96	99.99
			5.34	99.11
			6.51	97.94
			6.50	97.95
			6.49	98.01
Cor				
			2.26	102.20
			3.40	101.05
			4.36	100.09
			5.15	99.30
TP			1.79	102.66
	2.78	105.44		
			5.40	100.04

Sta.	+	X	-	e/e.v	
D2			4.67	100.34	
D1			2.85	102.16	
			3.78	101.23	
E ~~0~~ 1			2.70	102.31	
			3.44	101.57	
E ~~0~~ 2			4.89	100.13	
E ~~0~~ 3			5.02	99.99	
E ~~0~~ 4			5.16	99.85	
E ~~0~~ 4+16			6.05	99.96	
F #4+15			5.15	99.86	
F #4			5.22	99.79	
F #3			5.69	99.32	
F #2			4.80	100.21	
F #1			2.20	102.81	
			2.78	102.23	
G1			3.28	101.73	
			4.25	100.76	
G2			3.97	101.04	
G3			5.28	99.73	
G4			5.28	99.73	
G4+16			5.05	99.96	
TP	~~5.41~~		5.01	100.00	

5

69

NE corner Carson Ford Building on pavement.

Carson
Ford

Br'wn b'g

WALL Street 4-10-63 83

STA.	B.S.	H.I.	F.S.	elev.	REMARKS
B.M.'	4.44	104.44		100.00	
0+00 South			7.70	96.74	
2nd 0+00			5.09	99.35	
0+00 North			5.77	98.67	
1+00 bottom ditch			5.94	98.50	
2+00			5.42	99.02	
3+00			4.78	99.66	
4+00			4.44	100.00	
5+00			4.10	100.34	
T.P.			2.45	101.99	
	8.50	110.49			
6+00			9.56	100.93	
7+00			8.22	101.27	
8+00			8.72	101.77	
8+30			8.15	102.34	Tile opening in ditch
9+00			5.75	104.74	
10+00			5.70	104.79	
10+88			7.54	102.95	Tile opening in ditch
11+00			7.60	102.89	
12+00			7.30	103.19	
13+00			7.34	103.15	
T.P.			5.20	105.29	
	5.00	110.29			
14+00			6.90	103.39	
15+10			6.69	103.69	

85

STA.	B.S.	H.I.	F.S.	ELEV.	
16+00			6.65	103.64	
17+00			6.06	104.23	
18+00			6.25	104.04	
19+00			5.70	104.59	
20+00			4.65	105.64	
21+00			4.98	105.31	
22+00			5.47	104.82	
T.P.			4.60	105.69	
	6.88	112.57			
23+00			7.95	104.62	
24+00			8.25	104.32	
25+00			7.40	105.17	
26+00			6.20	106.37	Last stake
27+00			6.04	106.53	
28+00			5.46	107.11	
29+00			5.02	107.55	
30+00			5.30	107.27	
31+00			5.55	107.02	
T.P.			4.60	107.97	
	3.22	111.19			
32+00			4.60	106.59	
33+00			5.50	105.69	✓
34+00			5.49	105.70	
35+00			5.83	105.36	
36+00			7.03	104.16	

Telephone pole 0+45 RW
Line on East South

STA.	B.S.	H.I.	F.S.	Elev	
37+00			7.42	103.77	
38+00			7.45	103.74	
39+00			7.25	103.94	
39+42			6.65	104.54	
39+62			6.00	105.19	℄ Rd
B.m.2			1.95		Fence post N. 39+42

89

Inspection Made March 5, 1963 10:20 A.M
Treads had been Freshly Nailed Not over 2 or 3 days prior to Inspection. Stair banister Loose & Wobly From First Floor to Landing. Treads broken and cracked. Hall Lighted by small 15 watt Light bulb. Light at top of Stairs Also 15 watt bulb. Hallway was clean & No Loose material at time of inspection.

Lee Taylor

12240 - 12291

91

Wall st. Pike & Griswold Rd. 92

STA.	B.S.	H.I.	F.S.	ELEV.
B.M'	4.96	104.96		100.00
0+00			5.20	99.76
1+00			5.45	99.51
2+00			4.50	100.46
3+00			3.84	101.12
4+00			3.18	101.78
5+00			2.95	102.01
T.P.			2.60	102.36
	8.00	110.36		
6+00			7.19	103.17
7+00			7.27	103.09
8+00			6.03	104.33
9+00			3.70	106.66
10+00			4.52	105.84
11+00			4.72	105.64
T.P.			4.77	105.59
	4.50	110.09		
12+00			4.49	105.60
13+00			4.45	105.64
14+00			4.68	105.41
15+00			4.55	105.54
16+00			4.83	105.26
17+00			4.55	105.54
18+00			4.35	105.74
T.P.			3.60	106.49
	4.30	110.79		

93

Spike in Telephone pole at 40 S. side Rd.

STA.	B.S.	H.I.	F.S.	Elev.
19+00				
20+00			3.62	107.17
21+00			3.90	106.89
22+00			5.02	105.77
23+00			5.04	105.75
24+00			5.25	105.54
T.P.			4.91	105.88
	6.50	112.38		
25+00			5.80	106.58
26+00			4.99	107.39
27+00			5.31	107.07
28+00			4.27	108.11
29+00			3.09	109.29
T.P.	3.20	112.49		
30+00			4.00	108.49
31+00			3.95	108.54
32+00			4.25	108.24
33+00			5.13	107.36
34+00			5.35	107.14
35+00			5.05	107.44
36+00			6.60	105.89
37+00			7.42	105.07
38+00			7.57	104.92
T.P.			7.65	104.84
	5.00	109.84		
39+00			4.56	105.28
39+56			4.06	105.78
40+00			4.36	105.48

℄ Griswold Rd.

4.42.

B.M.2 0.35 Fence post 39+56 N. side Rd. 109.49

WALL Street + Pike 7-12-62

STA.	B.S.	H.I.	F.S.	ELEV.
BM # 1				100.00
	5.47	105.47		
0+00			6.00	99.47
2+00			5.46	100.01
4+00			3.66	101.81
6+00			2.37	103.10
8+00			0.62	104.85
⊙			0.62	104.85
	4.92	109.77		
10+00			3.63	106.14
12+00			3.80	105.97
14+00			4.50	105.27
16+00			4.65	105.12
18+00			3.92	105.85
⊙			3.92	105.85
	3.74	109.59		
20+00			1.81	107.78
22+00			3.75	105.84
24+00			4.12	105.47

elev. at sta. are on top of stakes 35' Lt ℄ Rd.

Sta	+	↑	−	elev.
26+00			2.50	107.09
⊙			2.50	107.09
	5.16	112.25		
28+00			4.66	107.59
30+00			3.90	108.35
32+00			3.97	108.28
34+00			5.08	107.17
36+00			6.37	105.88
⊙			6.37	105.88
	2.69	108.57		
38+00			3.70	104.87
40+00			3.26	105.31
BM# 2			+0.66	109.23

top of corner post NE of intersection

Intersection 300N & 800E

sta	+	⊼	-	elev.
BM # 1				100.00
	1.54	101.54		
S Road				
0+26				
2+00				
4+00				
6+00				
⊙			6.25	95.29
	5.51	100.80		
8+00				
10+00				
10+88				
11+43				

top of first step of steps up to porch of house

Ditches

LH	RH
5.65	5.50
95.89	96.04
6.44	5.95
95.10	95.59
6.55	6.81
94.99	94.73
6.81	7.18
94.73	94.36
5.08	5.00
95.72	95.80
6.08	6.13
94.72	94.67
10.10	
90.70	
	10.23
	90.57

Sta	+	π	−	elev
BM #1				100.00
	2.60	102.60		
E Road				
0+15				
2+00				
4+00				
5+77				
2+83				
W Road				
BM #1				100.00
	1.01	101.01		
℄ Intr.			4.29	96.72
0+19				

Ditches

Lf	Rt
6.26	6.51
96.34	96.09
5.37	5.15
97.23	97.45
6.03	6.17
96.57	96.43
10.27	10.36
92.33	92.24
4.40	1.60
98.20	98.00
5.60	4.72
95.41	96.29

sta	+	ft	−	elev
2+00				
4+00				
6+00				
⊙			2.81	98.20
	2.08	100.28		
8+00				
10+00				
12+00				
14+00				
16+00				

Ditches

LT	RT	
4.96	5.18	
96.05	95.83	
4.60	4.75	
96.41	96.26	
4.32	4.43	
96.69	96.58	
3.05	3.00	
97.23	97.28	
4.70	4.86	
95.58	95.42	
5.84	6.14	
94.44	94.14	
7.41	7.35	
92.87	92.93	
12.01	12.25	bridge
88.27	88.03	

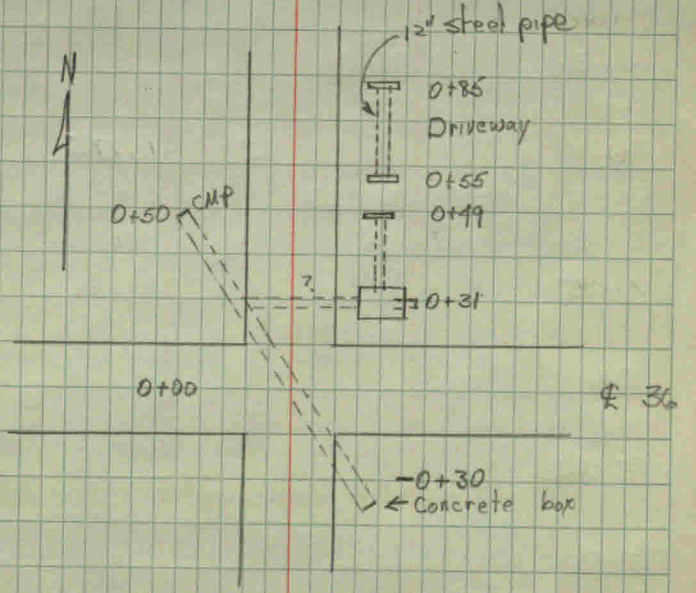
U.S. 36 & Griswold Rd N.

