



CURVE FORMULAS

$$\begin{array}{l}
 T = R \tan \frac{1}{2} I \\
 T = \frac{50 \tan \frac{1}{2} I}{\text{Sin. } \frac{1}{2} D} \\
 \text{Sin. } \frac{1}{2} D = \frac{50}{R} \\
 \text{Sin. } \frac{1}{2} D = \frac{50 \tan \frac{1}{2} I}{T}
 \end{array}
 \quad
 \begin{array}{l}
 R = T \cot. \frac{1}{2} I \\
 R = \frac{50}{\text{Sin. } \frac{1}{2} D} \\
 E = R \text{ ex. sec } \frac{1}{2} I \\
 E = T \tan \frac{1}{4} I
 \end{array}
 \quad
 \begin{array}{l}
 \text{Chord def.} = \frac{\text{chord}^2}{R} \\
 \text{No. chords} = \frac{I}{D} \\
 \text{Tan. def.} = \frac{1}{2} \text{ chord def.}
 \end{array}$$

The square of any distance, divided by twice the radius, will equal the distance from tangent to curve, very nearly.

To find angle for a given distance and deflection.

Rule 1. Multiply the given distance by .01745 (def. for 1° for 1 ft.) and divide given deflection by the product.

Rule 2. Multiply given deflection by 57.3, and divide the product by the given distance.

To find deflection for a given angle and distance. Multiply the angle by .01745, and the product by the distance.

GENERAL DATA

RIGHT ANGLE TRIANGLES. Square the altitude, divide by twice the base. Add quotient to base for hypotenuse.

Given Base 100, Alt. $10.10^2 \div 200 = .5$. $100 + .5 = 100.5$ hyp.

Given Hyp. 100, Alt. $25.25^2 \div 200 = 3.125$. $100 - 3.125 = 96.875 =$ Base.

Error in first example, .002; in last, .045.

To find Tons of Rail in one mile of track: multiply weight per yard by 11, and divide by 7.

LEVELING. The correction for curvature and refraction, in feet and decimals of feet is equal to $0.574 d^2$, where d is the distance in miles. The correction for curvature alone is closely, $\frac{3}{8} d^2$. The combined correction is negative.

PROBABLE ERROR. If d_1, d_2, d_3 , etc. are the discrepancies of various results from the mean, and if $\sum d^2$ = the sum of the squares of these differences and n = the number of observations, then the probable error of the mean =

$$\pm 0.6745 \sqrt{\frac{\sum d^2}{n(n-1)}}$$

MINUTES IN DECIMALS OF A DEGREE

1'	.0167	11'	.1833	21'	.3500	31'	.5167	41'	.6833	51'	.8500
2	.0333	12	.2000	22	.3667	32	.5333	42	.7000	52	.8667
3	.0500	13	.2167	23	.3833	33	.5500	43	.7167	53	.8833
4	.0667	14	.2333	24	.4000	34	.5667	44	.7333	54	.9000
5	.0833	15	.2500	25	.4167	35	.5833	45	.7500	55	.9167
6	.1000	16	.2667	26	.4333	36	.6000	46	.7667	56	.9333
7	.1167	17	.2833	27	.4500	37	.6167	47	.7833	57	.9500
8	.1333	18	.3000	28	.4667	38	.6333	48	.8000	58	.9667
9	.1500	19	.3167	29	.4833	39	.6500	49	.8167	59	.9833
10	.1667	20	.3333	30	.5000	40	.6667	50	.8333	60	1.0000

INCHES IN DECIMALS OF A FOOT

1-16	3-32	$\frac{1}{8}$	3-16	$\frac{1}{4}$	5-16	$\frac{3}{8}$	$\frac{1}{2}$	$\frac{5}{8}$	$\frac{3}{4}$	$\frac{7}{8}$
.0052	.0078	.0104	.0156	.0208	.0260	.0313	.0417	.0521	.0625	.0729
1	2	3	4	5	6	7	8	9	10	11
.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167