7-25-63 Hot, sunny

Lee
Darrell
George

Sta	+	↑	−	elev	Ditch LF	Ditch Rt
BM#1				100.00		
	3.46	103.46				
-0+30				8.47		
0+31				7.95		
0+50				7.83		
0+49				7.48		
0+55				6.80		
0+85				6.06		
2+00					5.15	5.15

Nail on West side of power pole
1' above ground Sta 0+38 20' Rt



Sta	+	I	−	elev
2+94				
3+16				
3+87				
4+03				
⊙			1.71	101.75
	4.48	106.23		
4+75				
5+20				
5+52				
5+70				
6+00				
6+60				

Lf	Rt	
4.50		12" CMP
4.24		
	4.01	12" Conc.
	4.03	
5.66		12" Conc.
6.65		
	6.53	12" Conc.
	6.45	
6.33	6.05	
6.18		12" CMP (Long)

Sta	+	=	−	elev
6+70				
6+92				
7+77				
7+91				
8+00				
8+15				
8+68				
8+89				
10+00				
⓪			3.50	102.73
	6.94	109.67		

Lf	Rt	
	6.03	conc
		12"
	6.18	Metal
	6.14	
		12" CMP
	6.19	
	5.91	
5.92		12" Conc. (Long)
	5.80	
		12" CMP
	5.89	
5.00	4.37	

Sta	+	π	−	elev
12+00				
13+33				
13+52				
14+00				
⊙			4.57	105.10
	3.89	108.94		
16+00				
18+00				
19+86				
20+07				
20+00				

Lf	Rt	
7.75	6.52	
7.16		
		12" CMP
7.18		
6.89	5.63	
5.65	4.62	
6.10	5.08	
5.89		
6.01		
	5.20	

Sta.	+	HI	−	elev.
22+00				
24+00				
①			4.10	104.84
	5.23	110.07		
26+00				
28+00				
30+00				
32+00				
①			5.09	104.98
	5.59	110.57		
34+00				
36+00				

118

LF	Rt
5.69	4.53
5.16	4.84
6.20	5.70
6.35	4.73
6.00	4.70
6.90	5.35
6.83	4.98
6.83	4.50

119

sta	+	π	−	elev.
38+00				
39+96				
BM#2			5.01	105.56
	5.01	110.57		
⊙			4.94	105.63
	3.62	109.25		
⊙			4.42	104.83
	1.71	106.54		
⊙			7.46	99.08
	4.32	103.40		
BM#1			3.34	100.06

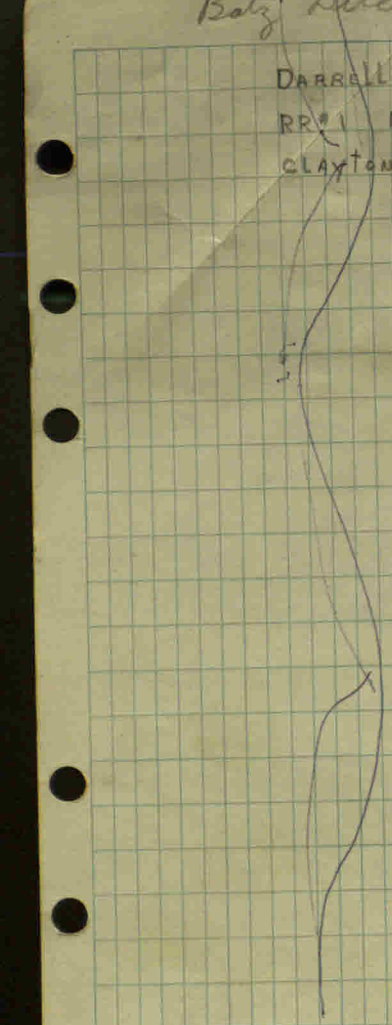
Lf	Rt
8.55	6.90
11.49	11.60

top of East headwall on SW corner

Batz Hitch

123

DARRELL A. WRIGHT
RR #1 BOX 117
CLAYTON, INDIANA



6-12-61 Sunny hot 1:00-4:00

124

STA	+	I	−	elev.
BM#1				200.00
	8.08	208.08		
⊙			0.53	
				207.55
	5.32	212.87		
⊙			4.61	
				209.26
	9.84	218.10		
⊙			5.89	
				212.21
	6.75	218.96		
⊙			5.38	
				213.58
	1.91	215.49		
BM#2			6.26	
				209.23
	9.32	218.55		
⊙			6.04	
				212.51
	7.89	220.40		
⊙			6.10	
				214.30
	4.15	218.45		
⊙			3.82	
				214.63

125

BM#2		5.24	109.25	

6-19-61 SUNNY - WARM 1:30-4:00

127

STA	+	↑	−	elev
BM#1				100.00
	6.02	106.02		
⊙			1.53	
				104.49
	7.43	111.92		
⊙			4.00	
				107.92
	5.02	112.94		
⊙			5.25	
				107.69
	5.67	113.36		
⊙			4.18	
				109.18
	8.17	117.35		
⊙			3.55	
				113.80
	~~4.57~~ 4.57	118.37		
⊙			5.66	112.71
	5.59	118.30		
⊙			4.73	113.57
	5.38	118.95		##
⊙			7.83	
~~⊙~~				111.12
	3.37	114.49		

129

	4.41	113.31		
⊙			5.08	
				108.23
	6.72	114.95		
⊙			5.76	
				109.19
	4.99	114.18		
⊙			3.69	
				110.49
	1.27	111.76		
BM#2			3.85	107.91

6-16-61 HAZY - WARM 2:00 - 4:00

131

STA	+	π	−	elev.
BM#2	~~5.95~~			100.00
	5.95	105.95		
⊙			1.46	
				104.49
	3.35	107.84		
⊙			3.44	
				104.40
	7.00	111.40		
⊙			5.85	
				105.55
	3.98	109.53		
⊙			6.06	
				103.47
	6.04	109.51		
⊙			4.59	
				104.92
	5.69	110.61		
⊙			5.04	
				105.57
	8.83	114.40		
⊙			6.14	
				108.26
	5.17	113.43		
⊙			4.53	
				108.90

133

STA	+	π	−	elev.
	1.71	204.46		
BM#1			5.94	198.52

STA	+	π	−	elev
BM#2			6.27	207.39
	5.35	212.69		
⊙			3.44	
				209.25
	7.90	217.15		
⊙			5.46	
				211.69
	4.55	216.24		
⊙			5.34	
				210.90
	5.45	216.35		
⊙			5.27	
				211.08
	4.66	215.74		
⊙			8.38	
				207.36
	4.45	211.81		
⊙			5.94	
				205.87
	5.80	211.67		
⊙			5.22	
				206.45
	4.31	210.76		
⊙			8.01	
				202.75

STA	+	π	−	elev
	5.37	221.93		
⊙			6.27	
				215.66
	5.51	221.17		
⊙			4.50	
				216.67
	4.73	221.40		
⊙			7.71	
				213.69
	4.67	218.36		
⊙			5.58	
				212.78
	4.18	216.96		
⊙			6.05	
				210.91
	5.86	216.77		
⊙			3.79	
				212.98
	5.62	218.60		
⊙			7.22	2
				211.38
	3.79	215.17		
⊙			3.30	
				211.87
	1.74	213.61		

STA	+	π	−	elev.
	3.27	220.98		
BM#4			2.00	218.98
	3.77	222.75		
⊙			3.18	
				219.57
	3.18	222.75		
⊙			3.02	
				219.73
	5.39	225.12		
⊙			7.70	
				217.42
	1.51	218.93		
⊙			4.69	214.24
	3.75	217.99		
⊙			4.72	213.27
	4.94	218.21		
BM#3			2.91	215.30
	3.71	219.01		
⊙			1.78	217.23
	4.05	221.28		
⊙			4.72	216.56

STA	+	π	−	elev.
	4.50	228.84		
⊙			4.88	
				223.96
	4.73	228.69		
⊙			3.82	
				224.87
	1.91	226.78		
⊙			4.40	
				222.38
	2.91	225.29		
⊙			2.51	222.78
	2.23	225.01		
BM#5			4.06	220.95
	5.54	226.49		
⊙			6.47	
				220.02
	4.37	224.39		
⊙			5.67	
				218.72
	5.47	224.19		
⊙			6.12	
				218.07
	5.39	223.46		
⊙			5.75	217.71

6-15-61 cloudy - cool 8:00 - 4:00

143

STA	+	π	−	elev
BM#7				225.54
	3.10	228.64		
⊙			4.20	
				224.44
	8.77	233.21		
⊙			7.37	
				225.84
	4.55	230.39		
⊙			4.54	
				225.85
	4.00	229.85		
⊙			6.02	223.83
	6.05	229.88		
⊙			5.66	
				224.22
	6.69	230.91		
⊙			7.53	223.38
	5.52	228.90		
⊙			4.75	
				224.15
	4.69	228.84		
BM#6			4.50	
				224.34

145

STA	+	π	−	elev.
⊙			4.30	
				223.69
	4.41	228.10		
BM#7			2.56	225.54

Kenny Steve Darrell 146

6-14-61 Cloudy - WARM 11:00 - 2:30 147

STA	+	π	−	elev.
BM# 9				228.02
	6.27	234.29		
⊙			2.88	
				231.41
	4.49	235.90		
⊙			5.03	
				230.87
	4.47	235.34		
⊙			6.73	
				228.61
	1.36	229.97		
⊙			4.21	
				225.76
	3.55	229.31		
⊙			5.09	
				224.22
	4.43	228.65		
BM#8			4.05	224.60
	3.30	227.90		
⊙			3.39	224.51
	4.12	228.63		
⊙			5.23	
				223.40
	4.59	227.99		

Nail in W side of N tree of two ash trees appear Station 234 S18 T17N R2E

SW wing of abutment at the start of ditch, about 3' above water level. S18 T17N R2E

STA	+	T	−	elev.
	2.81	228.20		
BM#8			3.55	
				(229.65)
	3.70	228.35		
⊙			4.11	229.24
	5.08	229.32		
⊙			4.00	225.32
	9.50	234.82		
⊙			3.46	231.36
	4.93	236.29		
BM#9			8.27	
				(228.02)

SW wing of bridge, next to railing,
1200' E of SW corner S 18 T 17N
R 2E

STA	+	π	−	elev.
⊙			4.88	
				225.98
	7.33	233.31		
⊙			8.79	224.52
	4.44	228.96		
BM#7			3.28	225.68
	3.28	228.96		
⊙			4.38	
				224.58
	8.51	233.09		
⊙			7.21	
				225.88
	4.10	229.98		
⊙			5.14	
				224.84
	8.67	233.51		
⊙			5.01	~~228.50~~
				228.50
	2.04	230.54		
⊙			3.96	~~226.58~~
				226.58
	4.43	231.01		
⊙			5.62	
				225.39

Nail in ash tree 1½' in diameter on W side of track. Approx. Station 161

NW wing of bridge next to railing. E 1200' from W section line, and on road between NW¼ & SW¼ of S17 T17N R2E

STA	+	↗	−	elev.
BM #5			4.99	221.39
	6.00	227.39		
⊙			4.99	~~228.38~~
				223.40
	3.46	225.86		
⊙			1.10	~~224.76~~
		~~229.03~~		~~225.24~~
	4.27	~~228.3~~		
⊙			4.81	
				224.22
	5.45	229.67		
BM # 6			5.05	224.62
	4.95	229.57		
⊙			5.84	
				223.73
	4.84	228.57		
⊙			2.68	
				225.89
	3.74	229.63		
⊙			4.75	
				224.88
	4.06	228.94		
⊙			3.21	
				225.73
	5.13	230.86		

Recorded on previous page.

Nail in SE side of 3½' in diameter beach tree approx Station 134. S 30 T17N R2E

16'00
3'00
2.90

6-13-61 Sunny - hot! 8:00 - 5:00

STA	+	I	−	elev.
BM #3		~~218.48~~		~~216.06~~
	2.42	~~218.46~~		216.06
⊙			2.77	
		~~219.29~~		~~215.71~~
	3.58	~~219.27~~		~~215.69~~
⊙			3.82	~~215.47~~
		~~222.30~~		~~215.45~~
	6.83	~~222.28~~		
⊙			1.88	~~220.42~~
		~~224.20~~		~~220.40~~
	3.78	~~224.18~~		
⊙			4.11	~~220.09~~
		~~223.86~~		~~220.07~~
	3.27	~~223.84~~		
BM #4		~~222.30~~	3.81	~~219.55~~ ~~219.53~~
	2.75	~~222.28~~		
⊙			2.22	~~220.08~~
		~~225.28~~		~~220.06~~
	5.20	~~225.26~~		
⊙			5.04	~~220.24~~
		~~224.93~~		~~220.22~~
	4.69	~~224.91~~		
⊙			2.06	~~222.87~~
		~~226.38~~		~~222.85~~
	3.51	~~226.36~~		

SW wing of bridge, next to the railing.
Approx 300' W of the section line between
the 25th and 30th sections, T17N R2E

STA	+	T	−	elev.
	5.39	220.02		
①			2.26	
				217.76
	5.19	222.95		
①			5.28	
				217.67
	6.09	223.76		
①			4.18	
				219.58
BM #3	3.65			216.09

King Star Road

SW wing of bridge next to the railing.
SW corner S 31 T 17N R 2E

SW wing of bridge, next to the railing.
approx. 800' E of SW corner of NE 1/4
S 36 T 17N R 2E

Oct 31, 1961 159

Griswold Road

Start 1 mile N of

10th St. & run N for

1 mile from Wall St. to 30th St

Stop B.M.#2

Nov. 1, 1961

~~Stop~~

Start B.M.#2

Stop & Finish 53+50

160

Sta	+S	H	-S	Elev.
B.M. #1	3.29	103.29		100.00
0+00				
2+00				
4+00				
⊙	4.20	103.31	4.18	99.11
6+00				
8+00				
10+00				
⊙	7.86	105.57	5.60	97.71
12+00				
14+00				
16+00				

161

N ↑ — S

Ditch Elev	Ditch Bottom	Sta Elev	Sta Top
96.19	7.10	~~7.10~~ 96.29	~~5.90~~ 5.00
98.10	5.19	99.55	3.74
99.00	4.29	100.04	3.25
			~~3.60~~
98.61	4.70	99.71	3.60
97.68	5.63	98.95	4.36
97.22	6.09	98.31	5.00
98.95	6.62	99.97	5.60
99.84	5.73	101.37	4.20
101.59	3.98	103.95	2.62

Sta	+S	℄	-S	Elev.
⊙	4.15	106.37	3.35	102.22
18+00				
20+00				
22+00				
⊙	4.34	105.27	5.99	100.93
24+00				
26+00				
28+00				
30+00				
⊙	4.69	106.14	3.82	101.45
32+00				
34+00				

↑ N — -S

Ditch Elev	Ditch Bottom	Stk Elev	Stk Top
101.93	4.98	102.94	3.38
100.77	5.60	102.22	4.15
100.17	6.20	101.78	4.59
99.57	5.70	101.13	4.14
99.62	5.65	100.78	4.49
100.26	5.01	101.96	3.31
100.77	4.50	102.22	3.05
100.59	5.55	101.84	4.30
101.00	5.14	102.16	3.98

164

Sta	+S	℄	-S	Elev
36+00				
38+00				
⊙	7.67	110.52	3.29	102.85
40+00				
42+00				
B.M #2	3.08	109.19	4.41	106.11
44+00				
46+00				
⊙	5.97	108.86	5.80	103.39
48+06				
49+56				
50+36				

165

Ditch ↑N

Sta		Elev	Sta	
Elev	8.40m		Elev	9.0m
100.58	5.56		101.70	4.44
101.88	4.26		103.34	2.80
104.03	C.99		105.21	5.31
105.38	5.14		106.52	4.00
104.04	5.15		104.82	4.32
103.44	5.75		104.44	4.70
103.32	5.54		104.12	4.74
103.57	5.29		104.20	4.66
103.98	4.88		104.65	4.21

Sta	+S	H	-S	Elev
52+00				
⊙	5.55	109.55	4.86	104.00
53+50				

Ditch

Elev Bottom		Elev Top	
103.39	5.52	109.81	4.05
104.04	5.51	105.18	4.37

170

Sta	+	Π	−	elev
BM				740.00
	0.92	740.92		
			12.51	728.41
	1.11	729.52		
11+75				
			1.11	728.41
	11.59	740.00		
11+50				
11+25				

171

top of railing on S side, the east end

1+00	0+95	0+90	0+83	0+72
6.02	7.90	8.20	7.68	7.75
723.50	721.62	721.32	721.84	721.77

1+00	0+93	0+89	0+86	0+81	0+68	0+64
8.32	9.19	10.17	9.16	8.80	3.82	3.25
731.68	730.81	729.83	730.59	731.20	736.18	736.75

0+59
2.02
737.32

1+00	0+91	0+88	0+85	0+80	0+68	0+61
0.20	6.29	7.21	6.29	5.91	3.36	2.76
739.80	733.76	732.79	733.71	734.09	736.64	737.29

11+00				
10+75				
TP			3.27	736.73
	8.47	745.20		
10+50				
10+25				
10+00				

1+00	0+98	0+90	0+87	0+84	0+71	0+64
-.50	0.00	5.10	6.02	5.12	3.01	2.68
740.50	740.00	739.90	733.98	739.88	736.99	737.32

1+00	0+94	0+88	0+84	0+76	0+66
0.51	2.63	5.82	3.70	2.88	2.67
739.49	737.37	739.18	736.30	737.12	737.33

1+00	0+88	0+86	0+84	0+79	0+65
2.75	10.27	10.93	9.95	9.19	7.89
742.15	739.93	739.27	735.25	737.01	737.31

1+00	0+85	0+83	0+81	0+75	0+65
1.62	9.87	10.95	9.23	8.30	7.85
743.58	736.23	734.25	735.97	736.90	737.35

1+00	0+85	0+83	0+80	0+79	0+65
0.87	9.15	10.63	9.22	8.29	7.85
749.33	736.05	739.57	735.98	736.91	737.35

174

Sta	+	HI	−	elev
9+75				
BM				740.00
	1.67	741.67		
			A.14	737.23
	8.75	745.98		
9+50				
9+25				
9+00				
8+75				

175

1+00	0+89	0+82	0+80	0+79	0+65
0.68	9.25	10.81	9.39	8.29	7.81
744.52	735.95	739.39	735.86	736.91	737.39

1+00	0+97	0+89	0+82	0+80	0+79	0+66
1.16	1.00	9.93	11.10	9.94	8.86	8.50
744.82	744.98	736.05	739.88	736.09	737.12	737.48

1+00	0+98	0+89	0+82	0+80	0+75	0+66
1.17	1.85	9.59	11.19	9.53	8.90	8.47
744.51	744.13	736.39	739.79	736.45	737.08	737.51

1+00	0+98	0+89	0+82	0+80	0+75	0+66
1.57	1.87	9.39	10.91	9.50	8.77	8.43
744.91	744.11	736.59	735.07	736.38	737.21	737.55

1+00	0+98	0+89	0+82	0+80	0+75	0+66
1.50	1.80	9.52	10.78	9.27	8.71	8.28
744.98	744.18	736.52	735.20	736.71	737.27	737.70

176

Sta	+	π	−	elev
8+50				
8+25				
8+00				
7+75				
7+50				
TP			7.16	738.52
	8.87	747.39		
7+25				

177

1+00	0+97	0+89	0+82	0+80	0+75	0+66
1.72	1.96	9.30	10.51	9.06	8.62	8.19
749.26	749.02	738.68	737.47	738.92	737.36	737.89

1+00	0+97	0+89	0+82	0+80	0+75	0+66
1.56	1.86	8.68	10.66	8.89	8.49	8.09
749.42	749.12	737.30	735.32	737.09	737.49	737.99

1+00	0+97	0+82	0+81	0+80	0+74	0+66
1.44	1.96	9.72	10.29	8.90	8.27	7.89
749.54	749.02	736.26	735.69	737.08	737.71	738.09

1+00	0+97	0+83	0+81	0+80	0+75	0+65
1.36	1.75	9.18	10.96	8.79	8.20	7.69
749.62	749.23	736.80	735.53	737.19	737.78	738.29

1+00	0+97	0+84	0+82	0+80	0+74	0+65
1.16	1.65	8.80	10.11	8.62	8.03	7.96
749.82	749.33	737.18	735.87	737.36	737.95	738.52

1+00	0+96	0+84	0+82	0+80	0+73	0+65
2.91	3.21	10.45	11.51	10.03	9.23	9.71
749.98	749.68	738.95	737.89	739.36	738.16	737.68

Sta	+	R	-	elev
7+00				
6+75				
6+50				
6+25				
6+00				
5+75				

1+00	0+97	0+85	0+82	0+80	0+73	0+69
2.44	2.78	9.20	11.55	10.18	9.06	8.50
749.95	749.61	738.19	735.84	737.21	738.33	738.89

1+00	0+97	0+84	0+82	0+80	0+74	0+69
2.16	2.82	9.58	11.13	9.64	8.88	8.36
745.23	749.57	737.81	736.26	737.75	738.51	739.09

1+00	0+96	0+85	0+83	0+80	0+73	0+63
2.72	3.34	9.28	10.84	9.50	8.61	8.10
749.67	749.05	738.11	736.55	737.89	738.78	739.29

1+00	0+ 94	0+85	0+83	0+80	0+73	0+63
3.56	4.20	9.31	11.00	9.52	8.40	7.92
742.93	743.18	738.98	736.39	737.87	738.99	739.47

100	0+96	0+85	0+83	0+81	0+71	0+62
4.95	4.51	9.83	10.98	9.54	8.28	7.63
743.94	743.88	738.06	736.99	737.84	739.11	739.76

1+00	0+96	0+85	0+83	0+81	0+71	0+62
4.50	5.00	8.90	10.71	9.19	8.19	7.97
742.89	742.39	738.49	736.68	738.25	739.25	739.92

Sta.	+	T	−	elev
5+50				
5+25				
~~5+11~~				
5+00				
BM#2			5.98	741.91
	2.65	744.06		
4+75				

1+80	0+96	0+85	0+81	0+79	0+70	0+60
4.62	5.01	9.23	10.92	8.63	7.86	7.16
742.77	742.38	738.16	736.97	738.76	739.53	740.23
1+00	0+93	0+89	0+82	0+78	0+70	0+69
5.98	8.16	9.03	10.36	8.38	7.68	7.18
741.91	739.23	738.36	737.03	739.01	739.71	740.29
0+60						
6.83						
740.56						
1+00	0+90	0+86	0+83	0+81	0+70	0+60
6.88	7.30	8.08	10.23	8.29	7.16	6.58
740.51	740.09	739.31	737.16	739.10	740.23	740.80
1+23	1+00	0+94	0+90	0+88	0+85	0+76
2.99	4.13	9.63	5.73	6.26	4.98	3.95
741.07	739.93	739.43	738.33	737.81	739.08	740.11
0+66	0+57					
3.53	2.91					
740.53	741.15					