T	T	-	EL
126+00	5.89	863.14 ✓	857.25
125+00			
124+00			
123+00			
122+00			
①	6.12	864.78 ✓	858.66 ✓
121+00			
120+00			

10-18-71 T STEVE G-N

AL J e

JOHN WILSON d

	11.74	6.46
	851.40	856.68
	11.23	5.92
	851.91	857.22
	11.18	5.70
	851.96	857.44
	10.88	5.44
	852.26	857.70
12' 5'	10.74	4.74
6.89	10.54	4.80
856.25	852.61	858.40
	852.40	857.97
	852.83	858.34
44'	4.79	
64'	5.52	
	858.35	857.62
	12.20	4.89
	852.58	859.91
	12.18	5.55
	852.60	859.23

+ π - EL

119+00

118+00

0

5.65 865.73 ✓

4.70 860.08 ✓

CS

117+00

116+00

115+00

114+00

0

6.29 866.71 ✓

5.31 860.42 ✓

113+00

L

L

Z

R

11.85

852.93

5.22

859.56

11.54

853.24

4.94

859.84

H1

23' 13' 5' 4' 2' 13' 23' 43'

6.77 6.31 11.82 12.20 12.00 6.52 5.60 6.13

858.96 859.42 853.91 853.53 853.73 859.21 860.07 859.60

12.03

853.70

5.74

859.99

11.88

853.85

5.97

859.76

11.45

854.28

5.59

860.14

H1

12.52

854.19

5.84

860.87

+ π - EL
CS
112+00

111+00

110+00

109+00

0
6.56 \checkmark 868.32 \checkmark 4.95 861.76 \checkmark

108+00

CS
107+00

106+00

105+00

L
24' 114' 9' 2' 12' 22' 42' R3
7.02 6.82 11.96 12.23 11.89 5.82 5.66 5.90
859.69 859.89 854.75 854.48 854.82 860.89 861.05 860.81

12.26 5.16
854.45 861.55

12.07 5.69
854.64 861.02

11.45 5.07
855.26 861.64

HI
12.60 7.15
855.72 861.17

23' 13' 5' 2' 3' 13' 23' 48'
8.12 8.49 11.60 12.17 11.91 7.10 6.01 7.31
860.20 859.83 856.72 856.15 856.61 861.22 862.31 861.01

12.60 5.85
855.72 862.49

12.55 5.70
855.77 862.62

+ π - EL.

104+00

0

6.15

868.92[✓]

5.55 862.77[✓]

103+00

CS

102+00

101+00

100+00

99+00

0

6.34

870.58[✓]

4.689 864.24[✓]

98+00

L.

Q

R.

4

11.96

856.36

5.80

862.52

4.7

12.70

856.22

6.07

862.85

26'

16'

5'

2

3'

13'

33'

53'

7.30

7.52

12.13

12.74

11.86

6.40

5.46

6.49

861.62

861.40

856.79

856.18

857.06

862.52

863.46

862.43

12.52

856.40

5.40

863.52

12.39

856.53

5.52

863.40

11.99

856.93

5.46

863.46

4.7

13.51

857.07

6.44

864.14

CS
97+00

96+00

95+00

94+00

93+00

483 869.82 ✓ 5.59 864.99 ✓

CS
92+00

B.M. GA. 4.34 865.48 ✓ (865.41)

91+00

CS
90+00

L. R.
25' 15' 5' 4' 3' 13' 28' 53' 5"
7.96 8.60 12.99 13.33 13.00 7.20 6.07 7.10
862.62 861.98 857.59 857.25 857.58 863.38 864.51 865.48