4+50				
			2.65	741.91
	7.52	748.93		
5+00				
5+25				
5+50				
5+75				
6+00				

Rt In of culvert

1+45	1+11	1+08	1+06	1+00	0+89
3.03	4.86	5.87	4.77	3.89	2.66
741.03	739.20	738.19	739.29	740.17	740.40

1+25	1+50	1+75	2+00	2+25
7.66	6.04	5.11	5.19	4.37
741.27	742.89	743.82	743.74	744.56

1+25	1+50	1+75	2+00	2+25
6.65	5+69	4.32	3.99	4.19
742.28	743.29	744.61	744.94	744.79

1+25	1+50	1+75	2+00	2+25
5.93	4.70	3.72	3.60	4.07
743.58	744.23	745.21	745.33	744.86

1+25	1+50	1+75	2+00	2+25
5.13	4.35	3.88	3.35	3.55
743.80	744.58	745.05	745.58	745.38

1+25	1+50	1+75	2+00	2+25
5.36	4.50	3.95	3.80	3.62
743.57	744.43	744.98	745.10	745.31

6+25

6+50

6+75

7+00

7+25

7+50

1+25	1+50	1+75	2+00	2+25
4.61	4.00	4.09	4.18	3.80
744.32	744.93	744.84	744.75	745.13

1+25	1+50	1+75	2+00	2+25
4.00	3.70	4.03	4.10	3.86
744.93	745.23	744.90	744.83	745.07

1+25	1+50	1+75	2+00	2+25
3.98	3.63	3.83	3.95	4.02
744.95	745.30	745.10	744.98	744.91

1+25	1+50	1+75	2+00	2+25
3.90	4.00	3.87	3.82	3.89
744.95	744.93	745.06	745.11	745.04

1+25	1+50	1+75	2+00	2+25
3.96	4.00	3.90	3.87	3.81
744.97	744.93	745.03	745.06	745.12

1+25	1+50	1+75	2+00	2+25
4.16	3.91	3.73	3.74	3.79
744.78	745.02	745.20	745.19	744.99

7+75				
TP			4.23	744.70
	4.43	749.13		
8+00				
8+25				
			4.63	744.50
	4.78	749.28		
8+50				
8+75				
9+00				

1+25	1+50	1+75	2+00	2+25
4.35	4.05	3.86	4.16	4.07
744.58	744.88	745.07	744.77	744.86

1+25	1+50	1+75	2+00	2+25
4.64	4.75	4.70	4.96	4.93
744.99	744.38	744.93	744.67	744.70

1+25	1+50	1+75	2+00	2+25
4.93	4.92	4.60	4.83	4.78
744.20	744.21	744.53	744.30	744.35

1+25	1+50	1+75	2+00	2+25
5.03	4.95	5.04	4.91	4.74
744.25	744.33	744.24	744.37	744.54

1+25	1+50	1+75	2+00	2+25
5.01	5.08	4.94	5.31	5.91
744.27	744.20	744.34	743.97	743.87

1+25	1+50	1+75	2+00	2+25
5.07	5.28	5.24	5.26	5.23
744.21	743.99	743.94	744.02	744.05

9+25				
9+50				
9+75				
10+00				
TP			4.72	749.56
	1.65	746.21		
10+25				
10+50				

1+25	1+50	1+75	2+00	2+25
5.00	5.25	5.32	5.47	5.37
744.28	744.03	743.98	743.81	743.91

1+25	1+50	1+75	2+00	2+25
4.89	5.15	5.56	5.51	5.35
744.39	744.13	743.72	743.77	743.97

1+25	1+50	1+75	2+00	2+25
5.70	5.13	5.51	5.62	5.70
743.58	744.15	743.77	743.66	743.58

1+25	1+50	1+75	2+00	2+25
4.50	4.65	5.47	5.33	6.35
744.78	744.63	743.81	743.95	742.93

1+25	1+50	1+75	2+00	2+25
2.20	2.116	2.59	3.36	4.10
744.01	744.05	743.62	742.85	742.11

1+25	1+50	1+75	2+00	2+25
2.76	3.36	3.83	4.14	4.18
743.45	742.85	742.38	742.07	742.03

10+75					
~~11+~~					
11+00					
11+25					
TP			2.69	743.52	
	3.15	746.67			
11+25					
11+50					
11+75					

1+25	1+50	1+75	2+00	2+25
5.75	5.39	5.27	4.30	3.79
740.46	740.82	740.94	741.91	742.42

1+25	1+50	1+75	2+00	2+25
4.99	4.30	3.52	3.41	3.80
741.22	741.91	742.69	742.80	742.41

1+25	1+50	1+75
5.60	3.95	in house
740.61	742.26	

2

2+00	2+25
3.65	3.62
743.02	743.05

1+25	1+50	1+75	2+00	2+25
12.28	8.30	4.28	3.87	3.65
734.39	738.37	742.39	742.85	743.02

~~1+25~~	~~1+50~~	~~1+75~~	2+00	2+25
			5.25	4.31
			741.92	742.86

192

TP			12.12	734.65	
	5.25	739.80			
11+75					

193

1+25	1+50	1+75
12.60	9.69	3.69
727.20	730.11	736.11

CO. LINE ROAD
S. PLAINFIELD

5-31-62
CLEAR WARM
Lee [illegible] Larry

STA	+	HI	−	ELEV.
BM.	9.61	109.61		100.00
TP			0.14	109.47
	3.20	112.67		
TP			7.00	105.67
	3.32	108.99		
TP			12.18	96.81
	1.66	98.47		
TP			12.50	85.97
	2.17	88.14		
TP			11.85	76.29
	2.70	78.99		
BM 2		?	1.59	77.40
BM 2	1.60			
TP			2.10	
	12.45			
TP			1.54	
	10.00			
TP			1.50	
	8.96			

Spike 2.8' Above Ground in Telephone pole
N. Side at STA 100+00

Spike 2.5' Above Ground N. Side Tel Pole
STA 16+85

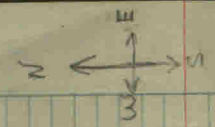
198

STA	+	⊼	−	ELEV
TP			1.45	
	7.80			
TP			2.45	
	5.95			
TP			11.25	
	1.64			
BM'			5.51	

CO. LINE Road CLEAR & WARM 64-62 200

Lee ⊼ STEVE GEN LATTY

STA	+	⊼	−	ELEV.
BM.	4.31	104.31		100.00
STA 100				
02+00				
TP			1.15	103.16
	9.90	113.06		
03+00				
04+00				
04+35				
TP			2.24	110.82
	2.77	113.59		



-11	-7'	℄	+18.9'	+10.7'	+11.7'	+13'	+29'	+30'		
6.71	6.85	6.51	6.84	6.99	7.72	6.96	2.53			
97.60	97.46	97.77	97.47	97.32	96.59	97.41	101.78	105.52		
-30'	-20'	-15'	9.4'	℄	+6.6'	+7.8'	+11.8'	+12.9'	+19.7'	+25'
7.90	5.99	4.68	4.06	3.84	3.82	3.95	4.91	3.87	1.45	
96.91	98.87	99.63	100.25	100.47	101.19	100.46	99.40	100.44	103.82	103.72
-38'	-26'	-15.1'	-10.4'	℄	+7'	+11.2'	+16.9'	+26'	36'	
10.66	11.05	9.21	9.31	7.71	8.05	8.51	7.04	5.65	1.79	
102.40	102.01	103.85	104.75	105.35	105.01	104.55	106.02	107.41	108.12	
-22'	-16'	-9.4'	℄	+7.2'	+12'	+13'	+18'	+25'	+35'	
3.01	3.18	3.08	2.60	2.79	2.40	3.37	2.31	1.91	1.89	
110.34	109.77	109.87	110.46	110.32	110.26	109.69	110.72	111.15	111.22	
-20'	-18'	-8'	℄	+7.6'	+10'	+12'	+22		+32	
3.80	3.42	2.30	1.76	2.00	2.19	2.79	0.75		1.20	
109.36	109.69	110.76	111.30	111.06	110.87	110.27	112.31		111.82	

STA	+	X	-	ELEV.
05+00				
06+00				
TP			6.40	107.19
	2.93	109.62		
07+00				
08+00				
09+00				
TP			4.51	105.11
	6.65	111.76		
10+00				

-28'	-16.8'	-9'	℄	+7'	+12'	+20'	+35'
4.90	3.69	3.16	2.73	2.72	2.81	1.35	1.29
104.19	104.90	105.43	105.86	105.87	105.78	107.26	107.30

-26'	-17'	+9'	℄	+6.5'	+10'	+18'	30'
6.89	6.01	4.94	4.06	4.89	5.59	1.85	1.42
106.70	107.58	108.65	108.93	108.70	108.50	111.74	112.17

-24'	-17'	-9'	℄	+7'	+10'
5.31	4.95	4.54	4.35	4.73	5.23
104.31	104.67	105.08	105.27	105.09	104.39

-15'	-9'	℄	+6'	+9'	+12'
10.34	6.02	5.51	5.75	6.32	6.75
99.28	103.60	104.11	103.87	103.30	102.87

-35'	-12'	℄	+6'	+10'	+24'	40'
5.60	4.70	4.51	4.68	4.91	6.49	9.00
104.02	104.92	105.11	104.93	104.71	101.13	100.62

-24'	-15'	-9'	℄	+7'	+9'	+13	+25'	+40'
7.99	5.87	5.50	5.19	5.37	5.70	4.97	6.39	6.19
109.32	105.89	106.24	106.57	106.39	106.06	106.79	105.37	105.57

204

STA.	+	⊼	→	ELEV.
11+00				
TP			5.90	106.36
	2.89	109.25		
12+00				
13+00				
TP			4.69	109.56
	2.59	107.15		
13+70				
14+00				
15+00			11.65	95.50
TP	1.89	97.39		

205

S E N

-26'	-15'	-11'	-10'		+7'	+12'	+15'	+21'	+40'
8.02	7.25	6.17	5.86	5.22	5.34	5.74	5.25	8.24	7.95
103.74	104.51	105.59	105.90	106.54	106.42	106.02	106.51	103.52	104.31

-24'	-9'			+7'	+8	+9'	+30'	+46'
3.99	3.13		3.02	3.30	3.45	2.60	4.77	4.95
105.26	106.12		106.25	105.95	105.79	106.65	104.28	104.30

+23	-18'		+7'	+9'	+15'
3.73	1.31		4.25	4.51	5.18	2.89
105.52	104.99		105.00	104.74	104.07	106.91