13.22 6.02
857.56 864.56

13.21 6.70
857.37 865.88

13.26 6.23
857.32 864.35

12.98 5.74
857.60 864.84

H1
20' 10' 4' CL 4' 14' 24'
4.85 8.49 11.53 12.08 11.58 6.20 6.54
864.97 861.35 858.29 857.74 858.18 863.62 863.28

12.42 5.53
857.40 864.29

27' 14' 5' CL 4' 18' 30'
5.11 5.16 11.47 11.89 11.45 5.73 5.55
864.71 864.66 858.35 857.93 858.37 864.09 864.27

FLOW LINE
11.91 12.04
857.91 857.78

GARVEY-NEAL CONT. FROM LAST PAGE

+ π - EL

879.56

o

5.44 888.12

5.06 873.78

o

5.10 868.08

10.27 878.35

BM

2.49 870.86

BM

870.61

NE CORNER N W CORNER

POST,

Fg. 5N.

L

L

R 6

73100

6.52

13.91

6.08

867.04

860.15

867.48

72100

6.75

13.09

5.98

866.81

860.97

867.58

HI

40 20 5' 71+00 5' 17 35

701 6.52 12.13 13.28 11.92 5.22 5.06

866.17 866.66 861.05 859.90 861.26 867.96 868.12

10-19-71

POLLARD-TODD

+

π

-

EL

TBM #2

1.55

865.50

863.95

112+00

111+00

110+00

109+00

108+00

0

5.87

867.24

4.13

861.37

107+00

CS
106+00

π STEVE

φ JOHN & AL

R7

11.70

853.80

5.81

859.69

11.29

854.21

5.74

859.76

11.49

854.01

5.53

859.97

10.90

854.60

4.87

860.63

10.68

854.82

4.97

860.53

H1

12.25

854.99

6.36

860.89

24'

14'

4'

4'

16'

36'

46'

7.09

7.57

11.73

12.14

11.83

6.35

5.69

6.36

860.15

859.67

855.51

855.10

855.41

860.89

861.55

860.88

+ π - 82

L

Q

R8

105+00

104+00

103+00

0 3.74⁰ 863.50

6.16 869.66

102+00

101+00

100+00

99+00

98+00



	11.78	5.04
	855.46	862.20
	11.68	4.93
	855.56	862.31
	11.53	4.19
	855.71	863.05
	H1	
	13.68	5.77
	855.98	863.89
	13.63	5.23
	856.03	864.43
	13.42	6.35
	856.24	863.31
	13.27	5.83
	856.39	863.83
	12.98	5.98
	856.68	863.68

+ π - EL

0 6.27⁹ 863.39

6.24 869.63

97+00

H1
12.91

5.41

856.72

864.22

LS

96+00

22' 12' 3' 2' 3' 15' 30' 55'
6.61 6.30 12.59 13.22 12.47 6.55 5.39 6.45

863.22 863.33 859.04 856.41 859.16 863.28 864.24 863.20

95+00

13.13

5.00

856.50

864.63

94+00

13.10

4.99

856.53

864.64

93+00

12.76

4.89

856.87

864.74

92+00

12.81

4.82

856.82

864.81

0 5.18 864.75

5.87 870.32

L

Q

R 9

+ π - EL

0 6.27⁹ 863.39

6.24 869.63

97+00

H1
12.91

5.41

856.72

861.22

65

96+00

22' 12' 3' 0 3' 15' 30' 55'

6.61 6.30 12.59 13.22 12.47 6.55 5.39 6.45

863.02 863.33 857.04 856.41 857.16 863.08 864.24 863.20

95+00

13.13

5.00

856.50

864.63

94+00

13.10

4.99

856.53

864.64

93+00

12.76

4.89

856.87

864.74

92+00

12.81

4.82

856.82

864.81

0

5.18 864.45

5.87 870.32

+

π

-

EL

L

E

R₁₀

91+00

H1
13.22

5.88

857.10

864.44

90+00

13.22

5.92

857.10

864.60

89+00

12.96

5.75

857.36

864.57

88+00

12.35

5.29

857.97

865.03

87+00

12.38

5.90

857.94

864.62

86+00

25'

15'

3'

E

3'

13'

28'

45'

6.30

5.35

11.83

12.34

11.87

6.19

5.26

6.55

864.02

864.97

858.49

857.98

858.45

864.13

865.16

863.77

85+00

12.19

5.69

858.13

864.63

①

5.71 864.61

6.45 871.06

	+	π	-	EL	S	L	Q	R11
84+00							12.66 858.40	5.91 865.15
83+00							12.50 858.56	5.42 865.64
82+00							12.29 858.77	5.36 865.70
81+00							12.19 858.87	5.65 865.41
80+00							12.45 858.61	5.40 865.66
79+00							12.18 858.88	5.71 865.35
78+00							12.23 858.83	5.67 865.39
⊙			5.97	865.09				
	5.89	870.98						

+ π - EL

77+00

76+00

75+00

74+00

73+00

72+00

71+00

70+00

①

5.82 871.63

5.17 865.81

L

E

R¹²

H¹

11.94

5.45

859.04

865.53

23'

13'

2' E

2'

12'

27'

52

6.12

5.95

11.28

11.84

11.46

5.64

5.31

6.34

864.86

865.03

859.70

859.14

859.52

865.34

965.07

864.04

11.67

4.40

859.31

866.58

11.76

4.98

859.22

866.00

11.59

5.77

859.41

865.21

11.43

5.59

859.55

865.39

11.53

5.61

859.45

865.37

11.51

5.06

859.47

865.92

+ π - EL

69+00										11.69	859.94	5.80	865.83
-------	--	--	--	--	--	--	--	--	--	-------	--------	------	--------

68+00										11.80	859.83	5.79	865.86
-------	--	--	--	--	--	--	--	--	--	-------	--------	------	--------

67+00										11.44	860.19	5.75	865.88
-------	--	--	--	--	--	--	--	--	--	-------	--------	------	--------

66+00	25'	15'	3'	4'	3'	13'	28'	48'		5.16	5.38	10.92	11.48	10.95	5.66	4.62	5.95
										866.17	866.25	860.71	860.15	860.68	865.97	867.01	865.68

65+00										11.34	860.29	4.11	867.52
-------	--	--	--	--	--	--	--	--	--	-------	--------	------	--------

64+00										11.37	860.26	5.29	866.34
-------	--	--	--	--	--	--	--	--	--	-------	--------	------	--------

63+00

62+00	6.12	872.99	4.76	866.87
-------	------	--------	------	--------

+ π - EL

63+00

62+00

T.B.m. #4P-A

5.78 867.21 (867.17)