-15'	-9'		+7'	+13'	+30'
0.77	2.66		2.39	2.74	2.71	3.19

-18'	-9'		+7'	+9'	+15'	+30'
2.41	3.54		3.79	4.15	3.70	2.49	2.99

-13'	-11'	-9'		+7'	+8'
11.92	12.50	11.79	11.65	11.95	12.15

206

STA	+	℄	−	ELEV
TP			9.25	98.14
	0.09	98.23		
16+00				
TP			11.66	76.57
	2.84	79.41		
17+00				
17+27				
TP			2.21	77.20
	10.05	47.25		
TP			0.45	86.80
	10.45	97.65		
TP			0.69	96.96
	11.00	107.96		
T.P.			0.29	107.67
	8.20	115.87		

207

℄

-18'	-14'	-13'	-11'	-9'	℄	+8'	+11'	+14'
1.60	3.70	5.02	3.02	3.15	2.98	3.30	4.91	2.10

-30	-8'	+9'	+30
5.64	4.93	4.94	5.42	6.99

-10'	+10'
6.40	6.50	6.79

208

STA	+	℄	−	ELEV
TP			8.20	107.67
	1.53	109.20		
TP			11.10	98.10
	0.33	98.43		
TP			11.71	86.72
	0.01	86.73		
B.M.2		78.17	8.56	

16 22

210

Sta	+	℄	−	Elev
BM2	10.24	87.64		77.40
0			0.41	87.23
	11.63	98.86		
	~~12.13~~ ~~+0.59~~	~~110.60~~ ~~+13~~	0.39	98.47
13+00				
0			6.47	104.13
	7.26	111.39		
13+70				
19+00				
0			4.04	107.35
	3.86	111.21		
0			6.56	104.65
	3.49	108.14		
15+00				
15+67				

↖ Break on 267

211

S ℄ N

Driveway to House

110.60
6.47
104. 3

-50 +40 +50
4.52 4.99 5.20

-50 -45 -25' -16 -11 +40 +50
5.78 5.31 4.72 4.78 7.84 8.11 8.87

-45' -18 -11 -9 +7 +13 +35' +50
5.82 4.36 9.04 8.61 8.72 8.95 7.48 7.73 8.34

-50 -35 -25 +25 +35 +50
4.30 4.02 3.44 5.64 5.04 5.38

-45 -40 -30 +30 +40 +53
5.77 5.58 5.41 6.84 6.69 6.72

Sta.	+	H	−	Elev	212
①			4.68	103.46	
	0.98	104.44			
15+00					
①			11.82	92.62	
	1.57	94.19			
15+69					
①			12.41	81.78	
	5.25	87.03			
~~16+00~~					
①			7.37	~~86.66~~	
	7.87	94.53			
16+00					
①			11.10	83.43	
	3.10	86.53			
BM 2			9.11	77.42	

N 50' Sor ℄ ℄ 15+25 House S.
S 65 " " 15+30 " N.
213

S N

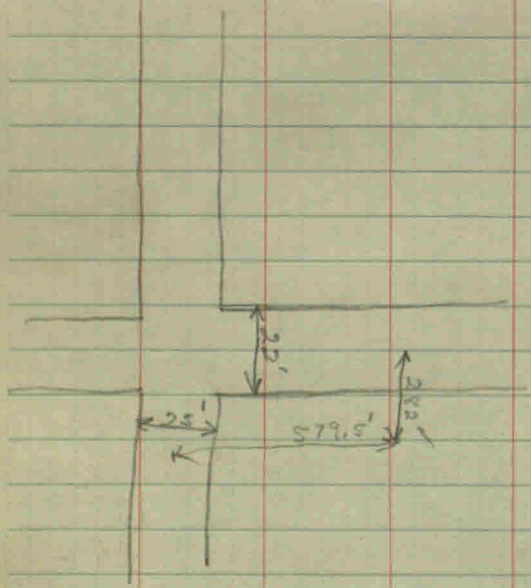
		-8		+8		
-		9.85	9.50	10.31		
		-8	℄		+8	
		6.27	6.48		6.63	
	-50	-40	-30	+25	+35	
	1.85	2.12	1.25	4.84	2.59	

Terre Haute 6-12-62

Power Poles

216

PSC 900 2027 OF I

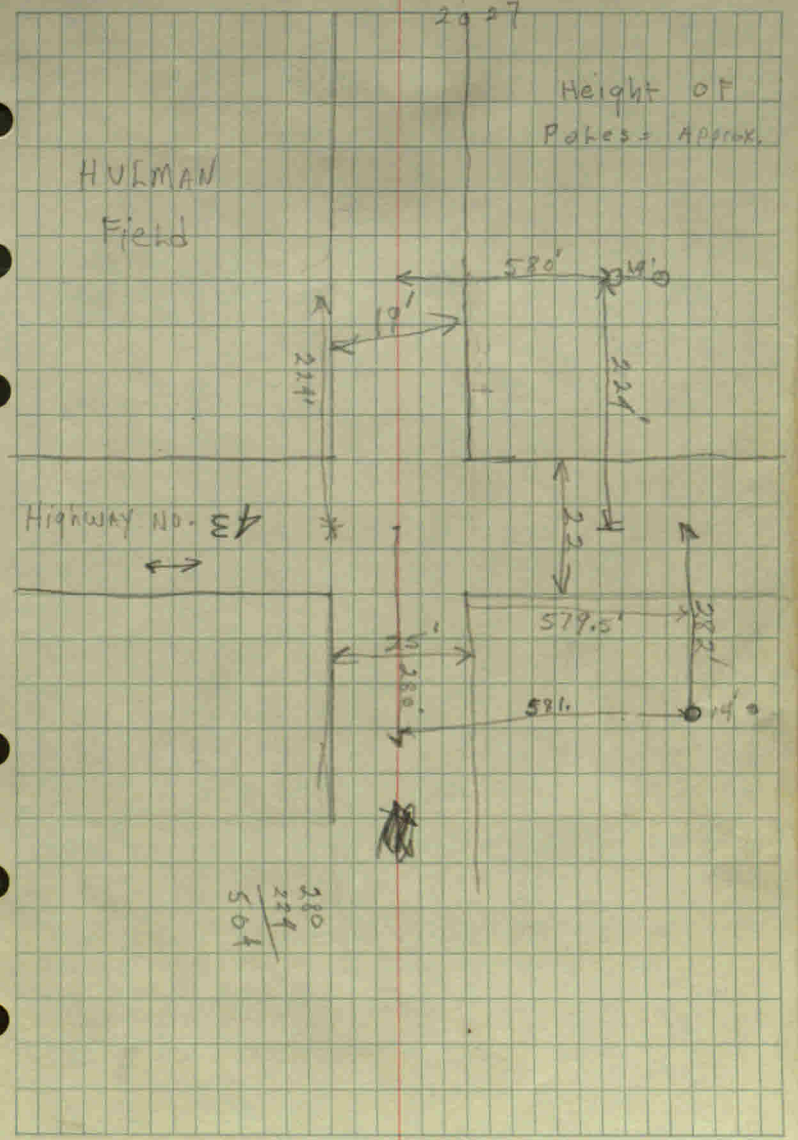


OSO

PSC OF IND INC 900 2027

217

Height of Poles = Approx.



Sta	+	π	−	elev
BM#3				97.19

≤ end of RR. culvert

222

Tie downs
30'

IN ducts OR Buried CABLE — Buried

How many? 8 How many OUT OF Weather IN or CABLEN Cab

Telephone CABLES → NO
IN duct or cable

FAA Gen.
2 LLS Control
2 LLS Power Circuit

5 ~~new~~ circuits (10 wires)

12 - 4" Ducts under TAXIWAY
Needs At least 3 more (Approx 20)
Buried IN Layers EXTEND 5' Each
Side TAXIWAY

Job 56-142

4-16

1-14-57

STA	+	=	−	elev.
BM# 1				(100.00)
	5.00	105.00		
⊙			4.03	100.97
	5.94	106.91		
⊙			3.54	103.37
	6.17	109.54		
BM# 2			1.94	(107.90)
	5.27	113.17		
⊙			4.25	108.92
	5.93	114.85		
⊙			4.15	110.70
	5.71	116.41		
BM# 3			4.35	(112.06)
⊙			4.30	112.11
	4.94	117.05		
⊙			4.13	112.92

N corner of culvert on West side of Gulf Drive

telephone pole on N side of road sta 9+80

power pole on N side of road sta 19+25

STA	+	HI	−	elev.
	5.58	118.50		
BM#4			2.91	(115.59)
⊙			5.52	112.98
	2.77	115.75		
⊙			7.08	108.67
	0.07	108.74		
BM#5			4.96	103.78
BM#5	4.96	108.74		103.78
⊙			0.99	108.20
	7.26	115.56		
⊙			2.38	113.18
	5.22	118.40		
BM#4			2.82	(115.58)
⊙			5.54	112.86

power pole N side of road Sta 29+00

228

STA	+	I	−	elev.
	4.00	116.86		
0			4.66	112.20
	4.19	116.39		
BM#3			4.34	112.05
0			5.78	110.61
	4.08	114.69		
0			5.76	108.93
	4.12	113.05		
BM#2			5.15	107.90
	1.99	109.89		
0			6.47	103.37
	3.75	107.12		
0			6.16	100.96
	4.59	105.53		
BM#1			5.52	100.01

230

STA	+	I	−	elev.
BM#1				100.00
	5.33	105.33		
2+00				
1+00				
0+41				
BM#1				100.00
0+00	5.32	105.32		

99.41	99.45	97.31	98.06	98.78	98.91	98.83
22.0	10.0	11.0	16.0	16.0	6.0	10.0
6.84	5.30	7.71	7.19	6.17	6.31	6.10

98.53	97.66	98.71	98.82
15.0	9.5	25.0	23.0
6.73	7.59	6.54	6.13

100.45	100.40	98.04	98.89	99.31	99.69	99.59
25.0	14.0	17.0	14.0	9.5	8.0	9.5
4.80	4.95	7.21	6.36	5.49	5.61	5.66

99.19	98.73	99.25	99.46
17.0	17.0	21.0	25.0
6.06	6.57	7.00	5.79

99.99	99.99	100.19	100.10
0.0	10.0	24.0	50.0
5.26	5.26	5.06	5.15

0+00

0+82

1+00

2+00

0 4.84 100.96

6.43 107.59

100.51 100.37 98.65 99.85 100.19 100.38 100.05

99.41 98.68 96.70 98.49 99.37

100.38 100.37 101.06 101.29

REVERSE ORDER

98.96

100.77 100.91 99.57 100.30 100.57 100.16

100.04 99.59 97.75 99.35 99.25

101.01 100.92 99.92 100.47 100.96 100.21 100.18

100.89 100.99 98.78 100.97 100.56

102.03 101.68 100.55 101.23 101.49 101.46
[illegible] 15.0 15.0 13.0 [illegible] 9.0
5.56 5.91 7.04 6.36 6.10 6.13

102.63
05.0
4.96

101.58 101.53 102.49 102.83
[illegible] 10.0 05.0 50.0
6.04 6.06 ~~4.96~~ 5.10 4.66

101.10
6.43 10" pipe south side of road

102.20 102.21 101.10 101.70 102.00 101.88
25.0 17.0 15.0 11.0 0.0 10.0
5.39 5.38 6.49 5.89 5.59 [illegible]

102.27
20.0
5.32

102.79 102.93 102.12 102.48 102.49 102.39
25.0 10.0 12.0 10.0 0.0 11.0
4.80 4.66 5.47 5.11 5.10 5.00

102.74 102.99
13.0 25.0
4.85 [illegible]

102.93 102.75 102.91 520 Reverse ORDER
0.0 10.0 25.0
4.66 4.84 4.63

0			0.00	104.00
~~5+00~~	4.33	108.33		
6+00				
7+00				
0			2.47	105.86
	4.55	110.41		
8+00				
0			3.34	107.07
	4.50	111.57		
9+00				
10+00				

103.18	102.79	103.25	102.79	103.25		
25.0	13.0	0.0	13.0	45.0		
5.15	5.54	5.00	5.54	5.05		
103.67	103.63	103.90	103.97	104.01	103.96	
25.0	13.0	0.0	13.0	12.4	25.0	
4.69	4.90	4.93	4.86	4.82	4.87	
104.71	104.64	104.86	104.94	104.93	104.96	
25.0	12.0	0.0	13.0	13.0	25.0	
5.70	5.77	5.55	5.90	5.92	5.95	
105.99	105.82	105.10	105.59	105.85	105.93	106.22
25.0	14.0	14.0	13.0	0.0	13.0	14.0
5.58	5.75	6.47	5.98	5.72	5.64	5.55
106.09						
25.0						
5.48						
107.70	106.82	105.97	106.80	107.27	106.79	107.24
25.0	12.0	14.0	13.5	0.0	13.0	14.0
3.87	4.75	5.60	4.77	4.30	4.78	4.33
107.08						
25.0						
4.94						

0			2.99	105.63
	4.32	112.95		
11+00				
BM# 3			5.10	107.85
0			5.59	108.36
	5.10	113.46		
12+00				
0			5.18	108.28
	5.17	113.45		
13+00				
14+00				
0			4.04	109.41
	5.16	114.57		
15+00				

107.75	107.50	106.69	107.23	108.20	107.69	107.67
65.0	110	150	13.0	0.0	12.0	25.0
6.80	5.91	4.76	5.32	4.25	4.96	5.27
107.25	107.69	106.85	107.86	108.29	107.81	107.69
65.0	17.0	15.0	15.0	0.0	14.0	25.0
6.0	5.32	4.81	5.0	5.17	5.45	5.27
107.50	107.29	108.39	107.93	107.84		
65.0	15.0	10.0	15.0	14.0		
5.93	6.16	6.06	5.53	5.41		
107.91	107.82	107.19	108.08	108.26	108.30	108.32
65.0	7.5	10.0	8.0	0.0	10.0	25.0
5.59	5.68	4.96	5.20	4.69	5.15	5.12
108.69	108.22	107.68	108.87	109.41	109.99	108.38
65.0	7.0	15.0	13.0	0.0	11.5	25.0
5.93	6.02	5.39	5.00	5.46	5.58	6.19

240

15+00

0 5.05 109.52

5.06 114.58

16+00

0 4.72 109.88

5.12 115.10

17+00

0 4.21 110.39

5.20 115.59

18+00

241

109.03 108.67
14.0 15.0
5.56 5.90

108.69 108.98 108.27 109.21 109.73 109.31 108.95
25.0 15.0 14.0 13.0 0.0 12.0 13.0
5.69 5.60 6.31 5.37 4.53 5.27 5.93

109.57 109.30
14.0 15.0
5.01 5.28

109.28 109.47 108.20 109.51 110.01 109.65 109.30
15.0 16.0 15.0 13.5 0.0 11.0 12.0
5.82 5.63 6.50 5.59 5.09 5.45 5.89

109.81 109.54
13.0 25.0
5.39 5.54

110.14 110.19 109.59 110.35 110.56 110.21 110.51
15.0 17.0 14.0 14.0 0.0 12.0 25.0
5.45 5.40 6.09 5.04 4.83 5.38 5.09

10

BAND 3

111.91

116.02

111.87

116.56

112.13

116.85

112.37

117.05

110.60 110.62 111.13 110.72 111.02

110.92 110.84 110.65 110.45 110.33

Reverse order

109.90

111.11 110.75 111.57 111.06 111.48

111.36 111.16 111.94 111.45 111.90

244

112.61

116.92

112.55

245

111.73 111.36 112.03 111.01 111.18

112.12 111.87 111.00

111.86 111.65 112.02 111.62 111.11

8-1-61 cloudy - warm 246

STA	+	I	−	elev
BM #3				112.05
	5.14	117.19		
0			1.49	112.70
	4.86	117.56		
24+00				
0			4.61	112.92
	5.21	118.13		
25+00				
0			5.16	112.97
	5.21	118.18		
26+00				
27+00				
0			4.45	113.73
	5.08	118.81		
28+00				

247

111.84	111.34	112.39	112.19	111.79	112.01	111.87
25.0	10.0	0.0	10.0	11.0	15.0	25.0
5.70	6.20	5.15	5.35	5.75	5.53	5.67
112.03	111.87	112.74	112.40	112.16	112.56	112.30
25.0	15.0	0.0	10.0	13.0	16.0	25.0
5.70	5.86	5.29	5.63	5.87	5.47	5.73
112.20	111.90	112.91	112.59	112.86	112.81	
25.0	14.0	0.0	11.0	14.0	25.0	
5.98	6.28	5.27	5.59	5.32	5.37	
112.47	112.08	113.14	112.63	112.82	112.78	112.88
25.0	14.0	0.0	11.0	13.0	17.0	25.0
5.71	6.10	5.04	5.55	5.36	5.40	5.30
112.95	112.68	113.36	112.92	113.86	113.49	
25.0	15.0	0.0	12.0	16.0	25.0	
5.36	6.23	5.15	5.59	4.65	5.27	

29+00

0 5.89 112.97

3.70 116.67

BM #4 1.09 115.59

30+00

30+61

31+00

31+00

0 5.70 110.97

2.12 113.09

32+00

113.87 113.66 113.23 113.88 113.56 114.91 113.95

112.97 112.92 112.71 112.96 111.74 113.75 113.10

112.45 112.35 112.28 112.03 112.28

111.84 111.78 111.57 111.81 111.39 112.47 112.06

110.93 110.51 110.11 110.98 110.96 111.66 111.99

110.09 109.56 109.21 109.84 109.97 112.07 109.38

33+39

37+70

34+69

35+00

36+00

⊙		11.45	101.69
℄	5.78	108.92	

109.96	109.21	108.92				
5.0	11.0	17.0				
3.53	3.88	4.14				
109.00	108.11	107.50	107.88	108.61	108.08	109.59
25.0	5.0	11.0	12.0	9.0	12.0	16.0
4.09	4.22	6.54	5.0	4.48	5.0	3.90

109.98
25.0
3.11

107.73	106.65	107.03				
37.0	15.0	0.0				
5.34	6.04	6.08				
107.18	106.25	106.72	106.15	107.22	107.19	
25.0	11.0	0.0	15.0	11.0	25.0	
5.91	6.51	6.27	6.44	5.92	5.90	
103.53	102.71	102.37	102.77	103.43	103.09	
4.50	15.0	14.0	10.0	9.0	11.0	
9.56	10.38	10.72	10.32	9.66	10.00	
103.27	105.89	106.64				
15.0	25.0	45.0				
9.82	7.60	6.45				

252

37+00

37+33

38+00

38+33

BM # 5 4.62 103.80

6.78 110.58

39+00

10+00

253

100.73	100.08	99.46	101.09	101.62	101.05	99.17
7.69	8.34	8.96	7.33	6.80	7.37	9.25
98.98						
101.53	101.10	101.31	101.02	101.95		
7.89	7.32	7.11	7.40	6.97		
101.08	101.25	101.69	100.98	99.67	99.59	
7.34	7.17	6.73	7.44	8.75	8.83	
102.96						
5.94						
107.46	107.73	104.98	104.58	102.44	103.12	103.27
2.72	2.45	5.20	5.60	7.74	7.06	6.91
103.08	102.07	102.66	102.80 ~~103.58~~			
7.50	8.51	7.92	7.78			
108.55	107.01	105.96	106.31	106.45	106.16	105.80
2.03	3.57	4.62	4.27	4.13	4.42	4.78

48.00

0 1.19 109.19

~~41.00~~ 3.12 115.26

41.00

42.00

106.83 106.23
6.0 25.0
3.75 3.75

109.81 109.45 108.12 108.84 108.95 109.12 108.88
25.0 17.0 19.0 12.0 9.0 2.0 3.0
5.45 5.21 7.10 6.42 0.31 4.19 1.37

108.33 109.08 108.52
11.0 15.0 25.0
6.13 4.18 3.70

110.47 110.19 109.33 110.35 110.97 110.21
37.5 25.0 19.0 10.0 0.0 2.0
8.79 5.07 5.43 4.91 4.79 5.05

109.52 110.98 110.02
11.0 17.0 25.0
5.79 4.78 5.14

BM #5	3.54 ~~3.70~~	107.32		103.78
Start 11+00				
0			3.61	103.81
	5.19	108.95		
12+00				
12+55				
0			3.36	105.59
	5.20	110.79		
13+00				

106.37 106.08 101.65 102.05 108.42 101.71 99.34
4.20 2.0 11.0 5.0 6.0 9.0 19.0
0.95 1.51 5.67 5.07 4.10 5.41 7.98

98.34
5.09
8.98

108.67 107.60 103.69 104.61 103.84 103.68 98.08
2.50 2.0 2.0 5.0 6.0 11.0 49.0
0.33 1.35 5.36 4.84 5.11 5.37 10.87

97.66
34.0
11.39

106.05 107.25 105.16 104.97
2.50 2.0 3.0 5.0
2.70 0.30 3.79 3.98

105.39 105.71 105.36 105.59 105.60 105.29 102.95
5.0 4.0 11.0 8.0 6.0 9.0 25.0
5.43 5.24 5.13 5.20 5.11 5.50 6.39

98.52
4.1
9.77

0 3.10 107.69

5.13 112.82

14+00

108.63	107.75	107.24	107.57	107.92	106.70	105.98
3.10	3.0	3.0	3.0	3.5	3.0	3.0
4.19	5.07	5.58	5.25	5.10	6.32	6.84

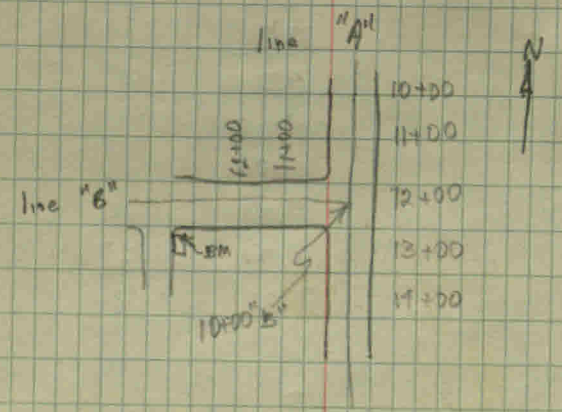
BM #5				103.78	
	3.96	107.74			
①			3.47	104.27	
	7.55	111.82			
9+00					
8+00					
7+00					