L C R 14

^{H1}
12.30 5.74
860.69 867.25

12.36 5.90
860.63 867.09

11.02 Slow line on pipe
861.37 at 800E outlet

11.36 Slow line inlet 800E
861.63

5.75 BM
867.24

10-20-71 POLLARD-TODD

+ π - EL

78M4P-A 867.17

5.61 872.78

61+00

60+00

59+00

58+00

57+00

^{CS}
56+00

55+00

50

54+00 5.77 873.15

5.40[↓] 867.38

π STEVE

Φ JOHN

⊙ AL

R15

11.99

861.29

6.20

11.33

861.45

5.56

11.32

861.46

5.89

11.29

861.49

5.47

11.00

861.78

4.73

23'	15'	9'	⊕	4'	14'	24'	54'
5.45	5.21	9.65	10.82	9.80	4.96	4.49	5.80
861.96							

10.85

861.93

5.07

✓ π - EL

5400

5300

5200

5100

5000

4900

4800

⊙

6.29

872.98

6.46

866.69

✓

4

RIL

11.04
862.11

5.83

10.79
862.34

5.43

10.65
862.50

5.66

10.70
862.45

5.79

10.55
862.60

5.07

10.84
862.31

5.78

10.05
863.10

6.24

9.74 outlet of pipe across 300 N. 863.24
9.98 inlet of pipe across 300 N. 863.00

474.00

467.00

457.00

447.00

437.00

427.00

417.00

①

7.50

878.65

1.83 871.15

L

Q

R 17

9.84
863.14

5.57
867.41

22' 12' 4' 2' 4' 12' 32' 17'
5.64 5.78 9.14 9.47 8.98 5.75 5.13 5.85
863.51

9.34
863.64

5.55

9.44
863.54

4.76

9.61
863.37

3.43

9.45
863.53

2.61

9.65
863.33

2.13

15.21 from line outside 863.44
14.72 " " inside 863.93

+ π - EL

40+00

39+00

38+00

37+00

36+00

35+00

34+00

33+00

L

Σ

R18

14.72

863.93

5.94

14.22

864.43

5.93

14.31

864.34

6.97

13.86

864.79

55' 30'

15'

3'

Σ

4'

17'

8.36

7.26

7.90

15.17

14.24

15.60

7.72

864.41

8.24

13.78

864.87

8.44

13.94

864.71

8.11

14.20

864.45

~~5.94~~

~~5.93~~

~~6.97~~

~~8.24~~

~~8.44~~

~~8.11~~

+	π	-	EL
+ BM#LP			871.38
3.60	874.98		

PIPE WASH OUT AT 31+95

874.98

5.12 869.86

5.67 875.53

L					E					R19
					HI					
35	25	10	3	32+00	3	11	20	30		
5.75	6.01	5.22	8.72	10.38	9.01	4.63	4.5	4.5		
869.23	868.97	869.76	866.26	864.60	865.97	870.35	870.48			
					50					
					4.23					
					870.25					
				31+00						
	5.50			10.54			5.15			
	869.98			864.94			869.83			
				30+00						
	5.06			10.35			5.16			
	869.92			864.63			869.82			
				29+00						
	5.29			10.38			4.71			
	869.69			864.60			870.27			
				28+00						
	5.30			10.09			5.22			
	869.68			864.88			869.76			
				HI						
	30'	20'	8'	3'	27+00	6'	20'	35'		
	6.12	5.95	5.44	8.65	10.10	9.90	4.82	5.29		
	869.41	869.58	870.09	866.88	865.43	865.63	870.71	870.24		

1 11 - EL

872.52

0

5.74 878.56

5.37 872.82

872.82

871.56

L

L

3

R 20

6.53
871.66

20+00
11.73
866.46

5.28
872.91

7.01
871.182

19+00
11.97
866.726

6.33
871.860

30	10	3	18+00	3	10	30
6.04	5.90	10.65	11.47	10.73	6.07	6.36
872.15	872.29	867.54	866.72	867.46	872.12	871.83

6.43
871.761

17+00
11.34
866.859

5.80
872.39

6.20
872.36

41
16+00
11.53
867.01

6.17
872.39

5.95
872.61

15+00
11.42
869.14

5.98
873.08

6.56
872.00

14+00
11.78
866.78

5.30
873.26

7 11 - EL

L

E

2

R24

	26+00	
5.68	10.28	5.23
869.85	865.25	870.30

	25+00	
5.09	10.45	4.1
870.99	865.09	871.95

	24+00	
4.68	9.84	4.25
870.85	865.69	871.28

30	20	10	3	23+00	3	15	35
5.16	5.0	4.10	8.50	9.57	8.77	3.05	3.15
870.37	870.53	871.43	867.03	865.96	866.76	872.48	872.38

	22+00	
4.45	9.32	4.31
871.08	866.21	871.22

	41	
6.63	21+00	
6.63	11.71	6.32
871.56	866.48	871.87

0 7.38 878.19 4.72 870.81

+ π - EL

878.56

9 R22

30	12	9	12100	4	16	40
717	6.92	10.55	11.81	11.05	6.23	6.94
871.39	871.64	868.61	866.75	867.51	872.33	871.62

	<u>12100</u>	
6.45	11.23	6.10
872.71	866.83	872.46

	<u>11100</u>	
6.46	11.23	6.20
872.210	867.33	872.36

	<u>10100</u>	
6.00	11.20	5.96
872.56	867.36	872.60

	<u>9100</u>	
5.86	11.00	5.92
872.70	867.56	873.74

30'	10	3'	8100	2'	12'	40'
6.25	5.80	10.09	10.90	10.58	6.03	6.60
872.31	872.76	868.47	867.56	867.98	872.53	871.96

⊙ 5.68 877.63 6.61 871.95

	<u>H.I 7100</u>	
4.93	10.07	4.63
872.70	867.56	873.00

+ π - EL

L		C	
		6+00	
5.91		9.91	9.46
871.72		867.92	873.17
		5+00	
4.60		9.78	9.17
873.03		867.85	873.96
		4+00	
9.12		9.42	9.37
873.51		868.21	873.26
		H1	
		15 10 3 3+00 2 10 15	
5.15	9.78	8.15	9.18
872.30	872.67	869.30	868.27
		868.81	872.90
		873.19	
		2+00	
4.5		9.03	9.57
872.95		868.42	873.08
		1+00	
3.72		8.91	3.81
873.23		868.59	873.69
		0+00	
4.20		8.83	3.62
873.25		868.62	873.83

T.BM STA 3475 TOP OF 2ND
WOOD FENCE EAST ~~WEST~~ OF
DITCH IN W FENCE EL 0.92

4.32 873.31
9.14 877.45

+ π - EL

0 4.21 873.24

3.22 876.46

0 5.33 871.13

6.49 878.12

0 6.38 871.74

5.25 876.99

T.B.M. #6A 5.44 871.55

SIGARUEY-NEAL

BM 865.41

6.00 877.41

L R

15	5	END	2	15	20	24
4.21	7.19	8.44	7.9	3.97	4.1	
873.24	870.26	869.01	869.55	873.98	873.35	

7/60

STEVEN
STEVE D 7-11-72

F	H	F
12	5	20
90+00		

5.78 13.03 13.95 13.63 7.00

865.65 858.38 857.96 858.38 864.41

89+00

6.53	13.36	8.41
864.88	858.05	863.00

88+00

7.47	13.12	7.01
863.94	858.29	864.40

+ A - EL

871.91

0

7.79

870.85

8.35 869.00

L

E

L 25

871.00

6.85

869.56

13.01

858.90

7.32

864.09

861.00

6.18

865.23

11.84

858.57

8.34

863.07

11

95

F
15

9

851.00

9

F
19

30

5.98

864.87

5.95

865.9

11.84

859.01

11.84

859.72

6.17

864.68

5.93

864.92

841.00

5.18

865.67

11.91

858.94

7.16

863.69

831.00

5.25

865.60

11.83

859.02

6.87

863.98

821.00

4.96

865.89

11.74

859.11

5.52

865.33

811.00

7.03

863.82

11.56

859.29

5.42

865.43

	+	π	-	EL
0			4.58	866.29
	5.74	872.01		

0			5.59	866.92
	7.14	873.56		

R 26

			HI			
30	15	9	80+11	3	15	30
5.85	6.34	12.25	12.60	12.25	6.57	6.50
866.16	865.67	859.76	859.91	859.76	865.44	865.51

	79+00	
6.32	12.47	6.15
865.69	859.59	865.86

	78+00	
6.21	12.29	6.44
865.80	859.72	865.57

	77+00	
7.46	12.29	5.53
864.55	859.72	866.48

	76+00	
6.13	12.20	5.30
865.88	859.81	866.71

			HI			
40	17	4	75+00	4	20	35
6.99	7.50	13.20	13.60	13.20	7.75	7.29
866.57	866.06	860.36	859.96	860.36	865.81	866.28

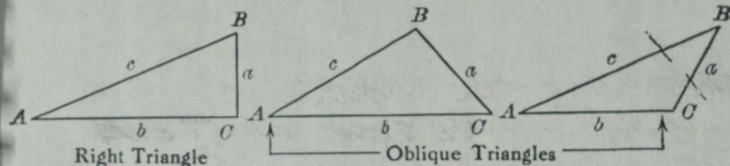
	74+00	
7.11	13.34	6.70
866.45	860.22	866.86

TBM #6-P-EL 841.38

NAIL IN NE SIDE OF 8" EMM
TREE W/ GRAZE MARK 40'E.
OF DITCH IN FENCE.