109.69	109.13	104.90	104.87	104.96	104.61	103.57
2.13	7.19	7.42	6.95	6.86	7.21	8.25
109.00						
7.72						
108.76	107.74	106.97	106.99	107.12	106.71	105.54
3.96	4.08	5.85	4.93	4.80	5.11	6.28
105.20						
6.72						
109.06	108.50	106.20	107.14	107.18	107.50	
2.76	2.37	5.02	4.68	4.69	4.37	
107.14	106.32	106.04				
4.68	5.50	5.78				

9-12-62 Lewis Lake Intersection

Sta	+	X	-	elev
BM				100.00
	8.00	108.00		
12+00 "B"				
25' L			17.40	90.60
13' L			14.01	93.99
11' L			13.57	94.43
0			13.50	94.50
11' R			13.81	94.19
14' R			14.58	93.42
25' R			18.10	89.90
11+00 "B"				
25' L			6.92	101.58
19' L			7.51	100.49
12' L			11.25	96.75
9' L			8.95	99.05
8' L			8.96	99.04
0			8.80	99.20
12' R			8.88	99.12
16' R			9.11	98.89
18' R			10.52	97.48
25' R			6.31	101.69

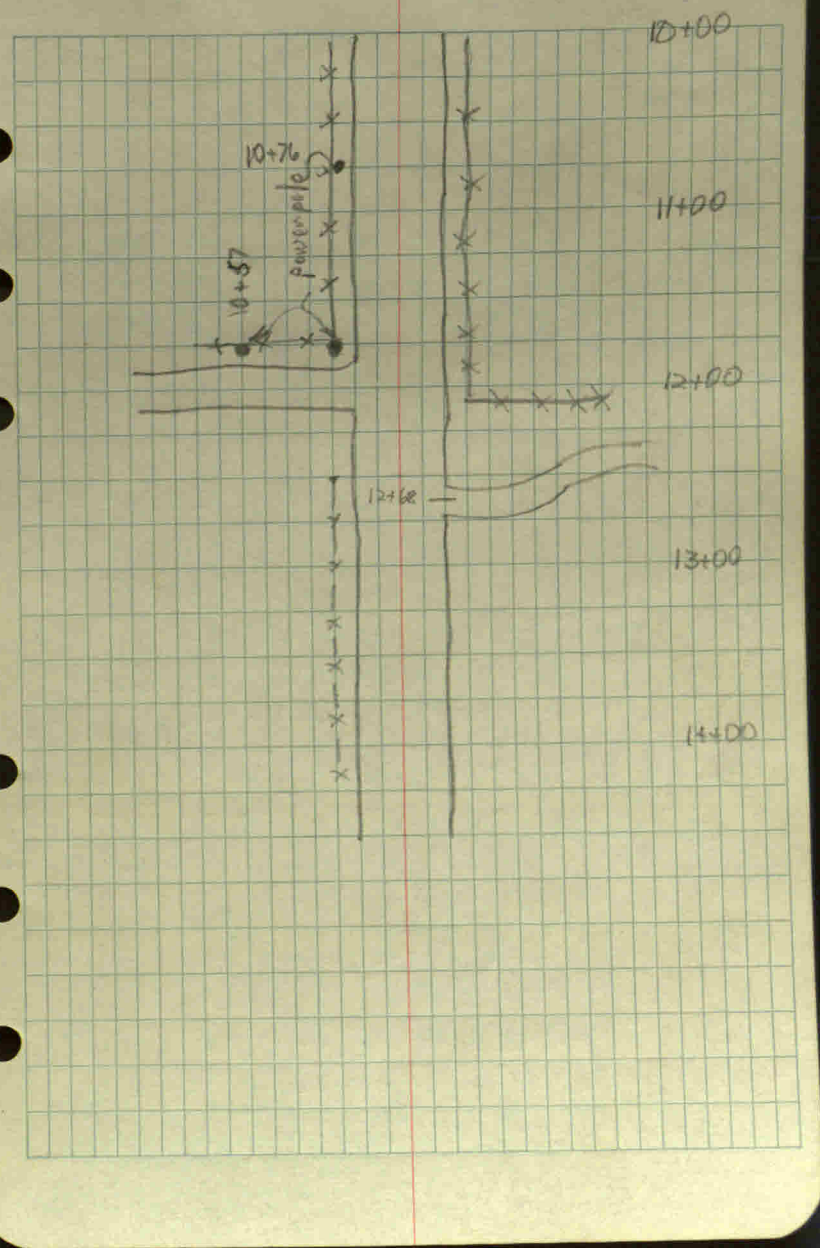
N corner of E driveway guard of Mrs Lewis' driveway



Sta	+	℄	−	elev
10+00 "A"			~~4.81~~	
25' L			4.89	103.16
20' L			4.66	103.34
11' L			6.11	101.89
7' L			6.55	101.45
0			6.53	101.47
9' R			6.90	101.10
11' R			7.05	100.95
15' R			6.73	101.27
25' R			8.20	99.80
11+00 "A"			~~4~~	
25' R			4.37	103.63
15' R			4.26	103.74
11' R			5.21	102.79
9' R			4.62	103.38
0			4.10	103.90
9' L			4.43	103.57
12' L			5.22	102.78
14' L			4.77	103.23
20' L			4.69	103.31
25' L			4.95	103.95

Sta	+	℄	−	elev
12+00 "A"				
25' L			4.74	103.26
20' L			4.71	103.29
16' L			4.96	103.04
11' L			4.51	103.49
8' L			4.62	103.38
0			4.05	103.95
7' R			4.28	103.72
15' R			4.58	103.42
25' R			5.13	102.87
13+00 "A"				
25' L			6.27	101.73
20' L			5.82	102.18
16' L			6.78	101.22
12' L			7.80	100.20
7' L			7.63	100.37
0			7.39	100.69
9' R			7.85	100.15
12' R			7.61	100.39
15' R			6.10	101.90
25' R			5.98	102.02

27° Sta	+	ft	−	elev
14+00 "A"				
25' R			11.64	96.36
15' R			11.00	97.00
14' R			11.97	96.03
11' R			14.25	93.75
8' R			13.89	94.11
0			13.58	99.42
8' L			13.92	94.08
11' L			14.19	93.81
20' L			13.13	94.87
25' L			14.01	93.99
15+00 "A"			16.38	91.62
8+00 "A"			11.84	96.16



223

Madison

Airport

W-Left ↑ N E.-right 274

Flow Line 18" CULVERT 0+15 South 8.51

Center Line

20'	17'	10'	7'	0	8'	11'	14'	18'	20'
1.12	2.16	7.65	7.13	7.43	7.80	9.17	7.53	4.84	2.74
106.83	105.79	100.30	100.82	100.52	100.15	98.78	100.42	103.11	105.11

20'	17'	11'	9'	8'	7'	Center Line	9'	12'	14'	23'
2.69	3.65	9.15	10.19	9.69	9.69	9.53	9.62	9.50	9.53	8.83
105.14	114.22	108.72	106.48	108.27	108.23	108.39	108.25	108.37	108.59	109.09

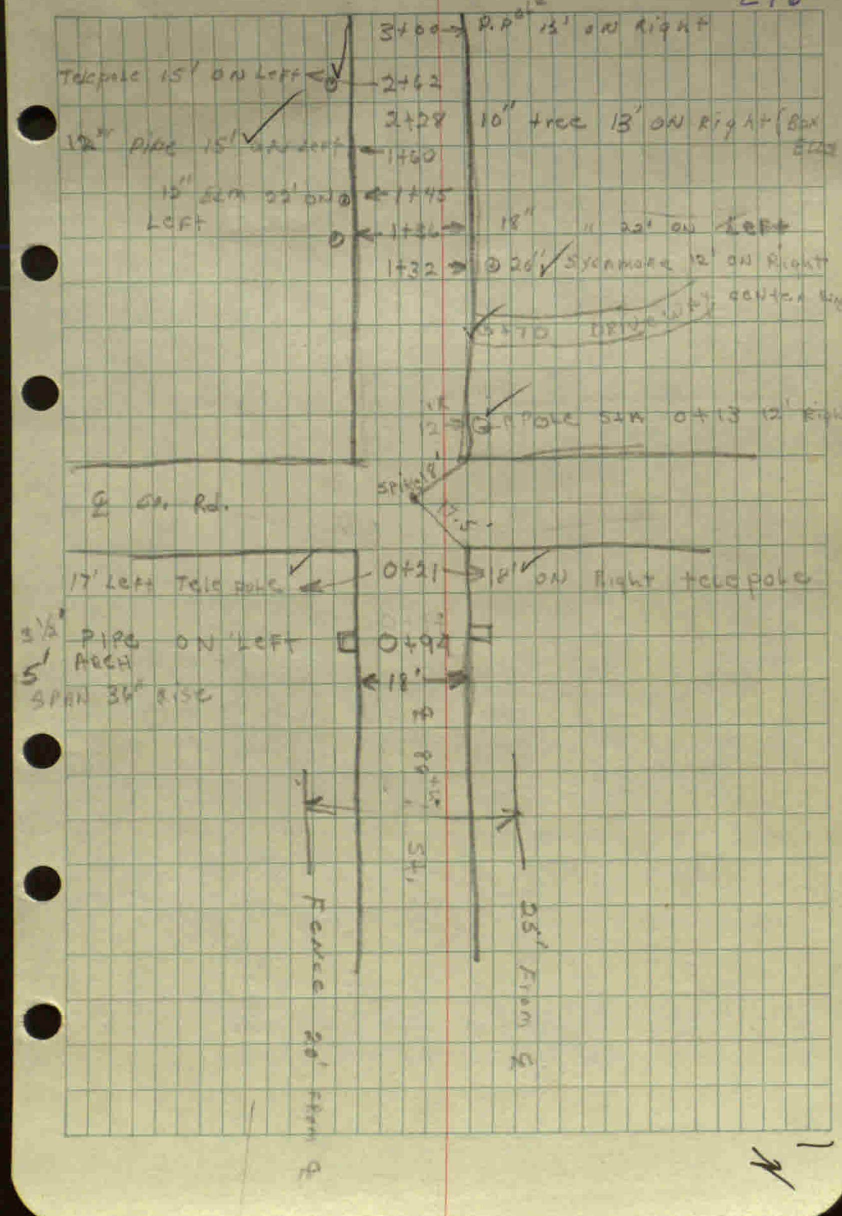
15'	12'	10'	7'	Center Line	5'	10'	12	14	21'
10.95	11.15	10.52	9.92	9.80	9.75	10.14	11.85	10.19	10.25
99.60	99.80	99.43	100.03	100.15	101.20	99.81	98.10	99.55	99.70

15'	13'	9'	6'	Center Line	6'	9'	10'	13'	18'
1.65	2.21	4.72	4.59	3.93	4.12	4.32	5.56	4.02	0.43
108.30	107.74	105.23	105.36	106.02	105.83	105.63	104.39	105.93	109.52

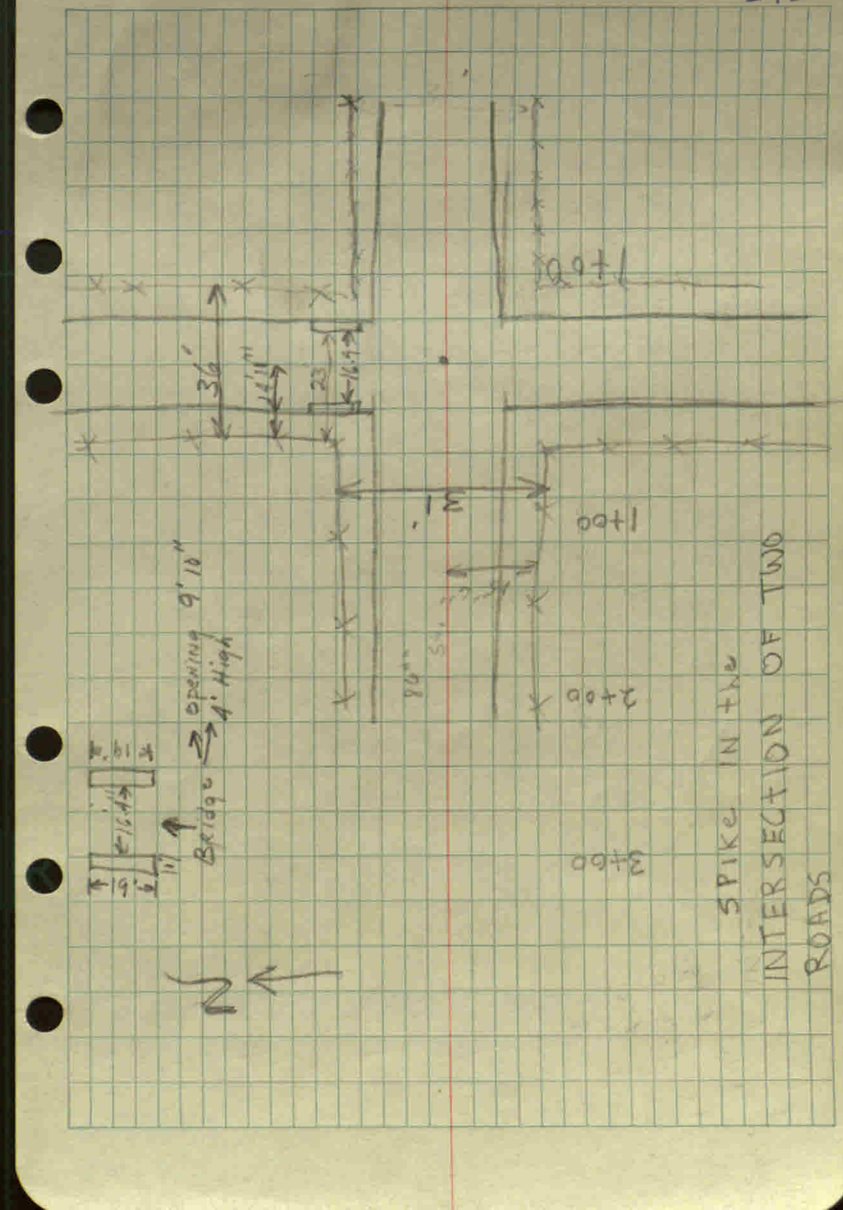
23' 2' higher than 18'

Saw Mill Rd + Plant St. 275

STA.	B.S.	H.I.	F.S	ELEV.	
B.M.	2.62	102.62		100.00	
10+15			8.51	94.11	Flow of Culvert
TP			2.10	100.52	
	7.43	107.95			
1+00 S					
TP			1.93		
	11.85	117.87			
2+00 S					
B.M	9.95	109.95		100.00	
0+22			16.40	93.55	Flow line of culvert
1+00 North					
2+00 North					



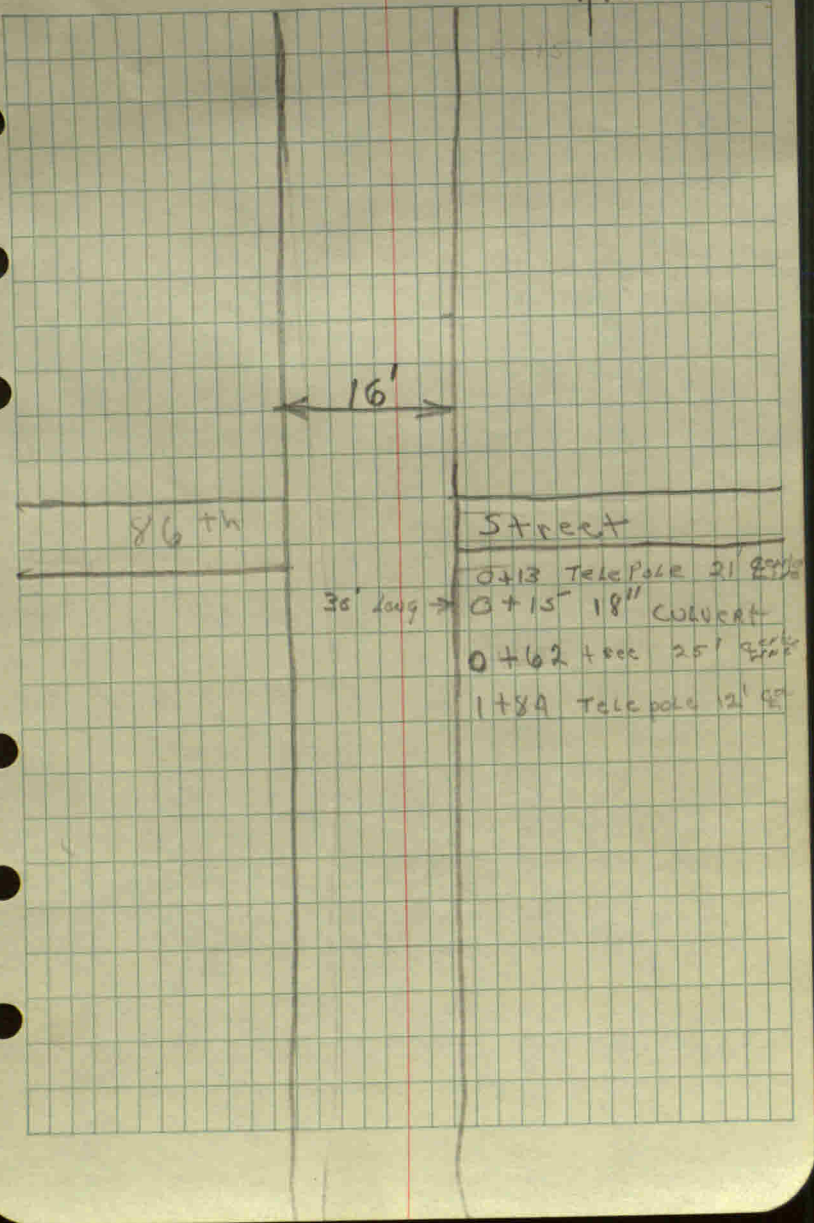
3+00 → D. P. pole 13' ON Right
Telepole 15' ON Left
2+42
2+28 10" tree 13' ON Right
12" Pipe 15' ON Left
1+60
1+45
LEFT
1+36 18" 22' ON Left
1+32 20" Sycamore 12' ON Right
center line
Driveway
POLE STA 0+13 12' Right
Spike
℄ Co. Rd.
0+21 8' ON Right telepole
17' Left Tele pole
3 1/2' Pipe ON Left
0+94
5' ARCH
SPAN 34" Rise
18'
Fence 20' from ℄
23' from ℄



36'
23'
31'
1+00
2+00
3+00
Bridge
opening 9' 10"
4' High
SPIKE IN the INTERSECTION OF TWO ROADS

N 45. ROAD

N



Left - South

Right - North

B.M.
SW wing of Bridge ℄

15'	13'	11'	10'	8'	0	9'	13'	
5.03	4.31	5.23	4.31	3.96	3.72	3.99	4.25	
100.00	99.57	96.78	97.87	99.22	99.46	98.29	97.93	

15'	12'	10'	8'	0	9'	13'	15'	
3.95	6.02	6.73	7.03	6.89	7.22	7.49	9.25	
103.26	101.19	100.48	100.18	100.32	99.99	99.72	97.96	

15'	13'	11'	10'	8'	0	9'	13'	
0.30	2.30	3.68	3.00	2.72	2.51	2.92	2.90	
106.91	104.91	103.53	104.21	104.49	104.70	104.29	104.31	

17'	12'	9'	0	10'	13'	14'	19'	24'	
7.60	5.15	4.70	4.99	4.85	6.40	7.69	5.79	5.32	
92.90	95.25	95.70	95.96	95.55	93.95	92.71	94.61	95.08	

18'	15'	12'	9'	0	9'	12'	13'	20'
7.57	7.15	6.19	4.96	4.53	4.92	5.51	4.94	0.49
92.83	93.25	94.26	95.50	95.97	95.58	94.99	95.92	99.91

10-1-62 SAW mill P.J & 76 T St. 284

STA	B.S.	H.I.	F.S.	ELEV.	Remarks
B.M.	2.18	102.18		100.00	
1+00 West					
TP 1			3.72	98.46	
	8.75	107.21			
1+60	OUTLET	OF Pipe.	=8.55	98.66	OUTLET OF 12" PIPE
2+00 West					
2+40			10.63	96.58	8" pitch 18' ON Right
3+00 West					
Bm	0.90	100.40		100.06	
1+00 East			8.91	91.49 -	FLOW LINE OF PIPE
2+00 East					

Madison Airport 9-16-62 285

STA.	B.S.	H.I.	F.S.	ELEV.
B.M. "J"	4.92	804.49		799.57
T.P. 1			4.15	800.34
	6.04	806.38		
T.P. 2			4.00	802.38
	4.15	806.53		
T.P. 3			10.30	796.23
	3.98	800.21		
B.M. "G"			4.90	795.31
T.P. 1			1.35	798.86
	7.65	806.51		
T.P. 2			3.67	802.84
	7.13	809.97		
T.P. 3			4.00	805.97
	5.30	811.27		
T.P. 4			4.05	807.22
	5.65	812.87		
B.M. "F"			3.56	809.31
B.M. "D"	4.63	826.29		821.66
T.P.			3.72	822.57
	5.26	827.83		
T.P.			7.63	820.20
	4.21	824.41		
T.P.			8.21	816.20
	3.15	819.35		
B.M. "H"			6.07	813.28