4.34-5

TRIGONOMETRIC FORMULAS



Solution of Right Triangles

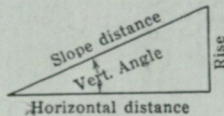
For Angle A. $\sin = \frac{a}{c}$, $\cos = \frac{b}{c}$, $\tan = \frac{a}{b}$, $\cot = \frac{b}{a}$, $\sec = \frac{c}{b}$, $\operatorname{cosec} = \frac{c}{a}$

Given	Required	Formulas
a, b	A, B, c	$\tan A = \frac{a}{b} = \cot B$, $c = \sqrt{a^2 + b^2} = a \sqrt{1 + \frac{b^2}{a^2}}$
a, c	A, B, b	$\sin A = \frac{a}{c} = \cos B$, $b = \sqrt{(c+a)(c-a)} = c \sqrt{1 - \frac{a^2}{c^2}}$
A, a	B, b, c	$B = 90^\circ - A$, $b = a \cot A$, $c = \frac{a}{\sin A}$
A, b	B, a, c	$B = 90^\circ - A$, $a = b \tan A$, $c = \frac{b}{\cos A}$
A, c	B, a, b	$B = 90^\circ - A$, $a = c \sin A$, $b = c \cos A$

Solution of Oblique Triangles

Given	Required	Formulas
A, B, a	b, c, C	$b = \frac{a \sin B}{\sin A}$, $C = 180^\circ - (A + B)$, $c = \frac{a \sin C}{\sin A}$
A, a, b	B, c, C	$\sin B = \frac{b \sin A}{a}$, $C = 180^\circ - (A + B)$, $c = \frac{a \sin C}{\sin A}$
a, b, C	A, B, c	$A + B = 180^\circ - C$, $\tan \frac{1}{2}(A - B) = \frac{(a - b) \tan \frac{1}{2}(A + B)}{a + b}$, $c = \frac{a \sin C}{\sin A}$
a, b, c	A, B, C	$s = \frac{a + b + c}{2}$, $\sin \frac{1}{2}A = \sqrt{\frac{(s - b)(s - c)}{bc}}$, $\sin \frac{1}{2}B = \sqrt{\frac{(s - a)(s - c)}{ac}}$, $C = 180^\circ - (A + B)$
a, b, c	Area	$s = \frac{a + b + c}{2}$, $\text{area} = \sqrt{s(s - a)(s - b)(s - c)}$
A, b, c	Area	$\text{area} = \frac{b c \sin A}{2}$
A, B, C, a	Area	$\text{area} = \frac{a^2 \sin B \sin C}{2 \sin A}$

REDUCTION TO HORIZONTAL



Horizontal distance = Slope distance multiplied by the cosine of the vertical angle. Thus: slope distance = 319.4 ft. Vert. angle = $5^\circ 10'$. Since $\cos 5^\circ 10' = .9959$, horizontal distance = $319.4 \times .9959 = 318.09$ ft.
Horizontal distance also = Slope distance minus slope distance times (1 - cosine of vertical angle). With the same figures as in the preceding example, the following result is obtained. $\operatorname{Cosec} 5^\circ 10' = .9959$. $1 - .9959 = .0041$. $319.4 \times .0041 = 1.31$. $319.4 - 1.31 = 318.09$ ft.

When the rise is known, the horizontal distance is approximately the slope distance less the square of the rise divided by twice the slope distance. Thus: rise = 14 ft., slope distance = 302.6 ft. Horizontal distance = $302.6 - \frac{14 \times 14}{2 \times 302.6} = 302.6 - 0.32 = 302.28$ ft.

